

Broccolini Limited Partnership No. 6

Geotechnical Investigation Building 1 12304 Heart Lake Road Caledon, Ontario

Project Number BRM-21004344-C0

Prepared By:

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TOWN OF CALEDON PLANNING RECEIVED Nov 26, 2021

Broccolini Limited Partnership No. 6 Proposed Commercial Development Building 1 12304 Heart Lake Road, Caledon, Ontario BRM-21004344-C0

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1. Introduction

This report presents the results of a Geotechnical Investigation carried out at the site of a proposed commercial/industrial building development at 12304 Heart Lake Road in the Town of Caledon, Ontario. The work was authorized by Mr. Ben Wilson on behalf of Broccolini Limited Partnership No. 6.

It is understood that the proposed construction will comprise one (1) single storey slab on grade building without basement, supporting truck loading docks, paved accessways, sewers, and truck and passenger vehicle parking areas. The proposed building is designated Building 1 and will have a footprint of approximately 42,223 m² (~454, 485 ft.²).

The purpose of this study was to determine the subsurface conditions at the site. In this regard, thirty (30) boreholes evenly located to provide representative coverage of the site were drilled for preliminary Geotechnical Investigation purposes with findings detailed in Preliminary Geotechnical report dated April 21, 2021. Upon receipt of the proposed development layout for Building 1 illustrated on a plan provided by the client, it was determined that the existing boreholes provided adequate coverage for design purposes for this building. Based on the existing information, geotechnical engineering guidelines for the design and construction of the proposed development would be provided.

The comments and recommendations given in this report are based on the assumption that the design concept described will proceed into construction. If changes are made either in the design phase or during construction, this office must be retained to review these modifications. The result of this review may be a modification of our recommendations or the requirement of additional field or laboratory work to check whether the changes are acceptable from a geotechnical viewpoint.



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2. Procedure

Drilling and sampling operations, carried out between March 16 and 25, 2021, were completed by a combination of auger and split-spoon techniques with drilling equipment owned and operated by a specialist contractor. A total of thirty (30) boreholes, designated as Boreholes 1 to 30, was drilled for this investigation. The boreholes were advanced to depths of approximately 7.8 to 8.2 m and spaced to provide representative coverage of the site. This report addresses the location of proposed Building 1 on the southwest portion of the site. As such Boreholes 17 to 20 and 24 to 27 are applicable. The approximate borehole locations are shown on the attached Borehole Location Plan (Drawing No. 1).

A representative of EXP Services Inc. (EXP) was present throughout the fieldwork to monitor and direct the drill operations, and to record borehole information. Representative samples of the subsurface soils were recovered at regular intervals using conventional 50 mm O.D. split spoon sampling equipment driven in accordance with Standard Penetration Test procedures (ASTM D1586). All split spoon samples were returned to EXP's Brampton laboratory for testing which included moisture content and unit weight determinations on selected samples. Water levels were monitored in the open boreholes prior to backfilling and in the monitoring well installed in Borehole 25.

The borehole locations were established in the field by EXP personnel. Elevations were measured using a Sokkia GCS3 Global Navigation Satellite System (GNSS) receiver based on information derived from the TopNET Live Network Service Global Positioning System (GPS).



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3. Site Description

The project site occupies an area of 37.04 hectares (91.52 acres) in the Town of Caledon, Ontario. The property consists of mainly farmland. Two (2) residences are located at the east-central and southeast portions of the property respectively, fronting onto Heart Lake Road. A third homestead and associated farm buildings are located in the north central portion of the site. The property is irregular in shape and is located on the west side of Heart Lake Road, with frontage centred approximately 845 m north of Mayfield Road. This report is specific to proposed Building 1 located on the southwest portion of the site.



4. Subsurface Conditions

The detailed soil profiles encountered in each borehole and the results of moisture content and unit weight determinations are indicated on the attached borehole logs. It should be noted that the soil boundaries indicated on the borehole logs are inferred from non-continuous sampling and observations during drilling. These boundaries are intended to reflect approximate transition zones for the purpose of geotechnical design and should not be interpreted as exact planes of geological change.

The "Notes on Sample Description" preceding the borehole logs form an integral part of and should be read in conjunction with this report.

The soil stratigraphy at the southwest portion of the site consists of surficial topsoil over a discontinuous fill layer underlain by native deposits of clayey silt till and sandy silt till. Following is a brief description of the soil conditions encountered during the investigation.

Topsoil

Surface cover comprises topsoil ranging in thickness from approximately 130 to 280 mm at all borehole locations. However, the boreholes were advanced in cultivated fields. As such, topsoil thicknesses up to approximately 600 mm associated with typical ploughed fields should be anticipated.

It should be noted that topsoil measurements were carried out at the borehole locations only and could differ at other locations on the site. If required, a more detailed test pit program should be carried out to more accurately quantify the amount of topsoil to be removed for construction purposes.

Fill

Fill was encountered following the topsoil in Boreholes 20 and 27. The fill extends to a depth of approximately 1.4 m (~Elevation 270.0 to 270.1 m). The fill constitutes brown clayey silt to sandy silt with trace gravel and minor stone fragments and appeared to be reworked on-site parent material. Moisture contents recorded in the fill ranged between approximately 12 and 15 percent. The higher moisture contents were recorded in the upper regions of the fill and are likely associated with the transition from recently melted snow in the topsoil overlying the fill.

Clayey Silt Till

A clayey silt till deposit underlies the fill in Boreholes 20 and 27 and the topsoil at all other borehole locations. The clayey till extends to termination depth of approximately 8.1 m (~Elevation 258.7 to 260.3 m) in Boreholes 17 and 25. The clayey silt till was fully



penetrated approximately 4.1 to 7.1 m depth (~Elevation 260.0 to 265.8 m) in the remaining boreholes. The clayey silt till was found to be disturbed in the upper 200 to 300 mm at several borehole locations. The clayey silt till contains trace sand or fine sand seams/pockets, trace gravel and occasional boulder fragments. The clayey silt till is typically brown in colour becoming grey with depth. The consistency of the clayey silt till is generally very stiff to hard. Localized stiff zones were noted at depth in Boreholes 24 and 27, generally consistent with the change in colour from brown to grey. Moisture contents of the clayey silt till were recorded between approximately 8 and 16 percent.

Sandy Silt Till

A sandy silt till deposit was intersected below the clayey silt till in Boreholes 18 to 20, 24, 26 and 27. All boreholes where the sandy silt till was encountered were terminated in this deposit at depths of approximately 7.8 to 8.1 m (~Elevation 259.0 to 263.6 m). The sandy silt till contains trace clay, silt partings, fine sand seams, trace gravel and occasional boulder fragments. The sandy silt till is grey in colour except for Boreholes 18 and 20 where the deposit is brown. The degree of compactness of the sandy silt till was assessed as dense to very dense. Moisture content of the sandy silt till generally ranges from approximately 6 to 18 percent.

Groundwater Conditions

Groundwater conditions were assessed in the open boreholes and in the monitoring well installed in Borehole 25 during the course of the fieldwork.

Short term groundwater levels are recorded on the attached borehole logs. Upon completion of drilling, free water was observed in Borehole 19 at a depth of approximately 6.4 m below existing grade. The remaining boreholes were dry upon completion of augering.

Subsequently, the groundwater level in the monitoring well installed in Borehole 25 was measured and recorded, with the results summarized in the following Table 1.

| Borehole No. | Elapsed Time | Water Level – Depth below grade (m) | Elevation (m) | | |
|--------------|---------------|--|---------------|--|--|
| 25 | After 17 Days | 1.5 | 266.9 | | |

Table 1: Groundwater Level Readings

Based on the information observed in the boreholes, the groundwater originates from the more pervious wet sand seams in the clayey silt till and sandy silt till on the site.



The groundwater elevations reflect the conditions at the time of the investigation. Groundwater elevations are subject to seasonal fluctuations.

The monitoring well was installed in general accordance with the Ontario Water Resources Act-R.R.O. 1990, Regulation 903 – Amended to O. Reg. 128/03 by CSD, by a licensed well contractor. When the use of the monitoring well is no longer required, it must be decommissioned in accordance with the procedure outlined in the Ontario Water Resources Act – R.R.O. 1990, Regulation 903 – Amended to O. Reg. 128/03.



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5. Geotechnical Assessment

5.1 Site Grading

It is our understanding that the final site grades have not been established at the time of this investigation. However, based on surface elevations at the borehole locations, relief of approximately 4.7 m exists over the southwest portion of the site. As such, it is anticipated that some regrading (cut and fill operations) will be carried out at the site. The following procedures are recommended for the construction of fill sections for pavement and building areas at the site, where required.

- All vegetation, topsoil, organic or deleterious materials, existing fill and former building foundations etc. should be removed from beneath the proposed building and pavement areas.
- The exposed subgrade surface should be proofrolled with a heavy vibratory roller and examined by a geotechnical engineer. Any soft areas detected during the proofrolling process should be subexcavated.
- The area can then be brought up to the final subgrade level with approved on-site or imported material placed in lifts not exceeding 200 mm and compacted to the following requirements:
 - I. Within the building areas minimum of 98 percent standard Proctor maximum dry density (SPMDD) for slab-on-grade support. If foundations are to be placed on engineered fill, the fill should be compacted to 100% SPMDD.
 - II. Pavement areas minimum of 95 percent SPMDD to within 600 mm of final subgrade level and 98 percent SPMDD for the upper 600 mm.
 - III. General backfill including trench backfill and backfill adjacent to foundation walls minimum of 98 percent SPMDD.
 - All backfilling and compaction operations should be monitored on a full-time basis by qualified geotechnical personnel to approve material, evaluate placement operations and confirm the specified degree of compaction is achieved uniformly throughout the fill.
 - Where free-draining backfill is required, or in confined areas, imported granular material conforming to OPSS Granular 'B' is recommended.



5.2 Foundation Considerations

Based on the results of the investigation, conditions suitable for support of the proposed structure were available at all borehole locations within or close to the proposed building envelope. The proposed structure can be supported on conventional spread and strip footings or augered piers founded at depths of 1.0 to 2.0 m (~Elevation 265.3 to 269.5 m) below all fill on the undisturbed native clayey silt till. The footings can be designed for a geotechnical reaction at Serviceability Limit States (SLS) of 300 kPa and factored geotechnical resistance of 450 kPa at Ultimate Limit States (ULS), subject to geotechnical inspection during construction.

Typically, the piers can be cleaned by the augers. The final cleaning of the bases can then be auger cleaned by mixing the loose materials at the base of the piers with 0.3 to 0.5 m thick concrete. The mixture should then be removed. During the installation of piers, a temporary steel liner will have to be installed to prevent caving of the drilled hole and to seal off any water which may be perched in the water bearing seams above the founding levels. A positive head of concrete inside the liner with respect to any exterior groundwater levels must be maintained during withdrawal of the liner. A 150 mm slump concrete is recommended for use to prevent the concrete from having a honeycombed structure and to avoid bridging in the liner upon its withdrawal.

The following Table 2 shows the highest elevations at the borehole locations where the afore mentioned bearing values in the native soils can be applied.

| Borehole No. | Existing Grade Elevation (m) | Founding Material | Spread and Strip Footing/Augered Pier SLS 300 kPa / ULS 450 kPa ~ Elevation (Depth Below Existing Grade (m)) | | | | |
|-----------------|---------------------------------------|----------------------|--|--|--|--|--|
| | | E | Building 1 | | | | |
| 17 | 266.8 | Clayey Silt Till | 265.3 (1.5) | | | | |
| 18 | 267.8 | Clayey Silt Till | 266.8 (1.0) | | | | |
| 19 | 268.7 | Clayey Silt Till | 267.7 (1.0) | | | | |
| 20 | 271.4 | Clayey Silt Till | 269.4 (2.0) | | | | |
| 24 | 267.1 | Clayey Silt Till | 266.1 (1.0) | | | | |
| 25 | 268.4 | Clayey Silt Till | 267.4 (1.0) | | | | |
| 26 | 270.2 | Clayey Silt Till | 269.2 (1.0) | | | | |
| 27 | 271.5 | Clayey Silt Till | 269.5 (2.0) | | | | |

Table 2: Highest Elevation at Borehole Locations Where Recommended Geotechnical Reaction/Resistance Can Be Applied

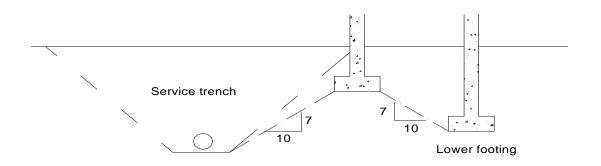


Alternatively, the structure can be supported at nominal depths on engineered fill placed on prepared subgrade and designed for geotechnical reaction of 150 kPa at SLS and factored geotechnical resistance of 225 kPa at ULS. General guidelines and requirements for foundation support on engineered fill are shown on Appendix A.

The engineered fill construction should be monitored on a full-time basis by geotechnical personnel from EXP to examine and approve fill materials, to evaluate placement operations, and to verify that the specified degree of compaction is being achieved uniformly throughout the fill.

5.3 Foundations General

Footings/piers at different elevations should be located such that higher footings/piers are set below a line drawn up at 10 Horizontal to 7 Vertical from the near edge of the lower footing/pier. This concept should also be applied to excavations for new foundations in relation to existing footings or underground services. This concept is illustrated in the following sketch.



FOOTINGS NEAR SERVICE TRENCHES OR AT DIFFERENT ELEVATIONS

All footings/ piers exposed to freezing conditions must be provided with a minimum of 1.2 m of earth cover or equivalent insulation for frost protection, depending on the final grade requirements.

Provided that the soil is not disturbed due to groundwater, precipitation, traffic, etc., and the aforementioned geotechnical reactions/resistances are not exceeded, then total and differential settlements should be small and within the normally tolerated limits of 25 mm and 19 mm, respectively.



The recommended bearing capacities have been calculated by EXP from the borehole information for the design stage only. The investigation and comments are necessarily ongoing as new information of underground conditions becomes available. For example, it should be appreciated that modifications to bearing levels may be required if unforeseen subsoil conditions are revealed after the excavation is exposed to full view or if final design decisions differ from those assumed in this report. For this reason, this office should be retained to review final foundation drawings and to provide field inspections during the construction stage.

5.4 Floor Slabs and Permanent Drainage

The native soil encountered in the boreholes appears generally suitable for floor slab support. For normal slab-on-grade construction, all topsoil, existing fill, former building foundations and other deleterious material should be removed from the entire underfloor area. Following site grading the exposed subgrade surface should then be thoroughly proof-rolled with a heavy vibratory roller. Any soft spots detected should be sub-excavated and replaced with compactible fill in the manner described in Section 5.6 - "Backfill Considerations" section of this report. The site can then be filled to the required grades as outlined in Section 5.1 - "Site Grading". This process also provides an opportunity for replacement of the fill as Engineered Fill capable of supporting foundations as discussed earlier.

A Modulus of Subgrade Reaction k_s of 27 MN/m³ (170 kcf) may be applied to subgrade prepared in accordance with the foregoing procedures for design purposes.

A 200 mm layer of 19 mm clear stone should be placed between the prepared subgrade and the floor slab to serve as a moisture barrier. Also, within any unheated areas and entrances to buildings, Styrofoam insulation should be provided below the floor slab and against the foundation walls to protect against frost heave.

Based on the soil and groundwater conditions at the Building 1 portion of the site, underfloor drains will not be required. Perimeter drains are not required if the floor slab of the building is set at least 200 mm above the existing exterior grade.

Around the perimeter of the building the ground surface should be sloped on a positive grade away from the structure to promote surface water run-off and reduce groundwater infiltration adjacent to the foundations.

5.5 Excavations and Groundwater Control

All excavation must be carried out in accordance with the most recent Occupational Health and Safety Act. The fill is classified as Type 3 soil. The clayey silt till and sandy silt till are



classified as Type 2 soils. Where loose/soft materials are encountered locally, or within zones of persistent seepage at depth, it may be necessary to flatten the side slopes.

It should be noted that the presence of cobbles and boulders in glacial till deposits may influence the progress of excavation. Consequently, provisions should be made in the contract documents to cover any delays caused by these obstructions.

Some seepage of free water from more pervious seams and layers within the native soils should be anticipated during construction. However, it should be possible to control and remove any such seepage by pumping from temporary sumps and ditches and/or oversized excavations.

5.6 Backfill Considerations

Backfill used to satisfy underfloor slab requirements, in footings and service trenches, etc., should be compactible fill, i.e., inorganic soil with its moisture content close to its optimum moisture content determined in the standard Proctor maximum dry density test. For ease of compaction and quality control in confined areas, sand fill such as Ontario Provincial Standard Specifications (OPSS) 1010 Granular 'B' is recommended. The backfill should be placed in lifts not more than 200 mm thick in the loose state, each lift being compacted to at least 98 percent SPMDD under the floor slab and 95 percent SPMDD elsewhere, before subsequent lifts are placed. The degree of compaction achieved in the field should be checked by in-place density tests.

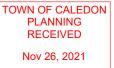
The majority of excavated material will likely consist of the upper fill and clayey silt till. In general, the moisture contents of the fill material are higher than optimum and may be reused for structural backfill only if they are free of topsoil inclusions or other obviously unsuitable material, and partial drying is carried out. Any organic or excessively wet or otherwise deleterious material should not be used for backfill purposes. Any shortfall of suitable on-site excavated material can be made up with imported granular material, OPSS Granular 'B' or equivalent.

In general, the overburden soils are not free draining and therefore should not be used where this characteristic is required, or in confined areas. Imported granular material conforming to OPSS Granular 'B' would also be suitable for these purposes.

5.7 Earthquake Considerations

The recommendations for the geotechnical aspects to determine the earthquake loading for design using the OBC 2012 are presented below.





5.7.1 Subsoil Conditions

The subsoil and groundwater information at this site have been examined in relation to Section 4.1.8.4 of the OBC 2012. The subsoils generally consist of clayey silt to sandy silt fill, clayey silt till and sandy silt till. It is anticipated that the floor slab of the proposed structure will be founded on stiff to hard clayey silt till.

