FUNCTIONAL SERVICING REPORT 6600 MAYFIELD ROAD

TOWN OF CALEDON REGION OF PEEL

PREPARED FOR: KHALSA GURMAT ACADEMY TORONTO

PREPARED BY:

C.F. CROZIER & ASSOCIATES INC. 2800 HIGH POINT DRIVE, SUITE 100 MILTON, ON L9T 6P4

MAY 2025

CFCA FILE NO. 2683-7127

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Revision Number	Date	Comments
Rev.0	May 2025	Issued for 1st Submission for Temporary ZBA

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1.0 Introduction

C.F. Crozier & Associates Inc. (Crozier) was retained by Khalsa Gurmat Academy Toronto (the Client) to prepare a Functional Servicing Report in support of a Temporary Zoning-By-Law Amendment Application (ZBA) for the existing place of worship located at 6600 Mayfield Road, in the Town of Caledon (Town), Region of Peel (Region).

This report will demonstrate that the proposed development can be serviced in accordance with the Town's guidelines from a water, septic wastewater, and stormwater management perspective.

The reports, drawings, and design standards referenced during the preparation of this report includes:

- Development Standards Manual (Town of Caledon, 2019)
- Linear Wastewater Standards (Region of Peel, 2023)
- Site Plan/Topographic Survey (Alex Marton Limited, February 8, 2024)
- Site Servicing Plan Drawing A-99 (MEM Engineering Inc., June 12, 2022)
- Stormwater Management Planning and Design Manual (Ministry of Environment, Conservation, and Parks, March 2003)
- Watermain Design Criteria (Region of Peel, 2010)

2.0 Site Description

The existing property (the Site) accounts for approximately 1.09 ha and currently consists of a 1- storey brick dwelling, a prefabricated addition, paved areas, a barn, landscaped areas, and cleared vegetation. The Site, located in a mixed industrial, commercial, and residential area, is bounded by residential properties to the east and west, agricultural lands to the north, and Mayfield Road to the south.

Based on the Request for Fee Proposal prepared by KLM Planning Partners Inc., dated April 26, 2024, we understand that the scope of work will consist of a 3-year Temporary Use Zoning By-Law Amendment Application for the existing place of worship. We understand that all existing buildings on-site will be maintained.

3.0 Water Servicing

The following sections outline the water servicing for the proposed development. The Region is responsible for the operation and maintenance of the water supply servicing the proposed development. Any local water supply systems will connect to the Region's municipal water supply network.

3.1 Existing Water Servicing

An As-Constructed Drawing obtained from the Region's External Peel Asset Locator (EPAL) was used to identify the existing watermain infrastructure surrounding the Site (Site Servicing Plan, Drawing A99, Region approval date stamped July 29 2022, C603070 3rd Submission).

Based on this information, there is an existing 200 mm watermain in Mayfield Road, with an existing fire hydrant immediately southwest of the driveway entrance into the Site. There is an existing valve and box located off the property frontage with a 25 mm Type 'K' copper service. Refer to Appendix A for the As-Constructed Drawings.

3.2 Water Demand

The proposed water demand for the development was calculated according to the Region of Peel's Watermain Design Criteria (2010), with respect to an institutional building use. Table 1 summarizes the estimated design water demand.

Table 1: Estimated Design Water Demand

Municipality	Average Daily	Max Day	Peak Hourly
	Water Demand	Demand	Demand
	(L/s)	(L/s)	(L/s)
Region of Peel	0.2	0.2	0.5

As shown in Table 1, the water service for the development must support a peak hourly demand of 0.50 L/s.

3.3 Fire Flow Demand

The Fire Underwriters Survey method was used to estimate the fire flow demand for the proposed development. Flow requirements are based on the Gross Floor Area (GFA) as depicted by the Topographic Survey prepared by Alex Marton Limited (February 8, 2024). Refer to Appendix A for supporting information.

This calculation is based on the following assumptions:

• The buildings will use Combustible Construction with a Construction Coefficient of 1.5

Table 2 summarizes the estimated fire flow requirements and durations necessary to meet fire protection for the proposed development. Refer to Appendix B for detailed calculations.

Table 2: Estimated Fire Flow

Fire Flow Wat	Duration			
(L/s)	(USGPM)	(hr)		
150.00	2377.55	2.0		

Note that the Fire Underwriters Survey value is a conservative estimate for comparison purposes only and the design of the fire flow of the fire protection system will be completed by others, if required.

