

12189 – 0 DIXIE ROAD, CALEDON, ON

STORMWATER MANAGEMENT BRIEF

MARCH 5, 2025

TOWN OF CALEDON
PLANNING
RECEIVED
October 23rd, 2025

CLIENT: 2572934 ONTARIO INC.

MUNICIPALITY: TOWN OF CALEDON



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Where Community Design & Develop

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PROJECT # 25109

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1.0 INTRODUCTION

1.1. STUDY OBJECTIVE

ARIK Engineering Ltd., has been retained by **2572934 Ontario Inc.** to prepare a stormwater management brief for the proposed development located at 12189 – 0 Dixie Road, Caledon, Ontario. The proposed development is located at the east side of Dixie Road and north of Spokane Street. The development is bounded by Dixie Road to the west, Spokane Street to the south and existing vacant lands to the north and east. An existing dwelling currently located on the property. The client would like to convert the existing dwelling to temporary office and provide gravel trailer parking area along north side of the existing building. The total area of the site is approximately 0.76ha.

The purpose of this report is to provide Stormwater Management Design Brief for the property 12189 – 0 Dixie Road legally know as Part of Lot 18, Concession 4, Town of Caledon. The site grading for the proposed trailer gravel parking extension area has been designed to follow the existing drainage pattern.

1.2. EXISTING TOPOGRAPHY AND DRAINAGE PATTERN

As per the natural topography of the subject site, most of the site drains from front to rear towards the existing culvert located along mid portion of the rear property line towards east. A small portion of the front of the existing building drains towards Dixie Road. Existing topographic survey is attached for reference.

2.0 STORMWATER MANAGEMENT ANALYSIS

2.1. PRE-DEVELOPMENT & POST-DEVELOPMENT RUNOFF VOLUME CALCULATIONS

Pre-development and post-development runoff volume have been calculated based on Town of Caledon IDF curves.

Design Storm –100-Year- 3 Hour Chicago Storm

100 -Year- IDF CURVE DATA (Town of Caledon)

$$I = A/(t + B)^c$$

I = Intensity (mm/hr)

A= 4688.00

B= 17.00

c= 0.9624

Refer to the attached SWMHYMO files for rainfall depth of 87.03mm for 100-Year storm event.

Following are the calculations for pre-development and post-development runoff volumes for the proposed parking extension based on 100-year storm event.

2.2. PRE-DEVELOPMENT RUNOFF VOLUME: (AS PER EXISTING CONDITONS)

Weighted Average Runoff Coefficient (C) (Pre-Development Conditions)

AREA -1

Existing Building/Concrete/Asphalt Impervious Area= 462.57 m²

Existing Grass Area= 642.48 m²

Total Area= 1105.05 m²

Weighted Ave. C=[(462.57 m² x 0.90)+ (642.48 m² x 0.25)]/(1105.05m²)

Weighted Ave. C= 0.52

D= 87.03mm (100-year storm rainfall depth)

PRE-DEVELOPMENT RUNOFF VOLUME ⇔ AxCxD= 1105.05m²x0.52x87.03mm-----50.01m³

Weighted Average Runoff Coefficient (C) (Pre-Development Conditions)

AREA -2

Existing Building/Concrete/Asphalt Impervious Area = 427.42 m²

Existing Grass Area= 6023.93 m²

Total Area= 6451.35 m²

Weighted Ave. C=[(427.42 m² x0.90 + 6023.93 m² x 0.25)]/(6451.35m²)

Weighted Ave. C= 0.29

D= 87.03mm (100-year storm rainfall depth)

PRE-DEVELOPMENT RUNOFF VOLUME ⇔ $A \times C \times D = 6451.35 \text{ m}^2 \times 0.29 \times 87.03 \text{ mm} \text{-----} 162.82 \text{ m}^3$

2.3. POST-DEVELOPMENT RUNOFF VOLUME:(AS PER PROPOSED GRADING)

Weighted Average Runoff Coefficient (C) (Post-Development Conditions)

AREA -1

Proposed/Existing Impervious Area= 573.38m²

Proposed Grass Area: 328.74 m²

Total Area= 902.12 m²

Weighted Ave.