5.7.2 Depth of Boreholes

Table 4.1.8.4.A. Site Classification for Seismic Site Response in OBC 2012 indicated that to determine the site classification, the average properties in the top 30 m (below the lowest basement level) are to be used. The deepest borehole advanced at this portion of the site was at about 8.1 m depth. Therefore, the site classification recommendation would be based on the available information as well as our interpretation of conditions below the boreholes based on our knowledge of the soil conditions in the area. The assumed undrained shear strength for the cohesive soils to 30 m depth will be greater than 100 kPa. The assumed N-values for the granular soil to 30 m depth will have an average value greater than 50.

5.7.3 Site Classification

Based on the above assumptions and currently available information, the Site Class for the proposed building is "C" as per Table 4.1.8.4.A, Site Classification for Seismic Site Response, OBC 2012.

5.8 Retaining Walls

Based on the relief over the Building 1 portion of the site as evidenced by the borehole collar elevations, retaining walls and loading dock walls may be required. Backfill behind the retaining walls should consist of free-draining granular material. Filter cloth should be placed between the retaining wall and the granular backfill material. A perimeter tile drain or weep holes should also be provided in the structure to prevent hydrostatic pressure build-up.



The lateral earth pressure acting on the retaining or loading dock walls may be calculated from the following equation:

$$p = k (\gamma h + q)$$

where:

p = the pressure in kPa acting against any retaining wall at depth,h, below the ground surface;

- k = the earth pressure coefficient;
- γ = the bulk unit weight of the retained free draining granular backfill;
- h = the depth in m below the ground surface at which the pressure, p, is to be computed; and
- q = the value of any adjacent surcharge in kPa which may be acting close to the wall.

The foregoing expression assumes an effective perimeter tile drain system will be incorporated to prevent the build-up of hydrostatic pressure behind the retaining wall. To minimize infiltration of surface water behind exterior retaining walls, the upper 600 mm of backfill should comprise compacted relatively impervious material.

For design purposes, the following physical properties of the on-site native soils can be used:

Coefficient of Lateral Earth Pressures: $K_a = 0.3$; $K_p = 3.0$

Unit Weight = 23 kN/m³

5.9 Parking Areas and Internal Access Roads

The recommended pavement structures provided in Table 3 are based upon an estimate of the subgrade soil properties determined from visual examination and textural classification of the soil samples. A functional design life of 8 to 10 years has been used to establish the pavement recommendations. This represents the number of years to the first rehabilitation, assuming regular maintenance is carried out. Other thickness combinations can be used provided the Granular Base Equivalency (GBE) is maintained and any minimum component thickness specified by the Town of Caledon is met.



| Pavement Layer | Compaction Requirements | Light-Duty Parking (Cars) | Heavy Duty Traffic (Trucks) Shipping Docks and Access Road | | |
|----------------------------------|----------------------------|------------------------------|---|--|--|
| Asphaltic Concrete (OPSS 310) | Minimum 92 % MRD** | 40 mm HL3 65 mm HL8 | 40 mm HL3 110 mm HL8 | | |
| 19 mm Crusher Run Limestone | 100% SPMDD* | 150 mm | 150 mm | | |
| 50 mm Crusher Run Limestone | 100% SPMDD* | 300 mm | 450 mm | | |

Table 3: Recommended Pavement Structure Thickness

* Denotes standard Proctor maximum dry density, ASTM-D698

** Denotes Maximum Relative density, MTO LS-264

Where rigid pavements are required such as the truck loading dock apron area and dolly pads for trailer parking, recommended pavement structures are summarized in Table 4.

| Pavement Layer | Compaction Requirements | Concrete Pads Adjacent to Loading Docks | Concrete Dolly Pads | |
|---|----------------------------|---|---------------------|--|
| Concrete CSA Class C-2 32 MPa | - | 230 mm | 200 mm (4) | |
| 19 mm Crusher-run Limestone (OPSS 1010) | 100% SPMDD (2) | 200 mm | 70 mm | |
| 50 mm Crusher-run Limestone (OPSS 1010) | 100% SPMDD (2) | - | 500 mm | |

Table 4: Recommended Pavement Structure Thickness (Rigid)

Notes: (2) Denotes standard Proctor maximum dry density, MTO LS-706 (Procedure 3)

(4) The concrete dolly pads should be 200mm thick with shrinkage steel.

The concrete for this project should be C-2 Class as a minimum, i.e., 32 MPa, 0.45 maximum water/cement ratio. The nominal aggregate size in the mix should be 37.5 mm and the air content should range from 4 to 7%.

The subgrade must be compacted to 98 percent SPMDD for at least the upper 600 mm.

The long-term performance of the pavement structure is highly dependent upon the subgrade support conditions. Stringent construction control procedures should be maintained to ensure uniform subgrade moisture and density conditions are achieved. In

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addition, the need for adequate drainage cannot be over-emphasized. The finished pavement surface should be free of depressions and should be sloped to provide effective surface drainage toward catch basins. Subdrains should be installed to intercept excess subsurface moisture and to prevent subgrade softening. This is particularly important in heavy-duty pavement areas.

Additional comments on the construction of parking areas and access roadways are as follows:

- 1. As part of the subgrade preparation, proposed parking areas and access roadways should be stripped of topsoil and other obvious objectionable material. Fill required to raise the grade to design elevations should conform to backfill requirements outlined in previous sections of this report. The subgrade should be proof-rolled in the full-time presence of qualified geotechnical personnel. Soft or spongy subgrade areas should be sub-excavated and properly replaced with suitable approved backfill compacted to 98 percent SPMDD. The final subgrade surface should then be properly shaped and crowned.
- 2. Assuming that satisfactory cross-falls have been provided for subdrainage, subdrains extending from and between catch basins may be satisfactory. Further, subdrains should also be installed along the perimeter of pavement areas as well as around landscaped areas and temporary snow storage areas.
- 3. The most severe loading conditions on light-duty pavement areas and the subgrade may occur during construction. Consequently, special provisions such as restricted access lanes, half-loads during paving, etc., may be required, especially if construction is carried out during unfavorable weather.
- 4. To minimize the problems of differential movement between the pavement and catchbasins/manholes due to frost action, the backfill around the structures should consist of free-draining granular.
- 5. To prevent water ponding at the lower pavement areas of loading docks, it is recommended that catchbasins be provided to drain the surface run-offs.



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6. Chemical Testing

6.1 Chemical Testing Program

The scope of work for this project included chemical testing of soil from the boreholes to assist in selection of disposal options for excess soils that may be generated through construction. Accordingly, nine (9) soil samples including one (1) duplicate from the boreholes and one (1) soil sample from a granular stockpile noted on site were submitted for bulk chemical testing. The samples were analyzed for minimum sampling requirements outlined in O. Reg. 406/19 for metals, hydride-forming metals, electrical conductivity (EC), sodium adsorption ratio (SAR), benzene, toluene, ethyl benzene and xylene (collectively 'BTEX') and petroleum hydrocarbons (PHC) in accordance with the Ministry of the Environment, Conservation and Parks (MECP) document "Rules For Excess Soil Management And Excess Soil Quality Standards" covered under O.Reg.406/19. One (1) of the samples from the boreholes was also tested for Sulphate to assess potential for sulphate attack on subsurface concrete.

In addition, three (3) selected soil samples were subjected to the modified Synthetic Precipitation Leaching Procedure ('mSPLP') analysis for metals covered under O.Reg.406/19.

Since these samples were submitted to the analytical laboratory under one (1) chain of custody, the Certificate of Analysis cannot be separated to reflect only those samples from the Proposed Building 1 portion of the site. As such, the test results are discussed for all samples submitted for analysis.

As of January 1, 2021, the foregoing testing program represents the testing most commonly required by private receiving sites requiring fill for site grading purposes.

The soil samples were submitted to an independent laboratory accredited by the Canadian Association for Laboratory Accreditation (CALA). Sample location and analytical data are summarized in the following table. The results of the chemical testing (Certificates of Analysis) are compiled in Appendix B attached.

Test results were compared to the applicable tables in the MECP document "Soil Ground Water and Sediment Standards for Use Under Part XV.1 of the Environmental Protection Act" – April 15, 2011 in accordance with O.Reg.153/04 as amended and the "Rules For Excess Soil Management And Excess Soil Quality Standards" in accordance with O.Reg.406/19.



| Sample ID | Sample ID Location | | Material Matrix | Analytical Parameters | | |
|------------|----------------------------------|-------------------|----------------------------|--|--|--|
| BH1 SS2 | Borehole 1 | 0.8 to 1.2 | Native Clayey Silt Till | Metals, EC, SAR, BTEX, PHC, mSPLP (Metals) | | |
| BH4 SS3 | Borehole 4 | 1.5 to 1.9 | Fill | Metals, EC, SAR, BTEX, PHC | | |
| BH11 SS2 | Borehole 11 | 0.8 to 1.2 | Native Clayey Silt Till | Metals, EC, SAR, BTEX, PHC | | |
| BH13 SS3 | Borehole 13 | 1.5 to 1.9 | Native Clayey Silt Till | Metals, EC, SAR, BTEX, PHC, mSPLP (Metals) | | |
| BH131 SS33 | Duplicate of BH13 SS3 | 1.5 to 1.9 | Native Clayey Silt Till | Metals, EC, SAR, BTEX, PHC | | |
| BH18 SS4 | Borehole 18 | 2.3 to 2.4 | Native Clayey Silt Till | Metals, EC, SAR, BTEX, PHC | | |
| BH21 SS2 | Borehole 21 | 0.8 to 1.2 | Fill | Metals, EC, SAR, BTEX, PHC, Sulphate | | |
| BH26 SS3 | Borehole 26 | 1.5 to 1.9 | Native Clayey Silt Till | Metals, EC, SAR, BTEX, PHC, mSPLP (Metals) | | |
| BH30 SS1 | BH30 SS1 Borehole 30 | | Native Clayey Silt Till | Metals, EC, SAR, BTEX, PHC | | |
| SP1 | On-Site Granular Stockpile | Not Applicable | Gravel | Metals, EC, SAR, BTEX, PHC | | |

Table 5: Summary of Soil Samples Submitted for Laboratory Analysis

Comparison with the MECP "Soil, Ground Water and Sediment Standards for Use under Part XV.1 of the Environmental Protection Act"

Comparison with criteria in Table 2 of the MECP Standards was selected as being most appropriate for soil samples recovered from the boreholes and stockpile. The selection of Table 2 was based on the following Site conditions:



- The subject property has not been identified as a sensitive site.
- The subject property and surrounding properties are located in an area which is rural; there may still be properties in the surrounding area which utilize local groundwater for potable purposes.
- Full depth restoration of contamination (if encountered) is assumed.

Based on the proposed subject property use (proposed industrial development), Industrial/Commercial/ Community (ICC) property use criteria under these Standards were considered to be applicable. Soils at the subject site were visually assessed and greater than $\frac{2}{3}$ of the soil was classified as medium to fine textured.

All analytical test results for Metals, EC and SAR for soil samples analyzed were within the Table 2 (potable groundwater) ICC property use criteria listed in the MECP Standards. These test results also met the more stringent Table 1 criteria covered under the MECP Standards.

All analytical test results for BTEX and PHC (F1 – F4) for soil samples analyzed were within the Table 2 (potable groundwater) ICC property use criteria listed in the MECP Standards. When compared with criteria in Table 1, an anomalous exceedance for PHC (F2 – Fraction) was recorded in a laboratory duplicate sample of BH18 SS4. All other BTEX and PHC concentrations, including those in BH18 SS4, met Table 1 criteria covered under the MECP Standards. Standards.

Comparison with the MECP "Rules For Excess Soil Management And Excess Soil Quality Standards"

Based on site conditions as described under the comparison with the MECP "Soil, Ground Water and Sediment Standards for Use under Part XV.1 of the Environmental Protection Act" section, Table 2.1 (ICC) would be the applicable criteria for comparison under O.Reg.406/19.

All analytical test results for Metals, EC and SAR for soil samples analyzed were within the Table 2.1 (potable groundwater) ICC property use criteria listed in the Rules For Excess Soil Management And Excess Soil Quality Standards.

All analytical test results for BTEX and PHC for soil samples analyzed were within the Table 2.1 (potable groundwater) ICC property use criteria listed in the Rules For Excess Soil Management And Excess Soil Quality Standards.

All mSPLP test results met the leachate screening levels covered in Table 2.1 of the MECP Standards under O.Reg.406/19.



Disposal Options

Based on the results of the chemical testing program, from an environmental standpoint, soil represented by the samples analyzed would be considered suitable for reuse on site or for shipment to land based sites requiring fill without restriction, subject to approval of receiving site authorities. Physical suitability of the material should be assessed by the receiver for its intended use prior to shipment. Excess soil from the site would also be considered suitable for receipt at MECP registered landfill sites licensed to receive excess soils. However, additional testing for a more complete suite of Inorganic parameters and testing for classification under O.Reg.558/00 may be required for shipment to the MECP registered landfill sites.

Potential for Sulphate Attack

One (1) native soil sample, identified as BH21 SS2 was also analyzed for water soluble sulphate. The soluble sulphate content in the sample analyzed was reported as <20 μ g/g (<0.002%). Table 3 of the Canadian Standards Association (CSA) A.23.1-09 lists 0.1 % sulphate as the minimum concentration of sulphate in soil that warrants additional requirements for concrete. At the measured concentration, the degree of exposure to sulphate attack is considered to be "negligible" and therefore normal Portland cement (Type 10) can be used in subsurface concrete.



7. General Comments

The information presented in this report is based on a limited investigation designed to provide information to support an overall assessment of the current geotechnical conditions of the subject property. The conclusions presented in this report reflect site conditions existing at the time of the investigation.

EXP should be retained for a general review of the final design and specifications to verify that this report has been properly interpreted and implemented. If not accorded the privilege of making this review, EXP will assume no responsibility for interpretation of the recommendations in the report.

The comments given in this report are intended only for the guidance of design engineers. The number of boreholes required to determine the localized underground conditions between boreholes affecting construction costs, techniques, sequencing, equipment, scheduling, etc., would be much greater than has been carried out for design purposes. Contractors bidding on or undertaking the works should, in this light, decide on their own investigations, as well as their own interpretations of the factual borehole results, so that they may draw their own conclusions as to how the subsurface conditions may affect them.

More specific information, with respect to the conditions between samples, or the lateral and vertical extent of materials, may become apparent during excavation operations. Consequently, during the future development of the property, conditions not observed during this investigation may become apparent; should this occur, EXP should be contacted to assess the situation, and additional testing and reporting may be required. EXP has qualified personnel to provide assistance in regards to future geotechnical and environmental issues related to this property.

We trust this report is satisfactory for your purposes. Should you have any questions, please do not hesitate to contact this office.

EXP Services Inc.

David Dennison, P. Eng. Senior Engineer Geotechnical Division



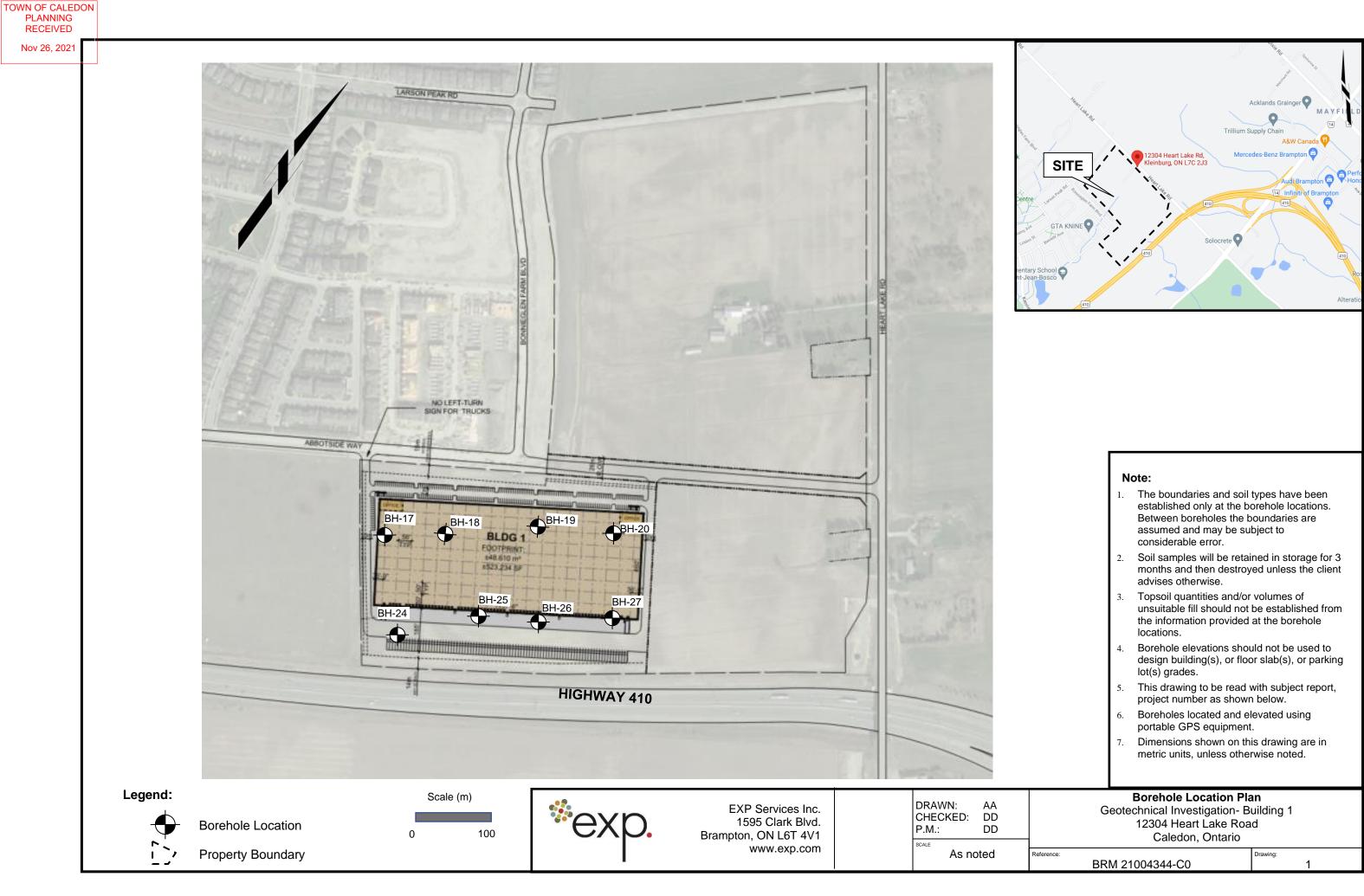
Stephen S.M. Cheng, P. Eng. Discipline Manager Geotechnical Division