Table 3: Total Fire Demand

Maximum Day Demand (L/s)	•	
0.2	150.00	150.20

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As shown in Table 3, the existing building will require a total fire demand of 150.20 L/s. The Site will undergo a rezoning to accommodate the current use of the property based on the City's updated Master Plan. It is assumed the 200 mm watermain in Mayfield Road has been sized to support the updated zoning for the area including the current land use of the Site. Therefore, it is assumed there is sufficient capacity to support the 150.20 L/s of total required demand.

3.4 Proposed Water Servicing

As per As-Constructed Drawing A-99 (Site Servicing Plan, Region approval date stamped July 29 2022, C603070 3rd Submission), a 25 mm diameter Type 'K' copper watermain connects the watermain in Mayfield Road to an existing valve and box off the property frontage. An extension of this 25 mm Type 'K' copper water service is proposed from the valve and box to service the existing site.

4.0 Sanitary Servicing

The Site is in a rural area that does not currently have municipal sanitary services available. The existing building is currently serviced by an 800-gallon holding tank. It is Crozier's opinion that this tank is undersized for the sanitary sewage flow, and a new sanitary servicing solution is necessary. Therefore, the existing building will need to be serviced by a new onsite sewage system.

4.1 Sanitary Design Calculations

Through discussions with the Client, it is Crozier's understanding that the existing building is used for religious services and large group gatherings with meals provided, as well as religious teachings. The total daily design sanitary sewage flow was calculated for the existing facility in accordance with Table 8.2.1.3.B of the Ontario Building Code (OBC), Part 8, as shown in Table 4. Note assumptions regarding the occupancy of the building have been made in consultation with the client and must be confirmed during detailed design. Detailed sanitary calculations are included in Appendix C.

Table 4: Proposed Total Maximum Daily Design Sanitary Sewage Flow

Existing Facilities	Area (m²)	Unit	Unit Flow (L)	Number of Units	Total Flow (L/day)
Place of Worship	n/a	Per Seat (with kitchen facilities)	36	100	3,600
Religious School	0	Per Student 30 45		45	1,350
Total Daily Design Sanitary Sewage Flow: 4,950			4,950		

Based on the results outlined in Table 4, the total daily design sanitary sewage flow is 4,950 L/day.

4.2 Proposed Sewage System

The daily design sanitary sewage flow for the existing building is approximately 4,950 L/day. Given the design flow and the available area on the northern portion of the property, septic tank pretreatment of the sewage prior to discharge to a conventional leaching bed is proposed. As outlined in clause 8.2.2.3.(1)(b) of the OBC, non-residential occupancies require a septic tank with a minimum working capacity of three times the calculated daily design sanitary sewage flow. For the existing building, a septic tank with a minimum working capacity of 14,850 L is necessary.

The septic tank effluent will be dosed by a pump chamber to a filter bed designed in accordance with the OBC for treatment and dispersal of the effluent. There are no background studies or information currently available regarding the Site soil conditions. Based on available soil mapping resources, the native soils on the Site are presumed to be clayey-silt soils for which a preliminary T-time of 50 min/cm has been assigned. Note that this T-time is an assumption for preliminary design purposes and an analysis of the soils in the area of the proposed leaching bed will be required for detailed design. The proposed filter bed will include a stone layer, sand contact area, and sand loading area as sized and described below.

A stone layer composed of septic stone meeting the criteria outlined in Table 8.7.3.3.A., Division B of the OBC will be installed to accommodate the effluent distribution piping. The minimum stone area is calculated using the following equation:

$$A = \frac{Q}{50}$$

Where:

A = the contact area between the base of the stone layer and the filter media layer.

Q =the total design sewage flow in L/d.

Given a total daily design flow of 4,950 L/day, a minimum stone area of 99 m^2 is required. The proposed stone area is $100~\mathrm{m}^2$, which is comprised of two (2) separate $50~\mathrm{m}^2$ beds spaced 5 metres apart and each equipped with a cell of distribution piping. Each cell will be comprised of four (4) runs of 9.0 m long, 75 mm perforated distribution pipes placed at 1.2 m centers. Effluent will be conveyed to the proposed leaching bed by a 50 mm sanitary force main and distributed to each of the beds by a tee fitting.

Below the stone area is a sand contact area. The minimum contact area is calculated using the following equation:

$$A = \frac{QT}{850}$$

Where:

A = the contact area in m² between the base of the filter media layer and the native soil.

Q = the total design sewage flow in L/d.

