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**FUNCTIONAL SERVICING AND
PRELIMINARY STORMWATER MANAGEMENT
REPORT**

**10249 HUNSDEN SIDEROAD
ESTATE RESIDENTIAL DEVELOPMENT**

TOWN OF CALEDON

PREPARED FOR:

CARRINGWOOD HOMES

PREPARED BY:

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1.0 Introduction

C.F. Crozier & Associates Inc. (Crozier) was retained by Carringwood Homes (Owner) to prepare a Functional Servicing and Preliminary Stormwater Management Report in support of the Zoning By-Law Amendment Application for the estate residential development located at 10249 Hunsden Sideroad (the site) in the Town of Caledon. The purpose of this report is to demonstrate that the proposed development is feasible from a functional servicing and stormwater management perspective and conforms with the requirements of the Town of Caledon (Town), Region of Peel (Region), and the Nottawasaga Valley Conservation Authority (Conservation Authority).

This report has been completed in accordance with the guidelines and Development Application Review Team meeting notes dated October 21, 2021. The relevant background studies and reports include:

- Region of Peel 2020 Water Master Plan
- Region of Peel Public Works Design Criteria Manual – Sanitary Sewer (March 2017)
- Region of Peel Watermain Design Criteria (June 2010)
- Town of Caledon As-Constructed Drawings (Drawing No. 402 & 403) (August 2017)
- Geotechnical Investigation prepared by Soil Engineers Ltd. (April 2022)
- Ministry of Environment Stormwater Management Planning and Design Manual (March 2003)
- Ministry of Transportation Drainage Management Manual (1997)
- Town of Caledon Development Application Review Team Meeting Notes (October 21, 2021)

This report has been prepared to support the first submission of the Zoning By-Law Amendment Application for the proposed estate residential development.

2.0 Site Description

The property encompasses an area of 21.60 ha with a developable area of approximately 9.63 ha. The site currently consists of an existing detached residential building and accessory buildings, vacant grassed agricultural fields, and forested areas. The site, located in an agricultural area within the Oak Ridges Moraine in the Town of Caledon, is bounded by Hunsden Sideroad to the north, natural heritage woodlot to the south, agricultural lands to the east, and detached residential dwellings to the west.

According to the Draft Plan of Subdivision prepared by Glen Schnarr & Associates Inc. dated September 16, 2021, it is understood that the proposed estate residential development will consist of the following elements:

- Nineteen (19) single detached residential lots with associated on-site sewage systems (8.14 ha).

- Internal 18.0 m municipal right-of-way with access to Hunsden Sideroad and the proposed residential development (Stinson Street) west of the site (1.04 ha).
- Designated Natural Heritage System Lands and 20.0 m Natural Heritage System buffer (11.97 ha).
- Site access from Hunsden Sideroad and Stinson Street.

The existing residential dwelling located at 10249 Hunsden Sideroad is to remain unchanged upon final buildout of the development.

3.0 Water Servicing

The Region of Peel is responsible for the operation and maintenance of the public watermain system surrounding the property. The existing and proposed water servicing are discussed in the following sections.

3.1 Existing Water Servicing

The existing water servicing infrastructure close to the site include:

- A 300 mm diameter polyvinyl chloride (PVC) watermain located on the east side of Mount Pleasant Road (Region of Peel As-Constructed Drawing (61334-D), October 2016).
- A 300 mm diameter PVC watermain located on the west side of Stinson Street (Flato Palgrave Mansions Inc. As-Constructed Drawing (Sheet 70321-D), August 2017).
- One (1) municipal hydrant located west of the site at the northern extent of Stinson Street (Flato Palgrave Mansions Inc. As-Constructed Drawing (Sheet 70321-D), August 2017).

The existing residential dwelling at 10249 Hunsden Sideroad is assumed to be serviced by a private well based on the Ministry of Environment, Conservation, and Parks Well Mapping Records. The existing well will remain in commission to service 10249 Hunsden Sideroad. The as-constructed drawings for Stinson Street can be referenced in Appendix A.

3.2 Water Demand Calculations

The water demand for the proposed residential development was calculated with reference to the Region of Peel 2020 Water Master Plan and the Region of Peel Public Works Design Criteria Manual – Sanitary Sewer (dated March 2017). The Region of Peel design criteria requires an average daily water demand of 270 L/capita/day for residential uses. A unit-based population density of 6.0 persons per unit based on similar developments in the Town of Caledon, was used along with the peaking factors outlined in the Region of Peel design criteria to obtain the estimated maximum daily demand and peak hourly demand for the proposed development.

Table 1 summarizes the overall water demand for the site. Appendix B contains the detailed water demand calculations.

Table 1: Proposed Water Demand

Standard	Type	Average Daily Water Demand (L/s)	Maximum Daily Water Demand (L/s)	Peak Hourly Water Demand (L/s)
Region of Peel	Residential	0.36	0.64	1.07

Note: References to design guidelines are provided in Appendix B

Using the Region of Peel design criteria for domestic water demand, the estimated average daily demand and peak hourly demand for the proposed development are 0.36 L/s and 1.07 L/s, respectively.

3.3 Fire Flow Calculations

The Fire Underwriters Survey (FUS) method was used to estimate the preliminary fire flow requirements for the proposed residential development. This calculation is based on the building type assumption of wood frame construction. The estimated fire flow requirements are used to estimate the preliminary watermain size required to service the development. The building architect and Mechanical Engineer will confirm the required fire flow demand during the Site Plan Approval and Building Permit stage.

Table 2 summarizes the estimated fire flow demand and duration necessary to meet fire protection for the proposed development. Appendix B contains the Fire Underwriters Survey calculations.

Table 2: Proposed Fire Flow Demand

Method	GFA (m ²)	Fire Flow (L/s)	Duration (hrs.)
Fire Underwriters Survey	347.6	133.3	2.0

Based on the fire flow calculations and a gross floor area of 347.6 m² (Lot 11), the required fire flow for the development was calculated to be 133.3 L/s for a duration of 2.0 hours.

It should be noted that the fire flows determined from the FUS method is a conservative estimate for comparison purposes only. The Mechanical Engineer for the development will complete the required analysis for fire protection and the Architect will design fire separation methods per the determined fire flow rate to meet municipally available flows and pressures. Based on the estimated peak hourly water demand (1.07 L/s) and fire flow demand (133.3 L/s) summarized in Table 1 and Table 2, the total design flow for the internal water distribution system is approximately 134.4 L/s.

Hydrant flow tests may need to be completed as part of the design process to determine the existing available pressures and flows within the Stinson Street watermain. These results will be used to confirm that the existing system has capacity to service the proposed development.

3.4 Proposed Water Servicing

A 150 mm diameter looped watermain is proposed to service the development. The looped watermain is located within the municipal road right-of-way and will connect to the existing 300 mm PVC watermain along Stinson Street, southwest of the site. All residential lots will be serviced with domestic water services connecting to the proposed internal watermain. The Preliminary Grading and Servicing Plan (Drawing C102) illustrates the location and design of the proposed watermain and water services.

As shown on the Preliminary Site Grading and Servicing Plan (Drawing C102) the proposed 150 mm PVC watermain will be extended along Hunsden Sideroad to provide municipal water to Lot 19. A flushing hydrant is proposed at Lot 19 to ensure water does not become stagnant in the watermain.

Private hydrants are proposed throughout the development with a maximum spacing of 150 m in accordance with Region of Peel Watermain Design Criteria (June 2010). A hydrant flow test may be required to confirm the available water flow and pressure within the Stinson Street watermain to service the proposed development.

4.0 Sanitary Servicing

The Site is in a rural area that does not currently have sanitary services available, and the surrounding properties are serviced via private septic systems. The Town of Caledon does not have plans to provide sanitary servicing in this area soon.

4.1 Sanitary Design Calculations

The Ontario Building Code (OBC) was referenced to estimate the sanitary design flows generated by the proposed estate residential development. The proposed development will consist of 19 residential dwellings per the Draft Plan of Subdivision prepared by Glen Schnarr & Associates Inc. (September 2021). A daily unit flow rate of 2,000 L/d day was utilized to determine the total daily design sanitary sewage flows from the proposed development.

Table 3 summarizes the design parameters and estimated design flows for the site.

Table 3: Sanitary Design Parameters and Daily Design Sewage Flow

Zoning/Use	Classification (per OBC 8.2.1.3.B.)	Units	Daily Unit Flow (L/d)
Residential Dwellings	Table 8.2.1.3.A "OBC 2016, Four-bedroom Dwelling"	19	2,000

The daily sanitary design flow for each unit was determined to be 2,000 L/d, per the Ontario Building Code. Details of the design calculations and on-site sewage systems will be confirmed during the building permit stage and complete by others.

4.2 Proposed Sanitary Servicing

All 19 lots located within the development will be serviced with private on-site sewage systems. The details, size, and location of the on-site sewage systems will be determined once individual house designs and building permits are prepared.

The individual lot design and site grading have conservatively allowed an on-site sewage footprint area of 400 m² for a conventional on-site sewage absorption bed and minimum setback requirements, as shown on the Preliminary Site Grading and Servicing Plan (Drawing C102). The size and layout of each on-site sewage system will be completed using actual design criteria during the building permit application phase for each lot to demonstrate that the proper separations are met.

5.0 Drainage Conditions

The drainage conditions for the site in both pre-development and post-development conditions are outlined in the following sections.

5.1 Existing Drainage Conditions

According to the topographic survey (J.D. Barnes Limited, April 4, 2022), the site currently consists of an existing detached residential dwelling and accessory buildings, vacant grassed agricultural fields, and forested areas. The site generally slopes from east to west and drains from back to front.

Most of the stormwater runoff from the site drains towards the Hunsden Sideroad ditch where it is directed to the 1000 mm diameter culvert flowing north below the roadway (Catchment 101 & Catchment 102). Under existing conditions, the catchment areas that are directed towards the Hunsden Sideroad culvert consist of primarily woodlot and cultivated lands. The southwestern portion of the site consists of primarily woodlot and cultivated lands and drains uncontrolled to the neighbouring residential properties to the southwest (Catchment 103) via sheet flow. The ultimate receiver of most of the stormwater from the site is the tributary located approximately 150 meters north of Hunsden Sideroad.

There are two outlets for the major overland flow route based on the existing site topographic survey (J.D. Barnes Limited, April 4, 2022). The main overland flow outlet discharges through the existing 1000 mm diameter corrugated steel culvert which crosses Hunsden Sideroad along the northwestern extent of the property and ultimately outlet to the tributary of Beeton Creek. The secondary overland flow outlet is along the southwestern property limits where water flows uncontrolled towards the existing residential properties. These overland flow outlets are proposed to remain under the post-development conditions.

Table 4 summarizes the pre-development catchment areas and Figure 1 illustrates the Pre-Development Drainage Plan.

Table 4: Pre-Development Catchment Areas and Percent Impervious

Catchment ID	Land-Use Description	Impervious Area (ha)	Pervious Area (ha)	Percent Impervious (%)	Outlet
101	Existing residential dwelling, woodlot, and cultivated lands	0.04	10.93	0.3	Hunsden Sideroad Culvert (Beeton Creek Tributary)
102	Existing cultivated lands and woodlot	-	4.84	0	
103	Existing cultivated lands and woodlot	-	4.57	0	Southwestern residential properties

5.2 Proposed Drainage Conditions

Based on the Draft Plan of Subdivision (Glen Schnarr & Associates Inc., September 16, 2021), the proposed development will consist of nineteen (19) single detached residential lots, associated paved internal roadway, and landscaped and natural heritage areas. The existing residential dwelling located at 10249 Hunsden Sideroad is to remain unchanged upon final buildout of the development. Access to the site will be provided from the proposed entrances on Hunsden Sideroad and Stinson Street.

The proposed site grading divides the site into six (6) post-development drainage catchment areas with two outlets, as shown on the Post-Development Drainage Plan (Figure 2):

- Catchment 201 (A = 12.4 ha) consists of uncontrolled drainage from the proposed building footprints, rear yards, and natural heritage wood lands. All storm events from this catchment are conveyed overland via sheet flow to the 1000 mm CSP culvert on Hunsden Road, mimicking the pre-development drainage conditions.
- Catchment 202 (A = 3.50 ha) consists of drainage from the internal roadway (Street 'A') and proposed residential lots. All storm events from this catchment are conveyed to roadside bioswales prior to being directed to the Hunsden Sideroad ditch and ultimately outletting at the Hunsden Sideroad 1000 mm CSP culvert.
- Catchment 203 (A = 0.07 ha) consists of uncontrolled drainage from landscaped areas along Hunsden Sideroad. All storm events from this catchment are conveyed to the Hunsden Sideroad ditch via sheet flow and ultimately outlet towards the Hunsden Sideroad 1000 mm CSP culvert.
- Catchment 204 (A = 1.39 ha) consists of drainage from the internal roadway (Street 'A' cul-de-sac) and proposed residential front yards. All storm events from this catchment are conveyed to roadside bioswales prior to being directed to the existing drainage swale within the Natural Heritage Block and ultimately outletting at the Hunsden Sideroad 1000 mm CSP culvert.
- Catchment 205 (A = 0.83 ha) consists of drainage from the internal roadway (Street 'B') and proposed residential lots. All storm events from this catchment are conveyed to roadside bioswales prior to being directed to the existing residential development and Stinson Street to the southwest.

- Catchment 206 (A = 2.15 ha) consists of uncontrolled drainage from natural heritage wood lands and landscaped areas. All storm events from this catchment are conveyed via sheet flow to the existing residential development and Stinson Street, southwest of the development, mimicking the pre-development drainage conditions.

Upon development, all storm events from the developable portion of the site (Catchment 202, 204 and 205) will be conveyed to proposed roadside bioswales for quantity and quality control. Following quantity and quality control, all stormwater will either infiltrate or be conveyed to the proposed drainage outlets which include the Hunsden Sideroad 1000 mm CSP culvert and the existing residential development and Stinson Street to the southwest. Details of the quantity, quality, and bioswale design will be further outlined in Section 6.0 of the report.

Table 5 provides details of the catchment areas and runoff coefficients for the post-development conditions.

Table 5: Post-Development Catchment Areas and Percent Impervious

Catchment ID	Description	Impervious Area (ha)	Pervious Area (ha)	Percent Impervious (%)	Outlet
201	Building footprints, rear yards, woodlot	0.29	12.15	2.3	Hunsden Sideroad Culvert (Beeton Creek Tributary)
202	Internal roadway and residential lots	0.46	3.04	13.1	
203	Landscaped area	-	0.07	0	
204	Internal roadway and front yards	0.28	1.11	20.0	
205	Internal roadway and residential lots	0.11	0.72	13.3	Neighbouring Residential Properties (Southwest)
206	Woodlot and landscaped areas	-	2.15	0	

Refer to the Post-Development Drainage Plan (Figure 2) for proposed drainage conditions and the Preliminary Site Grading and Servicing Plan (Drawing C102) that illustrates the proposed site drainage and servicing.

6.0 Stormwater Management

Stormwater management and site drainage for the proposed development must adhere to the policies and standards of the Town of Caledon, Nottawasaga Valley Conservation Authority, and Ministry of Environment, Conservation and Parks (MECP). It is important to note that efforts have been made to preserve and maintain the rural character of the property and passive stormwater management practices have been incorporated throughout the design.

The stormwater management criteria for the development have been summarized below:

Water Quantity Control

According to the Town of Caledon Development Standards Manual (2019), water quantity controls are required for the site. The water quantity requirements include controlling the post-development peak flow event to the pre-development peak flow event for storms up to and including the 100-year event.