$C = [(573.38 \text{ m}^2 \times 0.90) + (328.74 \text{ m}^2 \times 0.25)] / (902.12 \text{ m}^2)$

Weighted Ave. C= 0.66

D= 87.03mm (100-year storm rainfall depth)

POST-DEVELOPMENT RUNOFF VOLUME ⇔ $A \times C \times D = 902.12 \text{ m}^2 \times 0.66 \times 87.03 \text{ mm} \text{-----} 51.82 \text{ m}^3$

Weighted Average Runoff Coefficient (C) (Post-Development Conditions)

AREA -2

Proposed/Existing Impervious Area= 730.72m²

Proposed Gravel Area= 3115.41m²

Proposed Grass Area: 2808.15 m²

Total Area= 6654.28 m²

Weighted Ave.

$C = [(730.72 \text{ m}^2 \times 0.90) + (3115.41 \text{ m}^2 \times 0.70) + (2808.15 \text{ m}^2 \times 0.25)] / (6654.28 \text{ m}^2)$

Weighted Ave. C= 0.53

D= 87.03mm (100-year storm rainfall depth)

POST-DEVELOPMENT RUNOFF VOLUME ⇔ $A \times C \times D = 6654.28 \text{ m}^2 \times 0.53 \times 87.03 \text{ mm} \text{-----} 306.93 \text{ m}^3$

2.4. REQUIRED RUNOFF VOLUME

$$\begin{aligned}\text{REQUIRED VOLUME (AREA-1)} &= \text{POST-DEV. RUNOFF VOLUME} - \text{PRE-DEVE. RUNOFF VOLUME} \\ &= 51.82 \text{ m}^3 - 50.01 \text{ m}^3 \\ &= 1.81 \text{ m}^3\end{aligned}$$

The required volume is insignificant or post-development conditions are almost equivalent to the pre-development conditions, it has been noted that the post-development conditions will not impact the runoff volume as compared to the pre-development conditions in Area 1. All imperviousness in Area1 ultimately drains to the grass area which will infiltrate into the ground; therefore, no storage system is required in Area 1.

$$\begin{aligned}\text{REQUIRED VOLUME (AREA-2)} &= \text{POST-DEV. RUNOFF VOLUME} - \text{PRE-DEVE. RUNOFF VOLUME} \\ &= 306.93 \text{ m}^3 - 162.82 \text{ m}^3 \\ &= 144.11 \text{ m}^3\end{aligned}$$

2.5. PROPOSED INFILTRATION SYSTEM DESIGN

Gravel parking area has been proposed in replacement of the grass area to promote runoff to infiltrate into the ground similar to the existing grass area. The proposed gravel area infiltration system has been designed based on the required volume. The depth of infiltration system has been calculated as per MECP Manual Equation 4.2 as mentioned below:

$$d = PT/1000$$

d= Maximum allowable depth of the infiltration system (m)

P = Percolation Rate (mm/hr)

T= Drawdown Time (24 – 48 hrs) (hr.)

According to the Ministry of Northern Development, Mines, Natural Resources and Forestry geotechnical boreholes records, till/silty clay was found around the development area. It has been proposed to provide gravel parking area and provide 50mm clear stone layer under the gravel parking to promote slow infiltration in the ground for the additional runoff generated. The infiltration rate of 5mm/hr. has been assumed to design the infiltration system. Drawdown time of 48 hours has been used to calculate the depth of infiltration system as follows:

Depth of the proposed infiltration system (d) = $PT / 1000 = (5\text{mm/hr} \times 48 \text{ hrs}) / 1000 = 0.24\text{m}$
~0.30m

Figure 1 represents pre-development drainage area plan. **Figure 2** represents post-development drainage area plan including the proposed details for the 50mm clear stone under the gravel parking area.