T = the percolation time of the underlying soil in min/cm to a maximum of 50 min/cm.

Given a total daily design flow of 4,950 L/day and a percolation time of 50 min/cm for the underlying soils, the minimum size of the sand contact area required for the leaching bed is calculated to be 291 m². An area of 300 m² is proposed. The sand contact layer will be constructed of imported sand meeting the criteria outlined in OBC 8.7.5.3(3) with a minimum thickness of 750 mm directly below the stone layer and 250 mm surrounding the stone layer.

A loading area that surrounds the sand contact area and extends at least 15 m in the downgradient direction of the last distribution pipe in the stone layer is required. The minimum loading area is determined using Table 8.7.4.1 of the OBC. For the proposed system, the loading area is calculated using the following equation:

$$A = \frac{Q}{6}$$

Where:

A = the contact area in m^2 between the base of the loading area and the native soil.

Q = the total design sewage flow in L/d.

Given a total daily design flow of 4,950 L/day and a percolation time of 50 min/cm for the underlying soils, the minimum size of the loading area required for the leaching bed is calculated to be 825 m^2 . An area of 840 m^2 is proposed. The loading area will be constructed of imported sand with a percolation rate of 6-10 min/cm with a minimum thickness of 250 mm.

Refer to Figure A for details regarding the layout, orientation, and size of the proposed leaching bed.

5.0 Drainage Conditions

The following Sections 5 and 6 outline the stormwater drainage conditions and design for the proposed development. The City of Brampton is responsible for the operation and maintenance of the surrounding existing stormwater infrastructure.

5.1 Existing Drainage Conditions

Based on the topographic survey (Alex Marton Limited, project number 2022-003, dated February 2024) and site walk, the Site consists of one catchment that drains south into the northern ditch of Mayfield Road. This ditch conveys the drainage into a creek southeast of the Site. There is an existing floodplain east of the property, regulated by the Toronto and Region Conservation Authority (TRCA).

5.2 Proposed Drainage Conditions

No modifications are proposed to alter the current drainage on the property, due to no material changes to the Site and an adequate existing flow condition at the time of this application.

6.0 Erosion and Sediment Control During Construction

Erosion and sediment controls are recommended to be installed prior to the commencement of any construction activities and will be maintained until the Site is stabilized or as directed by the Site Engineer and/or the Town. Controls will be inspected after each significant rainfall event and maintained in proper working condition.

The following sediment and erosion controls are recommended during construction on the Site:

Silt Fencing

Silt fencing will be installed around the perimeter of the Site to intercept sheet flow. Additional silt fencing may be added based on field decisions by the Site Engineer and Owner, prior to, during and following construction.

Silt Sacks in Catchbasins

A silt sack will be installed in the existing nearby catchbasins. The filter cloth will provide sediment control to prevent silt and sediment from entering the stormwater system.

7.0 Conclusions and Recommendations

Based on the information provided in this report, we offer the following conclusions:

- 1. Water servicing for the proposed development is to be provided through the existing 25 mm diamond copper service connection. An identical 25 mm type 'k' copper watermain service is proposed to be installed that extends from the existing building to Mayfield Road.
- 1. Municipal servicing infrastructure is not available for the Site and therefore the existing site will be serviced by an onsite sewage system consisting of a septic tank, pump chamber and filter bed. Background information on the Site soils is not available at this time, however soil mapping resources indicate native soils that are primarily classified as clayey-silt soils. For preliminary design purposes, a T-time of 50 min/cm has been assigned. The total daily design sanitary sewage flow is 4,950 L/day. Septic tank effluent will be discharged to a filter bed with a total stone area of 100 m², contact area of 300 m², and loading area of 840 m².
- 2. Site drainage based on the existing topography and site visit is adequate for the current use of the site.
- 3. Erosion and Sediment Controls, such as silt fencing and silt sacks, are recommended to be installed prior to the commencement of any construction activities.