Water Quality Control

Provide at least 80% removal of Total Suspended Solids in accordance with “Enhanced Protection” (Ministry of the Environment, Planning, and Stormwater Management Manual, 2003)

6.1 Stormwater Quantity Control

The Nottawasaga Valley Conservation Authority, Town of Caledon, and Ministry of Transportation guidelines were referenced to determine the hydrologic parameters for the various catchment areas within the site. The topographic survey (J.D. Barnes Limited, April 4, 2022) for the site was referenced to confirm the land cover and drainage patterns under the existing site conditions. The Geotechnical Investigation prepared by Soil Engineers Ltd. (April 2022) was reviewed to determine the on-site soil conditions.

Based on the above, the hydrologic parameters for the pre-development and post-development conditions were determined and are summarized in Tables 6 and Table 7 below. The detailed hydrologic parameter sheets for each catchment area are included in Appendix C.

Table 6: Pre-Development Hydrologic Parameters

Catchment Description	101	102	103
Drainage Area (ha)	10.97	4.84	4.57
Total Imperviousness (%)	0.23	0	0
Curve Number (CN) ¹	56.1	57.8	57.0
Initial Abstraction (mm)	8.99	7.25	8.00
Time to peak (hrs)	0.38	0.27	0.32

1. Curve number presented as utilized in VO modeling. CN reflects composite curve number for rural catchments modeled using NASHYD routine and curve number for pervious areas only for urban catchments using STANDHYD routine.

Table 7: Post-Development Hydrologic Parameters

Catchment Description	201	202	203	204	205	206
Drainage Area (ha)	12.44	3.50	0.07	1.39	0.83	2.15
Total Imperviousness (%)	2.34	13.08	0	20.00	13.28	0
Curve Number (CN) ¹	58.1	65.8	61.0	61.0	65.9	58.4
Initial Abstraction (mm)	8.04	4.61	5.00	5.00	4.60	7.15
Time to peak (hrs)	0.39	0.18	0.10	-	0.14	0.12

1. Curve number presented as utilized in VO modeling. CN reflects composite curve number for rural catchments modeled using NASHYD routine and curve number for pervious areas only for urban catchments using STANDHYD routine.

As discussed in Section 6.0, stormwater quantity control requirements for the site include controlling the post-development peak flow to the pre-development peak flow event for storms up to and including the 100-year event.

Hunsden Sideroad Culvert Drainage Outlet (Beeton Creek Tributary)

Visual OTTHYMO (VO) was used to create pre-development, post-development, and post-development with mitigation model scenarios for the hydrology of the existing and proposed site drainage based on the Town of Caledon intensity-duration-frequency (IDF) data and hydrologic parameters outlined in Table 6 and 7. The pre-development and post-development flow rates for the outflows directed to the Hunsden Sideroad Culvert (Catchment 201, 202, 203 & 204) and the storage requirements are summarized below in Table 8. The VO model schematics, full modelling results, and output files are included in Appendix C.

Table 8: Peak Flows and Target Flows Summary (Discharge towards Hunsden Sideroad Culvert)

Storm	Pre-Dev. Peak Flow Rate ¹ (L/s)	Post-Dev. Uncontrolled Peak Flow Rate ² (L/s)	Post-Dev. Controlled Peak Flow Rate ² (L/s)	Storage Volume Required (m ³)	Storage Volume Provided (m ³)
2-yr	66	103	57	225	727
5-yr	148	216	123	432	
10-yr	218	302	178	596	
25-yr	321	432	258	701	
50-yr	411	542	334	727	
100-yr	506	658	484	727	

1. Includes runoff from Catchment 101 and 102.
2. Includes runoff from Catchment 201, 202, 203, and 204.

The Visual OTTHYMO results summarized in Table 8 indicate that water quantity controls are required to control the post-development peak flows to the pre-development peak flows for storm events up to and including the 100-year event. A total storage volume of 727 m³ is provided using bioswales along the internal roadways to meet the required storage volume.

The proposed bioswales have been sized to provide stormwater quantity controls for events up to and including the 100-year event for Catchment 202 and 204. The bioswales will be comprised of a 0.3 m deep filter media layer and 1.2 m deep gravel storage layer. Details of the bioswale design and sizing can be referenced on the Preliminary Site Grading and Servicing Plan (Drawing C102) and Appendix C.

Catchments 201 and 203 are to remain relatively unchanged under post development conditions and will continue to drain uncontrolled to the Hunsden Sideroad culvert; therefore, quantity controls have not been provided for these catchments.

Southwest Property Drainage Outlet

The catchments that are directed towards the southwest drainage outlet include Catchment 205 and 206 which consist of residential lots, internal roadway, and landscape runoff from the southwestern extents of the development. Stormwater runoff from Catchment 206 will continue to drain uncontrolled to the neighbouring residential properties consistent with the pre-development runoff conditions. Visual OTTHYMO was used to determine the pre-development and post-development flows directed to the neighbouring property to determine the required stormwater management controls for Catchment 205.

The pre-development and post-development flow rates for the outflows directed to the neighbouring residential properties (Catchments 205 & 206) and the storage requirements are summarized below in Table 9. The VO model schematics, full modelling results, and output files are included in Appendix C.

Table 9: Peak Flows and Target Flows Summary (Discharge towards Southwest Properties)

Storm	Pre-Dev. Peak Flow Rate ¹ (L/s)	Post-Dev. Uncontrolled Peak Flow Rate ² (L/s)	Post-Dev. Controlled Peak Flow Rate ² (L/s)	Storage Volume Required (m ³)	Storage Volume Provided (m ³)
2-yr	21	32	20	34	156
5-yr	47	68	45	68	
10-yr	69	97	63	96	
25-yr	102	139	91	133	
50-yr	130	175	115	156	
100-yr	160	212	141	156	

1. Includes runoff from Catchment 103.

2. Includes runoff from Catchment 205 and 206.

As per the Visual OTTHYMO results summarized in Table 9, water quantity controls are required to control the post-development peak flows to the pre-development peak flows for storm events up to and including the 100-year event. A total storage volume of 156 m³ of is provided using bioswales along the internal roadways to meet the required storage volume.

The proposed bioswales have been sized to provide stormwater quantity controls for events up to and including the 100-year event. The bioswales will be comprised of a 0.3 m deep filter media layer and 1.2 m deep gravel storage layer. Details of the bioswale design and sizing can be referenced on the Preliminary Site Grading and Servicing Plan (Drawing 102) and Appendix C.

Catchment 206 will remain relatively unchanged under post development conditions and will continue to drain uncontrolled to the neighbouring residential properties; therefore, quantity controls have not been provided for this catchment.

6.2 Stormwater Quality Control

Stormwater quality controls for the site must incorporate measures to provide “enhanced protection” as outlined by the Nottawasaga Valley Conservation Authority. Enhanced water quality protection involves the removal of at least 80% of the total suspended solids (TSS) from 90% of the annual runoff volume.

Water quality controls for Catchment 202, 204, and 205 will be provided using a combination of grassed swales and roadside bioswales complete with filter media. Stormwater runoff from the developable portion of the site will be directed to proposed side yard swales prior to the runoff being directed to the roadside bioswales. The bioswales and grassed swales will act in a treatment train approach to remove the total suspended solids from the stormwater runoff.

Catchments 201, 203, and 206 will remain relatively unchanged between pre-development and post-development conditions with no hard surfaces, producing only clean runoff (i.e., landscaped and woodlot areas). Therefore, quality controls have not been provided for these catchments.

7.0 Erosion and Sediment Controls During Construction

Erosion and sediment controls will be implemented prior to the commencement of any site servicing works for the development and will be maintained throughout construction until the site is stabilized or as directed by the Site Engineer and/or Town of Caledon.

Controls will be inspected after each significant rainfall event and maintained in proper working condition. A Preliminary Erosion and Sediment Control Plan (Drawing C101) has been prepared for the development outlining the site-specific erosion and sediment controls. This plan includes silt fencing, a mud mat, and more robust measures, such as check dams, in areas of concentrated flow.

Further details on the erosion and control measures have been summarized below:

Sediment Control Silt Fence

Sediment Control Silt Fence will be installed on the perimeter of the site to intercept sheet flow. Additional Sediment Control Silt Fence may be added based on field decisions by the Site Engineer and Owner prior to, during, and following construction.

Mud Mat

A rock mud mat will be installed at the entrance to the site off Hunsden Sideroad. The rock mud mat will help to prevent mud tracking. All construction traffic will be restricted to the construction entrance as indicated on the Preliminary Erosion and Sediment Control Plan (Drawing C101).

Rock Check Dams

Rock check dams installed according to OPSD 219.210 should be installed in the proposed swale to protect from erosion conveyance during construction.

8.0 Conclusions & Recommendations

This report was prepared in support of the Zoning By-Law Amendment Application for the property located at 10249 Hunsden Sideroad in the Town of Caledon. The proposed development can be serviced for water, sanitary, and stormwater management in accordance with the Town of Caledon Region of Peel, and Nottawasaga Valley Conservation Authority requirements and standards. Our conclusions and recommendations include:

Proposed Water Services

1. The domestic peak hourly water demand for the proposed development is 1.07 L/s. The design fire flow is 133.3 L/s for 2.0 hours.
2. Water servicing for the proposed development will be met by connecting a 150 mm diameter PVC watermain to the existing 300 mm diameter watermain on Stinson Street. The proposed 150 mm diameter PVC watermain will be looped throughout the development and provide municipal water servicing to each residential lot.

Proposed Sanitary Services

1. Total peak sanitary flow for the proposed development is 38,000 L/d.
2. Sanitary servicing for the proposed development will consist of private individual lot on-site sewage systems.

Stormwater Management

1. A passive stormwater management approach is proposed to preserve and maintain the rural character of the property.
2. The site's stormwater runoff from the developable area (Catchment 202, 204, and 205) will be collected in the proposed roadside bioswales for events up to and including the 100-year storm event. The proposed bioswales will control the post-development runoff event to the pre-development runoff event prior to infiltrating or outletting to their respective outlet. Stormwater runoff the undeveloped catchments (Catchment 201, 203, and 206) of the site will flow uncontrolled towards to their respective outlet.
3. Stormwater quantity controls are required to control the post-development peak flow to the pre-development peak flow event for storms up to and including the 100-year event. Roadside bioswales are proposed to provide the required stormwater quantity controls. Storm events larger than the 100-year event will flow uncontrolled to the Hunsden Sideroad culvert and the residential properties to the southwest.
4. Stormwater quality controls for the site will be provided by the proposed side yard swales and roadside bioswales through a treatment train approach.

Based on the above conclusions, we recommend the approval of the Zoning By-Law Amendment Application from the perspective of functional servicing and preliminary stormwater management.

Respectfully submitted,

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APPENDIX A

As-Constructed Drawings & Background Material

APPENDIX B

Water Servicing Calculations

Domestic Water Demand

Total Site Area:	21.6	ha
Developable Site Area:	9.63	ha
Population Density:	50	persons/ha
Number of units:	19	
Unit Population Density:	6	persons/unit
Population	114	persons (unit based)

Design Parameters

Average Demand (L/capita/d)
270

Water Demand:

Average Daily Demand = 30,780 L/day
0.36 L/s

Peaking Factors

Max Day = 1.8
 Peak Hour = 3.0

Average Day = 0.36 L/s
 Max Day = **0.64** L/s
 Peak Hour = **1.07** L/s

Municipality	Average Daily Water Demand (L/s)	Max Day Demand (L/s)	Peak Hourly Demand (L/s)
Region of Peel	0.36	0.64	1.07

Notes & References

Population Density from Section 2.1, Region of Peel Public Works Design Criteria Manual - Sanitary Sewer (dated March 2017)
 Unit counts per concept plan prepared by Glen Schnarr & Associates Inc. dated September 16, 2021
 Population Density per unit assumed based on size of houses and past jobs of similar subdivision design.

Region of Peel 2020 Water Master Plan, Section 2.2 - Design Criteria – Demands Projections

Region of Peel 2020 Water Master Plan, Section 2.2 - Design Criteria – Demands Projections

Max Day = Average Day Demand * Max Day
 Peak Hour = Average Day Demand * Peak Hour

Water Supply for Public Fire Protection - 1999
Fire Underwriters Survey

Part II - Guide for Determination of Required Fire Flow

1. An estimate of fire flow required for a given area may be determined by the formula:

$$F = 220 * C * \text{sqrt } A$$

where

- F = the required fire flow in litres per minute
- C = coefficient related to the type of construction
 - = 1.5 for wood frame construction (structure essentially all combustible)
 - = 1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior)
 - = 0.8 for non-combustible construction (unprotected metal structural components)
 - = 0.6 for fire-resistive construction (fully protected frame, floors, roof)
- A = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building considered.

Proposed Building

1.5 C
 347.6 sq.m. total floor area

Total Floor Area for the largest unit based on Site Plan prepared by Glen Schnarr & Associates Inc., dated September 16, 2021.

Therefore F= 6,200 L/min (rounded to nearest 1000 L/min)
Used F based on criteria below= 6,200 L/min

- Fire flow determined above shall not exceed:
- 30,000 L/min for wood frame construction
 - 30,000 L/min for ordinary construction
 - 25,000 L/min for non-combustible construction
 - 25,000 L/min for fire-resistive construction

2. Values obtained in No. 1 may be reduced by as much as 25% for occupancies having low contents fire hazard or may be increased by up to 25% surcharge for occupancies having a high fire hazard.

Non-Combustible	-25%	Free Burning	15%
Limited Combustible	-15%	Rapid Buring	25%
Combustible	No Charge		

0 L/min reduction

Note: Flow determined shall not be less than 2,000 L/min

3. Sprinklers - The value obtained in No. 2 above maybe reduce by up to 50% for complete automatic sprinkler protection.

0 L/min reduction

Water Supply for Public Fire Protection - 1999
Fire Underwriters Survey

Part II - Guide for Determination of Required Fire Flow

4. Exposure - To the value obtained in No. 2, a percentage should be added for structures exposed within 45 metres by the fire area under consideration. The percentage shall depend upon the height, area, and construction of the building(s) being exposed, the separation, openings in the exposed building(s), the length and height of exposure, the provision of automatic sprinklers and/or outside sprinklers in the building(s) exposed, the occupancy of the exposed building(s) and the effect of hillside locations on the possible spread of fire.

Separation	Charge	Separation	Charge
0 to 3 m	25%	20.1 to 30 m	10%
3.1 to 10 m	20%	30.1 to 45 m	5%
10.1 to 20 m	15%		

Exposed buildings relative to Lot 11 dwelling

Name	Distance (m)			
North	No Buildings within 45 m	0	0%	0
South	Lot 10 proposed residential building	16	15%	930
East	No Buildings within 45 m	0	0%	0
West	Lot 12 proposed residential building	16	15%	930
				1,860 L/min Surcharge

Determine Required Fire Flow

No. 1	6,200		
No. 2	0 reduction		
No. 3	0 reduction		
No. 4	<u>1,860</u> surcharge		
Required Flow:		8,060 L/min	
Rounded to nearest 1000l/min:		8,000 L/min	or 133.3 L/s 2,113 USGPM

Required Duration of Fire Flow

Flow Required L/min	Duration (hours)
2,000 or less	1.0
3,000	1.25
4,000	1.5
5,000	1.75
6,000	2.0
8,000	2.0
10,000	2.0
12,000	2.5
14,000	3.0
16,000	3.5
18,000	4.0
20,000	4.5
22,000	5.0
24,000	5.5
26,000	6.0
28,000	6.5
30,000	7.0
32,000	7.5
34,000	8.0
36,000	8.5
38,000	9.0
40,000 and over	9.5

Determine Required Fire Storage Volume

Flow from above	8,000 L/min
Required duration	2.00 hours
Therefore:	960,000 Litres or 960 cu.m. is the required fire storage volume.