REQUIRED STORAGE VOLUME AREA-2:

144.11 m³ (Gross post-development storm runoff 306.93 m³)

PROVIDED STORAGE VOLUME:

= DEPTH (m) x AREA (m²) x 40% (50mm CLEAR STONE VOIDS VOLUME)

= 0.30m x 3115.41m² x 40%

= 373.85 m³

PROVIDED STORAGE > REQUIRED STORAGE

Provided storage is 373.85m³ which is greater than the effective storage of 144.11m³ and also greater than the gross post-development storm storage of 306.93m³.

It has been proposed to provide 300mm depth of 50mm clear stone under the entire proposed gravel parking extension. Refer to **Figure 1** for detail “A” of the 50mm clear stone under the gravel parking area.

The proposed grading has been designed to follow the existing drainage pattern. It has been proposed to provide gravel with 50mm clear stone to match post-development runoff coefficient to pre-development conditions, also the provided storage is well above the required storage, therefore, the proposed development will not impact the existing storm drainage pattern.

It should be noted that the existing drainage from the subject site will remain undisturbed, however, additional runoff will be captured into the proposed 50mm clear stone and ultimately slowly infiltrate into the ground.

If you have any questions on this matter, please contact the undersigned.

Respectfully Submitted By:

ARIK ENGINEERING LTD.



Abdul Razzak, MEng., P.Eng.


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SSSSS W W M M H H Y Y M M 000 999 999 =====
S W W W MM MM H H Y Y MM MM 0 0 9 9 9 9
SSSSS W W W M M M HHHH Y M M M 0 0 ## 9 9 9 9 Ver 4.05
S W W M M H H Y M M 0 0 9999 9999 Sept 2011
SSSSS W W M M H H Y M M 000 9 9 =====
9 9 9 9 # 3124689
StormWater Management HYdrologic Model 999 999 =====
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*****
***** SWMHYMO Ver/4.05 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** OTTHYMO-83 and OTTHYMO-89. *****
*****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 836-3884 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhymo@jfsa.Com *****
*****
```

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+++++
+++++ Licensed user: ARIK ENGINEERING LTD +++++
+++++ Hannon SERIAL#:3124689 +++++
+++++
```