Respectfully submitted,

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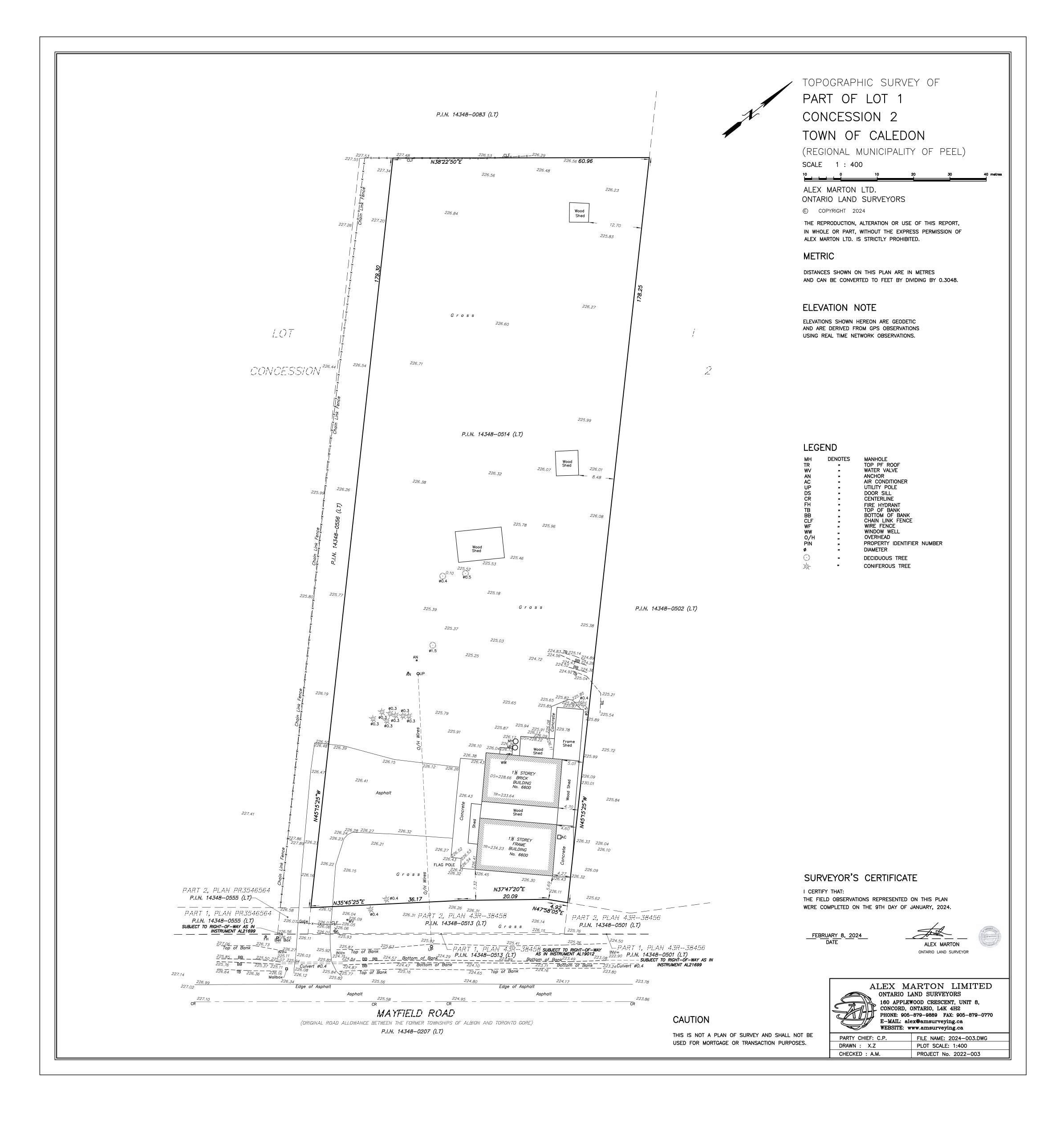
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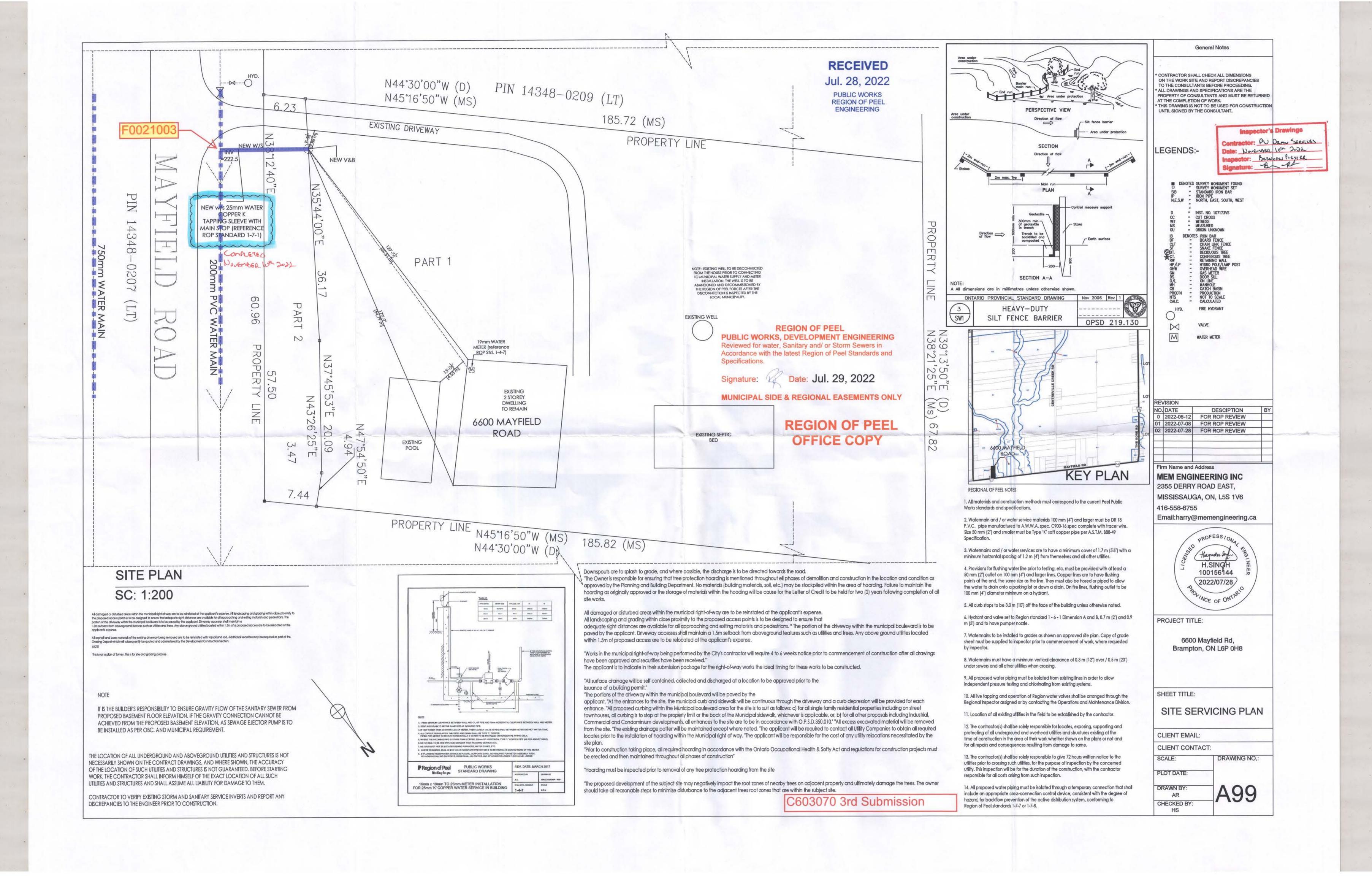
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APPENDIX A