APPENDIX C

Stormwater Servicing Calculations



Project Name: 10249 Hunsden Sideroad
 Project Number: 0952-6305
 Created By: AG/BP
 Reviewed By: TE

D.A. NAME 101
 D.A. AREA 10.97

Hydrologic Parameters: CALIB NASHYD Command
 Pre Development Drainage Area: Catchment 101

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic	% Area	Area
Sandy Silt	B	B	100	10.97
				0
				0
				0
Total Area				10.97

Impervious Landuses Present:												
Soils	Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
B					0.01	98	0.02	98			0.04	3.49
Subtotal											0.01	0.02
Pervious Landuses Present:												
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
B	7.35	55							3.59	58	10.93	612.16
Subtotal											7.35	3.59
					Composite Area Calculations		Total Pervious Area				10.93	
							Total Impervious Area				0.04	
							% Impervious				0.32%	
							Composite Curve Number				56.1	
							Total Area Check				10.97	

Initial Abstraction and Tp Calculations

Landuse	Initial Abstraction			Composite Runoff Coefficient								
	IA (mm)	Area (ha)	A * IA	Sandy Silt		0		0		0		A*RC
				RC	Area	RC	Area	RC	Area	RC	Area	
Woodland	10	7.35	73.47	0.21	7.35		0		0		0	1.54
Meadow	8	0	0		0		0		0		0	0
Wetland	16	0	0		0		0		0		0	0
Lawn	5	0	0		0		0		0		0	0
Cultivated	7	3.59	25.11	0.25	3.59		0		0		0	0.90
Impervious	2	0.04	0.07	0.90	0.04		0		0		0	0.03
Composite			10.97	8.99	Composite Runoff Coefficient							0.23

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp(hr)	TOTAL Tp (hr)	Tc (hr)	Tp(hr)	Tc (hr)	Tp(hr)
Overland	356.3	14.5	4.07%	2.3	0.46	0.21	0.14	0.14	0.20	0.13	0.56	0.38

Appropriate calculated time to peak: 0.38 | Appropriate Method: Airport



Project Name: 10249 Hunsden Sideroad
 Project Number: 0952-6305
 Created By: AG/BP
 Reviewed By: TE

D.A. NAME 102
 D.A. AREA 4.84

Hydrologic Parameters: CALIB NASHYD Command
 Pre Development Drainage Area: Catchment 102

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic	% Area	Area
Sandy Silt	B	B	100	4.84
				0
				0
				0
Total Area				4.84

Impervious Landuses Present:														
Soils	Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals			
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN		
B												0		
Subtotal											0	0		
Pervious Landuses Present:														
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals			
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN		
B	0.40	55							4.44	58	4.84	279.51		
Subtotal											0.40	4.44		
											Composite Area Calculations		Total Pervious Area	4.84
													Total Impervious Area	0
													% Impervious	0.00%
													Composite Curve Number	57.8
													Total Area Check	4.84

Initial Abstraction and Tp Calculations

Landuse	Initial Abstraction			Composite Runoff Coefficient								
	IA (mm)	Area (ha)	A * IA	Sandy Silt		0		0		0		A*RC
				RC	Area	RC	Area	RC	Area	RC	Area	
Woodland	10	0.40	4.02	0.21	0.40		0		0		0	0.08
Meadow	8	0	0		0		0		0		0	0
Wetland	16	0	0		0		0		0		0	0
Lawn	5	0	0		0		0		0		0	0
Cultivated	7	4.44	31.07	0.25	4.44		0		0		0	1.11
Impervious	2	0	0		0		0		0		0	0
Composite		4.84	7.25	Composite Runoff Coefficient								0.25

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp(hr)	TOTAL Tp (hr)	Tc (hr)	Tp(hr)	Tc (hr)	Tp(hr)
Overland	184.1	7.5	4.07%	2.3	0.46	0.11	0.07	0.07	0.11	0.08	0.40	0.27

Appropriate calculated time to peak: 0.27 | Appropriate Method: Airport



Project Name: 10249 Hunsden Sideroad
Project Number: 0952-6305
Created By: AG/BP
Reviewed By: TE

D.A. NAME 103
D.A. AREA 4.57

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment 103

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic	% Area	Area
Sandy Silt	B	B	100	4.57
				0
				0
				0
Total Area				4.57

Impervious Landuses Present:												
Soils	Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
B											0	0
Subtotal											0	0
Pervious Landuses Present:												
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN
B	1.52	55							3.05	58	4.57	260.49
Subtotal											1.52	3.05
										Total Pervious Area		4.57
										Total Impervious Area		0
										% Impervious		0.00%
										Composite Curve Number		57.0
										Total Area Check		4.57

Initial Abstraction and Tp Calculations

Initial Abstraction				Composite Runoff Coefficient								
Landuse	IA (mm)	Area (ha)	A * IA	Sandy Silt		0		0		0		A*RC
				RC	Area	RC	Area	RC	Area			
Woodland	10	1.52	15.23	0.21	1.52	0	0	0	0	0	0	0.32
Meadow	8	0	0		0	0	0	0	0	0	0	0
Wetland	16	0	0		0	0	0	0	0	0	0	0
Lawn	5	0	0		0	0	0	0	0	0	0	0
Cultivated	7	3.05	21.33	0.25	3.05	0	0	0	0	0	0	0.76
Impervious	2	0	0		0	0	0	0	0	0	0	0
Composite		4.57	8.00	Composite Runoff Coefficient								0.24

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp(hr)	TOTAL Tp (hr)	Tc (hr)	Tp(hr)	Tc (hr)	Tp(hr)
Overland	242.9	8.75	3.60%	2.3	0.44	0.15	0.10	0.10	0.15	0.10	0.48	0.32

Appropriate calculated time to peak: 0.32 Appropriate Method: Airport



Project Name: 10249 Hunsden Sideroad
 Project Number: 0952-6305
 Created By: AG/BP
 Reviewed By: TE

D.A. NAME 201
 D.A. AREA 12.44

Hydrologic Parameters: CALIB NASHYD Command
 Pre Development Drainage Area: Catchment 201

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic	% Area	Area
Sandy Silt	B	B	100	12.44
				0
				0
				0
Total Area				12.44

Impervious Landuses Present:														
Soils	Roadway		Sidewalk		Driveway		House		SWMF		Subtotals			
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN		
B					0.01	98	0.28	98			0.29	28.47		
Subtotal											0.01	0.28		
Pervious Landuses Present:														
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals			
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN		
B	7.74	55					4.41	61			12.15	694.70		
Subtotal											7.74	4.41		
											Composite Area Calculations		Total Pervious Area	12.15
													Total Impervious Area	0.29
													% Impervious	2.34%
													Composite Curve Number	58.1
													Total Area Check	12.44

Initial Abstraction and Tp Calculations

Landuse	Initial Abstraction			Composite Runoff Coefficient									
	IA (mm)	Area (ha)	A * IA	Sandy Silt		0		0		0		A*RC	
				RC	Area	RC	Area	RC	Area	RC	Area		
Woodland	10	7.74	77.36	0.21	7.74	0	0	0	0	0	0	1.62	
Meadow	8	0	0		0	0	0	0	0	0	0	0	
Wetland	16	0	0		0	0	0	0	0	0	0	0	
Lawn	5	4.41	22.07	0.12	4.41	0	0	0	0	0	0	0.53	
Cultivated	7	0	0		0	0	0	0	0	0	0	0	
Impervious	2	0.29	0.58	0.90	0.29	0	0	0	0	0	0	0.26	
Composite			12.44	8.04	Composite Runoff Coefficient								0.19

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp(hr)	TOTAL Tp (hr)	Tc (hr)	Tp(hr)	Tc (hr)	Tp(hr)
Overland	356.3	14.5	4.07%	2.3	0.46	0.21	0.14	0.14	0.20	0.13	0.58	0.39

Appropriate calculated time to peak: 0.39 | Appropriate Method: Airport



Project Name: 10249 Hunsden Sideroad
 Project Number: 0952-6305
 Created By: AG/BP
 Reviewed By: TE

D.A. NAME 202
 D.A. AREA 3.50

Hydrologic Parameters: CALIB NASHYD Command
 Pre Development Drainage Area: Catchment 202

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic	% Area	Area
Sandy Silt	B	B	100	3.50
				0
				0
				0
Total Area				3.50

Impervious Landuses Present:													
Soils	Roadway		Sidewalk		Driveway		House		SWMF		Subtotals		
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
B	0.19	98			0.13	98	0.14	98			0.46	44.85	
Subtotal	0.19				0.13		0.14						

Pervious Landuses Present:													
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals		
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
B							3.04	61			3.04	185.58	
Subtotal							3.04						

											Composite Area Calculations		Total Pervious Area	3.04
													Total Impervious Area	0.46
													% Impervious	13.08%
													Composite Curve Number	65.8
													Total Area Check	3.50

Initial Abstraction and Tp Calculations

Landuse	Initial Abstraction			Composite Runoff Coefficient								
	IA (mm)	Area (ha)	A * IA	Sandy Silt		0		0		0		A*RC
				RC	Area	RC	Area	RC	Area	RC	Area	
Woodland	10	0	0		0		0		0		0	0
Meadow	8	0	0		0		0		0		0	0
Wetland	16	0	0		0		0		0		0	0
Lawn	5	3.04	15.21	0.12	3.04		0		0		0	0.37
Cultivated	7	0	0		0		0		0		0	0
Impervious	2	0.46	0.92	0.90	0.46		0		0		0	0.41
Composite		3.50	4.61	Composite Runoff Coefficient								0.22

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp(hr)	TOTAL Tp (hr)	Tc (hr)	Tp(hr)	Tc (hr)	Tp(hr)
Overland	47.5	0.94	1.98%	2.3	0.32	0.04	0.03	0.03	0.03	0.02	0.26	0.18

Appropriate calculated time to peak: 0.18 | Appropriate Method: Airport



Project Name: 10249 Hunsden Sideroad
Project Number: 0952-6305
Created By: AG/BP
Reviewed By: TE

D.A. NAME 203
D.A. AREA 0.07

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment 203

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic	% Area	Area
Sandy Silt	B	B	100	0.07
				0
				0
				0
Total Area				0.07

Impervious Landuses Present:													
Soils	Roadway		Sidewalk		Driveway		House		SWMF		Subtotals		
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
B												0.00	0.00
Subtotal											0.00	0.00	
Pervious Landuses Present:													
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals		
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
B							0.07	61			0.07	4.27	
Subtotal											0.07	4.27	
							Composite Area Calculations		Total Pervious Area			0.07	
									Total Impervious Area			0.00	
									% Impervious			0.00%	
									Composite Curve Number			61.0	
									Total Area Check			0.07	

Initial Abstraction and Tp Calculations

Landuse	Initial Abstraction			Composite Runoff Coefficient								
	IA (mm)	Area (ha)	A * IA	Sandy Silt		0		0		0		A*RC
				RC	Area	RC	Area	RC	Area	RC	Area	
Woodland	10	0	0									0
Meadow	8	0	0									0
Wetland	16	0	0									0
Lawn	5	0.07	0.35	0.12	0.07							0.01
Cultivated	7	0	0									0
Impervious	2	0	0									0
Composite		0.07	5.00	Composite Runoff Coefficient								0.12

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp(hr)	TOTAL Tp (hr)	Tc (hr)	Tp(hr)	Tc (hr)	Tp(hr)
Overland	12.5	0.25	2.00%	2.3	0.33	0.01	0.01	0.01	0.01	0.01	0.15	0.10

Appropriate calculated time to peak: 0.10 | Appropriate Method: Airport



Project Name: 10249 Hunsden Sideroad **D.A. NAME** 204
Project Number: 0952-6305 **D.A. AREA (ha)** 1.39
Created By: AG/BP
Reviewed By: TE

Hydrologic Parameters: CALIB STANDHYD Command
Pre-Development Drainage Area: Catchment 204

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic	% Area	Area
Sandy Silt	B	B	100	1.39
				0
				0
				0
Total Area Check				1.39

Impervious Landuses Present:												
Soils	Roadway		Sidewalk		Driveway		Building		SWMF		Subtotals	
	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	A*CN
B	0.19	98			0.07	98	0.01	98			0.28	27.24
Subtotal Area		0.19			0.07		0.01					

Pervious Landuses Present:												
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals	
	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area (ha)	CN	Area	A*CN
B							1.11	61			1.11	67.83
Subtotal Area							1.11					

	Pervious Area Calculations	Total Pervious Area Composite Pervious Curve Number	1.11 61
	Impervious Area Calculations	Total Directly Connected Area	0.27
		Total Indirectly Connected Area	0.01
		Total Impervious Area	0.28
		% X imp	0.00
		% T imp	20.00
Total Area Check			1.39

Initial Abstraction and Tp Calculations

Landuse	IA (mm)	Area (ha)	A * IA
Woodland	10	0	0
Meadow	8	0	0
Wetland	16	0	0
Lawn	5	1.11	5.56
Cultivated	7	0	0

Land Use	IA (mm)	Slope (%)	Travel Length (m)	Manning's n
Pervious	5.0	2.00	25	0.25
Impervious	2.0	1.50	20	0.013



Project Name: 10249 Hunsden Sideroad
 Project Number: 0952-6305
 Created By: AG/BP
 Reviewed By: TE

D.A. NAME 205
 D.A. AREA 0.83

Hydrologic Parameters: CALIB NASHYD Command
 Pre Development Drainage Area: Catchment 205

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic	% Area	Area
Sandy Silt	B	B	100	0.83
				0
				0
				0
Total Area				0.83

Impervious Landuses Present:													
Soils	Roadway		Sidewalk		Driveway		House		SWMF		Subtotals		
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
B	0.06	98			0.01	98	0.03	98			0.11	10.80	
Subtotal	0.06				0.01		0.03						

Pervious Landuses Present:													
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals		
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN	
B							0.72	61			0.72	43.91	
Subtotal							0.72						

Composite Area Calculations											Total Pervious Area		0.72
											Total Impervious Area		0.11
											% Impervious		13.28%
											Composite Curve Number		65.9
											Total Area Check		0.83

Initial Abstraction and Tp Calculations

Landuse	Initial Abstraction			Composite Runoff Coefficient									
	IA (mm)	Area (ha)	A * IA	Sandy Silt			0			0			
				RC	Area	RC	Area	RC	Area	RC	Area	A*RC	
Woodland	10	0	0		0		0		0		0	0	
Meadow	8	0	0		0		0		0		0	0	
Wetland	16	0	0		0		0		0		0	0	
Lawn	5	0.72	3.60	0.12	0.72		0		0		0	0.09	
Cultivated	7	0	0		0		0		0		0	0	
Impervious	2	0.11	0.22	0.90	0.11		0		0		0	0.10	
Composite		0.83	4.60	Composite Runoff Coefficient									0.22

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp(hr)	TOTAL Tp (hr)	Tc (hr)	Tp(hr)	Tc (hr)	Tp(hr)
Overland	30	0.63	2.10%	2.3	0.33	0.03	0.02	0.02	0.03	0.02	0.20	0.14

Appropriate calculated time to peak: 0.14 | Appropriate Method: Airport



Project Name: 10249 Hunsden Sideroad
Project Number: 0952-6305
Created By: AG/BP
Reviewed By: TE

D.A. NAME 206
D.A. AREA 2.15

Hydrologic Parameters: CALIB NASHYD Command
Pre Development Drainage Area: Catchment 206

Curve Number Calculation

Soil Types Present:				
Type	ID	Hydrologic	% Area	Area
Sandy Silt	B	B	100	2.15
				0
				0
				0
Total Area				2.15

