

Mar 18, 2022



# Soil Engineers Ltd.

CONSULTING ENGINEERS

**GEOTECHNICAL • ENVIRONMENTAL • HYDROGEOLOGICAL • BUILDING SCIENCE**

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November 23, 2020

Reference No. 2009-S188

Page 1 of 7

8181926 Canada Inc.  
160 Avenue Labrosse  
Pointe-Claire, Quebec  
H9R 1A1

Attention: Mr. Raj Chahal

**Re: Geotechnical Investigation for Proposed Truck and Trailer Parking  
12541 and 12577 Airport Road  
Town of Caledon**

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Dear Sir:

In accordance with the written authorization dated September 29, 2020, we have completed the geotechnical investigation at the captioned property. The findings and resulting recommendations are presented in this report.

## **SITE CONDITION**

The subject property, encompassing an area of 11.85 hectares, is a farm field with barns, farm houses and a water pond, located on the east side of Airport Road in the Town of Caledon. The existing site gradient is relatively flat, with minor drops towards the east.

It is understood that the water pond will be filled in and the site will be regraded for truck and trailer parking.

## **FIELD WORK**

The field work, consisting of eleven (11) sampled boreholes extending to a depth of 3.5 m, was performed on October 15 and 16, 2020, at the locations shown on the Plan, Drawing No. 1.

The boreholes were advanced at intervals to the sampling depths by a track-mounted, continuous-flight power-auger machine equipped for soil sampling. Standard Penetration

Tests, using the procedures described on the enclosed “List of Abbreviations and Terms”, were performed at the sampling depths. The test results are recorded as the Standard Penetration Resistance (or ‘N’ values) of the subsoil. The relative density of the non-cohesive strata and the consistency of the cohesive strata are inferred from the ‘N’ values. Split-spoon samples were recovered for soil classification and laboratory testing. The field work was supervised, and the findings were recorded by a Geotechnical Technician.

The ground elevation at each borehole location was obtained using a hand-held Global Navigation Satellite System (GNSS) surveying equipment (Trimble Geoexplorer 6000).

### **SUBSURFACE CONDITIONS**

The area of investigation is a farm field. The investigation has disclosed that beneath a veneer of topsoil, with a layer of earth fill, the site is generally underlain by a stratum of silty clay and silty clay till.

Detailed descriptions of the encountered subsurface conditions are presented on the Borehole Logs, comprising Figures 1 to 11, inclusive. The revealed stratigraphy is plotted on the Subsurface Profile, Drawing Nos. 2 and 3. The engineering properties of the disclosed soils are discussed herein.

#### **Topsoil** (All Boreholes)

A layer of topsoil, 15 to 20 cm in thickness, was contacted at the ground surface.

#### **Earth Fill** (All Boreholes)

Beneath the topsoil, a layer of earth fill, extending to a depth of 0.4 to 1.7 m from the existing ground surface, was contacted at the borehole locations. It consists of silt and clay, with topsoil and organic inclusions. Part of the earth fill may represent the ploughed earth to a depth of 0.4 to 0.7 m from grade. The fill at the lower depth at Boreholes 4, 8 and 11 may represent earth filling in the past for pre-grading.

One must be aware that the samples retrieved from boreholes may not be truly representative of the geotechnical and environmental quality of the fill, and do not indicate whether the topsoil beneath the earth fill was completely stripped. This should be further assessed by laboratory testing and/or test pits.

**Silty Clay and Silty Clay Till** (All Boreholes)

The native stratum of silty clay and silty clay till was contacted below the earth fill. It is low to medium plasticity. Grain size analyses were conducted on 6 samples collected from the test pits for infiltration assessment; the results are presented on Figures 12 to 15, inclusive.

The obtained 'N' values range from 12 to 65, with a median of 24 blows per 30 cm of penetration, indicating the clay and clay till are stiff to hard, generally being very stiff in consistency.

The natural water content values of the soil samples were determined; the results are plotted on the Borehole Logs. The values range from 9% to 26%, with a median of 20%, showing a moist condition.

The engineering properties of the silty clay and silty clay till deposits are given below:

- High frost susceptibility.
- Low water erodibility.
- Low permeability, with an estimated coefficient of permeability of  $10^{-7}$  cm/sec, a percolation rate of more than 80 min/cm, and runoff coefficients of:

<b>Slope</b>	
0% - 2%	0.15
2% - 6%	0.20
6% +	0.28

- The shear strength is primarily derived from consistency and augmented by internal friction.
- In excavation, the clay deposit will be stable in relatively steep cut.
- Poor pavement-supportive material, with an estimated California Bearing Ratio value of 3% to 5%.
- High corrosivity to buried metal, with an estimated electrical resistivity of 2500 ohm·cm.

**GROUNDWATER CONDITIONS**

No free groundwater was recorded in the boreholes during the drilling operation and upon the completion of drilling. It is our opinion that continuous groundwater does not exist in the boreholes within the depth of investigation.

## **DISCUSSION AND RECOMMENDATIONS**

The investigation has disclosed that beneath a veneer of topsoil, with a layer of earth fill extending to a depth of 0.4 to 1.7 m, the site is underlain by a stratum of stiff to hard, generally being very stiff silty clay and silty clay till in a moist condition. Continuous groundwater does not exist in the boreholes within the depth of investigation.

It is understood that the pond will be filled in and the site will be regraded for truck and trailer parking. The geotechnical findings warranting special consideration are presented below.

### **Site Preparation**

Topsoil, vegetation and organic-containing material must be removed from the farm field. The exposed subgrade must be inspected and proof-rolled prior to regrading or any fill placement. Any soft spot or soils with high organic content should be sub-excavated and removed.

The existing pond will be backfilled to the pre-grade level. After the water is removed, the sediment and wet material must be removed from the bottom before backfilling.

The existing barns and houses will be left on site. In case any structure will be demolished, the debris and rubble must be removed and disposed off-site.

After the demolition, the cavities should be backfilled with selected material, free of organics, compacted in layers to the job specification and requirements. If imported fill is to be used, it should be inorganic soils, free of deleterious material and any environmental issue (contamination). The potential imported earth fill from off-site must be reviewed for geotechnical and environmental quality by the appropriate personnel as authorized by the developer or agency, before being hauled to the site.

### **Underground Services**

The subgrade for underground service pipes and manholes should consist of sound native soils or properly compacted inorganic earth fill. Where badly weathered soil or organic soil is encountered, it should be sub-excavated and replaced with the bedding material, compacted to at least 95% of Standard Proctor compaction. A Class 'B' granular bedding, consisting of compacted 20-mm Crusher-Run Limestone, or equivalent, is recommended for construction of underground services.

The pipe joints into catch basins and manholes must be leak-proof to prevent the migration of fines through the joints. Openings to subdrains and catch basins should be shielded with a fabric filter to prevent blockage by silting.

In order to prevent pipe floatation when the service trench is deluged with water, a soil cover of at least two times the pipe diameter should be in place at all times after completion of the pipe installation.

### **Backfilling in Trenches and Excavated Areas**

The on-site inorganic soils are generally suitable for use as trench backfill. The backfill should be compacted to at least 95% of its maximum Standard Proctor dry density. The compaction can be carried out on the wet side of the optimum to allow a wider latitude of lift thickness.

In the zone within 1.0 m below the pavement subgrade, the material should be compacted with the water content at 2% to 3% drier than the optimum and the compaction should be increased to at least 98% of the maximum Standard Proctor dry density. This is to provide the required stiffness for pavement and slab construction.

In normal construction practice, the problem areas of ground settlement largely occur adjacent to manholes, catch basins, services crossings, foundation walls and columns. In areas which are inaccessible to a heavy compactor, imported sand backfill should be used and compacted with a lighter equipment.

The narrow trenches should be cut at 1 vertical:2 or + horizontal so that the backfill can be effectively compacted. Otherwise, soil arching will prevent the achievement of proper compaction. The lift of each backfill layer should either be limited to a thickness of 20 cm, or the thickness should be determined by test strips.

### **Sidewalk and Structures**

The on-site subsoil is highly frost susceptible, the sidewalk and minor structures in open areas should be designed to tolerate the seasonal movement.

If no movement is tolerable, the structure should be supported on conventional footings extending into the native soil stratum or well-compacted earth fill, with a minimum earth cover of 1.2 m. The recommended soil bearing pressures for use in the design of conventional footings are given below:

- Maximum Allowable Bearing Pressure, at Serviceability Limit State (SLS) = 100 kPa
- Factored Ultimate Bearing Pressure, at Ultimate Limit State (ULS) = 150 kPa

The total and differential settlements of footing designing for the recommended bearing pressure at SLS are estimated to be 25 mm and 20 mm, respectively.