DD/dd/I:\2003-Brampton\Projects\Geotechnical Engineering\21000000\21004000\21004300\21004344-C0 12304 Heart Lake Rd. Detailed Geo Inv\Report\Building 1 Report\Geo Report Bldg 1.doc



Drawings





| 1. | The boundaries and soil types have been |
|----|---|
| | established only at the borehole locations. |
| | Between boreholes the boundaries are |
| | assumed and may be subject to |
| | considerable error. |

| Reference: | Drawing: |
|-----------------|----------|
| BRM 21004344-C0 | 1 |

Notes on Sample Descriptions and Soil Types

1. All sample descriptions included in this report follow the Canadian Foundations Engineering Manual soil classification system. This system follows the standard proposed by the International Society for Soil Mechanics and Foundation Engineering. Laboratory grain size analyses provided by EXP also follow the same system. Others may use different classification systems; one such system is the Unified Soil Classification. Please note that, with the exception of those samples where a grain size analysis has been made, all samples are classified visually. Visual classification is not sufficiently accurate to provide exact grain sizing or precise differentiation between size classification systems.

| ISSMFE SOIL CLASSIFICATION | | | | | | | | | | | |
|--|--------|--------|----------|--------|--------|--------|--------|--------|---------|----------|----|
| CLAY | | SILT | | SAND | | GRAVEL | | | COBBLES | BOULDERS | |
| FINE MEDIUM COARSE | | COARSE | FINE | MEDIUM | COARSE | FINE | MEDIUM | COARSE | | | |
| 0. | .002 (| 0.006 | 0.02 0.0 | 5 0.2 | 2 (| 0.6 2 | .0 | 6.0 | 20 60 | 20 | 00 |
| EQUIVALENT GRAIN DIAMETER IN MILLIMETERS | | | | | | | | | | | |
| CLAY (PLASTIC) TO | | | | FINE | М | EDIUM | COARSE | FINE | COARSE | | |
| SILT (NONPLASTIC) | | | | | SA | AND | | GR | AVEL | 7 | |

| UNIFIED | SOIL | CLASSIFICATION |
|----------------|------|----------------|
| UT III III III | DOIL | |

- 2. Fill: Where fill is designated on the borehole log it is defined as indicated by the sample recovered during the boring process. The reader is cautioned that fills are heterogeneous in nature and variable in density or degree of compaction. The borehole description may therefore not be applicable as a general description of site fill materials. All fills should be expected to contain obstruction such as wood, large concrete pieces or subsurface basements, floors, tanks, etc., none of these may have been encountered in the boreholes. Since boreholes cannot accurately define the contents of the fill, test pits are recommended to provide supplementary information. Despite the use of test pits, the heterogeneous nature of fill will leave some ambiguity as to the exact composition of the fill. Most fills contain pockets, seams, or layers of organically contaminated soil. This organic material can result in the generation of methane gas and/or significant ongoing and future settlements. Fill at this site may have been monitored for the presence of methane gas and, if so, the results are given on the borehole logs. The monitoring process does not indicate the volume of gas that can be potentially generated nor does it pinpoint the source of the gas. These readings are to advise of the presence of gas only, and a detailed study is recommended for sites where any explosive gas/methane is detected. Some fill material may be contaminated by toxic/hazardous waste that renders it unacceptable for deposition in any but designated land fill sites; unless specifically stated the fill on this site has not been tested for contaminants that may be considered toxic or hazardous. This testing and a potential hazard study can be undertaken if requested. In most residential/commercial areas undergoing reconstruction, buried oil tanks are common and are generally not detected in a conventional geotechnical site investigation.
- 3. Till: The term till on the borehole logs indicates that the material originates from a geological process associated with glaciation. Because of this geological process the till must be considered heterogeneous in composition and as such may contain pockets and/or seams of material such as sand, gravel, silt or clay. Till often contains cobbles (60 to 200 mm) or boulders (over 200 mm). Contractors may therefore encounter cobbles and boulders during excavation, even if they are not indicated by the borings. It should be appreciated that normal sampling equipment cannot differentiate the size or type of any obstruction. Because of the horizontal and vertical variability of

till, the sample description may be applicable to a very limited zone; caution is therefore essential when dealing with sensitive excavations or dewatering programs in till materials.

4. Excerpt from "OHSA Regulations for Construction Projects," Part III, Section 226:

• Soil Types

Type 1 Soil

- a) is hard, very dense and only able to be penetrated with difficulty by a small sharp object;
- b) has a low natural moisture content and a high degree of internal strength;
- c) has no signs of water seepage; and
- d) can be excavated only by mechanical equipment.

Type 2 Soil

- a) is very stiff, dense and can be penetrated with moderate difficulty by a small sharp object;
- b) has a low to medium natural moisture content and a medium degree of internal strength; and
- c) has a damp appearance after it is excavated.

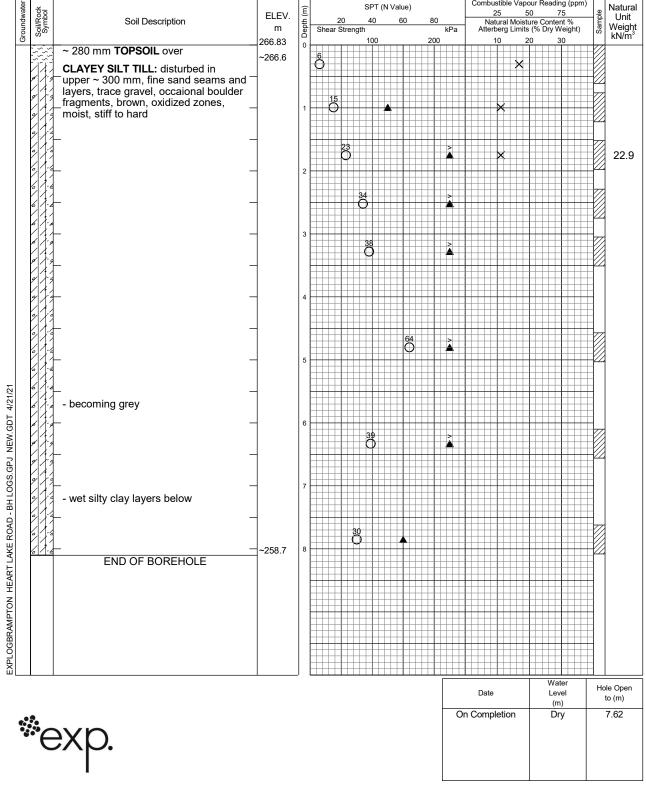
Type 3 Soil

- a) is stiff to firm and compact to loose in consistency or is previously excavated soil;
- b) exhibits signs of surface cracking;
- c) exhibits signs of water seepage;
- d) if it is dry, may run easily into a well-defined conical pile; and
- e) has a low degree of internal strength.

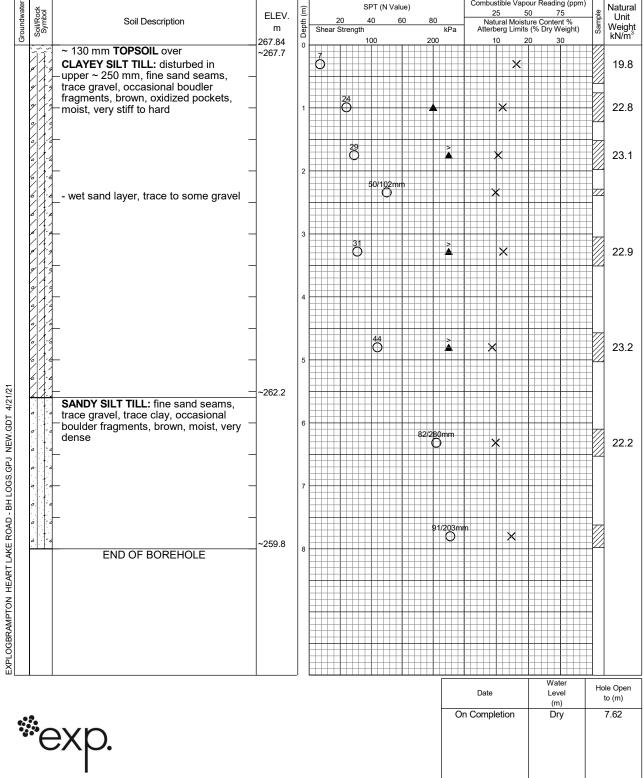
Type 4 Soil

- a) is soft to very soft and very loose in consistency, very sensitive and upon disturbance is significantly reduced in natural strength;
- b) runs easily or flows, unless it is completely supported before excavating procedures;
- c) has almost no internal strength;
- d) is wet or muddy; and
- e) exerts substantial fluid pressure on its supporting system. O. Reg. 213/91, s. 226.

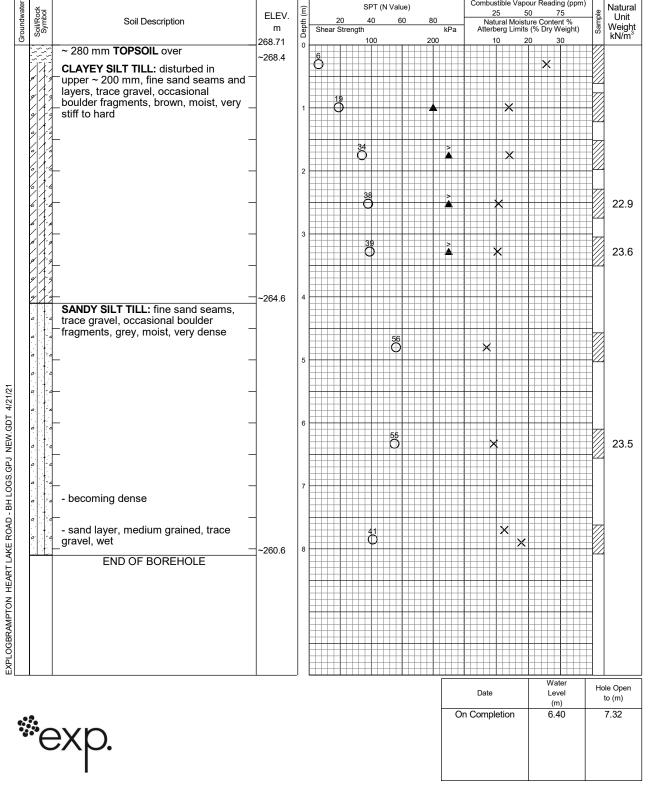
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|---|--------------------------------------|---|---|-------------|--|------------------|---|
| | | Caledon, Ontario Date Drilled: Mar 17, 2021 | Auger Sample | \boxtimes | Combustible Vapour Reading Natural Moisture | □ × | |
| | Drill Type: | CME55 Solid Auger Bomb | SPT (N) Value Dynamic Cone Test Shelby Tube | | Plastic and Liquid Limit Undrained Triaxial at % Strain at Failure | ⊢ −0 ⊕ | |
| Datum: | Datum: | Geodetic | Field Vane Test | \$ | Penetrometer | (m) | |



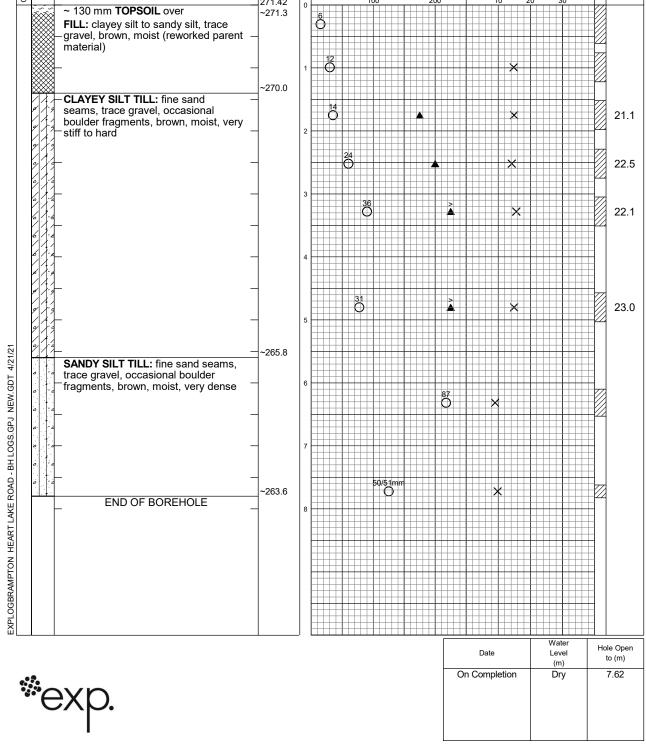
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| | Project: Location: | Geotechnical Investigation 12304 Heart Lake Road | | | Sheet No. | of | _1 |
| | Location. | Caledon, Ontario | _ | | Combustible Vapour Reading | | |
| | Date Drilled: | <u>Mar 18, 2021</u> | Auger Sample — SPT (N) Value | | Natural Moisture | × | |
| | Drill Type: | CME55 Solid Auger Bomb | Dynamic Cone Test Shelby Tube | | Plastic and Liquid Limit Undrained Triaxial at % Strain at Failure | ⊢—C ⊕ |) |
| | Datum: | Geodetic | _ Field Vane Test | s | Penetrometer | | |
| | 5 | | | | Combustible Vapour Reading (pr | om) | |



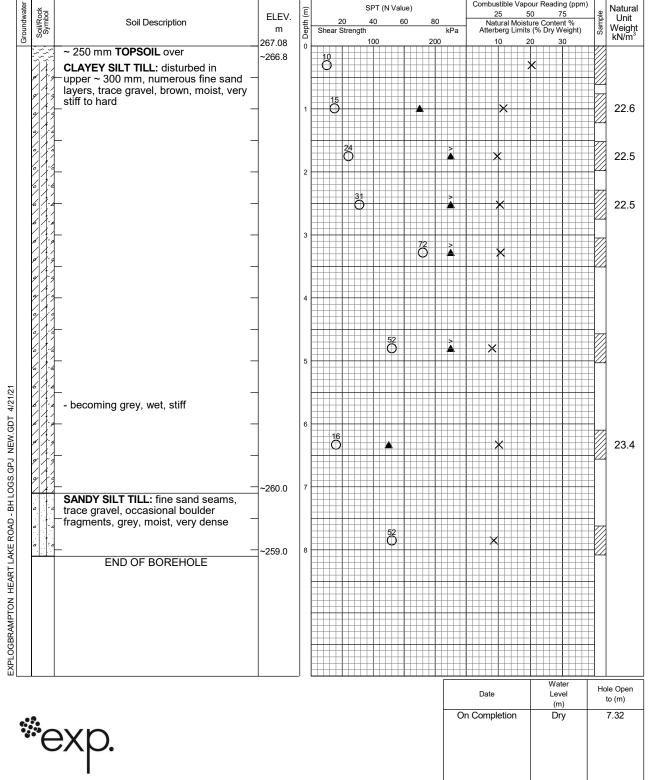
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| | Location. | Caledon, Ontario | | | Combustible Vapour Reading | | |
| | Date Drilled: | d: Mar 22, 2021 | Auger Sample SPT (N) Value | | Natural Moisture Plastic and Liquid Limit | × | |
| | Drill Type: | CME55 Solid Auger Bomb | Dynamic Cone Test Shelby Tube | | Undrained Triaxial at % Strain at Failure | • | |
| | Datum: | Geodetic | Field Vane Test | S | Penetrometer | | |
| | 5 | | | | Combustible Vapour Reading (pp | 2m) | |



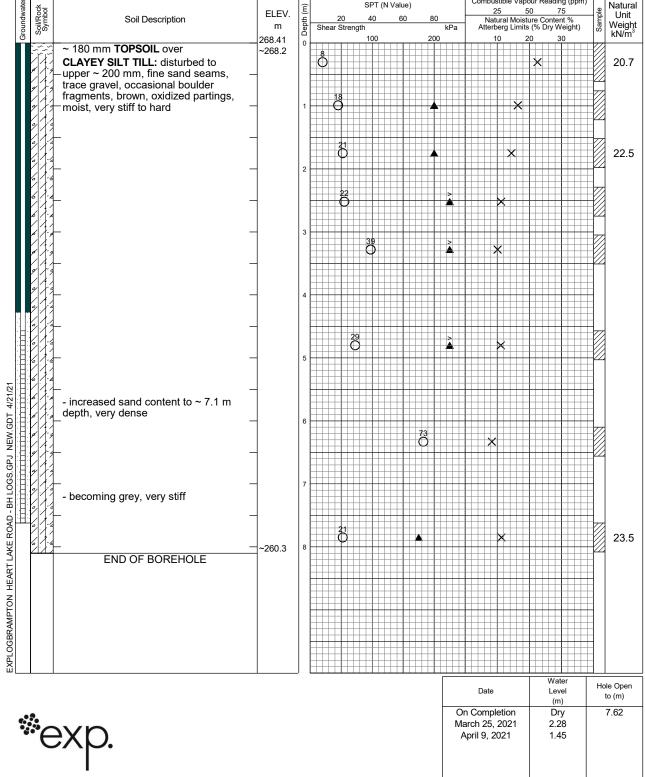
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| | Date Drilled: | Mar 22, 2021 | | Auger Sample SPT (N) Value | $\circ \boxtimes$ | | Moisture | _ > | x | |
| | Drill Type: | CME55 Solid Auger Bomb | | Dynamic Cone Test | <u> </u> | Undrain | and Liquid Limit ed Triaxial at | - | —0 ⊕ |) |
| Datum: | Datum: | Geodetic | | Shelby Tube Field Vane Test | s. | % Strair Penetro | n at Failure meter | 4 | ▲ | |
| | Groundwater Soli/Rock Symbol | Soil Description | ELEV. m 271.42 | E SPT (N Va £ 20 40 B Shear Strength 100 | lue) 60 80 kPa 200 | 25 Natu | ral Moisture Content % erg Limits (% Dry Weight | | We We | atural Jnit eight N/m ³ |
| | |) mm TOPSOIL over clayey silt to sandy silt, trace | ~271.3 | | | | | | | |