Impervious Landuses Present:														
Soils	Roadway		Sidewalk		Driveway		House		SWMF		Subtotals			
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN		
B												0.00	0.00	
Subtotal											0.00	0.00		
Pervious Landuses Present:														
Soils	Woodland		Meadow		Wetland		Lawn		Cultivated		Subtotals			
	Area	CN	Area	CN	Area	CN	Area (ha)	CN	Area	CN	Area	A*CN		
B	0.92	55					1.23	61			2.15	125.61		
Subtotal											0.92			
											Composite Area Calculations		Total Pervious Area	2.15
													Total Impervious Area	0.00
													% Impervious	0.00%
													Composite Curve Number	58.4
													Total Area Check	2.15

Initial Abstraction and Tp Calculations

Landuse	Initial Abstraction			Composite Runoff Coefficient								
	IA (mm)	Area (ha)	A * IA	Sandy Silt		0		0		0		A*RC
				RC	Area	RC	Area	RC	Area	RC	Area	
Woodland	10	0.92	9.24	0.21	0.92	0	0	0	0	0	0	0
Meadow	8	0	0		0	0	0	0	0	0	0	0
Wetland	16	0	0		0	0	0	0	0	0	0	0
Lawn	5	1.23	6.13	0.12	1.23	0	0	0	0	0	0	0.15
Cultivated	7	0	0		0	0	0	0	0	0	0	0
Impervious	2	0	0		0	0	0	0	0	0	0	0
Composite		2.15	7.15	Composite Runoff Coefficient								0.16

Time to Peak Inputs						Uplands			Bransby Williams		Airport	
Flow Path Description	Length (m)	Drop (m)	Slope (%)	V/S ^{0.5}	Velocity (m/s)	Tc (hr)	Tp(hr)	TOTAL Tp (hr)	Tc (hr)	Tp(hr)	Tc (hr)	Tp(hr)
Overland	50	4	8.00%	2.3	0.65	0.02	0.01	0.01	0.03	0.02	0.18	0.12

Appropriate calculated time to peak: 0.12 | Appropriate Method: Airport



Project: 10249 Hunsden Sideroad
Project No.: 0952-6305
Description: Bioswale Sizing

Date: 6/23/2022
Revised: 6/29/2022
Designed By: BP
Checked By: TE

Roadside Bioswale Sizing - Street 'A'

Parameter	Value	Units	Comment
Provided Bioswale Design Parameters			
Design Storm	100	year event	
Percolation Rate =	36.0	mm/hr	per Geotechnical Investigation (Soil Engineers Ltd., April 2022)
Safety Correction Factor =	2.50		
Design Percolation Rate =	15.00	mm/hr	
Bioswale Depth =	1.50	m	0.3 m filter media layer and 1.2 m gravel storage layer
Maximum Footprint Available =	1,144.0	m²	
LID Length =	520.0	m	
LID Width =	1.8	m	
Provided footprint =	936.0	m²	Length x width
Percolation Rate (Design) =	15.0	mm/hr	
Provided Ponding Depth =	0.00	m	assumed no surface ponding to be conservative
Gravel Storage Depth =	1.20	m	
Void Space Ratio =	0.40		
Surface storage (ponding) =	0.0	m ³	
Gravel storage =	449.3	m ³	
Total Bioswale Volume Provided =	449.3	m³	
Infiltration Rate =	0.00156	m³/s	used in VO model

NOTES:

1. Surface storage and filter media storage not included in volume calculation to be conservative.



Project: 10249 Hunsden Sideroad
Project No.: 0952-6305
Description: Bioswale Sizing

Date: 6/23/2022
Revised: 6/29/2022
Designed By: BP
Checked By: TE

Roadside Bioswale Sizing - Street 'A' Cul-de-sac

Parameter	Value	Units	Comment
Provided Bioswale Design Parameters			
Design Storm	100	year event	
Percolation Rate =	36.0	mm/hr	per Geotechnical Investigation (Soil Engineers Ltd., April 2022)
Safety Correction Factor =	2.50		
Design Percolation Rate =	15.00	mm/hr	
Bioswale Depth =	1.50	m	0.3 m filter media layer and 1.2 m gravel storage layer
Maximum Footprint Available =	1,144.0	m²	
LID Length =	320.0	m	
LID Width =	1.8	m	
Provided footprint =	576.0	m²	Length x width
Percolation Rate (Design) =	15.0	mm/hr	
Provided Ponding Depth =	0.00	m	assumed no surface ponding to be conservative
Gravel Storage Depth =	1.20	m	
Void Space Ratio =	0.40		
Surface storage (ponding) =	0.0	m ³	
Gravel storage =	276.5	m ³	
Total Bioswale Volume Provided =	276.5	m³	
Infiltration Rate =	0.00096	m³/s	used in VO model

NOTES:

1. Surface storage and filter media storage not included in volume calculation to be conservative.



Project: 10249 Hunsden Sideroad
Project No.: 0952-6305
Description: Bioswale Sizing

Date: 6/23/2022
Revised: 6/29/2022
Designed By: BP
Checked By: TE

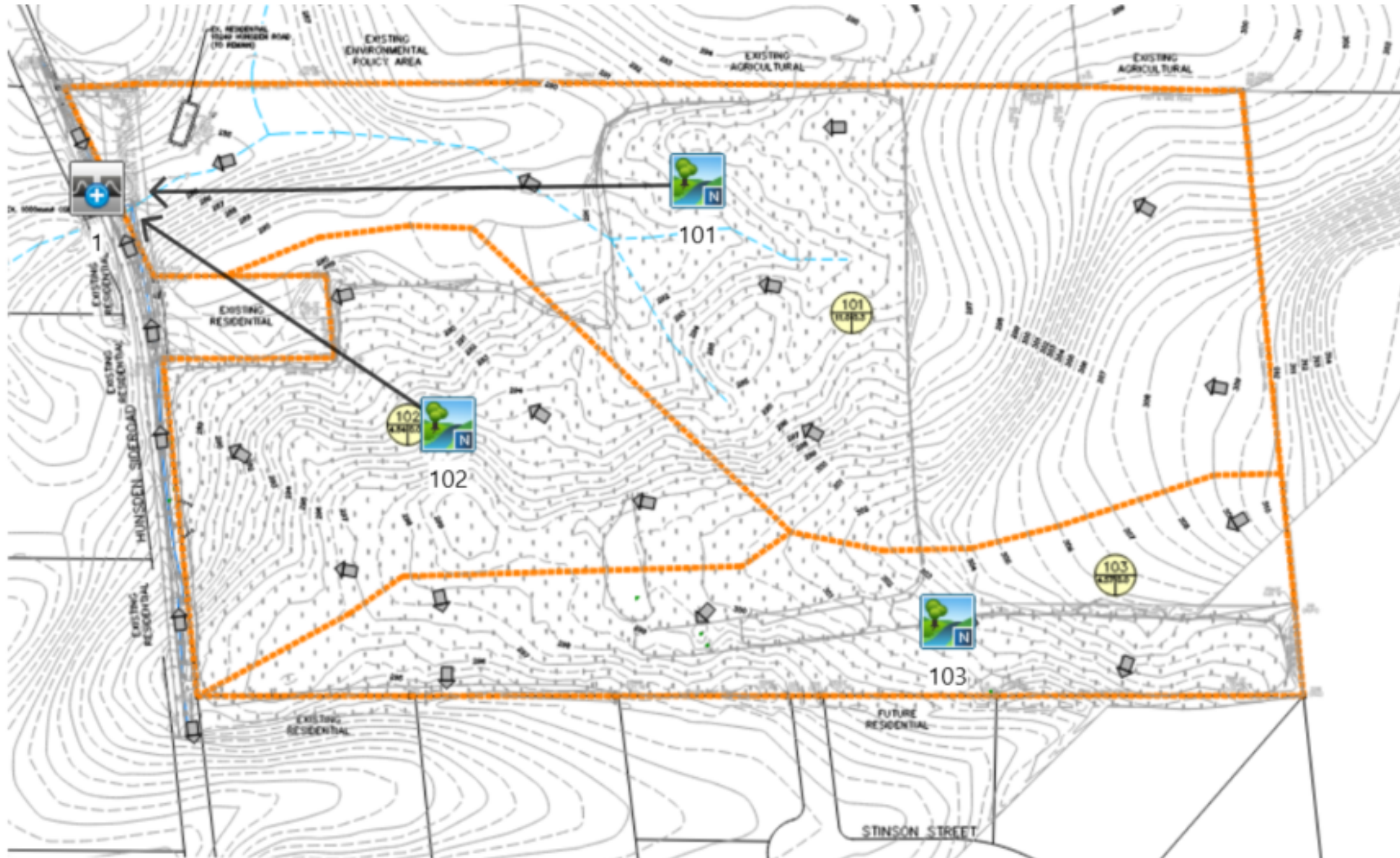
Roadside Bioswale Sizing - Street 'B'

Parameter	Value	Units	Comment
Provided Bioswale Design Parameters			
Design Storm	100	year event	
Percolation Rate =	36.0	mm/hr	per Geotechnical Investigation (Soil Engineers Ltd., April 2022)
Safety Correction Factor =	2.50		
Design Percolation Rate =	15.00	mm/hr	
Bioswale Depth =	1.50	m	0.3 m filter media layer and 1.2 m gravel storage layer
Maximum Footprint Available =	1,144.0	m²	
LID Length =	180.0	m	
LID Width =	1.8	m	
Provided footprint =	324.0	m²	Length x width
Percolation Rate (Design) =	15.0	mm/hr	
Provided Ponding Depth =	0.00	m	assumed no surface ponding to be conservative
Gravel Storage Depth =	1.20	m	
Void Space Ratio =	0.40		
Surface storage (ponding) =	0.0	m ³	
Gravel storage =	155.5	m ³	
Total Bioswale Volume Provided =	155.5	m³	
Infiltration Rate =	0.00054	m³/s	used in VO model

NOTES:

1. Surface storage and filter media storage not included in volume calculation to be conservative.

PRE-DEVELOPMENT – VO SCHEMATIC



=====

V V I SSSSS U U A L (v 6.2.2005)
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

000 TTTTT TTTTT H H Y Y M M 000 TM
O O T T H H Y Y MM MM O O
O O T T H H Y M M O O
000 T T H H Y M M 000

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\V02\voin.dat

Output filename:

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Summary filename:

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DATE: 06/29/2022

TIME: 12:14:22

USER:

COMMENTS: _____

** SIMULATION : 01 - 2yr Chicago **

| CHICAGO STORM |
Ptotal= 32.60 mm

IDF curve parameters: A= 425.932
B= 1.500
C= 0.721

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
 Storm time step = 10.00 min
 Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.17	2.60	1.17	14.29	2.17	5.35	3.17	3.01
0.33	2.92	1.33	73.21	2.33	4.68	3.33	2.83
0.50	3.35	1.50	18.03	2.50	4.19	3.50	2.67
0.67	3.99	1.67	10.56	2.67	3.80	3.67	2.53
0.83	5.01	1.83	7.80	2.83	3.49	3.83	2.40
1.00	7.05	2.00	6.31	3.00	3.23	4.00	2.29

CALIB			
NASHYD (0103)	Area (ha)=	4.57	Curve Number (CN)= 57.0
ID= 1 DT= 5.0 min	Ia (mm)=	8.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.32	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	2.60	1.083	14.29	2.083	5.35	3.08	3.01
0.167	2.60	1.167	14.29	2.167	5.35	3.17	3.01
0.250	2.92	1.250	73.21	2.250	4.68	3.25	2.83
0.333	2.92	1.333	73.21	2.333	4.68	3.33	2.83
0.417	3.35	1.417	18.03	2.417	4.19	3.42	2.67
0.500	3.35	1.500	18.03	2.500	4.19	3.50	2.67
0.583	3.99	1.583	10.56	2.583	3.80	3.58	2.53
0.667	3.99	1.667	10.56	2.667	3.80	3.67	2.53
0.750	5.01	1.750	7.80	2.750	3.49	3.75	2.40
0.833	5.01	1.833	7.80	2.833	3.49	3.83	2.40
0.917	7.05	1.917	6.31	2.917	3.23	3.92	2.29
1.000	7.05	2.000	6.31	3.000	3.23	4.00	2.29

Unit Hyd Qpeak (cms)= 0.545

PEAK FLOW (cms)= 0.021 (i)
 TIME TO PEAK (hrs)= 1.750
 RUNOFF VOLUME (mm)= 2.797
 TOTAL RAINFALL (mm)= 32.596
 RUNOFF COEFFICIENT = 0.086

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD ( 0101) | Area (ha)= 10.97 Curve Number (CN)= 56.1
| ID= 1 DT= 5.0 min | Ia (mm)= 8.99 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.38

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
0.083 2.60 | 1.083 14.29 | 2.083 5.35 | 3.08 3.01
0.167 2.60 | 1.167 14.29 | 2.167 5.35 | 3.17 3.01
0.250 2.92 | 1.250 73.21 | 2.250 4.68 | 3.25 2.83
0.333 2.92 | 1.333 73.21 | 2.333 4.68 | 3.33 2.83
0.417 3.35 | 1.417 18.03 | 2.417 4.19 | 3.42 2.67
0.500 3.35 | 1.500 18.03 | 2.500 4.19 | 3.50 2.67
0.583 3.99 | 1.583 10.56 | 2.583 3.80 | 3.58 2.53
0.667 3.99 | 1.667 10.56 | 2.667 3.80 | 3.67 2.53
0.750 5.01 | 1.750 7.80 | 2.750 3.49 | 3.75 2.40
0.833 5.01 | 1.833 7.80 | 2.833 3.49 | 3.83 2.40
0.917 7.05 | 1.917 6.31 | 2.917 3.23 | 3.92 2.29
1.000 7.05 | 2.000 6.31 | 3.000 3.23 | 4.00 2.29

```

Unit Hyd Qpeak (cms)= 1.103

PEAK FLOW (cms)= 0.041 (i)

TIME TO PEAK (hrs)= 1.917

RUNOFF VOLUME (mm)= 2.505

TOTAL RAINFALL (mm)= 32.596

RUNOFF COEFFICIENT = 0.077

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD ( 0102) | Area (ha)= 4.84 Curve Number (CN)= 57.8
| ID= 1 DT= 5.0 min | Ia (mm)= 7.25 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.27

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN

```


hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	2.60	1.083	14.29	2.083	5.35	3.08	3.01
0.167	2.60	1.167	14.29	2.167	5.35	3.17	3.01
0.250	2.92	1.250	73.21	2.250	4.68	3.25	2.83
0.333	2.92	1.333	73.21	2.333	4.68	3.33	2.83
0.417	3.35	1.417	18.03	2.417	4.19	3.42	2.67
0.500	3.35	1.500	18.03	2.500	4.19	3.50	2.67
0.583	3.99	1.583	10.56	2.583	3.80	3.58	2.53
0.667	3.99	1.667	10.56	2.667	3.80	3.67	2.53
0.750	5.01	1.750	7.80	2.750	3.49	3.75	2.40
0.833	5.01	1.833	7.80	2.833	3.49	3.83	2.40
0.917	7.05	1.917	6.31	2.917	3.23	3.92	2.29
1.000	7.05	2.000	6.31	3.000	3.23	4.00	2.29

Unit Hyd Qpeak (cms)= 0.685

PEAK FLOW (cms)= 0.028 (i)
 TIME TO PEAK (hrs)= 1.667
 RUNOFF VOLUME (mm)= 3.046
 TOTAL RAINFALL (mm)= 32.596
 RUNOFF COEFFICIENT = 0.093

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 0001) |
| 1 + 2 = 3 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0101):	10.97	0.041	1.92	2.51
+ ID2= 2 (0102):	4.84	0.028	1.67	3.05
=====				
ID = 3 (0001):	15.81	0.066	1.75	2.67