### **Pavement Design**

The recommended pavement design at the driveway entrance and heavy duty parking is presented below:

<b>Course</b>	<b>Thickness (mm)</b>	<b>OPS Specifications</b>
Asphalt Surface	40	HL 3
Asphalt Binder	65	HL 8
Granular Base	150	OPSS Granular 'A', 20-mm CRL or equivalent
Granular Sub-base	350	OPSS Granular 'B', 50-mm CRL or equivalent

In case a gravel lot will be constructed for the truck and trailer parking, a minimum of 200 mm of 20 mm crusher run limestone on 300 mm of 50 mm crusher run limestone is recommended.

The gravel must be placed on a woven geotextile of Terrafix 400W or Biaxial Geogrid of Terrafix TBX2000, or equivalent, to separate the soil and the granular fill, in order to maintain a continuous support, even the gravel and the subgrade is saturated after rainfall.

In preparation of the subgrade for pavement construction, compressible topsoil and high organic content material should be removed. The fine graded subgrade should be proof-rolled with a heavy roller or loaded dump-truck. Any soft subgrade as identified should be sub-excavated and replaced by selected organic-free material and compacted properly to the job specifications.

In the zone within 1.0 m below the pavement subgrade, the earth fill should be compacted to at least 98% of its maximum Standard Proctor dry density, with the water content 2% to 3% drier than the optimum. In the lower zone, a 95% or + Standard Proctor compaction is considered adequate.

All the granular bases should be compacted to their maximum Standard Proctor dry density.

The pavement subgrade will suffer a strength regression if water is allowed to infiltrate prior to

paving. The following measure should therefore be incorporated into the construction procedures and road design:

- The pavement subgrade should be properly crowned and smooth-rolled to allow interim precipitation to be properly drained.
- Subdrains connected into the catch basins should be provided to drain the infiltrated water at the lower spots. The subdrains should consist of filter-sleeved weepers to prevent blockage by silting.
- Areas adjacent to the pavement should be properly graded to prevent the ponding of large amounts of water. Swales should be provided to drain the surface water runoff from the pavement.

**LIMITATIONS OF REPORT**

This report was prepared by Soil Engineers Ltd. for the account of 8181926 Canada Inc., and for review by the designated consultants and government agencies. Use of this report is subject to the conditions and limitations of the contractual agreement.

The material in the report reflects the judgment of Daric Yang, B.A.Sc., and Bennett Sun, P.Eng., in light of the information available to it at the time of preparation. Any use which a Third Party makes of this report, or any reliance on decisions to be made based on it, is the responsibility of such Third Parties. Soil Engineers Ltd. accepts no responsibility for damages, if any, suffered by any Third Party as a result of decisions made or actions based on this report.

Yours truly,  
**SOIL ENGINEERS LTD.**



Daric Yang, B.A.Sc.  
DY/BS:



Bennett Sun, P.Eng.



**ENCLOSURES**

Log of Boreholes .....	Figures 1 to 11
Grain Size Distribution Curves .....	Figures 12 to 15
Borehole and Test Pit Location Plan .....	Drawing No. 1
Subsurface Profile .....	Drawing Nos. 2 and 3

c. Malone Given Parsons  
Attn. Mr. Rohan Sovig

## LIST OF ABBREVIATIONS AND DESCRIPTION OF TERMS

The abbreviations and terms commonly employed on the borehole logs and figures, and in the text of the report, are as follows:

### SAMPLE TYPES

AS	Auger sample
CS	Chunk sample
DO	Drive open (split spoon)
DS	Denison type sample
FS	Foil sample
RC	Rock core (with size and percentage recovery)
ST	Slotted tube
TO	Thin-walled, open
TP	Thin-walled, piston
WS	Wash sample

### SOIL DESCRIPTION

Cohesionless Soils:

<u>'N'</u> (blows/ft)	<u>Relative Density</u>
0 to 4	very loose
4 to 10	loose
10 to 30	compact
30 to 50	dense
over 50	very dense

Cohesive Soils:

<u>Undrained Shear Strength (ksf)</u>	<u>'N'</u> (blows/ft)	<u>Consistency</u>
less than 0.25	0 to 2	very soft
0.25 to 0.50	2 to 4	soft
0.50 to 1.0	4 to 8	firm
1.0 to 2.0	8 to 16	stiff
2.0 to 4.0	16 to 32	very stiff
over 4.0	over 32	hard

### PENETRATION RESISTANCE

Dynamic Cone Penetration Resistance:

A continuous profile showing the number of blows for each foot of penetration of a 2-inch diameter, 90° point cone driven by a 140-pound hammer falling 30 inches.

Plotted as '—●—'

Standard Penetration Resistance or 'N' Value:

The number of blows of a 140-pound hammer falling 30 inches required to advance a 2-inch O.D. drive open sampler one foot into undisturbed soil.

Plotted as '○'

WH	Sampler advanced by static weight
PH	Sampler advanced by hydraulic pressure
PM	Sampler advanced by manual pressure
NP	No penetration

Method of Determination of Undrained Shear Strength of Cohesive Soils:

x 0.0 Field vane test in borehole; the number denotes the sensitivity to remoulding

△ Laboratory vane test

□ Compression test in laboratory

For a saturated cohesive soil, the undrained shear strength is taken as one half of the undrained compressive strength