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*****
***** +++++ PROGRAM ARRAY DIMENSIONS +++++ *****
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 105408 *****
***** Max. number of flow points : 105408 *****
*****
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***** D E T A I L E D O U T P U T *****
*****
* DATE: 2025-02-17 TIME: 12:32:14 RUN COUNTER: 001264 *
*****
* Input filename: C:\SWMHYMO\12189DIX\12189DIX.DAT *
* Output filename: C:\SWMHYMO\12189DIX\12189DIX.out *
* Summary filename: C:\SWMHYMO\12189DIX\12189DIX.sum *
* User comments: *
* 1: _____ *
* 2: _____ *
* 3: _____ *
*****
```

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001:0001-----

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*#*****

*# Project Name: 12189-0 DIXIE ROAD, TOWN OF CALEDON

*# Project Number: 25109

*# Date : FEBRUARY 17, 2025

*# Modeller : ABDUL RAZZAK

*# Company : ARIK ENGINEERING LTD.

*# License # : 3124689

*#*****

| START | Project dir.: C:\SWMHYMO\12189DIX\

----- Rainfall dir.: C:\SWMHYMO\12189DIX\

TZERO = .00 hrs on 0

METOUT= 2 (output = METRIC)

NRUN = 001

NSTORM= 0

--

001:0002-----

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*+++++

*=====TOWN OF CALEDON IDF CURVES=====

*=====100 YEAR 3HR CHICAGO STORM=====

*+++++

*

*

*

| CHICAGO STORM | IDF curve parameters: A=4688.000

| Ptotal= 87.03 mm | B= 17.000

C= .962

used in: INTENSITY = A / (t + B)^C

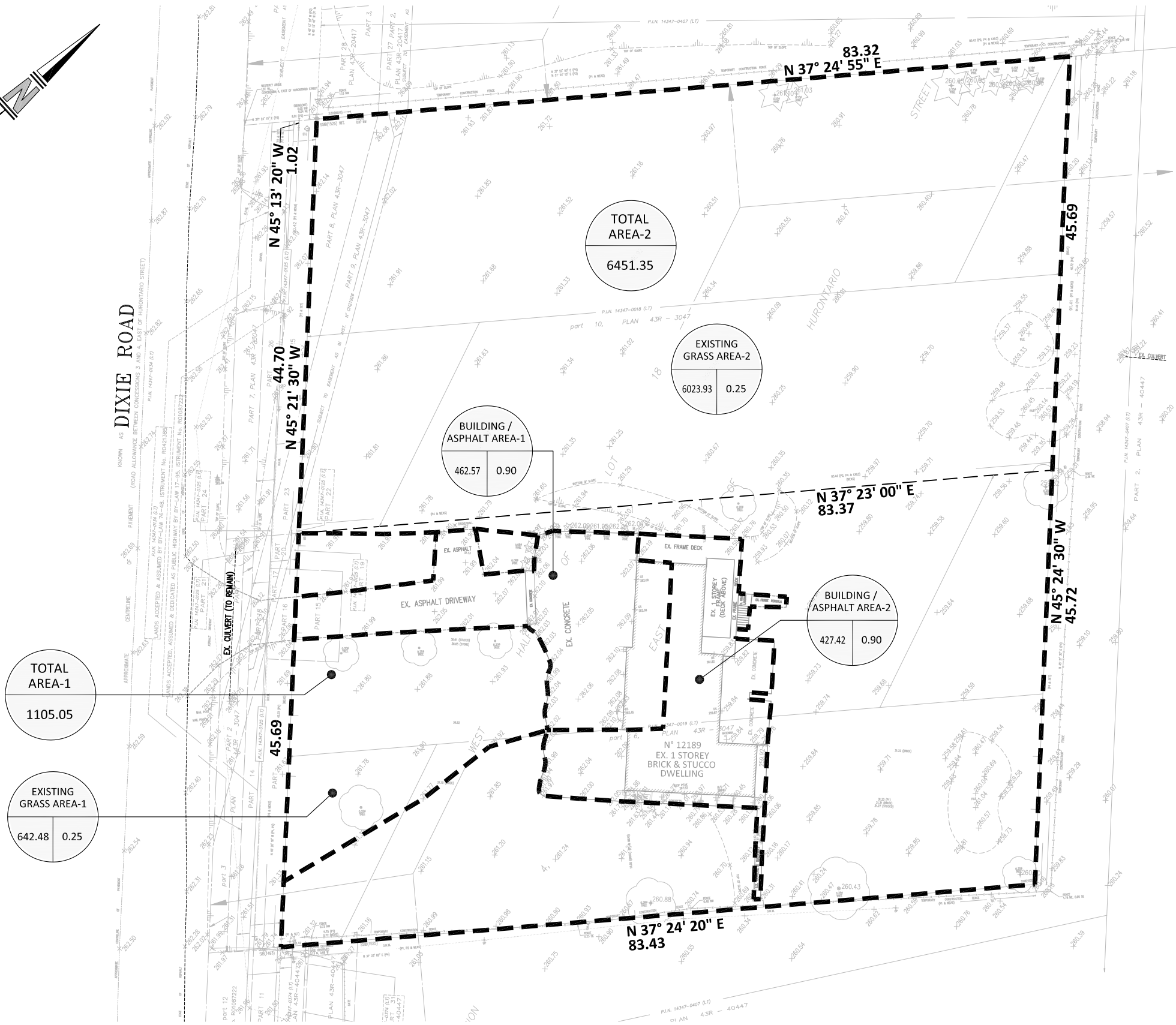
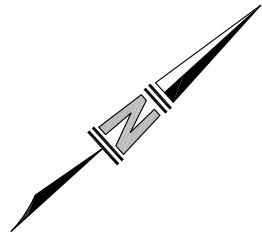
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Storm time step = 10.00 min

Time to peak ratio = .33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.17	4.882	1.00	196.536	1.83	12.479	2.67	4.509
.33	6.958	1.17	83.092	2.00	9.597	2.83	3.912
.50	11.016	1.33	41.245	2.17	7.658	3.00	3.436
.67	21.032	1.50	25.073	2.33	6.286		
.83	62.122	1.67	17.061	2.50	5.276		

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001:0003-----
--
      FINISH
-----
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*****
**
      WARNINGS / ERRORS / NOTES
      -----
      Simulation ended on 2025-02-17      at 12:32:14
=====
==
```