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

=====
=====
V V I SSSSS U U A L (v 6.2.2005)
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

OOO TTTTT TTTTT H H Y Y M M OOO TM
O O T T H H Y Y MM MM O O
O O T T H H Y M M O O
OOO T T H H Y M M OOO

```

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***** D E T A I L E D O U T P U T *****

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Output filename:

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Summary filename:

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 be-828c-4012-b47f-448f9e01413d\scenar

DATE: 06/29/2022

TIME: 12:14:22

USER:

COMMENTS: _____

 ** SIMULATION : 02 - 5yr Chicago **

 | CHICAGO STORM |
Ptotal= 44.01 mm

IDF curve parameters: A= 575.144
 B= 1.500
 C= 0.721

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs

Storm time step = 10.00 min

Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.17	3.50	1.17	19.29	2.17	7.23	3.17	4.07
0.33	3.94	1.33	98.86	2.33	6.33	3.33	3.82
0.50	4.53	1.50	24.35	2.50	5.65	3.50	3.60
0.67	5.38	1.67	14.25	2.67	5.13	3.67	3.41
0.83	6.77	1.83	10.53	2.83	4.71	3.83	3.25

1.00 9.52 | 2.00 8.52 | 3.00 4.36 | 4.00 3.10

```

-----
| CALIB |
| NASHYD ( 0103) | Area (ha)= 4.57 Curve Number (CN)= 57.0
| ID= 1 DT= 5.0 min | Ia (mm)= 8.00 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.32

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
0.083 3.50 | 1.083 19.29 | 2.083 7.23 | 3.08 4.07
0.167 3.50 | 1.167 19.29 | 2.167 7.23 | 3.17 4.07
0.250 3.94 | 1.250 98.86 | 2.250 6.33 | 3.25 3.82
0.333 3.94 | 1.333 98.86 | 2.333 6.33 | 3.33 3.82
0.417 4.53 | 1.417 24.35 | 2.417 5.65 | 3.42 3.60
0.500 4.53 | 1.500 24.35 | 2.500 5.65 | 3.50 3.60
0.583 5.38 | 1.583 14.25 | 2.583 5.13 | 3.58 3.41
0.667 5.38 | 1.667 14.25 | 2.667 5.13 | 3.67 3.41
0.750 6.77 | 1.750 10.53 | 2.750 4.71 | 3.75 3.25
0.833 6.77 | 1.833 10.53 | 2.833 4.71 | 3.83 3.25
0.917 9.52 | 1.917 8.52 | 2.917 4.36 | 3.92 3.10
1.000 9.52 | 2.000 8.52 | 3.000 4.36 | 4.00 3.10

```

Unit Hyd Qpeak (cms)= 0.545

PEAK FLOW (cms)= 0.047 (i)

TIME TO PEAK (hrs)= 1.750

RUNOFF VOLUME (mm)= 5.696

TOTAL RAINFALL (mm)= 44.015

RUNOFF COEFFICIENT = 0.129

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD ( 0101) | Area (ha)= 10.97 Curve Number (CN)= 56.1
| ID= 1 DT= 5.0 min | Ia (mm)= 8.99 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.38

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	3.50	1.083	19.29	2.083	7.23	3.08	4.07
0.167	3.50	1.167	19.29	2.167	7.23	3.17	4.07
0.250	3.94	1.250	98.86	2.250	6.33	3.25	3.82
0.333	3.94	1.333	98.86	2.333	6.33	3.33	3.82
0.417	4.53	1.417	24.35	2.417	5.65	3.42	3.60
0.500	4.53	1.500	24.35	2.500	5.65	3.50	3.60
0.583	5.38	1.583	14.25	2.583	5.13	3.58	3.41
0.667	5.38	1.667	14.25	2.667	5.13	3.67	3.41
0.750	6.77	1.750	10.53	2.750	4.71	3.75	3.25
0.833	6.77	1.833	10.53	2.833	4.71	3.83	3.25
0.917	9.52	1.917	8.52	2.917	4.36	3.92	3.10
1.000	9.52	2.000	8.52	3.000	4.36	4.00	3.10

Unit Hyd Qpeak (cms)= 1.103

PEAK FLOW (cms)= 0.093 (i)
 TIME TO PEAK (hrs)= 1.833
 RUNOFF VOLUME (mm)= 5.246
 TOTAL RAINFALL (mm)= 44.015
 RUNOFF COEFFICIENT = 0.119

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		
NASHYD (0102)	Area (ha)= 4.84	Curve Number (CN)= 57.8
ID= 1 DT= 5.0 min	Ia (mm)= 7.25	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= 0.27	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	3.50	1.083	19.29	2.083	7.23	3.08	4.07
0.167	3.50	1.167	19.29	2.167	7.23	3.17	4.07
0.250	3.94	1.250	98.86	2.250	6.33	3.25	3.82
0.333	3.94	1.333	98.86	2.333	6.33	3.33	3.82
0.417	4.53	1.417	24.35	2.417	5.65	3.42	3.60
0.500	4.53	1.500	24.35	2.500	5.65	3.50	3.60
0.583	5.38	1.583	14.25	2.583	5.13	3.58	3.41
0.667	5.38	1.667	14.25	2.667	5.13	3.67	3.41
0.750	6.77	1.750	10.53	2.750	4.71	3.75	3.25
0.833	6.77	1.833	10.53	2.833	4.71	3.83	3.25
0.917	9.52	1.917	8.52	2.917	4.36	3.92	3.10
1.000	9.52	2.000	8.52	3.000	4.36	4.00	3.10

Unit Hyd Qpeak (cms)= 0.685

PEAK FLOW (cms)= 0.060 (i)
TIME TO PEAK (hrs)= 1.667
RUNOFF VOLUME (mm)= 6.079
TOTAL RAINFALL (mm)= 44.015
RUNOFF COEFFICIENT = 0.138

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ADD HYD (0001) |
| 1 + 2 = 3 |

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0101):	10.97	0.093	1.83	5.25
+ ID2= 2 (0102):	4.84	0.060	1.67	6.08
=====				
ID = 3 (0001):	15.81	0.148	1.75	5.50

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

=====

V	V	I	SSSSS	U	U	A	L				(v 6.2.2005)
V	V	I	SS	U	U	A	A	L			
V	V	I	SS	U	U	AAAAA	L				
V	V	I	SS	U	U	A	A	L			
VV		I	SSSSS	UUUUU	A	A	LLLLL				
000	TTTTT	TTTTT	H	H	Y	Y	M	M	000	TM	
0	0	T	T	H	H	Y	Y	MM	MM	0	0
0	0	T	T	H	H	Y	M	M	0	0	
000	T	T	H	H	Y	M	M	000			

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\V02\voin.dat

Output filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\96c084ff-c1ce-4c12-b0b2-b95762b540f6\scenar

Summary filename:
 C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\96c084ff-c1ce-4c12-b0b2-b95762b540f6\scenar

DATE: 06/29/2022

TIME: 12:14:22

USER:

COMMENTS: _____

 ** SIMULATION : 03 - 10yr Chicago **

 | CHICAGO STORM |
Ptotal= 51.68 mm

IDF curve parameters: A= 667.963
 B= 1.500
 C= 0.719

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
 Storm time step = 10.00 min
 Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.17	4.14	1.17	22.67	2.17	8.53	3.17	4.81
0.33	4.65	1.33	115.37	2.33	7.46	3.33	4.51
0.50	5.35	1.50	28.60	2.50	6.67	3.50	4.26
0.67	6.36	1.67	16.77	2.67	6.05	3.67	4.04
0.83	7.99	1.83	12.41	2.83	5.56	3.83	3.84
1.00	11.21	2.00	10.04	3.00	5.15	4.00	3.66

 | CALIB |
 | NASHYD (0103) |
ID= 1 DT= 5.0 min

Area (ha)= 4.57 Curve Number (CN)= 57.0
 Ia (mm)= 8.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 0.32

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	4.14	1.083	22.67	2.083	8.53	3.08	4.81
0.167	4.14	1.167	22.67	2.167	8.53	3.17	4.81
0.250	4.65	1.250	115.37	2.250	7.46	3.25	4.51
0.333	4.65	1.333	115.37	2.333	7.46	3.33	4.51
0.417	5.35	1.417	28.60	2.417	6.67	3.42	4.26
0.500	5.35	1.500	28.60	2.500	6.67	3.50	4.26
0.583	6.36	1.583	16.77	2.583	6.05	3.58	4.04
0.667	6.36	1.667	16.77	2.667	6.05	3.67	4.04
0.750	7.99	1.750	12.41	2.750	5.56	3.75	3.84
0.833	7.99	1.833	12.41	2.833	5.56	3.83	3.84
0.917	11.21	1.917	10.04	2.917	5.15	3.92	3.66
1.000	11.21	2.000	10.04	3.000	5.15	4.00	3.66

Unit Hyd Qpeak (cms)= 0.545

PEAK FLOW (cms)= 0.069 (i)
 TIME TO PEAK (hrs)= 1.667
 RUNOFF VOLUME (mm)= 8.107
 TOTAL RAINFALL (mm)= 51.682
 RUNOFF COEFFICIENT = 0.157

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB |
 | NASHYD (0101) | Area (ha)= 10.97 Curve Number (CN)= 56.1
 | ID= 1 DT= 5.0 min | Ia (mm)= 8.99 # of Linear Res.(N)= 3.00

 U.H. Tp(hrs)= 0.38

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	4.14	1.083	22.67	2.083	8.53	3.08	4.81
0.167	4.14	1.167	22.67	2.167	8.53	3.17	4.81
0.250	4.65	1.250	115.37	2.250	7.46	3.25	4.51
0.333	4.65	1.333	115.37	2.333	7.46	3.33	4.51
0.417	5.35	1.417	28.60	2.417	6.67	3.42	4.26
0.500	5.35	1.500	28.60	2.500	6.67	3.50	4.26
0.583	6.36	1.583	16.77	2.583	6.05	3.58	4.04
0.667	6.36	1.667	16.77	2.667	6.05	3.67	4.04
0.750	7.99	1.750	12.41	2.750	5.56	3.75	3.84
0.833	7.99	1.833	12.41	2.833	5.56	3.83	3.84
0.917	11.21	1.917	10.04	2.917	5.15	3.92	3.66

1.000 11.21 | 2.000 10.04 | 3.000 5.15 | 4.00 3.66

Unit Hyd Qpeak (cms)= 1.103

PEAK FLOW (cms)= 0.138 (i)
 TIME TO PEAK (hrs)= 1.833
 RUNOFF VOLUME (mm)= 7.547
 TOTAL RAINFALL (mm)= 51.682
 RUNOFF COEFFICIENT = 0.146

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD ( 0102) | Area (ha)= 4.84 Curve Number (CN)= 57.8
| ID= 1 DT= 5.0 min | Ia (mm)= 7.25 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.27
  
```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
  TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
  hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
  0.083 4.14 | 1.083 22.67 | 2.083 8.53 | 3.08 4.81
  0.167 4.14 | 1.167 22.67 | 2.167 8.53 | 3.17 4.81
  0.250 4.65 | 1.250 115.37 | 2.250 7.46 | 3.25 4.51
  0.333 4.65 | 1.333 115.37 | 2.333 7.46 | 3.33 4.51
  0.417 5.35 | 1.417 28.60 | 2.417 6.67 | 3.42 4.26
  0.500 5.35 | 1.500 28.60 | 2.500 6.67 | 3.50 4.26
  0.583 6.36 | 1.583 16.77 | 2.583 6.05 | 3.58 4.04
  0.667 6.36 | 1.667 16.77 | 2.667 6.05 | 3.67 4.04
  0.750 7.99 | 1.750 12.41 | 2.750 5.56 | 3.75 3.84
  0.833 7.99 | 1.833 12.41 | 2.833 5.56 | 3.83 3.84
  0.917 11.21 | 1.917 10.04 | 2.917 5.15 | 3.92 3.66
  1.000 11.21 | 2.000 10.04 | 3.000 5.15 | 4.00 3.66
  
```

Unit Hyd Qpeak (cms)= 0.685

PEAK FLOW (cms)= 0.088 (i)
 TIME TO PEAK (hrs)= 1.583
 RUNOFF VOLUME (mm)= 8.583
 TOTAL RAINFALL (mm)= 51.682
 RUNOFF COEFFICIENT = 0.166

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.


```

-----
| ADD HYD ( 0001) |
| 1 + 2 = 3 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0101):	10.97	0.138	1.83	7.55
+ ID2= 2 (0102):	4.84	0.088	1.58	8.58
=====				
ID = 3 (0001):	15.81	0.218	1.75	7.86

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
=====
=====
V   V   I   SSSSS U   U   A   L           (v 6.2.2005)
V   V   I   SS   U   U   A A   L
V   V   I   SS   U   U   AAAAA L
V   V   I   SS   U   U   A   A   L
  VV   I   SSSSS UUUUU A   A   LLLLL
000   TTTTT TTTTT H   H   Y   Y   M   M   000   TM
0   0   T   T   H   H   Y   Y   MM MM 0   0
0   0   T   T   H   H   Y   M   M 0   0
000   T   T   H   H   Y   M   M   000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\V02\voin.dat

Output filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\febb593a-85c2-4d51-a64e-67a5a3f3ac7b\scenar

Summary filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\febb593a-85c2-4d51-a64e-67a5a3f3ac7b\scenar

DATE: 06/29/2022

TIME: 12:14:22

USER:

COMMENTS: _____

 ** SIMULATION : 04- 25yr Chicago **

 | CHICAGO STORM |
Ptotal= 61.16 mm

IDF curve parameters: A= 786.108
 B= 1.500
 C= 0.718

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
 Storm time step = 10.00 min
 Time to peak ratio = 0.33

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.17	4.92	1.17	26.84	2.17	10.11	3.17	5.70
0.33	5.52	1.33	136.11	2.33	8.85	3.33	5.36
0.50	6.35	1.50	33.84	2.50	7.91	3.50	5.05
0.67	7.54	1.67	19.87	2.67	7.18	3.67	4.79
0.83	9.47	1.83	14.70	2.83	6.60	3.83	4.56
1.00	13.29	2.00	11.90	3.00	6.11	4.00	4.35

 | CALIB |
 | NASHYD (0103) |
ID= 1 DT= 5.0 min

Area (ha)= 4.57 Curve Number (CN)= 57.0
 Ia (mm)= 8.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 0.32

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.083	4.92	1.083	26.84	2.083	10.11	3.08	5.70
0.167	4.92	1.167	26.84	2.167	10.11	3.17	5.70
0.250	5.52	1.250	136.11	2.250	8.85	3.25	5.36
0.333	5.52	1.333	136.11	2.333	8.85	3.33	5.36
0.417	6.35	1.417	33.84	2.417	7.91	3.42	5.05
0.500	6.35	1.500	33.84	2.500	7.91	3.50	5.05
0.583	7.54	1.583	19.87	2.583	7.18	3.58	4.79
0.667	7.54	1.667	19.87	2.667	7.18	3.67	4.79
0.750	9.47	1.750	14.70	2.750	6.60	3.75	4.56
0.833	9.47	1.833	14.70	2.833	6.60	3.83	4.56

0.917	13.29	1.917	11.90	2.917	6.11	3.92	4.35
1.000	13.29	2.000	11.90	3.000	6.11	4.00	4.35

Unit Hyd Qpeak (cms)= 0.545

PEAK FLOW (cms)= 0.102 (i)
 TIME TO PEAK (hrs)= 1.667
 RUNOFF VOLUME (mm)= 11.541
 TOTAL RAINFALL (mm)= 61.157
 RUNOFF COEFFICIENT = 0.189