### METRIC CONVERSION FACTORS

1 ft = 0.3048 metres

1lb = 0.454 kg

1 inch = 25.4 mm

1ksf = 47.88 kPa



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# LOG OF BOREHOLE NO.: 1

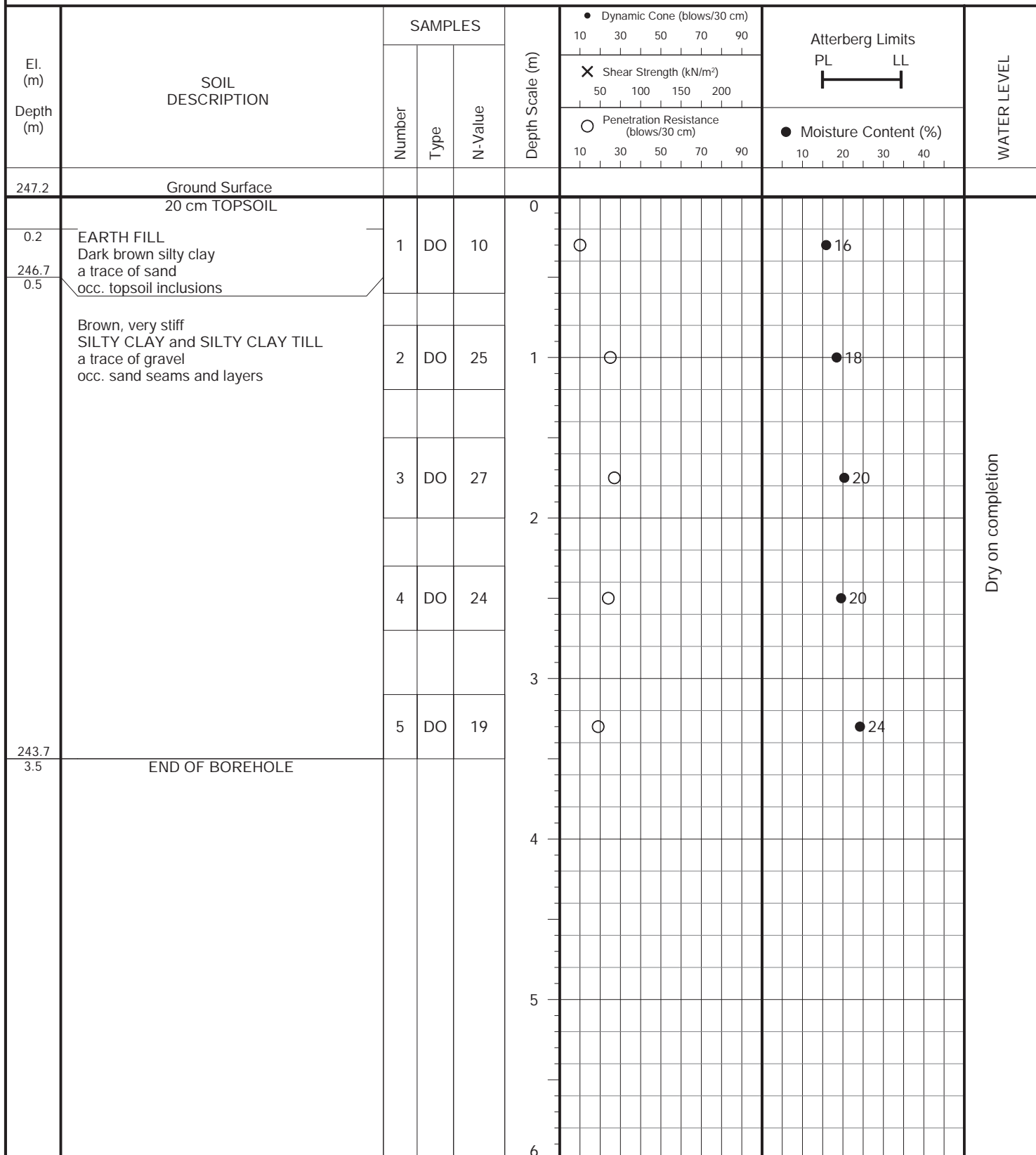
FIGURE NO.: 1

PROJECT DESCRIPTION: Proposed Truck and Trailer Parking

METHOD OF BORING: Flight Auger

PROJECT LOCATION: 12541 and 12577 Airport Road, Town of Caledon

DRILLING DATE: October 16, 2020



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# LOG OF BOREHOLE NO.: 10

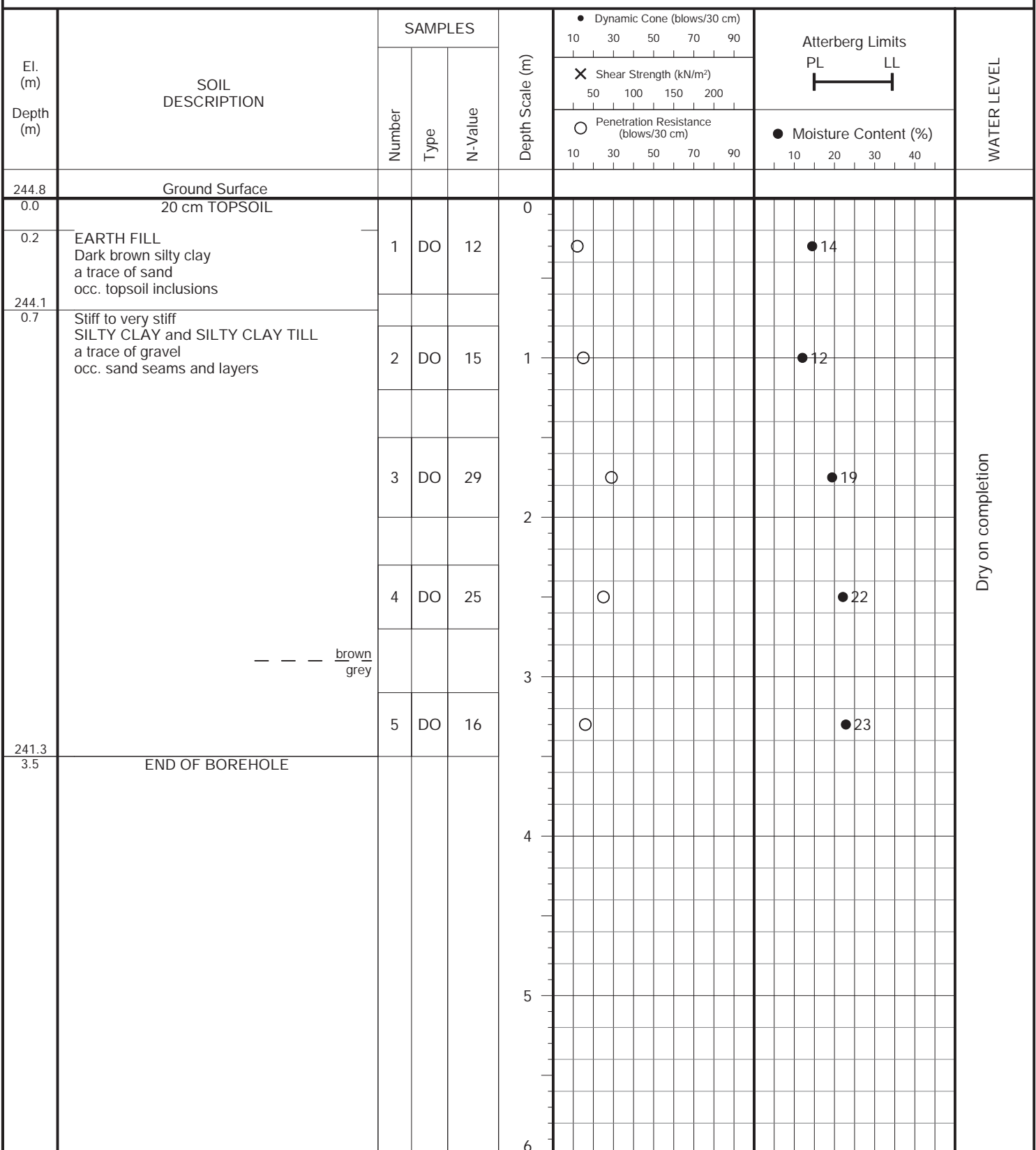
FIGURE NO.: 10

PROJECT DESCRIPTION: Proposed Truck and Trailer Parking

METHOD OF BORING: Flight Auger

PROJECT LOCATION: 12541 and 12577 Airport Road, Town of Caledon

DRILLING DATE: October 16, 2020



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# LOG OF BOREHOLE NO.: 11

FIGURE NO.: 11

PROJECT DESCRIPTION: Proposed Truck and Trailer Parking

METHOD OF BORING: Flight Auger

PROJECT LOCATION: 12541 and 12577 Airport Road, Town of Caledon

DRILLING DATE: October 16, 2020

El. (m)	SOIL DESCRIPTION	SAMPLES			Depth Scale (m)	Dynamic Cone (blows/30 cm)		Atterberg Limits		WATER LEVEL
		Number	Type	N-Value		10	30	50	70	
243.1	Ground Surface									
0.0	15 cm TOPSOIL				0					
0.1	EARTH FILL Dark brown silty clay a trace of sand occ. topsoil inclusions	1	DO	14		○			● 17	
242.0		2	DO	16	1	○			● 15	
1.1	Brown, very stiff SILTY CLAY and SILTY CLAY TILL a trace of gravel occ. sand seams and layers									
		3	DO	25	2	○			● 21	
		4	DO	24		○			● 22	
		5	DO	19	3	○			● 23	
239.6	END OF BOREHOLE				4					
3.5					5					
					6					