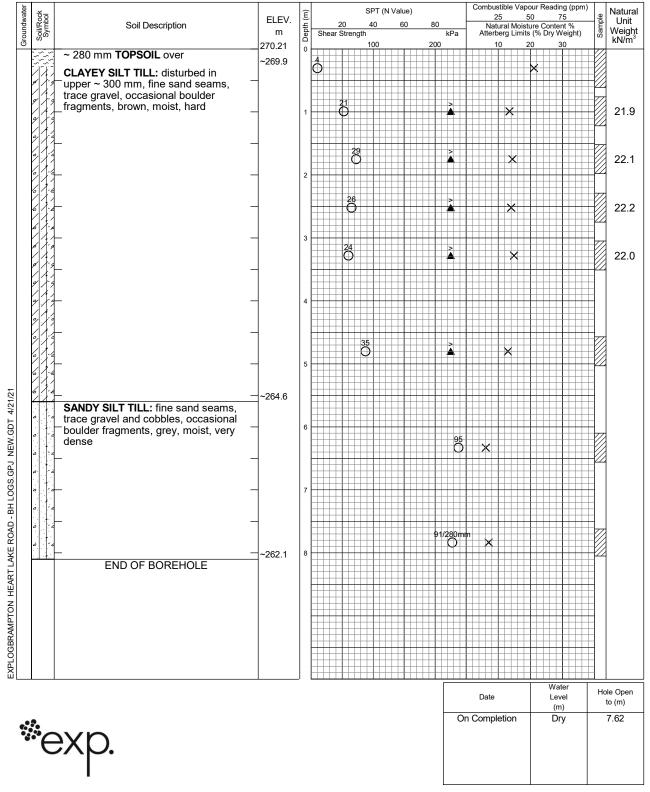
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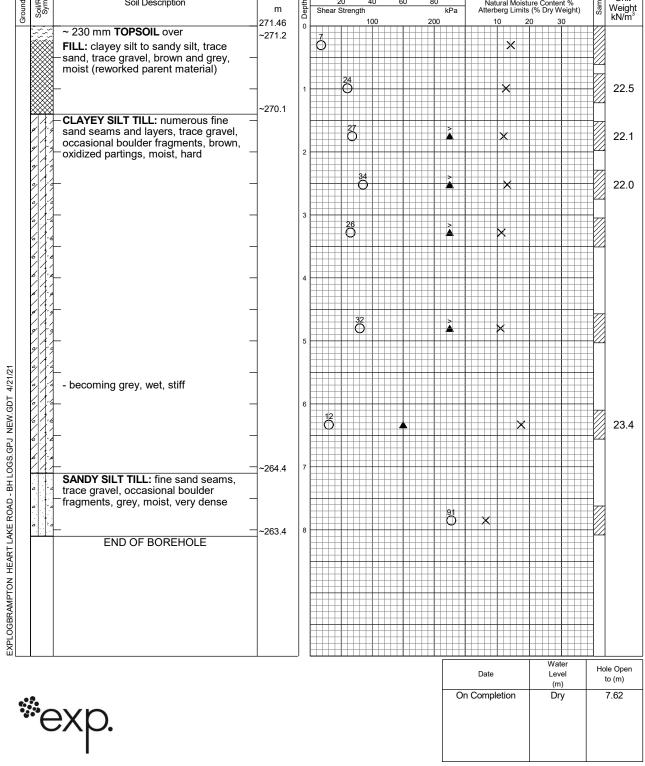


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| | Date Drilled: Drill Type: | Mar 23, 2021 CME55 Solid Auger Bomb | | SPT (N) Value Dynamic Cone Test | | Plastic Undrair | al Moisture c and Liquid Limit ined Triaxial at | × ⊢ ∉ | -0 | |
| Datum: | Datum: | Geodetic | | Shelby Tube Field Vane Test | S | % Strai | in at Failure ometer | _ ▲ | * | |
| | oundwater Symbol | Soil Description | ELEV. m | E SPT (N Va | 60 80 | 2 Nati | stible Vapour Reading (p 5 50 75 ural Moisture Content % verg Limits (% Dry Weigh | mple | Natur Unit Weigl | it |

TOWN OF CALEDON



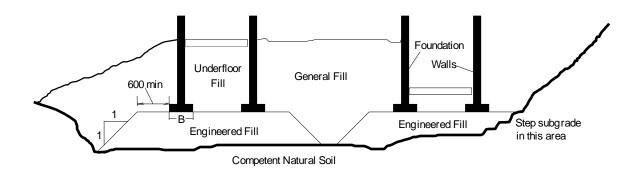
Appendix A: Engineered Fill Construction Guidelines



Foundations placed on engineered fill comprising native soil from the site - or imported materials - may be designed for an SLS geotechnical reaction of 150 kPa (ULS factored geotechnical resistance of 225 kPa).

Additional comments with regard to engineered fill are as follows:

- The area must be stripped of all topsoil, existing fill material or other deleterious material and proof-rolled. Soft spots must be dug out. The stripped native subgrade must be examined and approved by a geotechnical engineer prior to placement of fill.
- The approved engineered fill must be placed in loose lifts not exceeding 200 mm and compacted to 100% Standard Proctor dry density throughout. Granular fill is preferred.
- Full time geotechnical inspection during placement of engineered fill is required.
- The fill must be placed such that the specified geometry is achieved as follows:.



Foundations on Engineered Fill (schematic)

- A minimum footing width of 500 mm (20 inches) is suggested. Steel Reinforcement should be as designed by the Structural Engineer.
- All excavations must be done in accordance with the Occupational Health and Safety Regulations of Ontario.

Broccolini Limited Partnership No. 6 Proposed Commercial Development Building 1 12304 Heart Lake Road, Caledon, Ontario BRM-21004344-C0

Appendix B: Certificates of Analyses





Your P.O. #: BRM-GEO Your Project #: BRM-21004344-BO Site Location: 12304 HEARTLAKE RD Your C.O.C. #: 817848-01-01

Attention: David Dennison

exp Services Inc Brampton Branch 1595 Clark Blvd Brampton, ON CANADA L6T 4V1

> Report Date: 2021/04/12 Report #: R6590858 Version: 2 - Revision

CERTIFICATE OF ANALYSIS – REVISED REPORT

BV LABS JOB #: C180627

Received: 2021/03/26, 13:27

Sample Matrix: Soil # Samples Received: 10

| | | Date | Date | | |
|---|----------|------------|------------|-------------------|----------------------|
| Analyses | Quantity | Extracted | Analyzed | Laboratory Method | Analytical Method |
| Conductivity | 10 | 2021/03/31 | 2021/03/31 | CAM SOP-00414 | OMOE E3530 v1 m |
| Petroleum Hydro. CCME F1 & BTEX in Soil (1) | 10 | N/A | 2021/03/30 | CAM SOP-00315 | CCME PHC-CWS m |
| Petroleum Hydrocarbons F2-F4 in Soil (2) | 2 | 2021/03/29 | 2021/03/30 | CAM SOP-00316 | CCME CWS m |
| Petroleum Hydrocarbons F2-F4 in Soil (2) | 8 | 2021/03/30 | 2021/03/30 | CAM SOP-00316 | CCME CWS m |
| Strong Acid Leachable Metals by ICPMS | 9 | 2021/03/29 | 2021/03/30 | CAM SOP-00447 | EPA 6020B m |
| Strong Acid Leachable Metals by ICPMS | 1 | 2021/03/29 | 2021/03/31 | CAM SOP-00447 | EPA 6020B m |
| Total Metals in SPLP Leachate by ICPMS | 3 | 2021/04/09 | 2021/04/09 | CAM SOP-00447 | EPA 6020B m |
| Moisture | 10 | N/A | 2021/03/27 | CAM SOP-00445 | Carter 2nd ed 51.2 m |
| pH CaCl2 EXTRACT | 10 | 2021/03/30 | 2021/03/30 | CAM SOP-00413 | EPA 9045 D m |
| Sodium Adsorption Ratio (SAR) | 10 | N/A | 2021/03/31 | CAM SOP-00102 | EPA 6010C |
| Sulphate (20:1 Extract) | 1 | 2021/03/29 | 2021/03/31 | CAM SOP-00464 | EPA 375.4 m |
| SPLP Inorganic extraction - pH | 3 | N/A | 2021/04/08 | CAM SOP-00941 | EPA 1312 m |
| SPLP Inorganic extraction - Weight | 3 | N/A | 2021/04/08 | CAM SOP-00941 | EPA 1312 m |

Remarks:

Bureau Veritas is accredited to ISO/IEC 17025 for specific parameters on scopes of accreditation. Unless otherwise noted, procedures used by Bureau Veritas are based upon recognized Provincial, Federal or US method compendia such as CCME, MELCC, EPA, APHA.

All work recorded herein has been done in accordance with procedures and practices ordinarily exercised by professionals in Bureau Veritas' profession using accepted testing methodologies, quality assurance and quality control procedures (except where otherwise agreed by the client and Bureau Veritas in writing). All data is in statistical control and has met quality control and method performance criteria unless otherwise noted. All method blanks are reported; unless indicated otherwise, associated sample data are not blank corrected. Where applicable, unless otherwise noted, Measurement Uncertainty has not been accounted for when stating conformity to the referenced standard.

Bureau Veritas liability is limited to the actual cost of the requested analyses, unless otherwise agreed in writing. There is no other warranty expressed or implied. Bureau Veritas has been retained to provide analysis of samples provided by the Client using the testing methodology referenced in this report. Interpretation and use of test results are the sole responsibility of the Client and are not within the scope of services provided by Bureau Veritas, unless otherwise agreed in writing. Bureau Veritas is not responsible for the accuracy or any data impacts, that result from the information provided by the customer or their agent.

Solid sample results, except biota, are based on dry weight unless otherwise indicated. Organic analyses are not recovery corrected except for isotope dilution methods.

Page 1 of 24



Your P.O. #: BRM-GEO Your Project #: BRM-21004344-BO Site Location: 12304 HEARTLAKE RD Your C.O.C. #: 817848-01-01

Attention: David Dennison

exp Services Inc Brampton Branch 1595 Clark Blvd Brampton, ON CANADA L6T 4V1

> Report Date: 2021/04/12 Report #: R6590858 Version: 2 - Revision

CERTIFICATE OF ANALYSIS – REVISED REPORT

BV LABS JOB #: C180627

Received: 2021/03/26, 13:27

Results relate to samples tested. When sampling is not conducted by Bureau Veritas, results relate to the supplied samples tested.

This Certificate shall not be reproduced except in full, without the written approval of the laboratory.

Reference Method suffix "m" indicates test methods incorporate validated modifications from specific reference methods to improve performance.

* RPDs calculated using raw data. The rounding of final results may result in the apparent difference.

(1) No lab extraction date is given for F1BTEX & VOC samples that are field preserved with methanol. Extraction date is the date sampled unless otherwise stated. (2) All CCME PHC results met required criteria unless otherwise stated in the report. The CWS PHC methods employed by Bureau Veritas Laboratories conform to all prescribed elements of the reference method and performance based elements have been validated. All modifications have been validated and proven equivalent following "Alberta Environment's Interpretation of the Reference Method for the Canada-Wide Standard for Petroleum Hydrocarbons in Soil Validation of Performance-Based Alternative Methods September 2003". Documentation is available upon request. Modifications from Reference Method for the Canada-wide Standard for Petroleum Hydrocarbons in Soil-Tier 1 Method: F2/F3/F4 data reported using validated cold solvent extraction instead of Soxhlet extraction.

Encryption Key

Please direct all questions regarding this Certificate of Analysis to your Project Manager. Patricia Legette, Project Manager Email: Patricia.Legette@bureauveritas.com Phone# (905)817-5799

BV Labs has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per ISO/IEC 17025, signing the reports. For Service Group specific validation please refer to the Validation Signature Page.

Total Cover Pages : 2 Page 2 of 24



O.REG 406 EXCESS SOIL MIN. BULK S/SS PKG (SOIL)

| BV Labs ID | | PEF420 | | | PEF420 | | | PEF421 | | |
|----------------------------------|-------|---------------------|-------|----------|---------------------|-------|----------|---------------------|-------|----------|
| Sampling Date | | 2021/03/18 11:00 | | | 2021/03/18 11:00 | | | 2021/03/17 12:00 | | |
| COC Number | | 817848-01-01 | | | 817848-01-01 | | | 817848-01-01 | | |
| | UNITS | BH1 SS2 | RDL | QC Batch | BH1 SS2 Lab-Dup | RDL | QC Batch | BH4 SS3 | RDL | QC Batch |
| Calculated Parameters | | | | | | | | | | |
| Sodium Adsorption Ratio | N/A | 0.26 (1) | | 7268392 | | | | 0.30 (1) | | 7268392 |
| Inorganics | | | | | • | | | | | |
| Conductivity | mS/cm | 0.16 | 0.002 | 7275424 | | | | 0.12 | 0.002 | 7275424 |
| Moisture | % | 12 | 1.0 | 7270453 | | | | 13 | 1.0 | 7270453 |
| Available (CaCl2) pH | рН | 7.64 | | 7273142 | | | | 7.70 | | 7273142 |
| Metals | • | • | • | | • | • | • | | | |
| Acid Extractable Antimony (Sb) | ug/g | <0.20 | 0.20 | 7271605 | | | | <0.20 | 0.20 | 7271605 |
| Acid Extractable Arsenic (As) | ug/g | 4.6 | 1.0 | 7271605 | | | | 4.9 | 1.0 | 7271605 |
| Acid Extractable Barium (Ba) | ug/g | 66 | 0.50 | 7271605 | | | | 56 | 0.50 | 7271605 |
| Acid Extractable Beryllium (Be) | ug/g | 0.58 | 0.20 | 7271605 | | | | 0.59 | 0.20 | 7271605 |
| Acid Extractable Boron (B) | ug/g | 7.4 | 5.0 | 7271605 | | | | 7.8 | 5.0 | 7271605 |
| Acid Extractable Cadmium (Cd) | ug/g | <0.10 | 0.10 | 7271605 | | | | <0.10 | 0.10 | 7271605 |
| Acid Extractable Chromium (Cr) | ug/g | 18 | 1.0 | 7271605 | | | | 18 | 1.0 | 7271605 |
| Acid Extractable Cobalt (Co) | ug/g | 11 | 0.10 | 7271605 | | | | 12 | 0.10 | 7271605 |
| Acid Extractable Copper (Cu) | ug/g | 30 | 0.50 | 7271605 | | | | 39 | 0.50 | 7271605 |
| Acid Extractable Lead (Pb) | ug/g | 9.6 | 1.0 | 7271605 | | | | 12 | 1.0 | 7271605 |
| Acid Extractable Molybdenum (Mo) | ug/g | <0.50 | 0.50 | 7271605 | | | | <0.50 | 0.50 | 7271605 |
| Acid Extractable Nickel (Ni) | ug/g | 22 | 0.50 | 7271605 | | | | 23 | 0.50 | 7271605 |
| Acid Extractable Selenium (Se) | ug/g | <0.50 | 0.50 | 7271605 | | | | <0.50 | 0.50 | 7271605 |
| Acid Extractable Silver (Ag) | ug/g | <0.20 | 0.20 | 7271605 | | | | <0.20 | 0.20 | 7271605 |
| Acid Extractable Thallium (Tl) | ug/g | 0.14 | 0.050 | 7271605 | | | | 0.14 | 0.050 | 7271605 |
| Acid Extractable Uranium (U) | ug/g | 0.49 | 0.050 | 7271605 | | | | 0.44 | 0.050 | 7271605 |
| Acid Extractable Vanadium (V) | ug/g | 26 | 5.0 | 7271605 | | | | 26 | 5.0 | 7271605 |
| Acid Extractable Zinc (Zn) | ug/g | 51 | 5.0 | 7271605 | | | | 54 | 5.0 | 7271605 |
| BTEX & F1 Hydrocarbons | | | | | | | | | | |
| Benzene | ug/g | <0.020 | 0.020 | 7274245 | <0.020 | 0.020 | 7274245 | <0.020 | 0.020 | 7274245 |
| RDL = Reportable Detection Limit | | | | | | | | | | |
| | | | | | | | | | | |

QC Batch = Quality Control Batch

Lab-Dup = Laboratory Initiated Duplicate

(1) Sodium was not detected. To report SAR the sodium detection limit was used in the calculation. This value represents a maximum ratio.