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LEGEND

- PRE-DEVELOPMENT DRAINAGE AREA
- DRAINAGE AREA I.D
- RUNOFF COEFFICIENT
- AREA IN m²

PROJECT:

12189 - 0 DIXIE ROAD
TOWN OF CALEDON

FIGURE -1

PRE-DEVELOPMENT DRAINAGE
AREA PLAN

DATE:

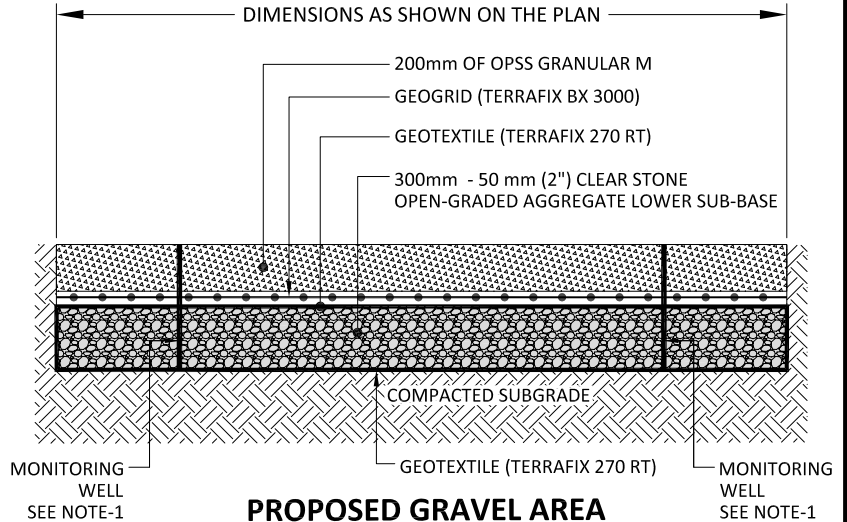
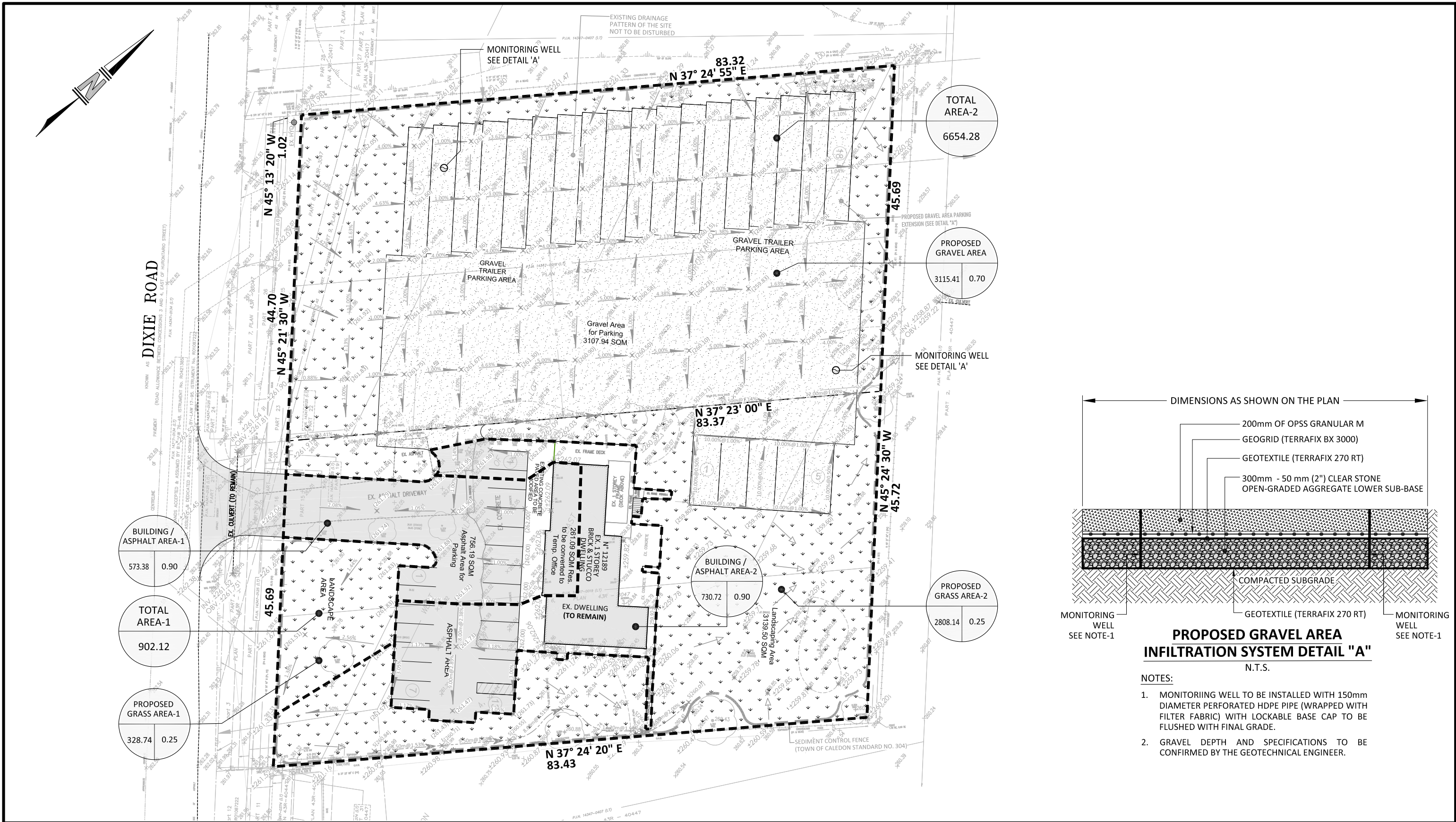
MARCH 05, 2025

SCALE:

1:500

PROJECT NO.

25109



PROPOSED GRAVEL AREA INFILTRATION SYSTEM DETAIL "A"

N.T.S.

NOTES:

1. MONITORING WELL TO BE INSTALLED WITH 150mm DIAMETER PERFORATED HDPE PIPE (WRAPPED WITH FILTER FABRIC) WITH LOCKABLE BASE CAP TO BE FLUSHED WITH FINAL GRADE.
2. GRAVEL DEPTH AND SPECIFICATIONS TO BE CONFIRMED BY THE GEOTECHNICAL ENGINEER.



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LEGEND

- STORM DRAINAGE AREA
- AREA
- 328.74 0.25
- DRAINAGE AREA I.D
- RUNOFF COEFFICIENT
- AREA IN m²

PROJECT:

12189 - 0 DIXIE ROAD
TOWN OF CALEDON

FIGURE -2

POST-DEVELOPMENT DRAINAGE
AREA PLAN

DATE:

MARCH 05, 2025

SCALE:

1:500

PROJECT NO.

25109