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# LOG OF BOREHOLE NO.: 2

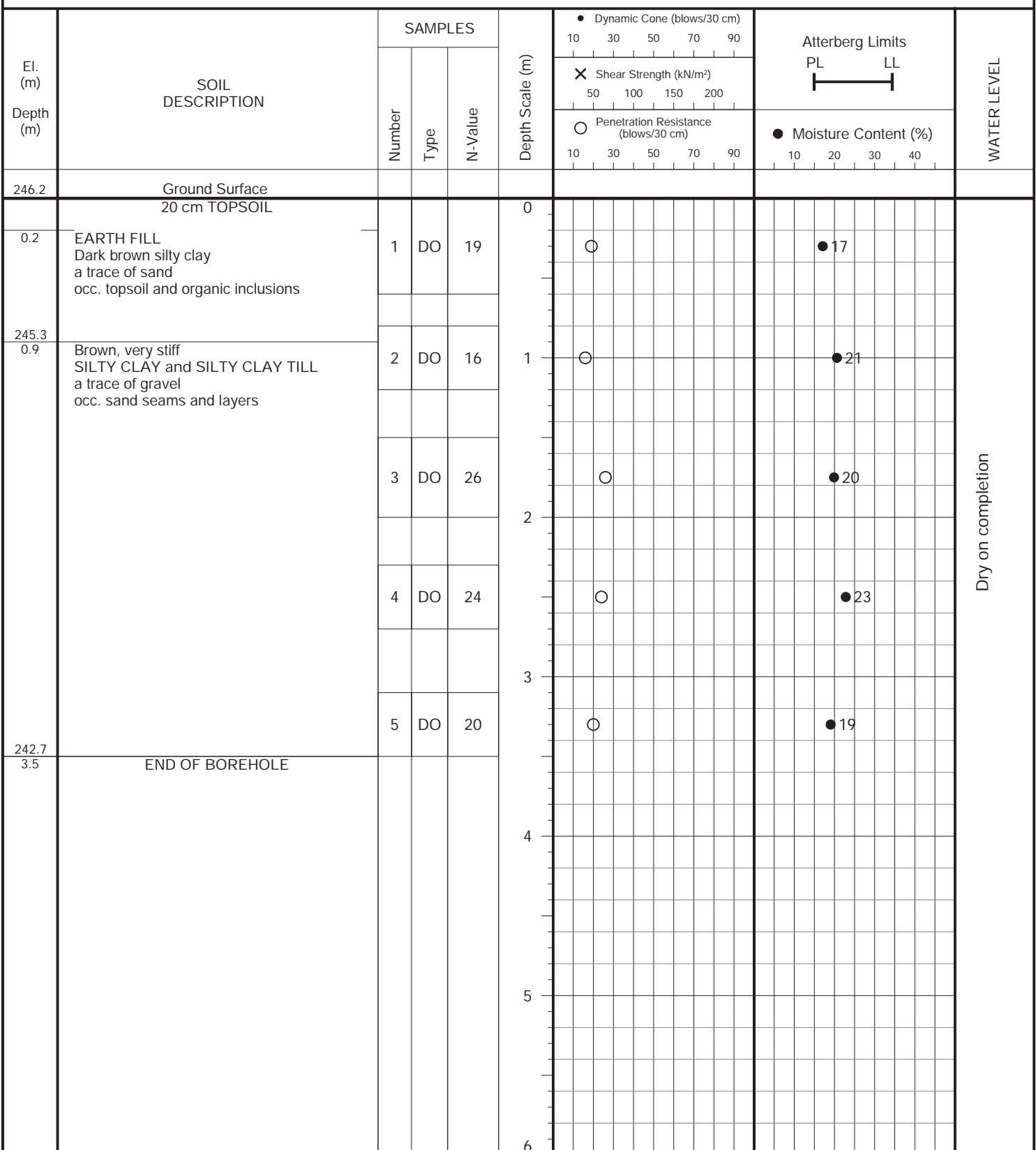
FIGURE NO.: 2

PROJECT DESCRIPTION: Proposed Truck and Trailer Parking

METHOD OF BORING: Flight Auger

PROJECT LOCATION: 12541 and 12577 Airport Road, Town of Caledon

DRILLING DATE: October 15, 2020



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# LOG OF BOREHOLE NO.: 3

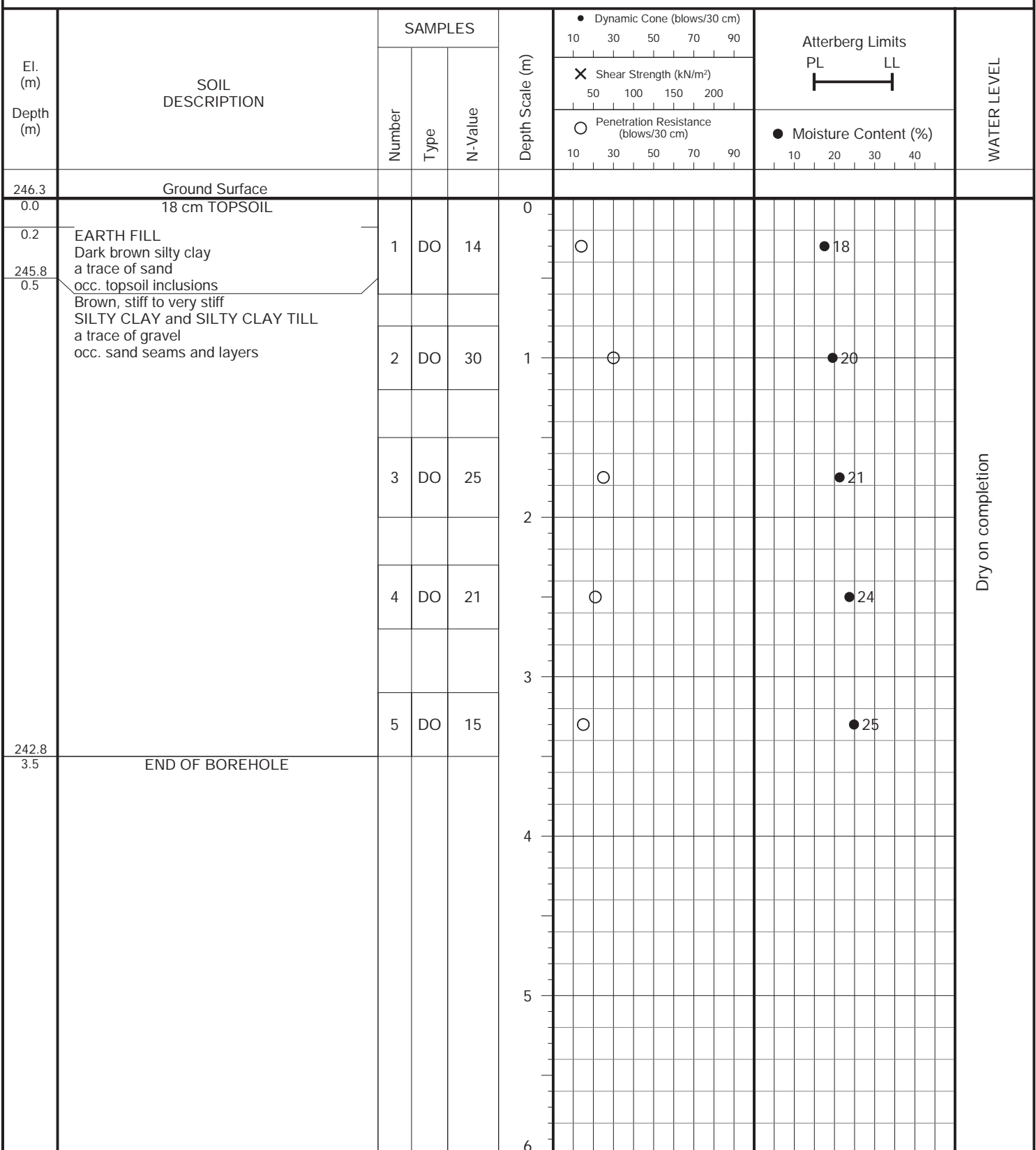
FIGURE NO.: 3

PROJECT DESCRIPTION: Proposed Truck and Trailer Parking

METHOD OF BORING: Flight Auger

PROJECT LOCATION: 12541 and 12577 Airport Road, Town of Caledon

DRILLING DATE: October 16, 2020



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# LOG OF BOREHOLE NO.: 4

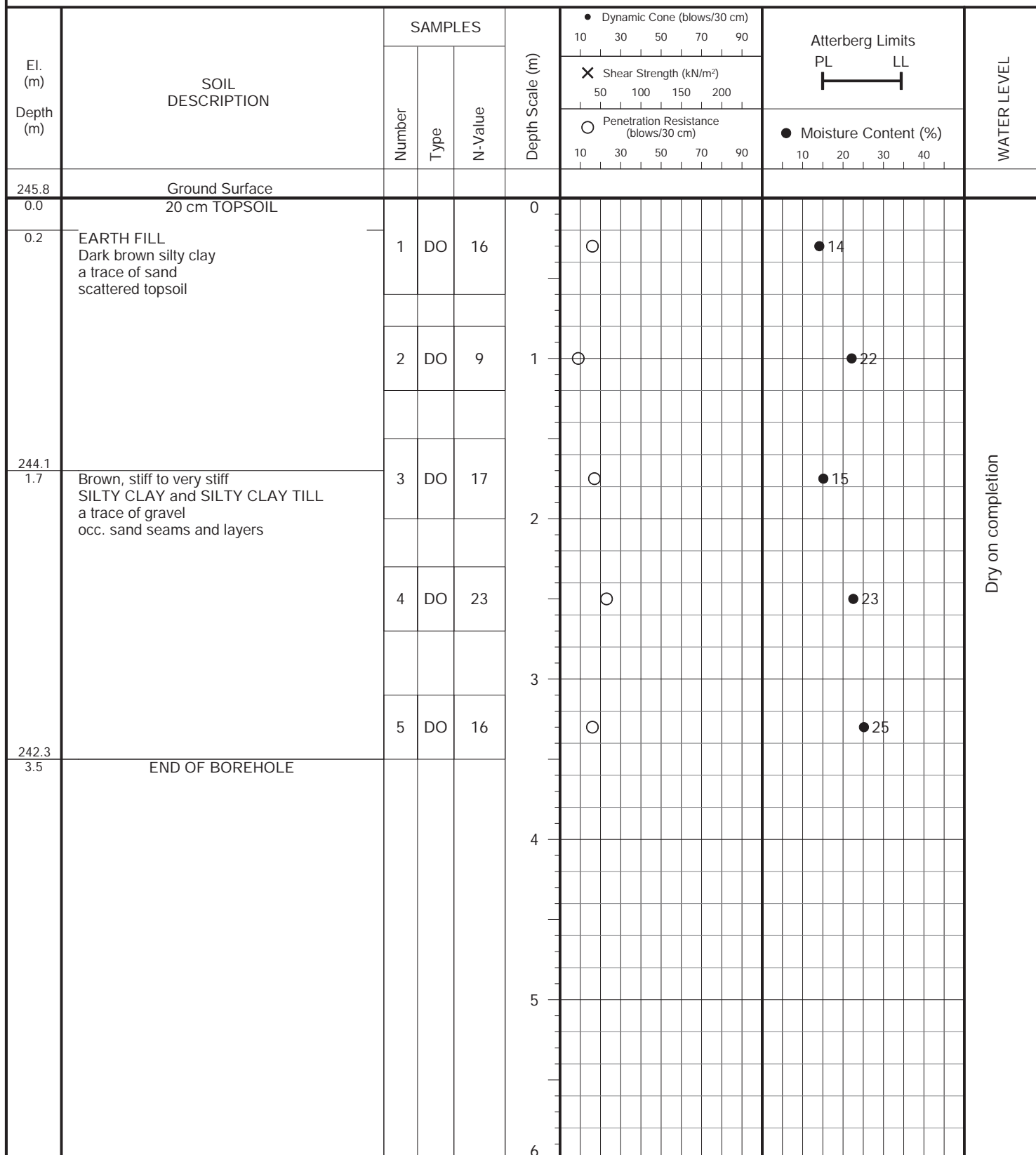
FIGURE NO.: 4

PROJECT DESCRIPTION: Proposed Truck and Trailer Parking

METHOD OF BORING: Flight Auger

PROJECT LOCATION: 12541 and 12577 Airport Road, Town of Caledon

DRILLING DATE: October 15, 2020



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# LOG OF BOREHOLE NO.: 5

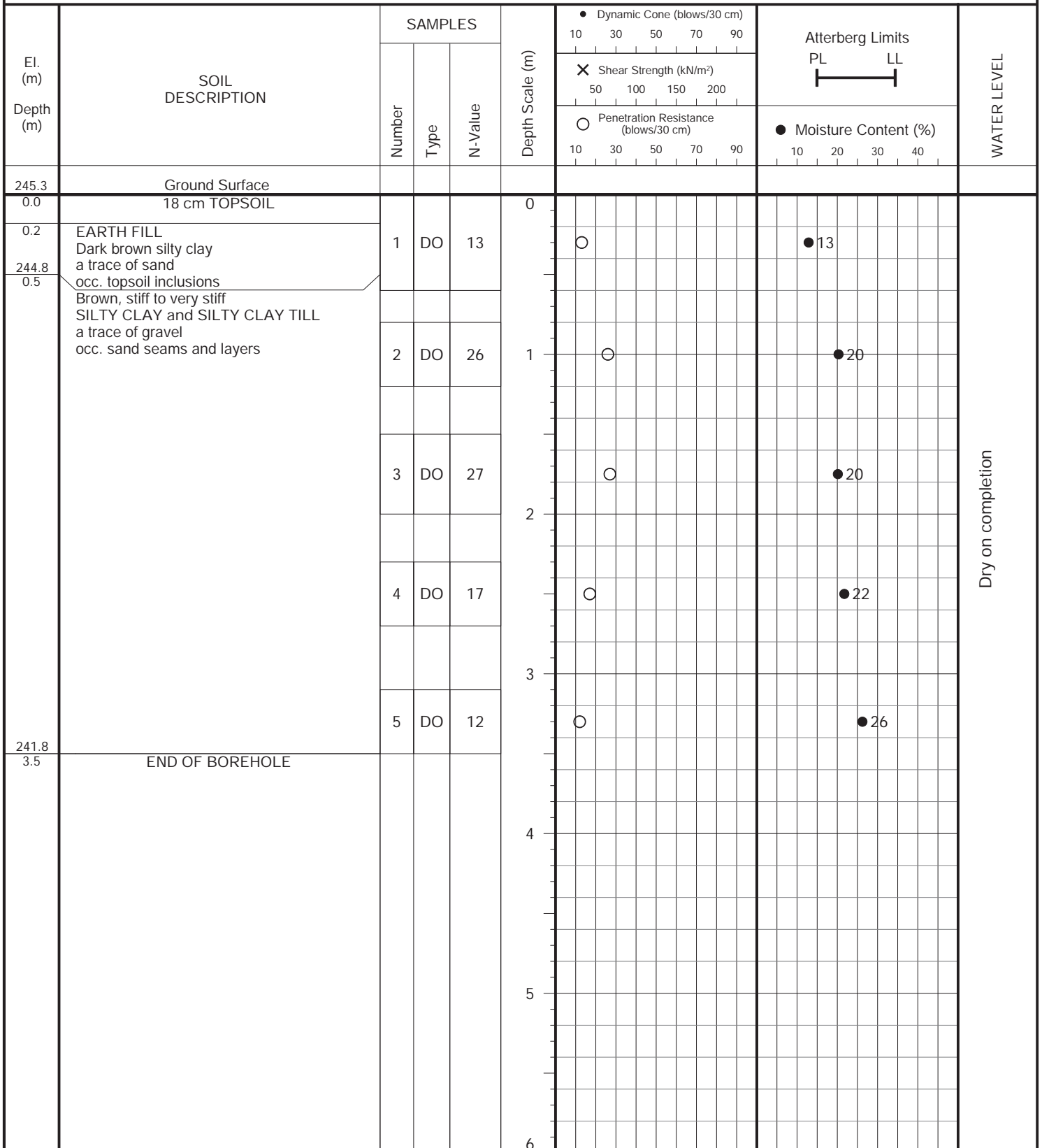
FIGURE NO.: 5

PROJECT DESCRIPTION: Proposed Truck and Trailer Parking

METHOD OF BORING: Flight Auger

PROJECT LOCATION: 12541 and 12577 Airport Road, Town of Caledon

DRILLING DATE: October 16, 2020



PROJECT DESCRIPTION: Proposed Truck and Trailer Parking

METHOD OF BORING: Flight Auger

PROJECT LOCATION: 12541 and 12577 Airport Road, Town of Caledon

DRILLING DATE: October 16, 2020

El. (m)	SOIL DESCRIPTION	SAMPLES			Depth Scale (m)	Dynamic Cone (blows/30 cm)		Atterberg Limits		WATER LEVEL			
		Number	Type	N-Value		10	30	50	70		90	PL	LL
245.8	Ground Surface												
0.0	20 cm TOPSOIL				0								
0.2	EARTH FILL Dark brown silty clay a trace of sand occ. topsoil and organic inclusions	1	DO	12		○			● 16				