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD ( 0101) | Area (ha)= 10.97 Curve Number (CN)= 56.1
| ID= 1 DT= 5.0 min | Ia (mm)= 8.99 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.38
  
```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
0.083 4.92 | 1.083 26.84 | 2.083 10.11 | 3.08 5.70
0.167 4.92 | 1.167 26.84 | 2.167 10.11 | 3.17 5.70
0.250 5.52 | 1.250 136.11 | 2.250 8.85 | 3.25 5.36
0.333 5.52 | 1.333 136.11 | 2.333 8.85 | 3.33 5.36
0.417 6.35 | 1.417 33.84 | 2.417 7.91 | 3.42 5.05
0.500 6.35 | 1.500 33.84 | 2.500 7.91 | 3.50 5.05
0.583 7.54 | 1.583 19.87 | 2.583 7.18 | 3.58 4.79
0.667 7.54 | 1.667 19.87 | 2.667 7.18 | 3.67 4.79
0.750 9.47 | 1.750 14.70 | 2.750 6.60 | 3.75 4.56
0.833 9.47 | 1.833 14.70 | 2.833 6.60 | 3.83 4.56
0.917 13.29 | 1.917 11.90 | 2.917 6.11 | 3.92 4.35
1.000 13.29 | 2.000 11.90 | 3.000 6.11 | 4.00 4.35
  
```

Unit Hyd Qpeak (cms)= 1.103

PEAK FLOW (cms)= 0.204 (i)
 TIME TO PEAK (hrs)= 1.750
 RUNOFF VOLUME (mm)= 10.844
 TOTAL RAINFALL (mm)= 61.157
 RUNOFF COEFFICIENT = 0.177

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD ( 0102) | Area (ha)= 4.84 Curve Number (CN)= 57.8
| ID= 1 DT= 5.0 min | Ia (mm)= 7.25 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= 0.27

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	4.92	1.083	26.84	2.083	10.11	3.08	5.70
0.167	4.92	1.167	26.84	2.167	10.11	3.17	5.70
0.250	5.52	1.250	136.11	2.250	8.85	3.25	5.36
0.333	5.52	1.333	136.11	2.333	8.85	3.33	5.36
0.417	6.35	1.417	33.84	2.417	7.91	3.42	5.05
0.500	6.35	1.500	33.84	2.500	7.91	3.50	5.05
0.583	7.54	1.583	19.87	2.583	7.18	3.58	4.79
0.667	7.54	1.667	19.87	2.667	7.18	3.67	4.79
0.750	9.47	1.750	14.70	2.750	6.60	3.75	4.56
0.833	9.47	1.833	14.70	2.833	6.60	3.83	4.56
0.917	13.29	1.917	11.90	2.917	6.11	3.92	4.35
1.000	13.29	2.000	11.90	3.000	6.11	4.00	4.35

Unit Hyd Qpeak (cms)= 0.685

PEAK FLOW (cms)= 0.128 (i)
 TIME TO PEAK (hrs)= 1.583
 RUNOFF VOLUME (mm)= 12.134
 TOTAL RAINFALL (mm)= 61.157
 RUNOFF COEFFICIENT = 0.198

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 0001) |
| 1 + 2 = 3 |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 1 ( 0101):  10.97  0.204    1.75    10.84
+ ID2= 2 ( 0102):   4.84  0.128    1.58    12.13
=====
ID = 3 ( 0001):  15.81  0.321    1.67    11.24

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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=====
=====

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V   V   I   SSSSS U   U   A   L           (v 6.2.2005)
V   V   I   SS    U   U   A A  L
V   V   I   SS    U   U   AAAAA L
V   V   I   SS    U   U   A   A  L
  VV    I   SSSSS UUUUU A   A  LLLLL

```

```

000  TTTTT  TTTTT  H   H   Y   Y   M   M   000  TM
0  0  T      T   H   H   Y Y   MM MM  0  0
0  0  T      T   H   H   Y   M   M  0  0
000  T      T   H   H   Y   M   M  000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\V02\voin.dat

Output filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\b1a44e
 a0-2f5c-483f-a91b-1afed2f0909a\scenar

Summary filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\b1a44e
 a0-2f5c-483f-a91b-1afed2f0909a\scenar

DATE: 06/29/2022

TIME: 12:14:22

USER:

COMMENTS: _____

```

-----
*****
** SIMULATION : 05 - 50yr Chicago          **
*****

```

```

-----
| CHICAGO STORM |
| Ptotal= 68.33 mm |
-----

```

```

IDF curve parameters: A= 878.307
                      B=   1.500
                      C=   0.718

```

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
 Storm time step = 10.00 min
 Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.17	5.49	1.17	29.99	2.17	11.30	3.17	6.37
0.33	6.17	1.33	152.08	2.33	9.89	3.33	5.98
0.50	7.09	1.50	37.81	2.50	8.84	3.50	5.65
0.67	8.43	1.67	22.20	2.67	8.03	3.67	5.35
0.83	10.58	1.83	16.43	2.83	7.37	3.83	5.09
1.00	14.85	2.00	13.30	3.00	6.83	4.00	4.86

CALIB			
NASHYD (0103)	Area (ha)=	4.57	Curve Number (CN)= 57.0
ID= 1 DT= 5.0 min	Ia (mm)=	8.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.32	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	5.49	1.083	29.99	2.083	11.30	3.08	6.37
0.167	5.49	1.167	29.99	2.167	11.30	3.17	6.37
0.250	6.17	1.250	152.08	2.250	9.89	3.25	5.98
0.333	6.17	1.333	152.08	2.333	9.89	3.33	5.98
0.417	7.09	1.417	37.81	2.417	8.84	3.42	5.65
0.500	7.09	1.500	37.81	2.500	8.84	3.50	5.65
0.583	8.43	1.583	22.20	2.583	8.03	3.58	5.35
0.667	8.43	1.667	22.20	2.667	8.03	3.67	5.35
0.750	10.58	1.750	16.43	2.750	7.37	3.75	5.09
0.833	10.58	1.833	16.43	2.833	7.37	3.83	5.09
0.917	14.85	1.917	13.30	2.917	6.83	3.92	4.86
1.000	14.85	2.000	13.30	3.000	6.83	4.00	4.86

Unit Hyd Qpeak (cms)= 0.545

PEAK FLOW (cms)= 0.130 (i)

TIME TO PEAK (hrs)= 1.667

RUNOFF VOLUME (mm)= 14.442

TOTAL RAINFALL (mm)= 68.330

RUNOFF COEFFICIENT = 0.211

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD ( 0101) | Area (ha)= 10.97 Curve Number (CN)= 56.1
| ID= 1 DT= 5.0 min | Ia (mm)= 8.99 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.38

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
0.083 5.49 | 1.083 29.99 | 2.083 11.30 | 3.08 6.37
0.167 5.49 | 1.167 29.99 | 2.167 11.30 | 3.17 6.37
0.250 6.17 | 1.250 152.08 | 2.250 9.89 | 3.25 5.98
0.333 6.17 | 1.333 152.08 | 2.333 9.89 | 3.33 5.98
0.417 7.09 | 1.417 37.81 | 2.417 8.84 | 3.42 5.65
0.500 7.09 | 1.500 37.81 | 2.500 8.84 | 3.50 5.65
0.583 8.43 | 1.583 22.20 | 2.583 8.03 | 3.58 5.35
0.667 8.43 | 1.667 22.20 | 2.667 8.03 | 3.67 5.35
0.750 10.58 | 1.750 16.43 | 2.750 7.37 | 3.75 5.09
0.833 10.58 | 1.833 16.43 | 2.833 7.37 | 3.83 5.09
0.917 14.85 | 1.917 13.30 | 2.917 6.83 | 3.92 4.86
1.000 14.85 | 2.000 13.30 | 3.000 6.83 | 4.00 4.86

```

Unit Hyd Qpeak (cms)= 1.103

PEAK FLOW (cms)= 0.261 (i)
 TIME TO PEAK (hrs)= 1.750
 RUNOFF VOLUME (mm)= 13.641
 TOTAL RAINFALL (mm)= 68.330
 RUNOFF COEFFICIENT = 0.200

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD ( 0102) | Area (ha)= 4.84 Curve Number (CN)= 57.8
| ID= 1 DT= 5.0 min | Ia (mm)= 7.25 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.27

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
0.083 5.49 | 1.083 29.99 | 2.083 11.30 | 3.08 6.37

```

0.167	5.49	1.167	29.99	2.167	11.30	3.17	6.37
0.250	6.17	1.250	152.08	2.250	9.89	3.25	5.98
0.333	6.17	1.333	152.08	2.333	9.89	3.33	5.98
0.417	7.09	1.417	37.81	2.417	8.84	3.42	5.65
0.500	7.09	1.500	37.81	2.500	8.84	3.50	5.65
0.583	8.43	1.583	22.20	2.583	8.03	3.58	5.35
0.667	8.43	1.667	22.20	2.667	8.03	3.67	5.35
0.750	10.58	1.750	16.43	2.750	7.37	3.75	5.09
0.833	10.58	1.833	16.43	2.833	7.37	3.83	5.09
0.917	14.85	1.917	13.30	2.917	6.83	3.92	4.86
1.000	14.85	2.000	13.30	3.000	6.83	4.00	4.86

Unit Hyd Qpeak (cms)= 0.685

PEAK FLOW (cms)= 0.162 (i)
 TIME TO PEAK (hrs)= 1.583
 RUNOFF VOLUME (mm)= 15.124
 TOTAL RAINFALL (mm)= 68.330
 RUNOFF COEFFICIENT = 0.221

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0001)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0101):	10.97	0.261	1.75	13.64
+ ID2= 2 (0102):	4.84	0.162	1.58	15.12
=====				
ID = 3 (0001):	15.81	0.411	1.67	14.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

=====

```

V  V  I  SSSSS  U  U  A  L  (v 6.2.2005)
V  V  I  SS    U  U  A  A  L
V  V  I  SS    U  U  AAAAA  L
V  V  I  SS    U  U  A  A  L
  VV  I  SSSSS  UUUUU  A  A  LLLLL

  000  TTTTT  TTTTT  H  H  Y  Y  M  M  000  TM
  0  0  T  T  H  H  Y  Y  MM  MM  0  0
  0  0  T  T  H  H  Y  M  M  0  0
  000  T  T  H  H  Y  M  M  000

```


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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\V02\voin.dat

Output filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\b19de36c-47a5-4bd5-a212-2edea42c35b8\scenar

Summary filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\b19de36c-47a5-4bd5-a212-2edea42c35b8\scenar

DATE: 06/29/2022

TIME: 12:14:22

USER:

COMMENTS: _____

** SIMULATION : 06 - 100yr Chicago **

| CHICAGO STORM |
Ptotal= 75.17 mm

IDF curve parameters: A= 971.524
B= 1.500
C= 0.719

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
Storm time step = 10.00 min
Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.17	6.02	1.17	32.97	2.17	12.40	3.17	6.99
0.33	6.77	1.33	167.81	2.33	10.86	3.33	6.56
0.50	7.78	1.50	41.59	2.50	9.70	3.50	6.19
0.67	9.24	1.67	24.40	2.67	8.81	3.67	5.87
0.83	11.62	1.83	18.04	2.83	8.08	3.83	5.58
1.00	16.31	2.00	14.60	3.00	7.49	4.00	5.33

```

-----
| CALIB |
| NASHYD ( 0103) | Area (ha)= 4.57 Curve Number (CN)= 57.0
| ID= 1 DT= 5.0 min | Ia (mm)= 8.00 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.32

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
0.083 6.02 | 1.083 32.97 | 2.083 12.40 | 3.08 6.99
0.167 6.02 | 1.167 32.97 | 2.167 12.40 | 3.17 6.99
0.250 6.77 | 1.250 167.81 | 2.250 10.86 | 3.25 6.56
0.333 6.77 | 1.333 167.81 | 2.333 10.86 | 3.33 6.56
0.417 7.78 | 1.417 41.59 | 2.417 9.70 | 3.42 6.19
0.500 7.78 | 1.500 41.59 | 2.500 9.70 | 3.50 6.19
0.583 9.24 | 1.583 24.40 | 2.583 8.81 | 3.58 5.87
0.667 9.24 | 1.667 24.40 | 2.667 8.81 | 3.67 5.87
0.750 11.62 | 1.750 18.04 | 2.750 8.08 | 3.75 5.58
0.833 11.62 | 1.833 18.04 | 2.833 8.08 | 3.83 5.58
0.917 16.31 | 1.917 14.60 | 2.917 7.49 | 3.92 5.33
1.000 16.31 | 2.000 14.60 | 3.000 7.49 | 4.00 5.33

```

Unit Hyd Qpeak (cms)= 0.545

PEAK FLOW (cms)= 0.160 (i)
 TIME TO PEAK (hrs)= 1.667
 RUNOFF VOLUME (mm)= 17.429
 TOTAL RAINFALL (mm)= 75.169
 RUNOFF COEFFICIENT = 0.232

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD ( 0101) | Area (ha)= 10.97 Curve Number (CN)= 56.1
| ID= 1 DT= 5.0 min | Ia (mm)= 8.99 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.38