O.REG 406 EXCESS SOIL MIN. BULK S/SS PKG (SOIL)

| BV Labs ID | | PEF420 | | | PEF420 | | | PEF421 | | |
|------------------------------------|--------|--------------|-------|----------|--------------------|-------|----------|--------------|-------|----------|
| Sampling Date | | 2021/03/18 | | | 2021/03/18 | | | 2021/03/17 | | |
| | | 11:00 | | | 11:00 | | | 12:00 | | |
| COC Number | | 817848-01-01 | | | 817848-01-01 | | | 817848-01-01 | | ļ |
| | UNITS | BH1 SS2 | RDL | QC Batch | BH1 SS2 Lab-Dup | RDL | QC Batch | BH4 SS3 | RDL | QC Batch |
| Toluene | ug/g | <0.020 | 0.020 | 7274245 | <0.020 | 0.020 | 7274245 | <0.020 | 0.020 | 7274245 |
| Ethylbenzene | ug/g | <0.020 | 0.020 | 7274245 | <0.020 | 0.020 | 7274245 | <0.020 | 0.020 | 7274245 |
| o-Xylene | ug/g | <0.020 | 0.020 | 7274245 | <0.020 | 0.020 | 7274245 | <0.020 | 0.020 | 7274245 |
| p+m-Xylene | ug/g | <0.040 | 0.040 | 7274245 | <0.040 | 0.040 | 7274245 | <0.040 | 0.040 | 7274245 |
| Total Xylenes | ug/g | <0.040 | 0.040 | 7274245 | <0.040 | 0.040 | 7274245 | <0.040 | 0.040 | 7274245 |
| F1 (C6-C10) | ug/g | <10 | 10 | 7274245 | <10 | 10 | 7274245 | <10 | 10 | 7274245 |
| F1 (C6-C10) - BTEX | ug/g | <10 | 10 | 7274245 | <10 | 10 | 7274245 | <10 | 10 | 7274245 |
| F2-F4 Hydrocarbons | | | | | | | | | | |
| F2 (C10-C16 Hydrocarbons) | ug/g | <10 | 10 | 7273498 | | | | <10 | 10 | 7273498 |
| F3 (C16-C34 Hydrocarbons) | ug/g | <50 | 50 | 7273498 | | | | <50 | 50 | 7273498 |
| F4 (C34-C50 Hydrocarbons) | ug/g | <50 | 50 | 7273498 | | | | <50 | 50 | 7273498 |
| Reached Baseline at C50 | ug/g | Yes | | 7273498 | | | | Yes | | 7273498 |
| Surrogate Recovery (%) | | | | | | | | | | |
| 1,4-Difluorobenzene | % | 102 | | 7274245 | 102 | | 7274245 | 101 | | 7274245 |
| 4-Bromofluorobenzene | % | 96 | | 7274245 | 88 | | 7274245 | 94 | | 7274245 |
| D10-o-Xylene | % | 88 | | 7274245 | 92 | | 7274245 | 84 | | 7274245 |
| D4-1,2-Dichloroethane | % | 96 | | 7274245 | 95 | | 7274245 | 97 | | 7274245 |
| o-Terphenyl | % | 97 | | 7273498 | | | | 96 | | 7273498 |
| RDL = Reportable Detection Limit | | | • | | | • | | | • | |
| QC Batch = Quality Control Batch | | | | | | | | | | |
| Lab-Dup = Laboratory Initiated Dup | licate | | | | | | | | | |



O.REG 406 EXCESS SOIL MIN. BULK S/SS PKG (SOIL)

| | PEF422 | | PEF423 | | PEF424 | | |
|-------|--|---|---|--|---|---|--|
| | 2021/03/18 12:00 | | 2021/03/25 11:00 | | 2021/03/22 11:00 | | |
| | 817848-01-01 | | 817848-01-01 | | 817848-01-01 | | |
| UNITS | BH11 SS2 | QC Batch | BH13 SS3 | QC Batch | BH18 SS4 | RDL | QC Batch |
| | · | • | · | • | | | - |
| N/A | 0.26 (1) | 7268392 | 0.29 (1) | 7268392 | 0.28 (1) | | 7268392 |
| | | | | | | | |
| mS/cm | 0.16 | 7275424 | 0.13 | 7275424 | 0.15 | 0.002 | 7275424 |
| % | 14 | 7270453 | 12 | 7270453 | 13 | 1.0 | 7270453 |
| рН | 7.74 | 7273142 | 7.66 | 7273142 | 7.77 | | 7273142 |
| | • | | | | | | |
| ug/g | <0.20 | 7271605 | <0.20 | 7271605 | <0.20 | 0.20 | 7271605 |
| ug/g | 4.4 | 7271605 | 4.8 | 7271605 | 4.7 | 1.0 | 7271605 |
| ug/g | 60 | 7271605 | 75 | 7271605 | 55 | 0.50 | 7271605 |
| ug/g | 0.55 | 7271605 | 0.61 | 7271605 | 0.47 | 0.20 | 7271605 |
| ug/g | 6.9 | 7271605 | 8.4 | 7271605 | 6.8 | 5.0 | 7271605 |
| ug/g | <0.10 | 7271605 | <0.10 | 7271605 | <0.10 | 0.10 | 7271605 |
| ug/g | 17 | 7271605 | 19 | 7271605 | 23 | 1.0 | 7271605 |
| ug/g | 9.2 | 7271605 | 13 | 7271605 | 9.6 | 0.10 | 7271605 |
| ug/g | 30 | 7271605 | 31 | 7271605 | 35 | 0.50 | 7271605 |
| ug/g | 7.4 | 7271605 | 8.3 | 7271605 | 9.5 | 1.0 | 7271605 |
| ug/g | <0.50 | 7271605 | <0.50 | 7271605 | 0.89 | 0.50 | 7271605 |
| ug/g | 19 | 7271605 | 25 | 7271605 | 19 | 0.50 | 7271605 |
| ug/g | <0.50 | 7271605 | <0.50 | 7271605 | <0.50 | 0.50 | 7271605 |
| ug/g | <0.20 | 7271605 | <0.20 | 7271605 | <0.20 | 0.20 | 7271605 |
| ug/g | 0.12 | 7271605 | 0.17 | 7271605 | 0.11 | 0.050 | 7271605 |
| ug/g | 0.42 | 7271605 | 0.43 | 7271605 | 0.38 | 0.050 | 7271605 |
| ug/g | 25 | 7271605 | 27 | 7271605 | 23 | 5.0 | 7271605 |
| ug/g | 43 | 7271605 | 54 | 7271605 | 49 | 5.0 | 7271605 |
| | | | • | | | | - |
| ug/g | <0.020 | 7274245 | <0.020 | 7274245 | <0.020 | 0.020 | 7274245 |
| ug/g | <0.020 | 7274245 | <0.020 | 7274245 | <0.020 | 0.020 | 7274245 |
| | N/A mS/cm % pH ug/g ug/g ug/g ug/g ug/g ug/g ug/g ug/ | 2021/03/18 12:00 817848-01-01 UNITS BH11 SS2 N/A 0.26 (1) mS/cm 0.16 % 14 pH 7.74 ug/g 0.20 ug/g 0.20 ug/g 0.16 % 14 pH 7.74 ug/g 0.20 ug/g 0.55 ug/g 0.10 ug/g 0.10 ug/g 17 ug/g 17 ug/g 30 ug/g 30 ug/g 19 ug/g 0.12 ug/g 0.12 ug/g 0.12 ug/g 0.12 ug/g 0.42 | 2021/03/18 12:00 2021/03/18 12:00 817848-01-01 817848-01-01 UNITS BH11 SS2 QC Batch N/A 0.26 (1) 7268392 mS/cm 0.16 7275424 % 14 7270453 pH 7.74 7273142 ug/g <0.20 | 2021/03/18 12:00 2021/03/25 11:00 817848-01-01 817848-01-01 UNITS BH11 SS2 QC Batch BH13 SS3 N/A 0.26 (1) 7268392 0.29 (1) mS/cm 0.16 7275424 0.13 % 14 7270453 12 pH 7.74 7273142 7.66 ug/g <0.20 | 2021/03/18 12:00 2021/03/25 11:00 817848-01-01 817848-01-01 UNITS BH11 SS2 QC Batch BH13 SS3 QC Batch N/A 0.26 (1) 7268392 0.29 (1) 7268392 mS/cm 0.16 7275424 0.13 7275424 % 14 7270453 12 7270453 pH 7.74 7273142 7.66 7271605 ug/g <0.20 | 2021/03/18 12:00 2021/03/25 11:00 2021/03/22 11:00 817848-01-01 817848-01-01 817848-01-01 UNITS BH11 SS2 QC Batch BH13 SS3 QC Batch BH18 SS4 N/A 0.26 (1) 7268392 0.29 (1) 7268392 0.28 (1) mS/cm 0.16 7275424 0.13 7275424 0.15 % 14 7270453 12 7270453 13 pH 7.74 7273142 7.66 7273142 7.77 ug/g <0.20 | 2021/03/18 12:00 2021/03/25 11:00 2021/03/25 11:00 2021/03/22 11:00 817848-01-01 817848-01-01 817848-01-01 817848-01-01 UNITS BH11 SS2 QC Batch BH13 SS3 QC Batch BH18 SS4 RDL N/A 0.26 (1) 7268392 0.29 (1) 7268392 0.28 (1) mS/cm 0.16 7275424 0.13 7275424 0.15 0.002 % 14 7270453 12 7270453 13 1.0 pH 7.74 7271605 <0.20 |

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

(1) Sodium was not detected. To report SAR the sodium detection limit was used in the calculation. This value represents a maximum ratio.



O.REG 406 EXCESS SOIL MIN. BULK S/SS PKG (SOIL)

| 2021/03/25 11:00 817848-01-01 BH13 SS3 <0.020 | QC Batch | 2021/03/22 11:00 817848-01-01 | | |
|---|---------------|-------------------------------------|-------|----------|
| BH13 SS3 <0.020 | QC Batch | 817848-01-01 | | |
| <0.020 | QC Batch | | 1 1 | 1 |
| | | BH18 SS4 | RDL | QC Batch |
| | 7274245 | <0.020 | 0.020 | 7274245 |
| <0.020 | 7274245 | <0.020 | 0.020 | 7274245 |
| <0.040 | 7274245 | <0.040 | 0.040 | 7274245 |
| <0.040 | 7274245 | <0.040 | 0.040 | 7274245 |
| <10 | 7274245 | <10 | 10 | 7274245 |
| <10 | 7274245 | <10 | 10 | 7274245 |
| | • | | | |
| <10 | 7272947 | <10 | 10 | 7273498 |
| <50 | 7272947 | <50 | 50 | 7273498 |
| <50 | 7272947 | <50 | 50 | 7273498 |
| Yes | 7272947 | Yes | | 7273498 |
| - | • | <u> </u> | | |
| 103 | 7274245 | 101 | | 7274245 |
| 92 | 7274245 | 96 | | 7274245 |
| 82 | 7274245 | 94 | | 7274245 |
| 93 | 7274245 | 96 | | 7274245 |
| | 7272947 | 93 | | 7273498 |
| 5 | 5 93 8 103 | | | |



O.REG 406 EXCESS SOIL MIN. BULK S/SS PKG (SOIL)

| BV Labs ID | | PEF424 | | | PEF425 | PEF426 | | |
|----------------------------------|-------|---------------------|-----|----------|--------------|--------------|-------|----------|
| Sampling Date | | 2021/03/22 | | | 2021/03/22 | 2021/03/23 | | |
| | | 11:00 | | | 12:00 | 12:00 | | |
| COC Number | | 817848-01-01 | | | 817848-01-01 | 817848-01-01 | | |
| | UNITS | BH18 SS4 Lab-Dup | RDL | QC Batch | BH21 SS2 | BH26 SS3 | RDL | QC Batch |
| Calculated Parameters | | | | | | | | |
| Sodium Adsorption Ratio | N/A | | | | 0.28 (1) | 0.26 (1) | | 7268392 |
| Inorganics | | | | | | • | • | |
| Conductivity | mS/cm | | | | 0.14 | 0.16 | 0.002 | 7275424 |
| Moisture | % | | | | 15 | 14 | 1.0 | 7270453 |
| Available (CaCl2) pH | рН | | | | 7.67 | 7.67 | | 7273142 |
| Metals | • | | | | • | | • | |
| Acid Extractable Antimony (Sb) | ug/g | | | | <0.20 | <0.20 | 0.20 | 7271605 |
| Acid Extractable Arsenic (As) | ug/g | | | | 4.5 | 3.7 | 1.0 | 7271605 |
| Acid Extractable Barium (Ba) | ug/g | | | | 45 | 92 | 0.50 | 7271605 |
| Acid Extractable Beryllium (Be) | ug/g | | | | 0.46 | 0.72 | 0.20 | 7271605 |
| Acid Extractable Boron (B) | ug/g | | | | 5.7 | 9.9 | 5.0 | 7271605 |
| Acid Extractable Cadmium (Cd) | ug/g | | | | <0.10 | <0.10 | 0.10 | 7271605 |
| Acid Extractable Chromium (Cr) | ug/g | | | | 14 | 23 | 1.0 | 7271605 |
| Acid Extractable Cobalt (Co) | ug/g | | | | 8.8 | 14 | 0.10 | 7271605 |
| Acid Extractable Copper (Cu) | ug/g | | | | 37 | 24 | 0.50 | 7271605 |
| Acid Extractable Lead (Pb) | ug/g | | | | 7.2 | 11 | 1.0 | 7271605 |
| Acid Extractable Molybdenum (Mo) | ug/g | | | | <0.50 | <0.50 | 0.50 | 7271605 |
| Acid Extractable Nickel (Ni) | ug/g | | | | 18 | 29 | 0.50 | 7271605 |
| Acid Extractable Selenium (Se) | ug/g | | | | <0.50 | <0.50 | 0.50 | 7271605 |
| Acid Extractable Silver (Ag) | ug/g | | | | <0.20 | <0.20 | 0.20 | 7271605 |
| Acid Extractable Thallium (Tl) | ug/g | | | | 0.096 | 0.18 | 0.050 | 7271605 |
| Acid Extractable Uranium (U) | ug/g | | | | 0.37 | 0.50 | 0.050 | 7271605 |
| Acid Extractable Vanadium (V) | ug/g | | | | 21 | 32 | 5.0 | 7271605 |
| Acid Extractable Zinc (Zn) | ug/g | | | | 44 | 60 | 5.0 | 7271605 |
| BTEX & F1 Hydrocarbons | | • | | • | • | • | | |
| Benzene | ug/g | | | | <0.020 | <0.020 | 0.020 | 7274245 |
| RDL = Reportable Detection Limit | • | | | | • | | | |

QC Batch = Quality Control Batch

Lab-Dup = Laboratory Initiated Duplicate

(1) Sodium was not detected. To report SAR the sodium detection limit was used in the calculation. This value represents a maximum ratio.



O.REG 406 EXCESS SOIL MIN. BULK S/SS PKG (SOIL)

| BV Labs ID | | PEF424 | | | PEF425 | PEF426 | | |
|--|-------|---------------------|-----|----------|--------------|--------------|----------|----------|
| Sampling Date | | 2021/03/22 | | | 2021/03/22 | 2021/03/23 | | |
| Sampling Date | | 11:00 | | | 12:00 | 12:00 | | |
| COC Number | | 817848-01-01 | | | 817848-01-01 | 817848-01-01 | | |
| | UNITS | BH18 SS4 Lab-Dup | RDL | QC Batch | BH21 SS2 | BH26 SS3 | RDL | QC Batch |
| Toluene | ug/g | | | | <0.020 | <0.020 | 0.020 | 7274245 |
| Ethylbenzene | ug/g | | | | <0.020 | <0.020 | 0.020 | 7274245 |
| o-Xylene | ug/g | | | | <0.020 | <0.020 | 0.020 | 7274245 |
| p+m-Xylene | ug/g | | | | <0.040 | <0.040 | 0.040 | 7274245 |
| Total Xylenes | ug/g | | | | <0.040 | <0.040 | 0.040 | 7274245 |
| F1 (C6-C10) | ug/g | | | | <10 | <10 | 10 | 7274245 |
| F1 (C6-C10) - BTEX | ug/g | | | | <10 | <10 | 10 | 7274245 |
| F2-F4 Hydrocarbons | | | | | | | | |
| F2 (C10-C16 Hydrocarbons) | ug/g | 12 | 10 | 7273498 | <10 | <10 | 10 | 7273498 |
| F3 (C16-C34 Hydrocarbons) | ug/g | <50 | 50 | 7273498 | <50 | <50 | 50 | 7273498 |
| F4 (C34-C50 Hydrocarbons) | ug/g | <50 | 50 | 7273498 | <50 | <50 | 50 | 7273498 |
| Reached Baseline at C50 | ug/g | Yes | | 7273498 | Yes | Yes | | 7273498 |
| Surrogate Recovery (%) | | | | | | • | • | |
| 1,4-Difluorobenzene | % | | | | 101 | 102 | | 7274245 |
| 4-Bromofluorobenzene | % | | | | 97 | 96 | | 7274245 |
| D10-o-Xylene | % | | | | 85 | 76 | | 7274245 |
| D4-1,2-Dichloroethane | % | | | | 97 | 94 | | 7274245 |
| o-Terphenyl | % | 93 | | 7273498 | 98 | 96 | | 7273498 |
| RDL = Reportable Detection Limit QC Batch = Quality Control Batch | | | • | | | | <u> </u> | |

Lab-Dup = Laboratory Initiated Duplicate



O.REG 406 EXCESS SOIL MIN. BULK S/SS PKG (SOIL)

| BV Labs ID | | PEF426 | | | PEF427 | | | PEF427 | |
|----------------------------------|-------|---------------------|-----|----------|--------------|-------|----------|---------------------|----------|
| Sampling Date | | 2021/03/23 | | | 2021/03/24 | | | 2021/03/24 | |
| | | 12:00 | | | 12:00 | | | 12:00 | |
| COC Number | | 817848-01-01 | | | 817848-01-01 | | | 817848-01-01 | |
| | UNITS | BH26 SS3 Lab-Dup | RDL | QC Batch | BH30 SS4 | RDL | QC Batch | BH30 SS4 Lab-Dup | QC Batch |
| Calculated Parameters | | | | | | | | | |
| Sodium Adsorption Ratio | N/A | | | | 0.28 (1) | | 7268392 | | |
| Inorganics | • | • | • | • | | | | | |
| Conductivity | mS/cm | | | | 0.14 | 0.002 | 7275424 | | |
| Moisture | % | 14 | 1.0 | 7270453 | 11 | 1.0 | 7270453 | | |
| Available (CaCl2) pH | pН | | | | 7.65 | | 7273142 | 7.60 | 7273142 |
| Metals | • | • | • | • | | | | | |
| Acid Extractable Antimony (Sb) | ug/g | | | | <0.20 | 0.20 | 7271820 | | |
| Acid Extractable Arsenic (As) | ug/g | | | | 4.8 | 1.0 | 7271820 | | |
| Acid Extractable Barium (Ba) | ug/g | | | | 56 | 0.50 | 7271820 | | |
| Acid Extractable Beryllium (Be) | ug/g | | | | 0.53 | 0.20 | 7271820 | | |
| Acid Extractable Boron (B) | ug/g | | | | 7.0 | 5.0 | 7271820 | | |
| Acid Extractable Cadmium (Cd) | ug/g | | | | <0.10 | 0.10 | 7271820 | | |
| Acid Extractable Chromium (Cr) | ug/g | | | | 20 | 1.0 | 7271820 | | |
| Acid Extractable Cobalt (Co) | ug/g | | | | 10 | 0.10 | 7271820 | | |
| Acid Extractable Copper (Cu) | ug/g | | | | 32 | 0.50 | 7271820 | | |
| Acid Extractable Lead (Pb) | ug/g | | | | 8.8 | 1.0 | 7271820 | | |
| Acid Extractable Molybdenum (Mo) | ug/g | | | | 0.50 | 0.50 | 7271820 | | |
| Acid Extractable Nickel (Ni) | ug/g | | | | 22 | 0.50 | 7271820 | | |
| Acid Extractable Selenium (Se) | ug/g | | | | <0.50 | 0.50 | 7271820 | | |
| Acid Extractable Silver (Ag) | ug/g | | | | <0.20 | 0.20 | 7271820 | | |
| Acid Extractable Thallium (Tl) | ug/g | | | | 0.11 | 0.050 | 7271820 | | |
| Acid Extractable Uranium (U) | ug/g | | | | 0.41 | 0.050 | 7271820 | | |
| Acid Extractable Vanadium (V) | ug/g | | | | 25 | 5.0 | 7271820 | | |
| Acid Extractable Zinc (Zn) | ug/g | | | | 52 | 5.0 | 7271820 | | |
| BTEX & F1 Hydrocarbons | | 1 | | | • | | | | |
| Benzene | ug/g | | | | <0.020 | 0.020 | 7274245 | | |
| RDL = Reportable Detection Limit | | 1 | | | | • | | | |
| OC Batch = Ouality Control Batch | | | | | | | | | |

QC Batch = Quality Control Batch

Lab-Dup = Laboratory Initiated Duplicate

(1) Sodium was not detected. To report SAR the sodium detection limit was used in the calculation. This value represents a maximum ratio.