244.9	Brown, stiff to hard SILTY CLAY and SILTY CLAY TILL a trace of gravel occ. sand seams and layers	2	DO	19	1	⊕			● 13				
0.9													
										○		● 22	
										○		● 24	
										○		● 25	
242.3	END OF BOREHOLE				3.5								

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# LOG OF BOREHOLE NO.: 7

FIGURE NO.: 7

PROJECT DESCRIPTION: Proposed Truck and Trailer Parking

METHOD OF BORING: Flight Auger

PROJECT LOCATION: 12541 and 12577 Airport Road, Town of Caledon

DRILLING DATE: October 16, 2020

El. (m)	Depth (m)	SOIL DESCRIPTION	SAMPLES			Depth Scale (m)	Dynamic Cone (blows/30 cm)		Atterberg Limits		WATER LEVEL
			Number	Type	N-Value		10	30	50	70	
246.3		Ground Surface									
0.0		18 cm TOPSOIL				0					
0.2		EARTH FILL Dark brown silty clay a trace of sand occ. topsoil and organic inclusions Stiff to hard SILTY CLAY and SILTY CLAY TILL a trace of gravel occ. sand seams and layers  --- brown grey	1	DO	15	0.2	○			● 15	
245.8			2	DO	24	1.0	○			● 14	
0.5			3	DO	31	1.8	○			● 16	
			4	DO	33	2.6	○			● 12	
			5	DO	65	3.4	○			● 9	
242.8		END OF BOREHOLE				3.5					

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# LOG OF BOREHOLE NO.: 8

FIGURE NO.: 8

PROJECT DESCRIPTION: Proposed Truck and Trailer Parking

METHOD OF BORING: Flight Auger

PROJECT LOCATION: 12541 and 12577 Airport Road, Town of Caledon

DRILLING DATE: October 16, 2020

El. (m)	SOIL DESCRIPTION	SAMPLES			Depth Scale (m)	Dynamic Cone (blows/30 cm)		Atterberg Limits		WATER LEVEL
		Number	Type	N-Value		10	30	50	70	
244.1	Ground Surface									
0.0	18 cm TOPSOIL				0					
0.2	EARTH FILL Dark brown silty clay a trace of sand occ. topsoil and organic inclusions	1	DO	10		○			● 17	
243.0		2	DO	20	1	○			● 15	
1.1	Brown, very stiff SILTY CLAY and SILTY CLAY TILL a trace of gravel occ. sand seams and layers	3	DO	28		○			● 12	
		4	DO	28		○			● 20	
		5	DO	24		○			● 19	
240.6	END OF BOREHOLE				3.5					