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr

```

0.083	6.02	1.083	32.97	2.083	12.40	3.08	6.99
0.167	6.02	1.167	32.97	2.167	12.40	3.17	6.99
0.250	6.77	1.250	167.81	2.250	10.86	3.25	6.56
0.333	6.77	1.333	167.81	2.333	10.86	3.33	6.56
0.417	7.78	1.417	41.59	2.417	9.70	3.42	6.19
0.500	7.78	1.500	41.59	2.500	9.70	3.50	6.19
0.583	9.24	1.583	24.40	2.583	8.81	3.58	5.87
0.667	9.24	1.667	24.40	2.667	8.81	3.67	5.87
0.750	11.62	1.750	18.04	2.750	8.08	3.75	5.58
0.833	11.62	1.833	18.04	2.833	8.08	3.83	5.58
0.917	16.31	1.917	14.60	2.917	7.49	3.92	5.33
1.000	16.31	2.000	14.60	3.000	7.49	4.00	5.33

Unit Hyd Qpeak (cms)= 1.103

PEAK FLOW (cms)= 0.323 (i)
 TIME TO PEAK (hrs)= 1.750
 RUNOFF VOLUME (mm)= 16.528
 TOTAL RAINFALL (mm)= 75.169
 RUNOFF COEFFICIENT = 0.220

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB |
 | NASHYD (0102) | Area (ha)= 4.84 Curve Number (CN)= 57.8
 | ID= 1 DT= 5.0 min | Ia (mm)= 7.25 # of Linear Res.(N)= 3.00
 ----- U.H. Tp(hrs)= 0.27

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	6.02	1.083	32.97	2.083	12.40	3.08	6.99
0.167	6.02	1.167	32.97	2.167	12.40	3.17	6.99
0.250	6.77	1.250	167.81	2.250	10.86	3.25	6.56
0.333	6.77	1.333	167.81	2.333	10.86	3.33	6.56
0.417	7.78	1.417	41.59	2.417	9.70	3.42	6.19
0.500	7.78	1.500	41.59	2.500	9.70	3.50	6.19
0.583	9.24	1.583	24.40	2.583	8.81	3.58	5.87
0.667	9.24	1.667	24.40	2.667	8.81	3.67	5.87
0.750	11.62	1.750	18.04	2.750	8.08	3.75	5.58
0.833	11.62	1.833	18.04	2.833	8.08	3.83	5.58
0.917	16.31	1.917	14.60	2.917	7.49	3.92	5.33
1.000	16.31	2.000	14.60	3.000	7.49	4.00	5.33

Unit Hyd Qpeak (cms)= 0.685

PEAK FLOW (cms)= 0.199 (i)
 TIME TO PEAK (hrs)= 1.583
 RUNOFF VOLUME (mm)= 18.196
 TOTAL RAINFALL (mm)= 75.169
 RUNOFF COEFFICIENT = 0.242

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0001)					
1 + 2 = 3					

	AREA	QPEAK	TPEAK	R.V.	
	(ha)	(cms)	(hrs)	(mm)	
ID1= 1 (0101):	10.97	0.323	1.75	16.53	
+ ID2= 2 (0102):	4.84	0.199	1.58	18.20	
=====					
ID = 3 (0001):	15.81	0.506	1.67	17.04	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

=====

=====

POST-DEVELOPMENT w/ MITIGATION – VO SCHEMATIC



=====

V V I SSSSS U U A L (v 6.2.2005)
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

000 TTTTT TTTTT H H Y Y M M 000 TM
O O T T H H Y Y MM MM O O
O O T T H H Y M M O O
000 T T H H Y M M 000

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\V02\voin.dat

Output filename:

C:\Users\bpond\AppData\Local\Civica\VH5\62082276-f617-4be2-807a-c20b5723c417\6f94bb4a-ba38-4a69-a6f9-b2ddbcbdeaf0\scenar

Summary filename:

C:\Users\bpond\AppData\Local\Civica\VH5\62082276-f617-4be2-807a-c20b5723c417\6f94bb4a-ba38-4a69-a6f9-b2ddbcbdeaf0\scenar

DATE: 06/29/2022

TIME: 12:14:26

USER:

COMMENTS: _____

** SIMULATION : 01 - 2yr Chicago **

| CHICAGO STORM |
Ptotal= 32.60 mm

IDF curve parameters: A= 425.932
B= 1.500
C= 0.721

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs

Storm time step = 10.00 min

Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.17	2.60	1.17	14.29	2.17	5.35	3.17	3.01
0.33	2.92	1.33	73.21	2.33	4.68	3.33	2.83
0.50	3.35	1.50	18.03	2.50	4.19	3.50	2.67
0.67	3.99	1.67	10.56	2.67	3.80	3.67	2.53
0.83	5.01	1.83	7.80	2.83	3.49	3.83	2.40
1.00	7.05	2.00	6.31	3.00	3.23	4.00	2.29

CALIB			
NASHYD (0201)	Area (ha)=	12.44	Curve Number (CN)= 58.1
ID= 1 DT= 5.0 min	Ia (mm)=	8.04	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.39	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	2.60	1.083	14.29	2.083	5.35	3.08	3.01
0.167	2.60	1.167	14.29	2.167	5.35	3.17	3.01
0.250	2.92	1.250	73.21	2.250	4.68	3.25	2.83
0.333	2.92	1.333	73.21	2.333	4.68	3.33	2.83
0.417	3.35	1.417	18.03	2.417	4.19	3.42	2.67
0.500	3.35	1.500	18.03	2.500	4.19	3.50	2.67
0.583	3.99	1.583	10.56	2.583	3.80	3.58	2.53
0.667	3.99	1.667	10.56	2.667	3.80	3.67	2.53
0.750	5.01	1.750	7.80	2.750	3.49	3.75	2.40
0.833	5.01	1.833	7.80	2.833	3.49	3.83	2.40
0.917	7.05	1.917	6.31	2.917	3.23	3.92	2.29
1.000	7.05	2.000	6.31	3.000	3.23	4.00	2.29

Unit Hyd Qpeak (cms)= 1.218

PEAK FLOW (cms)= 0.054 (i)

TIME TO PEAK (hrs)= 1.833

RUNOFF VOLUME (mm)= 2.902

TOTAL RAINFALL (mm)= 32.596

RUNOFF COEFFICIENT = 0.089

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD ( 0203) | Area (ha)= 0.07 Curve Number (CN)= 61.0
| ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.10

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
0.083 2.60 | 1.083 14.29 | 2.083 5.35 | 3.08 3.01
0.167 2.60 | 1.167 14.29 | 2.167 5.35 | 3.17 3.01
0.250 2.92 | 1.250 73.21 | 2.250 4.68 | 3.25 2.83
0.333 2.92 | 1.333 73.21 | 2.333 4.68 | 3.33 2.83
0.417 3.35 | 1.417 18.03 | 2.417 4.19 | 3.42 2.67
0.500 3.35 | 1.500 18.03 | 2.500 4.19 | 3.50 2.67
0.583 3.99 | 1.583 10.56 | 2.583 3.80 | 3.58 2.53
0.667 3.99 | 1.667 10.56 | 2.667 3.80 | 3.67 2.53
0.750 5.01 | 1.750 7.80 | 2.750 3.49 | 3.75 2.40
0.833 5.01 | 1.833 7.80 | 2.833 3.49 | 3.83 2.40
0.917 7.05 | 1.917 6.31 | 2.917 3.23 | 3.92 2.29
1.000 7.05 | 2.000 6.31 | 3.000 3.23 | 4.00 2.29

```

Unit Hyd Qpeak (cms)= 0.027

PEAK FLOW (cms)= 0.001 (i)

TIME TO PEAK (hrs)= 1.333

RUNOFF VOLUME (mm)= 3.899

TOTAL RAINFALL (mm)= 32.596

RUNOFF COEFFICIENT = 0.120

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD ( 0202) | Area (ha)= 3.50 Curve Number (CN)= 65.8
| ID= 1 DT= 5.0 min | Ia (mm)= 4.61 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.18

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN

```


hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	2.60	1.083	14.29	2.083	5.35	3.08	3.01
0.167	2.60	1.167	14.29	2.167	5.35	3.17	3.01
0.250	2.92	1.250	73.21	2.250	4.68	3.25	2.83
0.333	2.92	1.333	73.21	2.333	4.68	3.33	2.83
0.417	3.35	1.417	18.03	2.417	4.19	3.42	2.67
0.500	3.35	1.500	18.03	2.500	4.19	3.50	2.67
0.583	3.99	1.583	10.56	2.583	3.80	3.58	2.53
0.667	3.99	1.667	10.56	2.667	3.80	3.67	2.53
0.750	5.01	1.750	7.80	2.750	3.49	3.75	2.40
0.833	5.01	1.833	7.80	2.833	3.49	3.83	2.40
0.917	7.05	1.917	6.31	2.917	3.23	3.92	2.29
1.000	7.05	2.000	6.31	3.000	3.23	4.00	2.29

Unit Hyd Qpeak (cms)= 0.743

PEAK FLOW (cms)= 0.046 (i)
 TIME TO PEAK (hrs)= 1.500
 RUNOFF VOLUME (mm)= 4.881
 TOTAL RAINFALL (mm)= 32.596
 RUNOFF COEFFICIENT = 0.150

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR( 0050) | OVERFLOW IS OFF
| IN= 2----> OUT= 1 |
| DT= 5.0 min      |
-----
| OUTFLOW          | STORAGE          | OUTFLOW          | STORAGE          |
| (cms)            | (ha.m.)         | (cms)            | (ha.m.)         |
| **** WARNING :  | FIRST OUTFLOW IS NOT ZERO.
| 0.0016          | 0.0000          | 1.0000          | 0.0450          |
| 0.0016          | 0.0449          | 0.0000          | 0.0000          |
|
| AREA            | QPEAK           | TPEAK           | R.V.            |
| (ha)           | (cms)           | (hrs)           | (mm)            |
| INFLOW : ID= 2 ( 0202) | 3.500          | 0.046          | 1.50            | 4.88
| OUTFLOW: ID= 1 ( 0050) | 3.500          | 0.002          | 1.25            | 4.89
|
| PEAK FLOW REDUCTION [Qout/Qin](%)= 3.41
| TIME SHIFT OF PEAK FLOW (min)=-15.00
| MAXIMUM STORAGE USED (ha.m.)= 0.0152

```

```

-----
| CALIB
| STANDHYD ( 0204) | Area (ha)= 1.39
| ID= 1 DT= 5.0 min | Total Imp(%)= 20.00 Dir. Conn.(%)= 1.00
-----

```

IMPERVIOUS PERVIOUS (i)

Surface Area (ha)= 0.28 1.11
 Dep. Storage (mm)= 2.00 2.00
 Average Slope (%)= 1.50 2.00
 Length (m)= 20.00 25.00
 Mannings n = 0.013 0.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	2.60	1.083	14.29	2.083	5.35	3.08	3.01
0.167	2.60	1.167	14.29	2.167	5.35	3.17	3.01
0.250	2.92	1.250	73.21	2.250	4.68	3.25	2.83
0.333	2.92	1.333	73.21	2.333	4.68	3.33	2.83
0.417	3.35	1.417	18.03	2.417	4.19	3.42	2.67
0.500	3.35	1.500	18.03	2.500	4.19	3.50	2.67
0.583	3.99	1.583	10.56	2.583	3.80	3.58	2.53
0.667	3.99	1.667	10.56	2.667	3.80	3.67	2.53
0.750	5.01	1.750	7.80	2.750	3.49	3.75	2.40
0.833	5.01	1.833	7.80	2.833	3.49	3.83	2.40
0.917	7.05	1.917	6.31	2.917	3.23	3.92	2.29
1.000	7.05	2.000	6.31	3.000	3.23	4.00	2.29

Max.Eff.Inten.(mm/hr)= 73.21 10.58
 over (min) 5.00 15.00
 Storage Coeff. (min)= 0.98 (ii) 14.05 (ii)
 Unit Hyd. Tpeak (min)= 5.00 15.00
 Unit Hyd. peak (cms)= 0.34 0.08

TOTALS
 PEAK FLOW (cms)= 0.00 0.02 0.022 (iii)
 TIME TO PEAK (hrs)= 1.33 1.50 1.50
 RUNOFF VOLUME (mm)= 30.60 5.92 6.16
 TOTAL RAINFALL (mm)= 32.60 32.60 32.60
 RUNOFF COEFFICIENT = 0.94 0.18 0.19

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
 ***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 61.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | RESERVOIR(0051) | OVERFLOW IS OFF

```

| IN= 2---> OUT= 1 |
| DT= 5.0 min      |
-----
      OUTFLOW   STORAGE   |   OUTFLOW   STORAGE
      (cms)     (ha.m.)   |   (cms)     (ha.m.)
**** WARNING : FIRST OUTFLOW IS NOT ZERO.
      0.0010    0.0000    |   1.0000    0.0278
      0.0010    0.0277    |   0.0000    0.0000

```

```

              AREA      QPEAK      TPEAK      R.V.
              (ha)      (cms)      (hrs)      (mm)
INFLOW : ID= 2 ( 0204)  1.390      0.022      1.50      6.16
OUTFLOW: ID= 1 ( 0051)  1.390      0.001      1.08      6.17

```

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 4.38
TIME SHIFT OF PEAK FLOW (min)=-25.00
MAXIMUM STORAGE USED (ha.m.)= 0.0073

```

```

-----
| ADD HYD ( 0001) |
| 1 + 2 = 3      |
-----
      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)
      ID1= 1 ( 0201):  12.44    0.054      1.83      2.90
+ ID2= 2 ( 0203):    0.07    0.001      1.33      3.90
=====
      ID = 3 ( 0001):  12.51    0.055      1.83      2.91

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0001) |
| 3 + 2 = 1      |
-----
      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)
      ID1= 3 ( 0001):  12.51    0.055      1.83      2.91
+ ID2= 2 ( 0050):    3.50    0.002      1.25      4.89
=====
      ID = 1 ( 0001):  16.01    0.056      1.83      3.34

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0001) |
| 1 + 2 = 3      |
-----
      AREA      QPEAK      TPEAK      R.V.
      (ha)      (cms)      (hrs)      (mm)
      ID1= 1 ( 0001):  16.01    0.056      1.83      3.34
+ ID2= 2 ( 0051):    1.39    0.001      1.08      6.17
=====
      ID = 3 ( 0001):  17.40    0.057      1.83      3.57

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB |
| NASHYD ( 0205) | Area (ha)= 0.83 Curve Number (CN)= 65.9
| ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.14

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
      TIME    RAIN | TIME    RAIN | TIME    RAIN | TIME    RAIN
      hrs    mm/hr | hrs    mm/hr | hrs    mm/hr | hrs    mm/hr
0.083    2.60 | 1.083   14.29 | 2.083    5.35 | 3.08    3.01
0.167    2.60 | 1.167   14.29 | 2.167    5.35 | 3.17    3.01
0.250    2.92 | 1.250   73.21 | 2.250    4.68 | 3.25    2.83
0.333    2.92 | 1.333   73.21 | 2.333    4.68 | 3.33    2.83
0.417    3.35 | 1.417   18.03 | 2.417    4.19 | 3.42    2.67
0.500    3.35 | 1.500   18.03 | 2.500    4.19 | 3.50    2.67
0.583    3.99 | 1.583   10.56 | 2.583    3.80 | 3.58    2.53
0.667    3.99 | 1.667   10.56 | 2.667    3.80 | 3.67    2.53
0.750    5.01 | 1.750    7.80 | 2.750    3.49 | 3.75    2.40
0.833    5.01 | 1.833    7.80 | 2.833    3.49 | 3.83    2.40
0.917    7.05 | 1.917    6.31 | 2.917    3.23 | 3.92    2.29
1.000    7.05 | 2.000    6.31 | 3.000    3.23 | 4.00    2.29

```

Unit Hyd Qpeak (cms)= 0.226

PEAK FLOW (cms)= 0.013 (i)

TIME TO PEAK (hrs)= 1.417

RUNOFF VOLUME (mm)= 4.879

TOTAL RAINFALL (mm)= 32.596

RUNOFF COEFFICIENT = 0.150

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR( 0052) | OVERFLOW IS OFF
| IN= 2----> OUT= 1 |
| DT= 5.0 min |
-----
      OUTFLOW    STORAGE | OUTFLOW    STORAGE
      (cms)      (ha.m.) | (cms)      (ha.m.)
**** WARNING : FIRST OUTFLOW IS NOT ZERO.
      0.0005    0.0000 | 1.0000    0.0156
      0.0005    0.0155 | 0.0000    0.0000

```

```

      AREA    QPEAK    TPEAK    R.V.
      (ha)    (cms)    (hrs)    (mm)

```

INFLOW : ID= 2 (0205) 0.830 0.013 1.42 4.88
 OUTFLOW: ID= 1 (0052) 0.830 0.001 1.25 4.89

PEAK FLOW REDUCTION [Qout/Qin](%)= 4.30
 TIME SHIFT OF PEAK FLOW (min)=-10.00
 MAXIMUM STORAGE USED (ha.m.)= 0.0034

 | CALIB |
 | NASHYD (0206) | Area (ha)= 2.15 Curve Number (CN)= 58.4
 | ID= 1 DT= 5.0 min | Ia (mm)= 7.15 # of Linear Res.(N)= 3.00

 U.H. Tp(hrs)= 0.12

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	2.60	1.083	14.29	2.083	5.35	3.08	3.01
0.167	2.60	1.167	14.29	2.167	5.35	3.17	3.01
0.250	2.92	1.250	73.21	2.250	4.68	3.25	2.83
0.333	2.92	1.333	73.21	2.333	4.68	3.33	2.83
0.417	3.35	1.417	18.03	2.417	4.19	3.42	2.67
0.500	3.35	1.500	18.03	2.500	4.19	3.50	2.67
0.583	3.99	1.583	10.56	2.583	3.80	3.58	2.53
0.667	3.99	1.667	10.56	2.667	3.80	3.67	2.53
0.750	5.01	1.750	7.80	2.750	3.49	3.75	2.40
0.833	5.01	1.833	7.80	2.833	3.49	3.83	2.40
0.917	7.05	1.917	6.31	2.917	3.23	3.92	2.29
1.000	7.05	2.000	6.31	3.000	3.23	4.00	2.29