Background Documentation





APPENDIX B

Water Servicing Supporting Calculations



Project: 6600 Mayfield Road **Project No.:** 2683-7127

Created By: JL Checked By: PS

Date: 2025.05.21 **Updated:** 2025.05.21

Domestic Water Demand - Proposed Conditions

Total Site Area: 1.09 ha Population: 50 persons

Design Parameters

Average Demand (L/capita/d)

Water Demand:

Average Daily Demand = 15,000 L/day 0.2 L/s

Peaking Factors (ICI)

Max Day = 1.40 Peak Hour = 3.00

Average Day = 0.2 L/s Max Day = 0.2 L/s Peak Hour = 0.5 L/s

Average Daily Max Day Demand Peak Municipality **Water Demand Hourly Demand** (L/s) (L/s) (L/s) Region of Peel 0.2 0.2 0.5

Notes & References

Average Demand from Section 2.3 of Region of Peel Watermain Design Criteria (Revised June 2010)

Peaking Factors from Section 2.3 of Region of Peel Watermain Design Criteria (Revised June 2010)

Max Day = Average Day Demand * Max Day Peak Hour = Average Day Demand * Peak Hour

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Water Supply for Public Fire Protection - 1999 Fire Underwriters Survey

Part II - Guide for Determination of Required Fire Flow

1. An estimate of fire flow required for a given area may be determined by the formula:

F = 220 * C * sqrt A

where

F = the required fire flow in litres per minute

C = coefficient related to the type of construction

- = 1.5 for wood frame construction (structure essentially all combustible)
- = 1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior)
- = 0.8 for non-combustible construction (unprotected metal structural components)
- = 0.6 for fire-resistive construction (fully protected frame, floors, roof)

A = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building considered.