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# LOG OF BOREHOLE NO.: 9

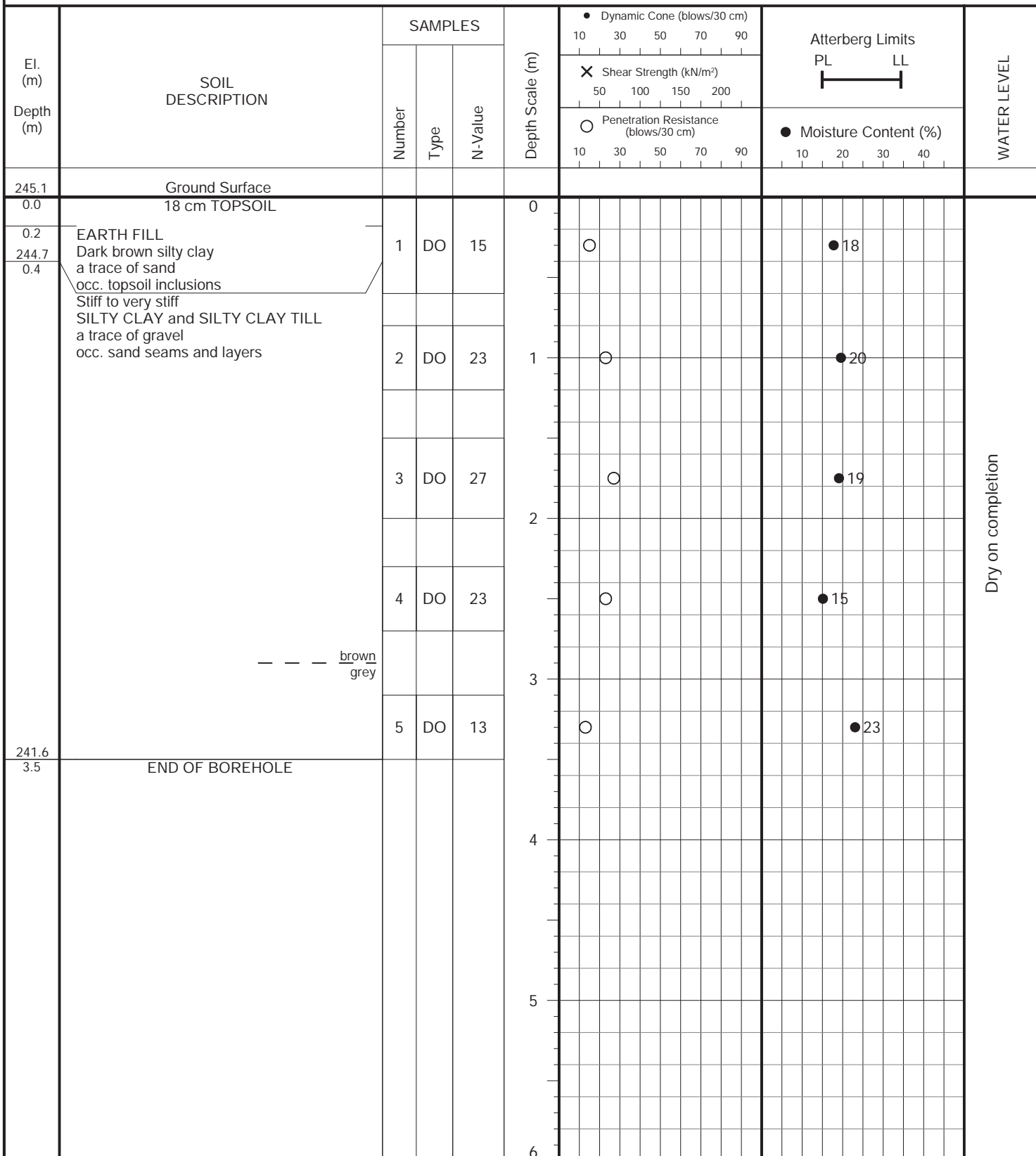
FIGURE NO.: 9

PROJECT DESCRIPTION: Proposed Truck and Trailer Parking

METHOD OF BORING: Flight Auger

PROJECT LOCATION: 12541 and 12577 Airport Road, Town of Caledon

DRILLING DATE: October 16, 2020





# GRAIN SIZE DISTRIBUTION

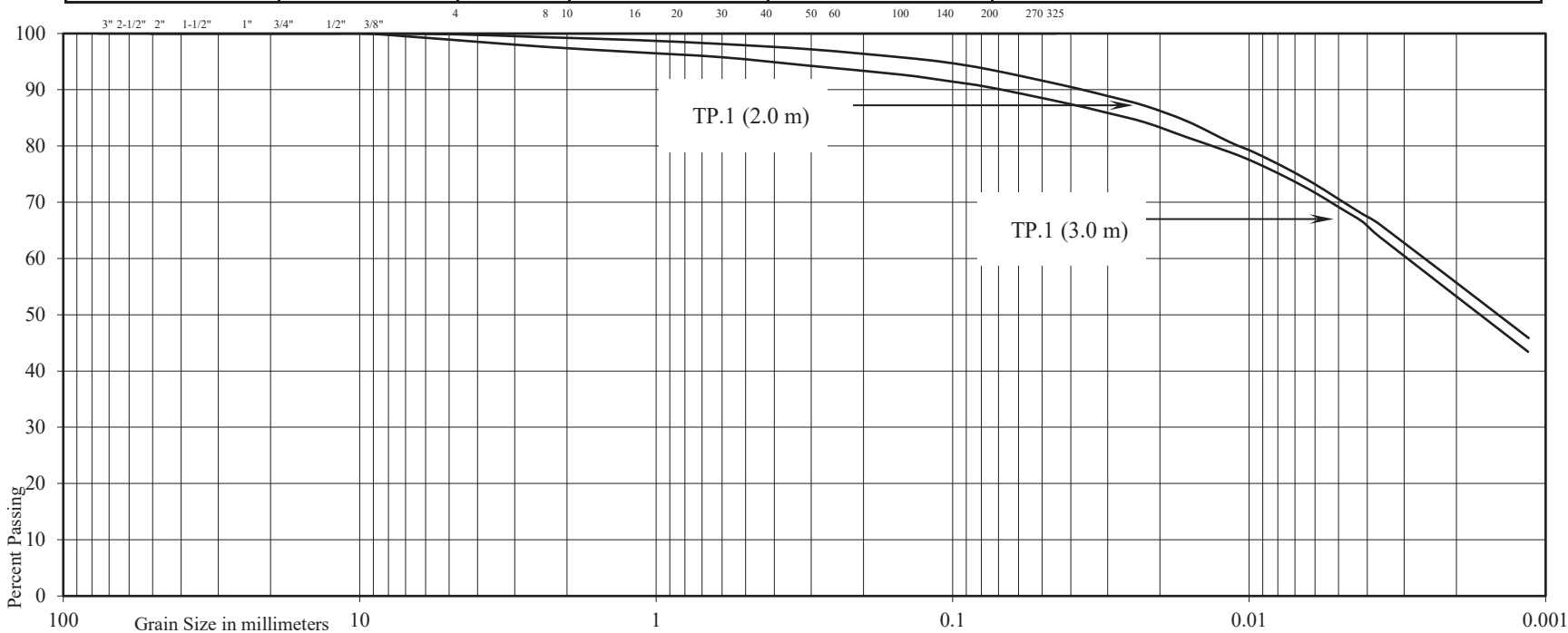
Reference No: 2009-W188

U.S. BUREAU OF SOILS CLASSIFICATION

GRAVEL				SAND				SILT	CLAY
COARSE		FINE		COARSE	MEDIUM	FINE	V. FINE		

UNIFIED SOIL CLASSIFICATION

GRAVEL			SAND				SILT & CLAY
COARSE	FINE		COARSE	MEDIUM	FINE		



Project: Proposed Truck and Trailer Parking  
 Location: 12541 and 12577 Airport Road, Town of Caledon  
 Test Pit No: 1 1  
 Sample No: - -  
 Depth (m): 2.0 3.0  
 Elevation (m): - -

	TP. 1 (2.0 m)	1 (3.0 m)
Liquid Limit (%) =	-	-
Plastic Limit (%) =	-	-
Plasticity Index (%) =	-	-
Moisture Content (%) =	-	-
Estimated Permeability		
(cm./sec.) =	10 <sup>-7</sup>	10 <sup>-7</sup>

Classification of Sample [& Group Symbol]:	TP.1 (2.0 m) - SILTY CLAY, a trace of sand
	TP.1 (3.0 m) - SILTY CLAY TILL, traces of sand and gravel