O.REG 406 EXCESS SOIL MIN. BULK S/SS PKG (SOIL)

| BV Labs ID | | PEF426 | | | PEF427 | | | PEF427 | |
|---|-------|---------------------|-----|----------|---------------------|-------|----------|---------------------|----------|
| Sampling Date | | 2021/03/23 12:00 | | | 2021/03/24 12:00 | | | 2021/03/24 12:00 | |
| COC Number | | 817848-01-01 | | | 817848-01-01 | | | 817848-01-01 | |
| | UNITS | BH26 SS3 Lab-Dup | RDL | QC Batch | BH30 SS4 | RDL | QC Batch | BH30 SS4 Lab-Dup | QC Batch |
| Toluene | ug/g | | | | <0.020 | 0.020 | 7274245 | | |
| Ethylbenzene | ug/g | | | | <0.020 | 0.020 | 7274245 | | |
| o-Xylene | ug/g | | | | <0.020 | 0.020 | 7274245 | | |
| p+m-Xylene | ug/g | | | | <0.040 | 0.040 | 7274245 | | |
| Total Xylenes | ug/g | | | | <0.040 | 0.040 | 7274245 | | |
| F1 (C6-C10) | ug/g | | | | <10 | 10 | 7274245 | | |
| F1 (C6-C10) - BTEX | ug/g | | | | <10 | 10 | 7274245 | | |
| F2-F4 Hydrocarbons | | • | | | | | | • | |
| F2 (C10-C16 Hydrocarbons) | ug/g | | | | <10 | 10 | 7273498 | | |
| F3 (C16-C34 Hydrocarbons) | ug/g | | | | <50 | 50 | 7273498 | | |
| F4 (C34-C50 Hydrocarbons) | ug/g | | | | <50 | 50 | 7273498 | | |
| Reached Baseline at C50 | ug/g | | | | Yes | | 7273498 | | |
| Surrogate Recovery (%) | | | | | | | | | |
| 1,4-Difluorobenzene | % | | | | 103 | | 7274245 | | |
| 4-Bromofluorobenzene | % | | | | 93 | | 7274245 | | |
| D10-o-Xylene | % | | | | 81 | | 7274245 | | |
| D4-1,2-Dichloroethane | % | | | | 96 | | 7274245 | | |
| o-Terphenyl | % | | | | 96 | | 7273498 | | |
| RDL = Reportable Detection Limit QC Batch = Quality Control Batch Lab-Dup = Laboratory Initiated Duplic | ate | | | | | | | | |



O.REG 406 EXCESS SOIL MIN. BULK S/SS PKG (SOIL)

| BV Labs ID | | PEF428 | | PEF429 | | |
|----------------------------------|-------|---------------------|----------|---------------------|-------|----------|
| Sampling Date | | 2021/03/25 12:00 | | 2021/03/25 13:00 | | |
| COC Number | | 817848-01-01 | | 817848-01-01 | | |
| | UNITS | BH131 SS33 | QC Batch | SP1 | RDL | QC Batch |
| Calculated Parameters | | | | | • | |
| Sodium Adsorption Ratio | N/A | 0.29 (1) | 7268392 | 0.31 | | 7268392 |
| Inorganics | | • | • | | | |
| Conductivity | mS/cm | 0.13 | 7275424 | 0.25 | 0.002 | 7275424 |
| Moisture | % | 13 | 7270453 | 4.3 | 1.0 | 7270453 |
| Available (CaCl2) pH | pН | 7.67 | 7273142 | 7.94 | | 7273142 |
| Metals | * | • | | | | |
| Acid Extractable Antimony (Sb) | ug/g | <0.20 | 7271605 | 0.24 | 0.20 | 7271605 |
| Acid Extractable Arsenic (As) | ug/g | 4.6 | 7271605 | 3.7 | 1.0 | 7271605 |
| Acid Extractable Barium (Ba) | ug/g | 64 | 7271605 | 19 | 0.50 | 7271605 |
| Acid Extractable Beryllium (Be) | ug/g | 0.59 | 7271605 | 0.20 | 0.20 | 7271605 |
| Acid Extractable Boron (B) | ug/g | 8.1 | 7271605 | 9.4 | 5.0 | 7271605 |
| Acid Extractable Cadmium (Cd) | ug/g | <0.10 | 7271605 | 0.41 | 0.10 | 7271605 |
| Acid Extractable Chromium (Cr) | ug/g | 17 | 7271605 | 5.7 | 1.0 | 7271605 |
| Acid Extractable Cobalt (Co) | ug/g | 11 | 7271605 | 3.5 | 0.10 | 7271605 |
| Acid Extractable Copper (Cu) | ug/g | 31 | 7271605 | 8.2 | 0.50 | 7271605 |
| Acid Extractable Lead (Pb) | ug/g | 11 | 7271605 | 32 | 1.0 | 7271605 |
| Acid Extractable Molybdenum (Mo) | ug/g | <0.50 | 7271605 | <0.50 | 0.50 | 7271605 |
| Acid Extractable Nickel (Ni) | ug/g | 25 | 7271605 | 8.2 | 0.50 | 7271605 |
| Acid Extractable Selenium (Se) | ug/g | <0.50 | 7271605 | <0.50 | 0.50 | 7271605 |
| Acid Extractable Silver (Ag) | ug/g | <0.20 | 7271605 | <0.20 | 0.20 | 7271605 |
| Acid Extractable Thallium (Tl) | ug/g | 0.14 | 7271605 | 0.062 | 0.050 | 7271605 |
| Acid Extractable Uranium (U) | ug/g | 0.70 | 7271605 | 0.20 | 0.050 | 7271605 |
| Acid Extractable Vanadium (V) | ug/g | 26 | 7271605 | 8.5 | 5.0 | 7271605 |
| Acid Extractable Zinc (Zn) | ug/g | 51 | 7271605 | 170 | 5.0 | 7271605 |
| BTEX & F1 Hydrocarbons | • | | | | - | - |
| Benzene | ug/g | <0.020 | 7274245 | <0.020 | 0.020 | 7274245 |
| Toluene | ug/g | <0.020 | 7274245 | <0.020 | 0.020 | 7274245 |
| RDL = Reportable Detection Limit | • | • | | • | • | |
| OC Batch = Quality Control Batch | | | | | | |

QC Batch = Quality Control Batch

(1) Sodium was not detected. To report SAR the sodium detection limit was used in the calculation. This value represents a maximum ratio.



O.REG 406 EXCESS SOIL MIN. BULK S/SS PKG (SOIL)

| BV Labs ID | | PEF428 | | PEF429 | | |
|--|-------|--------------|----------|--------------|-------|----------|
| Sampling Date | | 2021/03/25 | | 2021/03/25 | | |
| | | 12:00 | | 13:00 | | |
| COC Number | | 817848-01-01 | | 817848-01-01 | | |
| | UNITS | BH131 SS33 | QC Batch | SP1 | RDL | QC Batch |
| Ethylbenzene | ug/g | <0.020 | 7274245 | <0.020 | 0.020 | 7274245 |
| o-Xylene | ug/g | <0.020 | 7274245 | <0.020 | 0.020 | 7274245 |
| p+m-Xylene | ug/g | <0.040 | 7274245 | <0.040 | 0.040 | 7274245 |
| Total Xylenes | ug/g | <0.040 | 7274245 | <0.040 | 0.040 | 7274245 |
| F1 (C6-C10) | ug/g | <10 | 7274245 | <10 | 10 | 7274245 |
| F1 (C6-C10) - BTEX | ug/g | <10 | 7274245 | <10 | 10 | 7274245 |
| F2-F4 Hydrocarbons | | | | | | |
| F2 (C10-C16 Hydrocarbons) | ug/g | <10 | 7273498 | <10 | 10 | 7272947 |
| F3 (C16-C34 Hydrocarbons) | ug/g | <50 | 7273498 | <50 | 50 | 7272947 |
| F4 (C34-C50 Hydrocarbons) | ug/g | <50 | 7273498 | <50 | 50 | 7272947 |
| Reached Baseline at C50 | ug/g | Yes | 7273498 | Yes | | 7272947 |
| Surrogate Recovery (%) | ŗ | | | | | |
| 1,4-Difluorobenzene | % | 104 | 7274245 | 104 | | 7274245 |
| 4-Bromofluorobenzene | % | 90 | 7274245 | 92 | | 7274245 |
| D10-o-Xylene | % | 85 | 7274245 | 86 | | 7274245 |
| D4-1,2-Dichloroethane | % | 94 | 7274245 | 94 | | 7274245 |
| o-Terphenyl | % | 96 | 7273498 | 111 | | 7272947 |
| RDL = Reportable Detection Limit QC Batch = Quality Control Batch | | • | | | - | |



O.REG 406 EXCESS SOIL SPLP METALS (SOIL)

| | | | - | - | | |
|----------------------------------|-------|--------------|--------------|--------------|------|----------|
| BV Labs ID | | PEF420 | PEF423 | PEF426 | | |
| Sampling Date | | 2021/03/18 | 2021/03/25 | 2021/03/23 | | |
| | | 11:00 | 11:00 | 12:00 | | |
| COC Number | | 817848-01-01 | 817848-01-01 | 817848-01-01 | | |
| | UNITS | BH1 SS2 | BH13 SS3 | BH26 SS3 | RDL | QC Batch |
| Metals | | | | | | |
| Leachable (SPLP) Antimony (Sb) | ug/L | <0.5 | <0.5 | <0.5 | 0.5 | 7290197 |
| Leachable (SPLP) Arsenic (As) | ug/L | <1 | <1 | <1 | 1 | 7290197 |
| Leachable (SPLP) Barium (Ba) | ug/L | <5 | <5 | <5 | 5 | 7290197 |
| Leachable (SPLP) Beryllium (Be) | ug/L | <0.5 | <0.5 | <0.5 | 0.5 | 7290197 |
| Leachable (SPLP) Boron (B) | ug/L | 97 | 83 | 190 | 10 | 7290197 |
| Leachable (SPLP) Cadmium (Cd) | ug/L | <0.1 | <0.1 | <0.1 | 0.1 | 7290197 |
| Leachable (SPLP) Chromium (Cr) | ug/L | <5 | <5 | <5 | 5 | 7290197 |
| Leachable (SPLP) Cobalt (Co) | ug/L | <0.5 | <0.5 | <0.5 | 0.5 | 7290197 |
| Leachable (SPLP) Copper (Cu) | ug/L | 1 | <1 | 2 | 1 | 7290197 |
| Leachable (SPLP) Lead (Pb) | ug/L | <0.5 | <0.5 | <0.5 | 0.5 | 7290197 |
| Leachable (SPLP) Molybdenum (Mo) | ug/L | <1 | <1 | <1 | 1 | 7290197 |
| Leachable (SPLP) Nickel (Ni) | ug/L | <1 | <1 | <1 | 1 | 7290197 |
| Leachable (SPLP) Selenium (Se) | ug/L | <2 | <2 | <2 | 2 | 7290197 |
| Leachable (SPLP) Silver (Ag) | ug/L | <0.1 | <0.1 | <0.1 | 0.1 | 7290197 |
| Leachable (SPLP) Thallium (Tl) | ug/L | <0.05 | <0.05 | <0.05 | 0.05 | 7290197 |
| Leachable (SPLP) Uranium (U) | ug/L | <0.1 | <0.1 | <0.1 | 0.1 | 7290197 |
| Leachable (SPLP) Vanadium (V) | ug/L | <1 | <1 | 1 | 1 | 7290197 |
| Leachable (SPLP) Zinc (Zn) | ug/L | <5 | <5 | <5 | 5 | 7290197 |
| RDL = Reportable Detection Limit | | | | | • | |
| QC Batch = Quality Control Batch | | | | | | |
| · | | | | | | |



| | | | • | • | | | | |
|----------------------------------|------------|---------------------|---------------------|---------------------|----------|--|--|--|
| BV Labs ID | | PEF420 | PEF423 | PEF426 | | | | |
| Sampling Date | | 2021/03/18 11:00 | 2021/03/25 11:00 | 2021/03/23 12:00 | | | | |
| COC Number | | 817848-01-01 | 817848-01-01 | 817848-01-01 | | | | |
| | UNITS | BH1 SS2 | BH13 SS3 | BH26 SS3 | QC Batch | | | |
| Inorganics | Inorganics | | | | | | | |
| Dry Weight | g | 100 | 100 | 100 | 7286299 | | | |
| Final pH | рН | 9.18 | 9.21 | 9.12 | 7286282 | | | |
| QC Batch = Quality Control Batch | | | | | | | | |

SPLP LEACHATE PREPARATION (SOIL)



RESULTS OF ANALYSES OF SOIL

| BV Labs ID | | PEF425 | | | |
|-------------------------------|-------|---------------------|-----|----------|--|
| Sampling Date | | 2021/03/22 12:00 | | | |
| COC Number | | 817848-01-01 | | | |
| | UNITS | BH21 SS2 | RDL | QC Batch | |
| Inorganics | | | | | |
| | | | | | |
| Soluble (20:1) Sulphate (SO4) | ug/g | <20 | 20 | 7271490 | |



TEST SUMMARY

| BV Labs ID: | PEF420 |
|-------------|---------|
| Sample ID: | BH1 SS2 |
| Matrix: | Soil |

| Collected: | 2021/03/18 |
|------------|------------|
| Shipped: | |
| Received: | 2021/03/26 |

2021/03/18 2021/03/26

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|---|-----------------|---------|------------|---------------|-------------------------|
| Conductivity | AT | 7275424 | 2021/03/31 | 2021/03/31 | Tarunpreet Kaur |
| Petroleum Hydro. CCME F1 & BTEX in Soil | HSGC/MSFD | 7274245 | N/A | 2021/03/30 | Joe Paino |
| Petroleum Hydrocarbons F2-F4 in Soil | GC/FID | 7273498 | 2021/03/30 | 2021/03/30 | Margaret Kulczyk-Stanko |
| Strong Acid Leachable Metals by ICPMS | ICP/MS | 7271605 | 2021/03/29 | 2021/03/30 | Viviana Canzonieri |
| Total Metals in SPLP Leachate by ICPMS | ICP/MS | 7290197 | 2021/04/09 | 2021/04/09 | Nan Raykha |
| Moisture | BAL | 7270453 | N/A | 2021/03/27 | Gurpreet Kaur (ONT) |
| pH CaCl2 EXTRACT | AT | 7273142 | 2021/03/30 | 2021/03/30 | Surinder Rai |
| Sodium Adsorption Ratio (SAR) | CALC/MET | 7268392 | N/A | 2021/03/31 | Automated Statchk |
| SPLP Inorganic extraction - pH | PH | 7286282 | N/A | 2021/04/08 | Daruish Karimi |
| SPLP Inorganic extraction - Weight | | 7286299 | N/A | 2021/04/08 | Daruish Karimi |

| BV Labs ID: Sample ID: Matrix: | PEF420 Dup BH1 SS2 Soil | | | | | Collected: Shipped: Received: | |
|--------------------------------------|-------------------------------|-----------------|---------|-----------|---------------|-------------------------------------|--|
| Test Description | | Instrumentation | Batch | Extracted | Date Analyzed | Analyst | |
| Petroleum Hydro. CCME | F1 & BTEX in Soil | HSGC/MSFD | 7274245 | N/A | 2021/03/30 | Joe Paino | |

| BV Labs ID: PEF421 Sample ID: BH4 SS3 Matrix: Soil | | | | | Collected: 2021/03/17 Shipped: Received: 2021/03/26 |
|--|-----------------|---------|------------|---------------|---|
| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
| Conductivity | AT | 7275424 | 2021/03/31 | 2021/03/31 | Tarunpreet Kaur |
| Petroleum Hydro. CCME F1 & BTEX in Soil | HSGC/MSFD | 7274245 | N/A | 2021/03/30 | Joe Paino |
| Petroleum Hydrocarbons F2-F4 in Soil | GC/FID | 7273498 | 2021/03/30 | 2021/03/30 | Margaret Kulczyk-Stanko |
| Strong Acid Leachable Metals by ICPMS | ICP/MS | 7271605 | 2021/03/29 | 2021/03/30 | Viviana Canzonieri |
| Moisture | BAL | 7270453 | N/A | 2021/03/27 | Gurpreet Kaur (ONT) |
| pH CaCl2 EXTRACT | AT | 7273142 | 2021/03/30 | 2021/03/30 | Surinder Rai |
| Sodium Adsorption Ratio (SAR) | CALC/MET | 7268392 | N/A | 2021/03/31 | Automated Statchk |

| BV Labs ID: | PEF422 |
|-------------|----------|
| Sample ID: | BH11 SS2 |
| Matrix: | Soil |

Collected: 2021/03/18 Shipped: Received: 2021/03/26

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|---|-----------------|---------|------------|---------------|-------------------------|
| Conductivity | AT | 7275424 | 2021/03/31 | 2021/03/31 | Tarunpreet Kaur |
| Petroleum Hydro. CCME F1 & BTEX in Soil | HSGC/MSFD | 7274245 | N/A | 2021/03/30 | Joe Paino |
| Petroleum Hydrocarbons F2-F4 in Soil | GC/FID | 7273498 | 2021/03/30 | 2021/03/30 | Margaret Kulczyk-Stanko |
| Strong Acid Leachable Metals by ICPMS | ICP/MS | 7271605 | 2021/03/29 | 2021/03/30 | Viviana Canzonieri |
| Moisture | BAL | 7270453 | N/A | 2021/03/27 | Gurpreet Kaur (ONT) |
| pH CaCl2 EXTRACT | AT | 7273142 | 2021/03/30 | 2021/03/30 | Surinder Rai |
| Sodium Adsorption Ratio (SAR) | CALC/MET | 7268392 | N/A | 2021/03/31 | Automated Statchk |