Existing Building Wood Frame

1.5 C

705.24 sq.m. floor area of largest floor Per Topographic Survey provided by Alex Marton Limited dated

Februray 8, 2024.

"Non-combustible; fire breaks between each storey; fire resistive

N/A 25% of immediately adjoining floor construction"

705.24 Total Area

Therefore F= 9,000 L/min (rounded to nearest 1000 L/min)

Fire flow determined above shall not exceed:

30,000 L/min for wood frame construction

30,000 L/min for ordinary construction

25,000 L/min for non-combustible construction

25,000 L/min for fire-resistive construction

2. Values obtained in No. 1 may be reduced by as much as 25% for occupancies having low contents fire hazard or may be increased by up to 25% surcharge for occupancies having a high fire hazard.

Non-Combustible -25% Free Burning 15% Limited Combustible -15% Rapid Buring 25%

Combustible No Charge

Combustible 0% reduction

0 L/min reduction

Therefore UPDATED F= 9,000 L/min (rounded to nearest 1000 L/min)

Note: Flow determined shall not be less than 2,000 L/min

3. Sprinklers - The value obtained in No. 2 above maybe reduce by up to 50% for complete automatic sprinkler protection.

Sprinkler System Assume 0% reduction, since there are no sprinklers.

0 L/min reduction

May 21, 2025

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Water Supply for Public Fire Protection - 1999 Fire Underwriters Survey

Part II - Guide for Determination of Required Fire Flow

4. Exposure - To the value obtained in No. 2, a percentage should be added for structures exposed within 45 metres by the fire area under consideration. The percentage shall depend upon the height, area, and construction of the building(s) being exposed, the separation, openings in the exposed building(s), the length and height of exposure, the provision of automatic sprinklers and/or outside sprinklers in the building(s) esposed, the occupancy of the exposed building(s) and the effect of hillside locations on the possible spread of fire.

Separation	Charge	Separation	Charge
0 to 3 m	25%	20.1 to 30 m	10%
3.1 to 10 m	20%	30.1 to 45 m	5%
10.1 to 20 m	15%		

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Name	Distance (m)		
North	38	5%	450
South	80	0%	0
East	60	0%	0
West	100	0%	0

450 L/min Surcharge

Determine Required Fire Flow

No.1 9,000

No. 2 0 reduction
No. 3 0 reduction
No. 4 450 surcharge

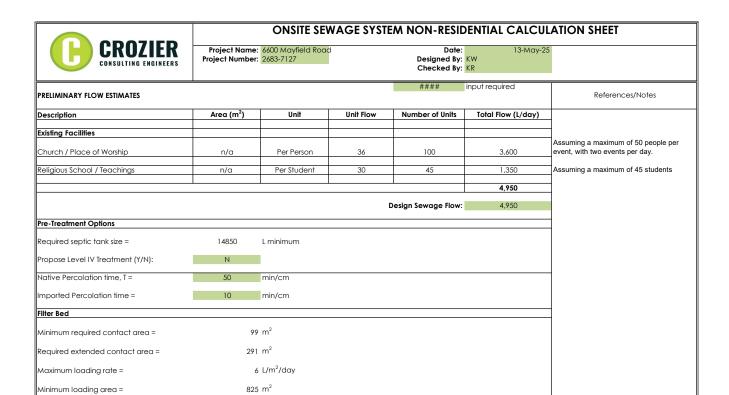
Required Flow: 9,450 L/min

Rounded to nearest 1000l/min: 9,000 L/min or 150.0 L/s 2,377.55 USGPM

Required Duration of Fire Flow				
Flow Required	Duration			
L/min	(hours)			
2,000 or less	1.0			
3,000	1.25			
4,000	1.5			
5,000	1.75			
6,000	2.0			
8,000	2.0			
10,000	2.0			
12,000	2.5			
14,000	3.0			
16,000	3.5			
18,000	4.0			
20,000	4.5			
22,000	5.0			
24,000	5.5			
26,000	6.0			
28,000	6.5			
30,000	7.0			
32,000	7.5			
34,000	8.0			
36,000	8.5			
38,000	9.0			
40,000 and over	9.5			

APPENDIX C

Sanitary Servicing Supporting Calculations



FIGURES

Figure A: Site Servicing Concept