Figure: 12



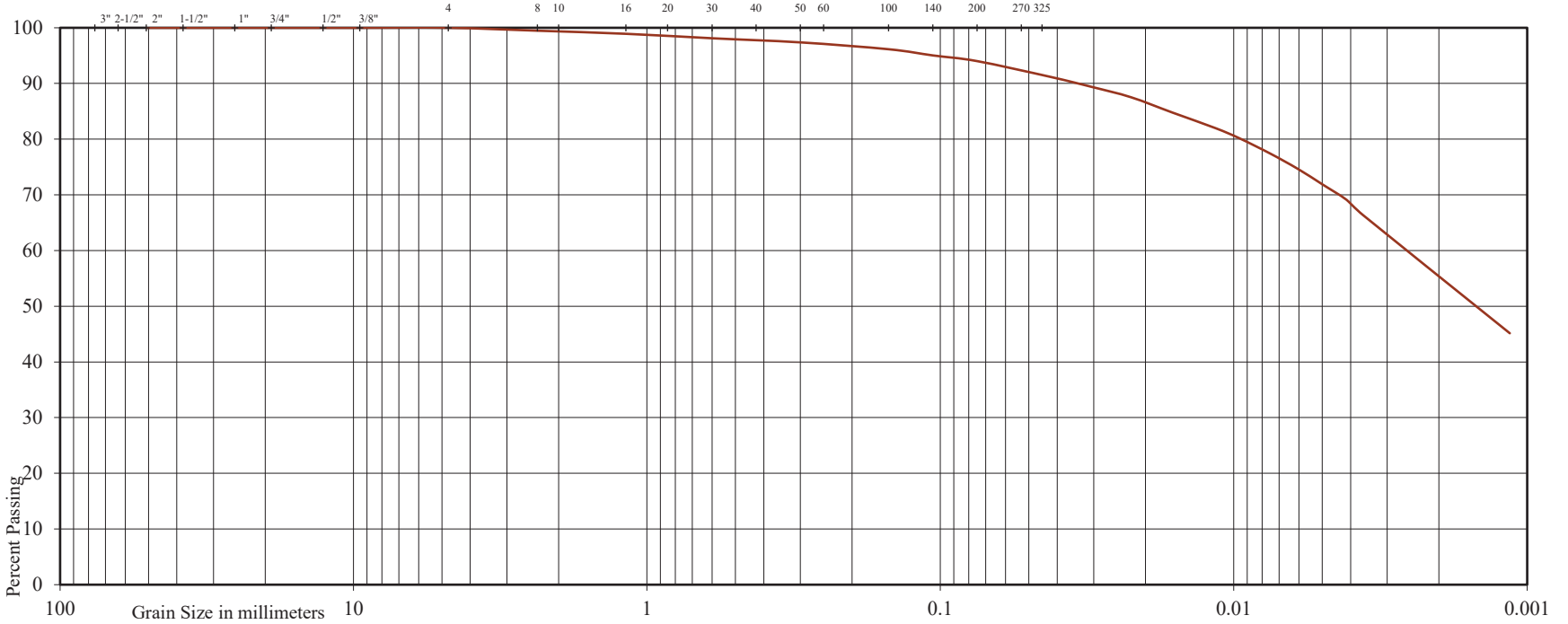
**GRAIN SIZE DISTRIBUTION**

U.S. BUREAU OF SOILS CLASSIFICATION

GRAVEL			SAND				SILT	CLAY
COARSE	FINE		COARSE	MEDIUM	FINE	V. FINE		

UNIFIED SOIL CLASSIFICATION

GRAVEL		SAND					SILT & CLAY
COARSE	FINE	COARSE	MEDIUM	FINE			



Project: Proposed Truck and Trailer Parking

Location: 12541 and 12577 Airport Road, Town of Caledon

Test Pit No: 2

Sample No: -

Depth (m): 4.0

Elevation (m): -

Liquid Limit (%) = -

Plastic Limit (%) = -

Plasticity Index (%) = -

Moisture Content (%) = -

Estimated Permeability

(cm./sec.) = 10<sup>-7</sup>

Classification of Sample [& Group Symbol]: SILTY CLAY, a trace of sand

Figure: 13



# GRAIN SIZE DISTRIBUTION

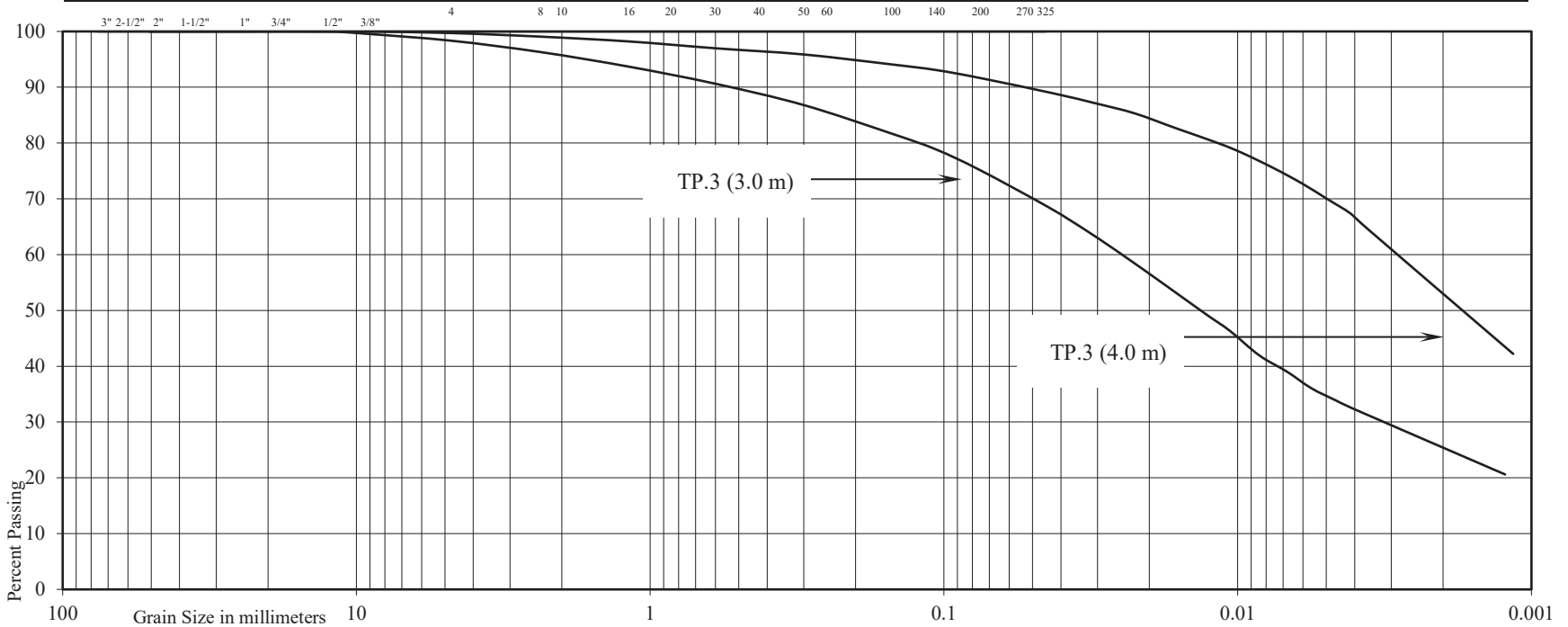
Reference No: 2009-S188

U.S. BUREAU OF SOILS CLASSIFICATION

GRAVEL				SAND				SILT	CLAY
COARSE		FINE		COARSE	MEDIUM	FINE	V. FINE		

UNIFIED SOIL CLASSIFICATION

GRAVEL			SAND					SILT & CLAY	
COARSE	FINE		COARSE	MEDIUM	FINE				



Project: Proposed Truck and Trailer Parking  
 Location: 12541 and 12577 Airport Road, Town of Caledon  
 Test Pit No: 3 3  
 Sample No: - -  
 Depth (m): 3.0 4.0  
 Elevation (m): - -

	TP. 3 (3.0 m)	3 (4.0 m)
Liquid Limit (%) =	-	-
Plastic Limit (%) =	-	-
Plasticity Index (%) =	-	-
Moisture Content (%) =	-	-
Estimated Permeability		
(cm./sec.) =	10 <sup>-7</sup>	10 <sup>-7</sup>

Classification of Sample [& Group Symbol]:	TP.3 (3.0 m) - SILTY CLAY TILL, sandy, a trace of gravel
	TP.3 (4.0 m) - SILTY CLAY, a trace of sand