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TEST SUMMARY

| BV Labs ID: | PEF423 |
|-------------|----------|
| Sample ID: | BH13 SS3 |
| Matrix: | Soil |

| Collected: | 2021/03/25 |
|------------|------------|
| Shipped: | |
| Received: | 2021/03/26 |

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|---|-----------------|---------|------------|---------------|---------------------|
| Conductivity | AT | 7275424 | 2021/03/31 | 2021/03/31 | Tarunpreet Kaur |
| Petroleum Hydro. CCME F1 & BTEX in Soil | HSGC/MSFD | 7274245 | N/A | 2021/03/30 | Joe Paino |
| Petroleum Hydrocarbons F2-F4 in Soil | GC/FID | 7272947 | 2021/03/29 | 2021/03/30 | Prabhjot Gulati |
| Strong Acid Leachable Metals by ICPMS | ICP/MS | 7271605 | 2021/03/29 | 2021/03/30 | Viviana Canzonieri |
| Total Metals in SPLP Leachate by ICPMS | ICP/MS | 7290197 | 2021/04/09 | 2021/04/09 | Nan Raykha |
| Moisture | BAL | 7270453 | N/A | 2021/03/27 | Gurpreet Kaur (ONT) |
| pH CaCl2 EXTRACT | AT | 7273142 | 2021/03/30 | 2021/03/30 | Surinder Rai |
| Sodium Adsorption Ratio (SAR) | CALC/MET | 7268392 | N/A | 2021/03/31 | Automated Statchk |
| SPLP Inorganic extraction - pH | РН | 7286282 | N/A | 2021/04/08 | Daruish Karimi |
| SPLP Inorganic extraction - Weight | | 7286299 | N/A | 2021/04/08 | Daruish Karimi |

| BV Labs ID: | PEF424 |
|-------------|----------|
| Sample ID: | BH18 SS4 |
| Matrix: | Soil |

Sodium Adsorption Ratio (SAR)

| Collected: | 2021/03/22 |
|------------|------------|
| Shipped: | |
| Received: | 2021/03/26 |

Automated Statchk

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|---|-----------------|---------|------------|---------------|-------------------------|
| Conductivity | AT | 7275424 | 2021/03/31 | 2021/03/31 | Tarunpreet Kaur |
| Petroleum Hydro. CCME F1 & BTEX in Soil | HSGC/MSFD | 7274245 | N/A | 2021/03/30 | Joe Paino |
| Petroleum Hydrocarbons F2-F4 in Soil | GC/FID | 7273498 | 2021/03/30 | 2021/03/30 | Margaret Kulczyk-Stanko |
| Strong Acid Leachable Metals by ICPMS | ICP/MS | 7271605 | 2021/03/29 | 2021/03/30 | Viviana Canzonieri |
| Moisture | BAL | 7270453 | N/A | 2021/03/27 | Gurpreet Kaur (ONT) |
| pH CaCl2 EXTRACT | AT | 7273142 | 2021/03/30 | 2021/03/30 | Surinder Rai |
| Sodium Adsorption Ratio (SAR) | CALC/MET | 7268392 | N/A | 2021/03/31 | Automated Statchk |

| BV Labs ID: Sample ID: Matrix: | PEF424 Dup BH18 SS4 Soil | | | | | Collected: Shipped: Received: | 2021/03/22 2021/03/26 |
|--------------------------------------|--------------------------------|-----------------|---------|------------|---------------|-------------------------------------|--------------------------|
| Test Description | | Instrumentation | Batch | Extracted | Date Analyzed | Analyst | |
| Petroleum Hydrocarbons | F2-F4 in Soil | GC/FID | 7273498 | 2021/03/30 | 2021/03/30 | Margaret | Kulczyk-Stanko |
| BV Labs ID: Sample ID: Matrix: | PEF425 BH21 SS2 Soil | | | | | Collected: Shipped: Received: | 2021/03/22 2021/03/26 |
| Test Description | | Instrumentation | Batch | Extracted | Date Analyzed | Analyst | |
| Conductivity | | AT | 7275424 | 2021/03/31 | 2021/03/31 | Tarunpree | t Kaur |
| Petroleum Hydro. CCME | F1 & BTEX in Soil | HSGC/MSFD | 7274245 | N/A | 2021/03/30 | Joe Paino | |
| Petroleum Hydrocarbons | F2-F4 in Soil | GC/FID | 7273498 | 2021/03/30 | 2021/03/30 | Margaret | Kulczyk-Stanko |
| Strong Acid Leachable Me | etals by ICPMS | ICP/MS | 7271605 | 2021/03/29 | 2021/03/30 | Viviana Ca | nzonieri |
| Moisture | | BAL | 7270453 | N/A | 2021/03/27 | Gurpreet I | Kaur (ONT) |
| pH CaCl2 EXTRACT | | AT | 7273142 | 2021/03/30 | 2021/03/30 | Surinder R | ai |

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N/A

2021/03/31

7268392

CALC/MET



TEST SUMMARY

| BV Labs ID: PEF425 Sample ID: BH21 SS2 Matrix: Soil | | | | | Collected: 2021/03/22 Shipped: Received: 2021/03/26 |
|--|--|---|--|--|--|
| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
| Sulphate (20:1 Extract) | KONE/EC | 7271490 | 2021/03/29 | 2021/03/31 | Avneet Kour Sudan |
| BV Labs ID: PEF426 Sample ID: BH26 SS3 Matrix: Soil | | | | | Collected: 2021/03/23 Shipped: Received: 2021/03/26 |
| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
| Conductivity | AT | 7275424 | 2021/03/31 | 2021/03/31 | Tarunpreet Kaur |
| Petroleum Hydro. CCME F1 & BTEX in Soil | HSGC/MSFD | 7274245 | N/A | 2021/03/30 | Joe Paino |
| Petroleum Hydrocarbons F2-F4 in Soil | GC/FID | 7273498 | 2021/03/30 | 2021/03/30 | Margaret Kulczyk-Stanko |
| Strong Acid Leachable Metals by ICPMS | ICP/MS | 7271605 | 2021/03/29 | 2021/03/30 | Viviana Canzonieri |
| Total Metals in SPLP Leachate by ICPMS | ICP/MS | 7290197 | 2021/04/09 | 2021/04/09 | Nan Raykha |
| Moisture | BAL | 7270453 | N/A | 2021/03/27 | Gurpreet Kaur (ONT) |
| pH CaCl2 EXTRACT | AT | 7273142 | 2021/03/30 | 2021/03/30 | Surinder Rai |
| Sodium Adsorption Ratio (SAR) | CALC/MET | 7268392 | N/A | 2021/03/31 | Automated Statchk |
| SPLP Inorganic extraction - pH | РН | 7286282 | N/A | 2021/04/08 | Daruish Karimi |
| SPLP Inorganic extraction - Weight | | 7286299 | N/A | 2021/04/08 | Daruish Karimi |
| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Received: 2021/03/26 Analyst |
| Moisture | BAL | 7270453 | N/A | 2021/03/27 | Gurpreet Kaur (ONT) |
| BV Labs ID: PEF427 Sample ID: BH30 SS4 Matrix: Soil | | | | | Collected: 2021/03/24 Shipped: Received: 2021/03/26 |
| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
| | | | | | |
| Conductivity | AT | 7275424 | 2021/03/31 | 2021/03/31 | Tarunpreet Kaur |
| , | AT HSGC/MSFD | 7275424 7274245 | 2021/03/31 N/A | 2021/03/31 2021/03/30 | • |
| Petroleum Hydro. CCME F1 & BTEX in Soil | | | | | Tarunpreet Kaur |
| Petroleum Hydro. CCME F1 & BTEX in Soil Petroleum Hydrocarbons F2-F4 in Soil | HSGC/MSFD | 7274245 | N/A | 2021/03/30 | Tarunpreet Kaur Joe Paino |
| Petroleum Hydro. CCME F1 & BTEX in Soil Petroleum Hydrocarbons F2-F4 in Soil Strong Acid Leachable Metals by ICPMS | HSGC/MSFD GC/FID | 7274245 7273498 | N/A 2021/03/30 | 2021/03/30 2021/03/30 | Tarunpreet Kaur Joe Paino Margaret Kulczyk-Stanko |
| Petroleum Hydro. CCME F1 & BTEX in Soil Petroleum Hydrocarbons F2-F4 in Soil Strong Acid Leachable Metals by ICPMS Moisture | HSGC/MSFD GC/FID ICP/MS | 7274245 7273498 7271820 | N/A 2021/03/30 2021/03/29 | 2021/03/30 2021/03/30 2021/03/31 2021/03/27 2021/03/30 | Tarunpreet Kaur Joe Paino Margaret Kulczyk-Stanko Daniel Teclu |
| Conductivity Petroleum Hydro. CCME F1 & BTEX in Soil Petroleum Hydrocarbons F2-F4 in Soil Strong Acid Leachable Metals by ICPMS Moisture pH CaCl2 EXTRACT Sodium Adsorption Ratio (SAR) | HSGC/MSFD GC/FID ICP/MS BAL | 7274245 7273498 7271820 7270453 | N/A 2021/03/30 2021/03/29 N/A | 2021/03/30 2021/03/30 2021/03/31 2021/03/27 | Tarunpreet Kaur Joe Paino Margaret Kulczyk-Stanko Daniel Teclu Gurpreet Kaur (ONT) |
| Petroleum Hydro. CCME F1 & BTEX in Soil Petroleum Hydrocarbons F2-F4 in Soil Strong Acid Leachable Metals by ICPMS Moisture pH CaCl2 EXTRACT | HSGC/MSFD GC/FID ICP/MS BAL AT | 7274245 7273498 7271820 7270453 7273142 | N/A 2021/03/30 2021/03/29 N/A 2021/03/30 | 2021/03/30 2021/03/30 2021/03/31 2021/03/27 2021/03/30 | Tarunpreet Kaur Joe Paino Margaret Kulczyk-Stanko Daniel Teclu Gurpreet Kaur (ONT) Surinder Rai |
| Petroleum Hydro. CCME F1 & BTEX in Soil Petroleum Hydrocarbons F2-F4 in Soil Strong Acid Leachable Metals by ICPMS Moisture pH CaCl2 EXTRACT Sodium Adsorption Ratio (SAR) BV Labs ID: PEF427 Dup Sample ID: BH30 SS4 | HSGC/MSFD GC/FID ICP/MS BAL AT | 7274245 7273498 7271820 7270453 7273142 | N/A 2021/03/30 2021/03/29 N/A 2021/03/30 | 2021/03/30 2021/03/30 2021/03/31 2021/03/27 2021/03/30 | Tarunpreet Kaur Joe Paino Margaret Kulczyk-Stanko Daniel Teclu Gurpreet Kaur (ONT) Surinder Rai Automated Statchk Collected: 2021/03/24 Shipped: |



TEST SUMMARY

| BV Labs ID: | PEF428 |
|-------------|------------|
| Sample ID: | BH131 SS33 |
| Matrix: | Soil |

| Collected: | 2021/03/25 |
|------------|------------|
| Shipped: | |
| Received: | 2021/03/26 |

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|---|-----------------|---------|------------|---------------|-------------------------|
| Conductivity | AT | 7275424 | 2021/03/31 | 2021/03/31 | Tarunpreet Kaur |
| Petroleum Hydro. CCME F1 & BTEX in Soil | HSGC/MSFD | 7274245 | N/A | 2021/03/30 | Joe Paino |
| Petroleum Hydrocarbons F2-F4 in Soil | GC/FID | 7273498 | 2021/03/30 | 2021/03/30 | Margaret Kulczyk-Stanko |
| Strong Acid Leachable Metals by ICPMS | ICP/MS | 7271605 | 2021/03/29 | 2021/03/30 | Viviana Canzonieri |
| Moisture | BAL | 7270453 | N/A | 2021/03/27 | Gurpreet Kaur (ONT) |
| pH CaCl2 EXTRACT | AT | 7273142 | 2021/03/30 | 2021/03/30 | Surinder Rai |
| Sodium Adsorption Ratio (SAR) | CALC/MET | 7268392 | N/A | 2021/03/31 | Automated Statchk |

| BV Labs ID: | PEF429 |
|-------------|--------|
| Sample ID: | SP1 |
| Matrix: | Soil |

| Collected: | 2021/03/25 |
|------------|------------|
| Shipped: | |
| Received: | 2021/03/26 |

| Test Description | Instrumentation | Batch | Extracted | Date Analyzed | Analyst |
|---|-----------------|---------|------------|---------------|---------------------|
| Conductivity | AT | 7275424 | 2021/03/31 | 2021/03/31 | Tarunpreet Kaur |
| Petroleum Hydro. CCME F1 & BTEX in Soil | HSGC/MSFD | 7274245 | N/A | 2021/03/30 | Joe Paino |
| Petroleum Hydrocarbons F2-F4 in Soil | GC/FID | 7272947 | 2021/03/29 | 2021/03/30 | Prabhjot Gulati |
| Strong Acid Leachable Metals by ICPMS | ICP/MS | 7271605 | 2021/03/29 | 2021/03/30 | Viviana Canzonieri |
| Moisture | BAL | 7270453 | N/A | 2021/03/27 | Gurpreet Kaur (ONT) |
| pH CaCl2 EXTRACT | AT | 7273142 | 2021/03/30 | 2021/03/30 | Surinder Rai |
| Sodium Adsorption Ratio (SAR) | CALC/MET | 7268392 | N/A | 2021/03/31 | Automated Statchk |



GENERAL COMMENTS

| Package 1 3.0°C Revised Report (2021/04/12): Additional analysis for SPLP Metals reported under samples BH1 SS2, BH13 SS3 and BH 26 SS3 as per David Dennison's |
|---|
| Revised Report (2021/04/12): Additional analysis for SPLP Metals reported under samples BH1 SS2, BH13 SS3 and BH 26 SS3 as per David Dennison's |
| request. |
| Sample PEF421 [BH4 SS3] : F1/BTEX Analysis: Soil weight exceeds the protocol specification of approximately 5g in the field preserved vial. Additional methanol was added to the vial to ensure extraction efficiency. |
| Sample PEF422 [BH11 SS2] : F1/BTEX Analysis: Soil weight exceeds the protocol specification of approximately 5g in the field preserved vial. Additional methanol was added to the vial to ensure extraction efficiency. |
| Sample PEF423 [BH13 SS3] : F1/BTEX Analysis: Soil weight exceeds the protocol specification of approximately 5g in the field preserved vial. Additional methanol was added to the vial to ensure extraction efficiency. |
| Sample PEF425 [BH21 SS2] : F1/BTEX Analysis: Soil weight exceeds the protocol specification of approximately 5g in the field preserved vial. Additional methanol was added to the vial to ensure extraction efficiency. |
| Results relate only to the items tested. |



QUALITY ASSURANCE REPORT

exp Services Inc Client Project #: BRM-21004344-B0 Site Location: 12304 HEARTLAKE RD Your P.O. #: BRM-GEO Sampler Initials: BH

| | | | Matrix | Spike | SPIKED | BLANK | Method | Blank | RPD | | Leachate | Blank |
|----------|-----------------------------------|------------|------------|-----------|------------|-------------|--------|-------------|------|-----------|----------|-------|
| QC Batch | Parameter | Date | % Recovery | QC Limits | % Recovery | QC Limits | Value | Value UNITS | | QC Limits | Value | UNITS |
| 7272947 | o-Terphenyl | 2021/03/30 | 108 | 60 - 130 | 105 | 60 - 130 | 110 | % | | | | |
| 7273498 | 8 o-Terphenyl 2021/03/30 | | 90 | 60 - 130 | 91 | 91 60 - 130 | | % | | | | |
| 7274245 | 45 1,4-Difluorobenzene 2021/03/30 | | 99 | 60 - 140 | 101 | 60 - 140 | 101 | % | | | | |
| 7274245 | 4-Bromofluorobenzene | 2021/03/30 | 99 | 60 - 140 | 97 | 60 - 140 | 94 | % | | | | |
| 7274245 | D10-o-Xylene | 2021/03/30 | 80 | 60 - 140 | 90 | 60 - 140 | 78 | % | | | | |
| 7274245 | D4-1,2-Dichloroethane | 2021/03/30 | 91 | 60 - 140 | 89 | 60 - 140 | 94 | % | | | | |
| 7270453 | Moisture | 2021/03/27 | | | | | | | 0 | 20 | | |
| 7271490 | Soluble (20:1) Sulphate (SO4) | 2021/03/31 | 128 | 70 - 130 | 107 | 70 - 130 | <20 | ug/g | NC | 35 | | |
| 7271605 | Acid Extractable Antimony (Sb) | 2021/03/30 | 93 | 75 - 125 | 103 | 80 - 120 | <0.20 | ug/g | NC | 30 | | |
| 7271605 | Acid Extractable Arsenic (As) | 2021/03/30 | 91 | 75 - 125 | 104 | 80 - 120 | <1.0 | ug/g | 3.2 | 30 | | |
| 7271605 | Acid Extractable Barium (Ba) | 2021/03/30 | 98 | 75 - 125 | 104 | 80 - 120 | <0.50 | ug/g | 3.3 | 30 | | |
| 7271605 | Acid Extractable Beryllium (Be) | 2021/03/30 | 98 | 75 - 125 | 106 | 80 - 120 | <0.20 | ug/g | NC | 30 | | |
| 7271605 | Acid Extractable Boron (B) | 2021/03/30 | 98 | 75 - 125 | 108 | 80 - 120 | <5.0 | ug/g | NC | 30 | | |
| 7271605 | Acid Extractable Cadmium (Cd) | 2021/03/30 | 92 | 75 - 125 | 101 | 80 - 120 | <0.10 | ug/g | NC | 30 | | |
| 7271605 | Acid Extractable Chromium (Cr) | 2021/03/30 | 93 | 75 - 125 | 104 | 80 - 120 | <1.0 | ug/g | 6.5 | 30 | | |
| 7271605 | Acid Extractable Cobalt (Co) | 2021/03/30 | 92 | 75 - 125 | 105 | 80 - 120 | <0.10 | ug/g | 1.6 | 30 | | |
| 7271605 | Acid Extractable Copper (Cu) | 2021/03/30 | 89 | 75 - 125 | 102 | 80 - 120 | <0.50 | ug/g | 0.47 | 30 | | |
| 7271605 | Acid Extractable Lead (Pb) | 2021/03/30 | NC | 75 - 125 | 102 | 80 - 120 | <1.0 | ug/g | 3.7 | 30 | | |
| 7271605 | Acid Extractable Molybdenum (Mo) | 2021/03/30 | 90 | 75 - 125 | 98 | 80 - 120 | <0.50 | ug/g | NC | 30 | | |
| 7271605 | Acid Extractable Nickel (Ni) | 2021/03/30 | 93 | 75 - 125 | 106 | 80 - 120 | <0.50 | ug/g | 3.9 | 30 | | |
| 7271605 | Acid Extractable Selenium (Se) | 2021/03/30 | 91 | 75 - 125 | 104 | 80 - 120 | <0.50 | ug/g | NC | 30 | | |
| 7271605 | Acid Extractable Silver (Ag) | 2021/03/30 | 91 | 75 - 125 | 102 | 80 - 120 | <0.20 | ug/g | NC | 30 | | |
| 7271605 | Acid Extractable Thallium (TI) | 2021/03/30 | 90 | 75 - 125 | 104 | 80 - 120 | <0.050 | ug/g | NC | 30 | | |
| 7271605 | Acid Extractable Uranium (U) | 2021/03/30 | 89 | 75 - 125 | 100 | 80 - 120 | <0.050 | ug/g | 12 | 30 | | |
| 7271605 | Acid Extractable Vanadium (V) | 2021/03/30 | 96 | 75 - 125 | 105 | 80 - 120 | <5.0 | ug/g | 12 | 30 | | |
| 7271605 | Acid Extractable Zinc (Zn) | 2021/03/30 | NC | 75 - 125 | 105 | 80 - 120 | <5.0 | ug/g | 8.8 | 30 | | |
| 7271820 | Acid Extractable Antimony (Sb) | 2021/03/30 | 89 | 75 - 125 | 101 | 80 - 120 | <0.20 | ug/g | 10 | 30 | | |
| 7271820 | Acid Extractable Arsenic (As) | 2021/03/30 | 95 | 75 - 125 | 102 | 80 - 120 | <1.0 | ug/g | 0.62 | 30 | | |
| 7271820 | Acid Extractable Barium (Ba) | 2021/03/30 | NC | 75 - 125 | 101 | 80 - 120 | <0.50 | ug/g | 0.10 | 30 | | |
| 7271820 | Acid Extractable Beryllium (Be) | 2021/03/30 | 92 | 75 - 125 | 100 | 80 - 120 | <0.20 | ug/g | 7.5 | 30 | | |

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QUALITY ASSURANCE REPORT(CONT'D)

exp Services Inc Client Project #: BRM-21004344-B0 Site Location: 12304 HEARTLAKE RD Your P.O. #: BRM-GEO Sampler Initials: BH

| | | | Matrix | Spike | SPIKED | BLANK | Method | Blank | RP | D | Leachate | Blank |
|----------|----------------------------------|------------|------------|-----------|------------|-----------|--------|-------------|------|-----------|----------|-------|
| QC Batch | Parameter | Date | % Recovery | QC Limits | % Recovery | QC Limits | Value | Value UNITS | | QC Limits | Value | UNITS |
| 7271820 | Acid Extractable Boron (B) | 2021/03/30 | 88 | 75 - 125 | 99 | 80 - 120 | <5.0 | ug/g | 14 | 30 | | |
| 7271820 | Acid Extractable Cadmium (Cd) | 2021/03/30 | 94 | 75 - 125 | 100 | 80 - 120 | <0.10 | ug/g | 2.7 | 30 | | |
| 7271820 | Acid Extractable Chromium (Cr) | 2021/03/30 | 94 | 75 - 125 | 103 | 80 - 120 | <1.0 | ug/g | 1.5 | 30 | | |
| 7271820 | Acid Extractable Cobalt (Co) | 2021/03/30 | 90 | 75 - 125 | 102 | 80 - 120 | <0.10 | ug/g | 8.5 | 30 | | |
| 7271820 | Acid Extractable Copper (Cu) | 2021/03/30 | 90 | 75 - 125 | 103 | 80 - 120 | <0.50 | ug/g | 4.0 | 30 | | |
| 7271820 | Acid Extractable Lead (Pb) | 2021/03/30 | NC | 75 - 125 | 99 | 80 - 120 | <1.0 | ug/g | 1.3 | 30 | | |
| 7271820 | Acid Extractable Molybdenum (Mo) | 2021/03/30 | 91 | 75 - 125 | 97 | 80 - 120 | <0.50 | ug/g | NC | 30 | | |
| 7271820 | Acid Extractable Nickel (Ni) | 2021/03/30 | 94 | 75 - 125 | 106 | 80 - 120 | <0.50 | ug/g | 0.98 | 30 | | |
| 7271820 | Acid Extractable Selenium (Se) | 2021/03/30 | 95 | 75 - 125 | 104 | 80 - 120 | <0.50 | ug/g | NC | 30 | | |
| 7271820 | Acid Extractable Silver (Ag) | 2021/03/30 | 93 | 75 - 125 | 101 | 80 - 120 | <0.20 | ug/g | NC | 30 | | |
| 7271820 | Acid Extractable Thallium (Tl) | 2021/03/30 | 89 | 75 - 125 | 99 | 80 - 120 | <0.050 | ug/g | 0.20 | 30 | | |
| 7271820 | Acid Extractable Uranium (U) | 2021/03/30 | 93 | 75 - 125 | 100 | 80 - 120 | <0.050 | ug/g | 0.33 | 30 | | |
| 7271820 | Acid Extractable Vanadium (V) | 2021/03/30 | NC | 75 - 125 | 100 | 80 - 120 | <5.0 | ug/g | 1.1 | 30 | | |
| 7271820 | Acid Extractable Zinc (Zn) | 2021/03/30 | NC | 75 - 125 | 99 | 80 - 120 | <5.0 | ug/g | 1.3 | 30 | | |
| 7272947 | F2 (C10-C16 Hydrocarbons) | 2021/03/30 | 119 | 50 - 130 | 114 | 80 - 120 | <10 | ug/g | NC | 30 | | |
| 7272947 | F3 (C16-C34 Hydrocarbons) | 2021/03/30 | 120 | 50 - 130 | 115 | 80 - 120 | <50 | ug/g | NC | 30 | | |
| 7272947 | F4 (C34-C50 Hydrocarbons) | 2021/03/30 | 119 | 50 - 130 | 115 | 80 - 120 | <50 | ug/g | NC | 30 | | |
| 7273142 | Available (CaCl2) pH | 2021/03/30 | | | 100 | 97 - 103 | | | 0.63 | N/A | | |
| 7273498 | F2 (C10-C16 Hydrocarbons) | 2021/03/30 | 99 | 50 - 130 | 97 | 80 - 120 | <10 | ug/g | 18 | 30 | | |
| 7273498 | F3 (C16-C34 Hydrocarbons) | 2021/03/30 | 99 | 50 - 130 | 97 | 80 - 120 | <50 | ug/g | NC | 30 | | |
| 7273498 | F4 (C34-C50 Hydrocarbons) | 2021/03/30 | 97 | 50 - 130 | 95 | 80 - 120 | <50 | ug/g | NC | 30 | | |
| 7274245 | Benzene | 2021/03/30 | 76 | 50 - 140 | 90 | 50 - 140 | <0.020 | ug/g | NC | 50 | | |
| 7274245 | Ethylbenzene | 2021/03/30 | 84 | 50 - 140 | 99 | 50 - 140 | <0.020 | ug/g | NC | 50 | | |
| 7274245 | F1 (C6-C10) - BTEX | 2021/03/30 | | | | | <10 | ug/g | NC | 30 | | |
| 7274245 | F1 (C6-C10) | 2021/03/30 | 77 | 60 - 140 | 81 | 80 - 120 | <10 | ug/g | NC | 30 | | |
| 7274245 | o-Xylene | 2021/03/30 | 83 | 50 - 140 | 95 | 50 - 140 | <0.020 | ug/g | NC | 50 | | |
| 7274245 | p+m-Xylene | 2021/03/30 | 80 | 50 - 140 | 94 | 50 - 140 | <0.040 | ug/g | NC | 50 | | |
| 7274245 | Toluene | 2021/03/30 | 77 | 50 - 140 | 91 | 50 - 140 | <0.020 | ug/g | NC | 50 | | |
| 7274245 | Total Xylenes | 2021/03/30 | | | | | <0.040 | ug/g | NC | 50 | | |
| 7275424 | Conductivity | 2021/03/31 | | | 102 | 90 - 110 | <0.002 | mS/cm | 0.31 | 10 | | |

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QUALITY ASSURANCE REPORT(CONT'D)

exp Services Inc Client Project #: BRM-21004344-B0 Site Location: 12304 HEARTLAKE RD Your P.O. #: BRM-GEO Sampler Initials: BH

| | | | | Matrix Spike | | BLANK | Method I | Blank | RP | D | Leachate Blank | | |
|----------|----------------------------------|------------|------------|--------------|-----|-----------|----------|-------|-----------|-----------|----------------|-------|--|
| QC Batch | Parameter | Date | % Recovery | - | | QC Limits | Value | UNITS | Value (%) | QC Limits | Value | UNITS | |
| 7290197 | Leachable (SPLP) Antimony (Sb) | 2021/04/09 | 105 | 80 - 120 | 105 | 80 - 120 | <0.5 | ug/L | 2.0 | 35 | <0.5 | ug/L | |
| 7290197 | Leachable (SPLP) Arsenic (As) | 2021/04/09 | 102 | 80 - 120 | 102 | 80 - 120 | <1 | ug/L | 5.1 | 35 | <1 | ug/L | |
| 7290197 | Leachable (SPLP) Barium (Ba) | 2021/04/09 | 101 | 80 - 120 | 103 | 80 - 120 | <5 | ug/L | NC | 35 | <5 | ug/L | |
| 7290197 | Leachable (SPLP) Beryllium (Be) | 2021/04/09 | 102 | 80 - 120 | 103 | 80 - 120 | <0.5 | ug/L | NC | 35 | <0.5 | ug/L | |
| 7290197 | Leachable (SPLP) Boron (B) | 2021/04/09 | 96 | 80 - 120 | 95 | 80 - 120 | <10 | ug/L | 2.1 | 35 | <10 | ug/L | |
| 7290197 | Leachable (SPLP) Cadmium (Cd) | 2021/04/09 | 104 | 80 - 120 | 105 | 80 - 120 | <0.1 | ug/L | NC | 35 | <0.1 | ug/L | |
| 7290197 | Leachable (SPLP) Chromium (Cr) | 2021/04/09 | 97 | 80 - 120 | 98 | 80 - 120 | <5 | ug/L | NC | 35 | <5 | ug/L | |
| 7290197 | Leachable (SPLP) Cobalt (Co) | 2021/04/09 | 99 | 80 - 120 | 100 | 80 - 120 | <0.5 | ug/L | NC | 35 | <0.5 | ug/L | |
| 7290197 | Leachable (SPLP) Copper (Cu) | 2021/04/09 | 104 | 80 - 120 | 105 | 80 - 120 | <1 | ug/L | 4.6 | 35 | <1 | ug/L | |
| 7290197 | Leachable (SPLP) Lead (Pb) | 2021/04/09 | 103 | 80 - 120 | 103 | 80 - 120 | <0.5 | ug/L | NC | 35 | <0.5 | ug/L | |
| 7290197 | Leachable (SPLP) Molybdenum (Mo) | 2021/04/09 | 103 | 80 - 120 | 105 | 80 - 120 | <1 | ug/L | 0 | 35 | <1 | ug/L | |
| 7290197 | Leachable (SPLP) Nickel (Ni) | 2021/04/09 | 97 | 80 - 120 | 98 | 80 - 120 | <1 | ug/L | NC | 35 | <1 | ug/L | |
| 7290197 | Leachable (SPLP) Selenium (Se) | 2021/04/09 | 104 | 80 - 120 | 106 | 80 - 120 | <2 | ug/L | NC | 35 | <2 | ug/L | |
| 7290197 | Leachable (SPLP) Silver (Ag) | 2021/04/09 | 102 | 80 - 120 | 103 | 80 - 120 | <0.1 | ug/L | NC | 35 | <0.1 | ug/L | |
| 7290197 | Leachable (SPLP) Thallium (TI) | 2021/04/09 | 103 | 80 - 120 | 104 | 80 - 120 | <0.05 | ug/L | NC | 35 | <0.05 | ug/L | |
| 7290197 | Leachable (SPLP) Uranium (U) | 2021/04/09 | 103 | 80 - 120 | 103 | 80 - 120 | <0.1 | ug/L | | | <0.1 | ug/L | |
| 7290197 | Leachable (SPLP) Vanadium (V) | 2021/04/09 | 100 | 80 - 120 | 100 | 80 - 120 | <1 | ug/L | 2.6 | 35 | <1 | ug/L | |
| 7290197 | Leachable (SPLP) Zinc (Zn) | 2021/04/09 | 104 | 80 - 120 | 105 | 80 - 120 | <5 | ug/L | NC | 35 | <5 | ug/L | |

N/A = Not Applicable

Duplicate: Paired analysis of a separate portion of the same sample. Used to evaluate the variance in the measurement.

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate sample matrix interference.

Leachate Blank: A blank matrix containing all reagents used in the leaching procedure. Used to determine any process contamination.

Spiked Blank: A blank matrix sample to which a known amount of the analyte, usually from a second source, has been added. Used to evaluate method accuracy.

Method Blank: A blank matrix containing all reagents used in the analytical procedure. Used to identify laboratory contamination.

Surrogate: A pure or isotopically labeled compound whose behavior mirrors the analytes of interest. Used to evaluate extraction efficiency.

NC (Matrix Spike): The recovery in the matrix spike was not calculated. The relative difference between the concentration in the parent sample and the spike amount was too small to permit a reliable recovery calculation (matrix spike concentration was less than the native sample concentration)

NC (Duplicate RPD): The duplicate RPD was not calculated. The concentration in the sample and/or duplicate was too low to permit a reliable RPD calculation (absolute difference <= 2x RDL).

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VALIDATION SIGNATURE PAGE

The analytical data and all QC contained in this report were reviewed and validated by the following individual(s).

Anastassia Hamanov, Scientific Specialist

BV Labs has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per ISO/IEC 17025, signing the reports. For Service Group specific validation please refer to the Validation Signature Page.

| OWN OF CALEDON PLANNING RECEIVED | |
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| Nov 26, 2021 | |

| | | | Bureau Veritas Laboratories 6740 Campobello Road, Mississauga, Or | ntario Canada L5N 2 | L8 Tel (905) 817-57 | 700 Toll-free:800- | 563-6266 Fax (90 | 05) 817-57 | 777 www.b | vlabs.com | | | | | | СН | 3 | 26-Mar-21 13 | :27 | Ρ | Page of |
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| Tel: | | (905) 793-9800 | Fax. (905) 793-064 | 1 Tab | anc/ | 797 90 | 00 - | | - 19 | | Project Na | me: | 1230 | 4 HEAVE | LA | ME ECL | | | | Project | Manager: |
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| | | | Other | | | | ilter tals | Exce | C Excess | | | - × - | | | | | Job Specifi Date Require | c Rush TAT (if applies to | | sion) Required: | _ |
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| | | Barcode Label | Sample (Location) Identification | Date Sampled | Time Sampled | Matrix | | 0 Å | Ó | <u> </u> | | | | | _ | | # or boules | | Commen | s | |
| 1 | BH 1 | 552 | BHI SS2 | 3118121 | II AM | SOIL | l se e | × | X | | | | | | | | 5 | 1 Pleas | e p | ut | |
| 2 | BH4 | 522 - | BH4 SS3 | 3117121 | 12 PM | N. | | × | × | | | | | | | | 5 | all | Anal | avsis | 2 |
| 3 | BHI | SS2 | BHII SS2 | 3118121 | 12.PM | | | X | × | | | | 2 | | | | 5 | Pors | 1 100 100 | 1 | TALS |
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| 4 | BH1. | 3 22 3 | BH13 553 | 3125121 | ILPM | | | × | × | | | | | | | | 5 | lon h | old | 2 | |
| 5 | BHI | 8 SS4 | BH 18 SJ4 | 3122121 | II PM | | | $ \times $ | \prec | | | | | | | | 5- | Cont | 24 | | - |
| 6 | BHZ | 1 SI2 | BHZI SJ2 | 3122121 | 12 PM | | | × | × | × | | | | | | | 5 | | | | |
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| 8 | BH 3 | 30 554 | BH 30 554 | 3/24/21 | 12 PM | | 2 | × | × | | | | | | | | 5 | | | | |
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| | | Bernd Hell | | and the second se | | | | | 21/03 | and automities | | | | Time Sensitive | Laboratory Use Only Ve Temperature (%C) on Recei Custody Seal Yes No | | | | | | |
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| * UNI | ESS OTHER | WISE AGREED TO IN W | RITING, WORK SUBMITTED ON THIS CHAIN | | | C' STANDADD TO | ME AND CONDIT | | | THE CHAN | | DV DOC' | | - | | | 15/ | 113 | Intact | | - |
| ACK | OWLEDGME | NT AND ACCEPTANCE | OF OUR TERMS WHICH ARE AVAILABLE F | OR VIEWING AT WW | W.BVLABS.COM/TE | RMS-AND-CONDI | TIONS. | IONS. SIC | JAING OF | THIS CHAIN | OF COSTC | JUT DUCU | MENT IS | 1.12 | | | the state | | White: BV | Labs | Yellow: Client |
| * IT IS | THE RESPO | NSIBILITY OF THE REL | INQUISHER TO ENSURE THE ACCURACY | OF THE CHAIN OF C | USTODY RECORD. | AN INCOMPLETE | CHAIN OF CUSTO | DY MAY F | RESULT IN | ANALYTIC | AL TAT DE | LAYS. | | SAM | PLES M | UST BE KEPT CO | OOL (< 10° C) ELIVERY TO BY | FROM TIME OF SAMPLIN | IG | | |
| ** SA | MPLE CONTA | INER, PRESERVATION | , HOLD TIME AND PACKAGE INFORMATIO | N CAN BE VIEWED A | T WWW.BVLABS.C | OM/RESOURCES/ | CHAIN-OF-CUSTC | DY-FORM | MS. | | | | | | | | | | | | |

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