Figure: 14

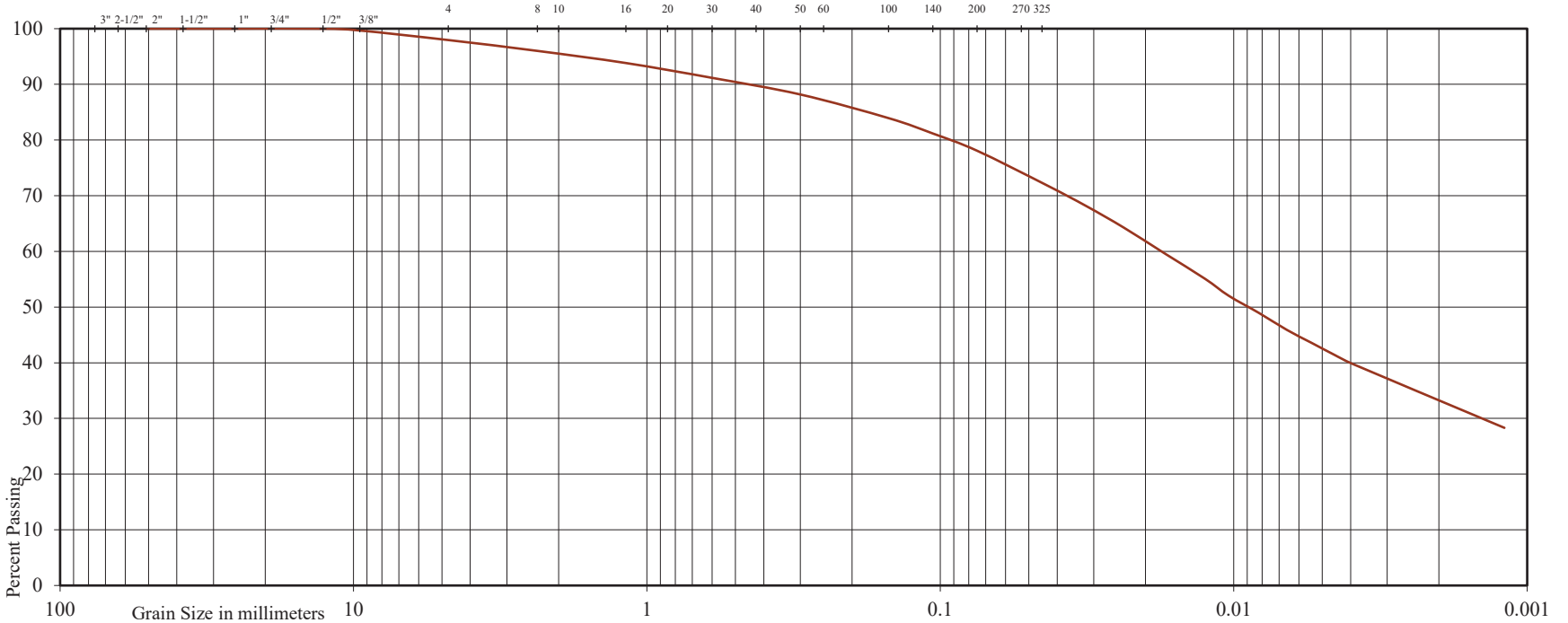


U.S. BUREAU OF SOILS CLASSIFICATION

GRAVEL			SAND				SILT	CLAY
COARSE	FINE		COARSE	MEDIUM	FINE	V. FINE		

UNIFIED SOIL CLASSIFICATION

GRAVEL		SAND				SILT & CLAY
COARSE	FINE	COARSE	MEDIUM	FINE		

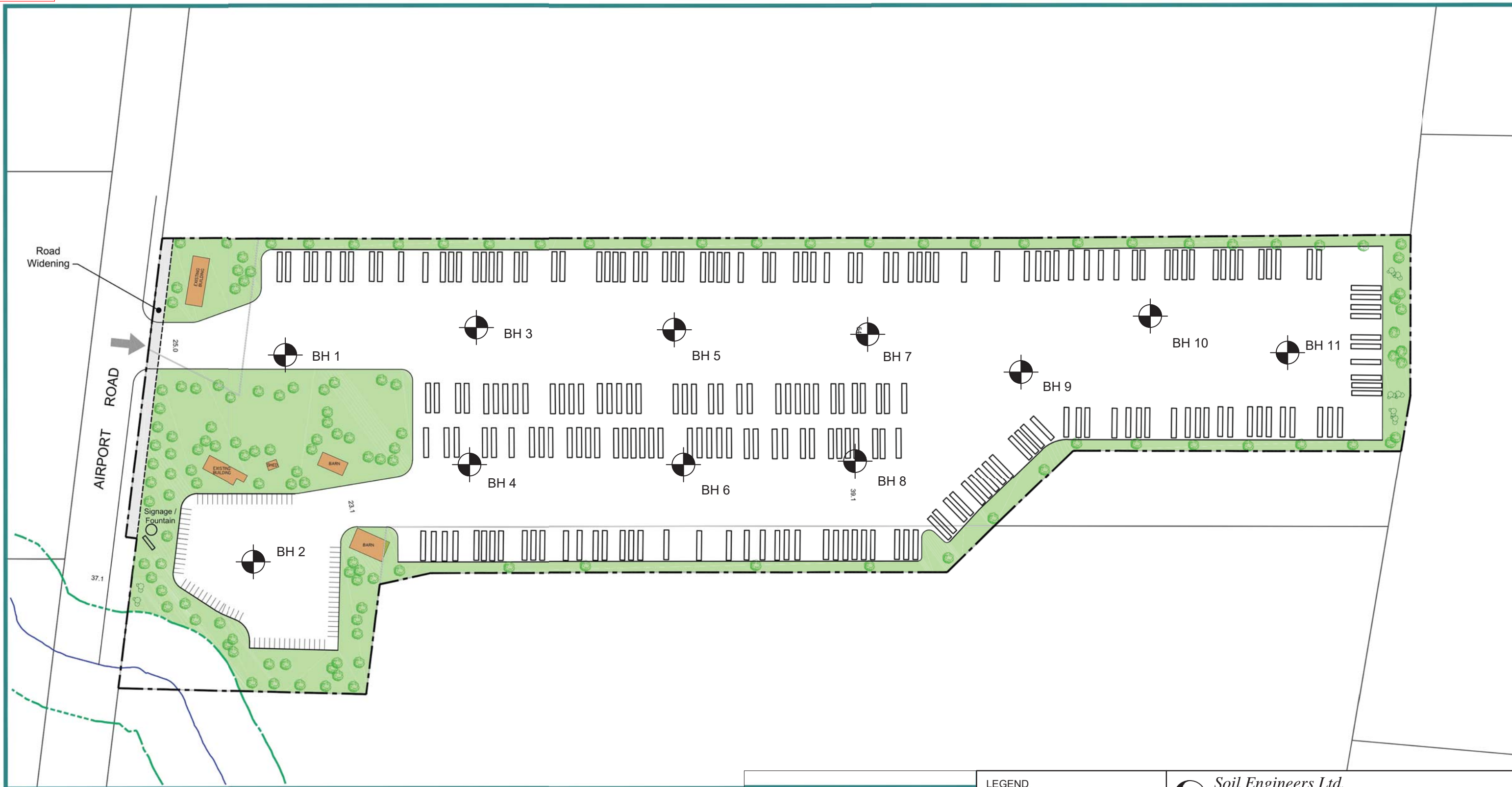


Project: Proposed Truck and Trailer Parking  
 Location: 12541 and 12577 Airport Road, Town of Caledon  
 Test Pit No: 4  
 Sample No:  
 Depth (m): 2.0  
 Elevation (m):

Liquid Limit (%) = -  
 Plastic Limit (%) = -  
 Plasticity Index (%) = -  
 Moisture Content (%) = -  
 Estimated Permeability  
 (cm./sec.) =  $10^{-7}$

Classification of Sample [& Group Symbol]: SILTY CLAY TILL, some sand to sandy, a trace of gravel

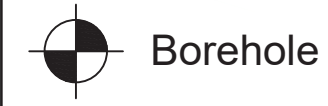
Figure: 15



--- Subject Lands - 11.85 ha  
 — Watercourse



LEGEND



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 90 WEST BEAVER CREEK ROAD, SUITE #100, RICHMOND HILL, ONTARIO L4B 1E7 - TEL: (416) 754-8515 - FAX: (905) 881-8335

Borehole Location Plan

SITE: 12541 and 12577 Airport Road, Town of Caledon

DESIGNED BY: D.Y.	CHECKED BY: B.S.	DWG NO.: 1
SCALE: 1:2000	REF. NO.: 2009-S188	DATE: November 2020
		REV





TOWN OF CALEDON  
PLANNING  
RECEIVED  
Mar 16, 2022



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SUBSURFACE PROFILE  
DRAWING NO. 3  
SCALE: AS SHOWN

JOB NO.: 2009-S188  
REPORT DATE: November 2020  
PROJECT DESCRIPTION: Proposed Truck and Trailer Parking  
PROJECT LOCATION: 12541 and 12577 Airport Road, Town of Caledon

**LEGEND**

TOPSOIL    FILL    SILTY CLAY and SILTY CLAY TILL

BH No.:	9	10	11
El. (m):	245.1	244.8	243.1