Unit Hyd Qpeak (cms)= 0.684

PEAK FLOW (cms)= 0.019 (i)
 TIME TO PEAK (hrs)= 1.417
 RUNOFF VOLUME (mm)= 3.095
 TOTAL RAINFALL (mm)= 32.596
 RUNOFF COEFFICIENT = 0.095

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | ADD HYD (0002) |
 | 1 + 2 = 3 | AREA QPEAK TPEAK R.V.
 ----- (ha) (cms) (hrs) (mm)
 ID1= 1 (0206): 2.15 0.019 1.42 3.10

```

+ ID2= 2 ( 0052):    0.83  0.001  1.25  4.89
=====
ID = 3 ( 0002):    2.98  0.020  1.42  3.59

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
=====
=====
V  V  I  SSSSS  U  U  A  L          (v 6.2.2005)
V  V  I  SS    U  U  A  A  L
V  V  I  SS    U  U  AAAAA  L
V  V  I  SS    U  U  A  A  L
VV   I  SSSSS  UUUUU  A  A  LLLLL

```

```

000  TTTTT  TTTTT  H  H  Y  Y  M  M  000  TM
O  O  T  T  H  H  Y  Y  MM  MM  O  O
O  O  T  T  H  H  Y  M  M  O  O
000  T  T  H  H  Y  M  M  000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\V02\voin.dat

Output filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\0cd7f066-c6ab-43a6-a69f-f2cca33ed49c\scenar

Summary filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\0cd7f066-c6ab-43a6-a69f-f2cca33ed49c\scenar

DATE: 06/29/2022

TIME: 12:14:26

USER:

COMMENTS: _____

```

-----
*****
** SIMULATION : 02 - 5yr Chicago **

```

```

-----
| CHICAGO STORM |
| Ptotal= 44.01 mm |
-----

```

IDF curve parameters: A= 575.144
 B= 1.500
 C= 0.721
 used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
 Storm time step = 10.00 min
 Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.17	3.50	1.17	19.29	2.17	7.23	3.17	4.07
0.33	3.94	1.33	98.86	2.33	6.33	3.33	3.82
0.50	4.53	1.50	24.35	2.50	5.65	3.50	3.60
0.67	5.38	1.67	14.25	2.67	5.13	3.67	3.41
0.83	6.77	1.83	10.53	2.83	4.71	3.83	3.25
1.00	9.52	2.00	8.52	3.00	4.36	4.00	3.10

```

-----
| CALIB |
| NASHYD ( 0201) |
| ID= 1 DT= 5.0 min |
-----

```

Area (ha)= 12.44 Curve Number (CN)= 58.1
 Ia (mm)= 8.04 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 0.39

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	3.50	1.083	19.29	2.083	7.23	3.08	4.07
0.167	3.50	1.167	19.29	2.167	7.23	3.17	4.07
0.250	3.94	1.250	98.86	2.250	6.33	3.25	3.82
0.333	3.94	1.333	98.86	2.333	6.33	3.33	3.82
0.417	4.53	1.417	24.35	2.417	5.65	3.42	3.60
0.500	4.53	1.500	24.35	2.500	5.65	3.50	3.60
0.583	5.38	1.583	14.25	2.583	5.13	3.58	3.41
0.667	5.38	1.667	14.25	2.667	5.13	3.67	3.41
0.750	6.77	1.750	10.53	2.750	4.71	3.75	3.25
0.833	6.77	1.833	10.53	2.833	4.71	3.83	3.25
0.917	9.52	1.917	8.52	2.917	4.36	3.92	3.10
1.000	9.52	2.000	8.52	3.000	4.36	4.00	3.10

Unit Hyd Qpeak (cms)= 1.218

PEAK FLOW (cms)= 0.120 (i)
 TIME TO PEAK (hrs)= 1.833
 RUNOFF VOLUME (mm)= 5.904
 TOTAL RAINFALL (mm)= 44.015
 RUNOFF COEFFICIENT = 0.134

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
NASHYD (0203)	Area (ha)= 0.07	Curve Number (CN)= 61.0	
ID= 1 DT= 5.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= 0.10		

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	3.50	1.083	19.29	2.083	7.23	3.08	4.07
0.167	3.50	1.167	19.29	2.167	7.23	3.17	4.07
0.250	3.94	1.250	98.86	2.250	6.33	3.25	3.82
0.333	3.94	1.333	98.86	2.333	6.33	3.33	3.82
0.417	4.53	1.417	24.35	2.417	5.65	3.42	3.60
0.500	4.53	1.500	24.35	2.500	5.65	3.50	3.60
0.583	5.38	1.583	14.25	2.583	5.13	3.58	3.41
0.667	5.38	1.667	14.25	2.667	5.13	3.67	3.41
0.750	6.77	1.750	10.53	2.750	4.71	3.75	3.25
0.833	6.77	1.833	10.53	2.833	4.71	3.83	3.25
0.917	9.52	1.917	8.52	2.917	4.36	3.92	3.10
1.000	9.52	2.000	8.52	3.000	4.36	4.00	3.10

Unit Hyd Qpeak (cms)= 0.027

PEAK FLOW (cms)= 0.002 (i)
 TIME TO PEAK (hrs)= 1.333
 RUNOFF VOLUME (mm)= 7.358
 TOTAL RAINFALL (mm)= 44.015
 RUNOFF COEFFICIENT = 0.167

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
NASHYD (0202)	Area (ha)= 3.50	Curve Number (CN)= 65.8	
ID= 1 DT= 5.0 min	Ia (mm)= 4.61	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= 0.18		

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	3.50	1.083	19.29	2.083	7.23	3.08	4.07
0.167	3.50	1.167	19.29	2.167	7.23	3.17	4.07
0.250	3.94	1.250	98.86	2.250	6.33	3.25	3.82
0.333	3.94	1.333	98.86	2.333	6.33	3.33	3.82
0.417	4.53	1.417	24.35	2.417	5.65	3.42	3.60
0.500	4.53	1.500	24.35	2.500	5.65	3.50	3.60
0.583	5.38	1.583	14.25	2.583	5.13	3.58	3.41
0.667	5.38	1.667	14.25	2.667	5.13	3.67	3.41
0.750	6.77	1.750	10.53	2.750	4.71	3.75	3.25
0.833	6.77	1.833	10.53	2.833	4.71	3.83	3.25
0.917	9.52	1.917	8.52	2.917	4.36	3.92	3.10
1.000	9.52	2.000	8.52	3.000	4.36	4.00	3.10

Unit Hyd Qpeak (cms)= 0.743

PEAK FLOW (cms)= 0.089 (i)
 TIME TO PEAK (hrs)= 1.500
 RUNOFF VOLUME (mm)= 9.032
 TOTAL RAINFALL (mm)= 44.015
 RUNOFF COEFFICIENT = 0.205

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR(0050)	OVERFLOW IS OFF			
IN= 2---> OUT= 1	OUTFLOW	STORAGE	OUTFLOW	STORAGE
DT= 5.0 min	(cms)	(ha.m.)	(cms)	(ha.m.)
**** WARNING : FIRST OUTFLOW IS NOT ZERO.				
	0.0016	0.0000	1.0000	0.0450
	0.0016	0.0449	0.0000	0.0000
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0202)	3.500	0.089	1.50	9.03
OUTFLOW: ID= 1 (0050)	3.500	0.002	1.17	9.04
	PEAK FLOW REDUCTION [Qout/Qin](%)=	1.75		
	TIME SHIFT OF PEAK FLOW (min)=	-20.00		
	MAXIMUM STORAGE USED (ha.m.)=	0.0297		

```

-----
| CALIB |
| STANDHYD ( 0204) |
| ID= 1 DT= 5.0 min |
-----

```

```

Area (ha)= 1.39
Total Imp(%)= 20.00 Dir. Conn.(%)= 1.00

```

```

                IMPERVIOUS      PERVIOUS (i)
Surface Area (ha)= 0.28          1.11
Dep. Storage (mm)= 2.00         2.00
Average Slope (%)= 1.50         2.00
Length (m)= 20.00              25.00
Mannings n = 0.013             0.250

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----

```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	3.50	1.083	19.29	2.083	7.23	3.08	4.07
0.167	3.50	1.167	19.29	2.167	7.23	3.17	4.07
0.250	3.94	1.250	98.86	2.250	6.33	3.25	3.82
0.333	3.94	1.333	98.86	2.333	6.33	3.33	3.82
0.417	4.53	1.417	24.35	2.417	5.65	3.42	3.60
0.500	4.53	1.500	24.35	2.500	5.65	3.50	3.60
0.583	5.38	1.583	14.25	2.583	5.13	3.58	3.41
0.667	5.38	1.667	14.25	2.667	5.13	3.67	3.41
0.750	6.77	1.750	10.53	2.750	4.71	3.75	3.25
0.833	6.77	1.833	10.53	2.833	4.71	3.83	3.25
0.917	9.52	1.917	8.52	2.917	4.36	3.92	3.10
1.000	9.52	2.000	8.52	3.000	4.36	4.00	3.10

```

Max.Eff.Inten.(mm/hr)= 98.86      24.10
over (min) 5.00 15.00
Storage Coeff. (min)= 0.87 (ii) 10.27 (ii)
Unit Hyd. Tpeak (min)= 5.00 15.00
Unit Hyd. peak (cms)= 0.34 0.09

```

TOTALS

```

PEAK FLOW (cms)= 0.00 0.04 0.045 (iii)
TIME TO PEAK (hrs)= 1.33 1.50 1.50
RUNOFF VOLUME (mm)= 42.01 10.35 10.67
TOTAL RAINFALL (mm)= 44.01 44.01 44.01
RUNOFF COEFFICIENT = 0.95 0.24 0.24

```

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 61.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR(0051)		OVERFLOW IS OFF			
IN= 2---> OUT= 1		OUTFLOW		STORAGE	
DT= 5.0 min		(cms)	(ha.m.)	(cms)	(ha.m.)
**** WARNING : FIRST OUTFLOW IS NOT ZERO.					
		0.0010	0.0000	1.0000	0.0278
		0.0010	0.0277	0.0000	0.0000

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0204)	1.390	0.045	1.50	10.67
OUTFLOW: ID= 1 (0051)	1.390	0.001	1.00	10.67

PEAK FLOW REDUCTION [Qout/Qin](%)= 2.13
 TIME SHIFT OF PEAK FLOW (min)=-30.00
 MAXIMUM STORAGE USED (ha.m.)= 0.0135

ADD HYD (0001)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0201):		12.44	0.120	1.83	5.90
+ ID2= 2 (0203):		0.07	0.002	1.33	7.36
=====					
ID = 3 (0001):		12.51	0.120	1.83	5.91

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0001)		AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1		(ha)	(cms)	(hrs)	(mm)
ID1= 3 (0001):		12.51	0.120	1.83	5.91
+ ID2= 2 (0050):		3.50	0.002	1.17	9.04
=====					
ID = 1 (0001):		16.01	0.122	1.83	6.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| ADD HYD (0001)|

1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0001):	16.01	0.122	1.83	6.60
+ ID2= 2 (0051):	1.39	0.001	1.00	10.67
=====				
ID = 3 (0001):	17.40	0.123	1.83	6.92

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area (ha)=	Curve Number (CN)=
NASHYD (0205)	0.83	65.9
ID= 1 DT= 5.0 min	Ia (mm)= 4.60	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= 0.14	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.083	3.50	1.083	19.29	2.083	7.23	3.08	4.07
0.167	3.50	1.167	19.29	2.167	7.23	3.17	4.07
0.250	3.94	1.250	98.86	2.250	6.33	3.25	3.82
0.333	3.94	1.333	98.86	2.333	6.33	3.33	3.82
0.417	4.53	1.417	24.35	2.417	5.65	3.42	3.60
0.500	4.53	1.500	24.35	2.500	5.65	3.50	3.60
0.583	5.38	1.583	14.25	2.583	5.13	3.58	3.41
0.667	5.38	1.667	14.25	2.667	5.13	3.67	3.41
0.750	6.77	1.750	10.53	2.750	4.71	3.75	3.25
0.833	6.77	1.833	10.53	2.833	4.71	3.83	3.25
0.917	9.52	1.917	8.52	2.917	4.36	3.92	3.10
1.000	9.52	2.000	8.52	3.000	4.36	4.00	3.10

Unit Hyd Qpeak (cms)= 0.226

PEAK FLOW (cms)= 0.025 (i)
 TIME TO PEAK (hrs)= 1.417
 RUNOFF VOLUME (mm)= 9.024
 TOTAL RAINFALL (mm)= 44.015
 RUNOFF COEFFICIENT = 0.205

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR(0052)	OVERFLOW IS OFF
IN= 2---> OUT= 1	
DT= 5.0 min	
	OUTFLOW STORAGE OUTFLOW STORAGE
	(cms) (ha.m.) (cms) (ha.m.)

**** WARNING : FIRST OUTFLOW IS NOT ZERO.

0.0005	0.0000	1.0000	0.0156
0.0005	0.0155	0.0000	0.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0205)	0.830	0.025	1.42	9.02
OUTFLOW: ID= 1 (0052)	0.830	0.001	1.17	9.03

PEAK FLOW REDUCTION [Qout/Qin](%)= 2.19
 TIME SHIFT OF PEAK FLOW (min)=-15.00
 MAXIMUM STORAGE USED (ha.m.)= 0.0068

CALIB			
NASHYD (0206)	Area (ha)=	2.15	Curve Number (CN)= 58.4
ID= 1 DT= 5.0 min	Ia (mm)=	7.15	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.12	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	3.50	1.083	19.29	2.083	7.23	3.08	4.07
0.167	3.50	1.167	19.29	2.167	7.23	3.17	4.07
0.250	3.94	1.250	98.86	2.250	6.33	3.25	3.82
0.333	3.94	1.333	98.86	2.333	6.33	3.33	3.82
0.417	4.53	1.417	24.35	2.417	5.65	3.42	3.60
0.500	4.53	1.500	24.35	2.500	5.65	3.50	3.60
0.583	5.38	1.583	14.25	2.583	5.13	3.58	3.41
0.667	5.38	1.667	14.25	2.667	5.13	3.67	3.41
0.750	6.77	1.750	10.53	2.750	4.71	3.75	3.25
0.833	6.77	1.833	10.53	2.833	4.71	3.83	3.25
0.917	9.52	1.917	8.52	2.917	4.36	3.92	3.10
1.000	9.52	2.000	8.52	3.000	4.36	4.00	3.10

Unit Hyd Qpeak (cms)= 0.684

PEAK FLOW (cms)= 0.043 (i)
 TIME TO PEAK (hrs)= 1.417
 RUNOFF VOLUME (mm)= 6.156
 TOTAL RAINFALL (mm)= 44.015
 RUNOFF COEFFICIENT = 0.140

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 0002) |
| 1 + 2 = 3 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0206):	2.15	0.043	1.42	6.16
+ ID2= 2 (0052):	0.83	0.001	1.17	9.03
=====				
ID = 3 (0002):	2.98	0.043	1.42	6.96

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

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=====
=====
V   V   I   SSSSS  U   U   A   L           (v 6.2.2005)
V   V   I   SS    U   U   A A  L
V   V   I   SS    U   U   AAAAA L
V   V   I   SS    U   U   A   A  L
  VV    I   SSSSS  UUUUU  A   A  LLLLL
000  TTTTT  TTTTT  H   H   Y   Y  M   M  000  TM
0  0  T     T   H   H   Y Y  MM MM  0  0
0  0  T     T   H   H   Y   M   M  0  0
000  T     T   H   H   Y   M   M  000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\V02\voin.dat

Output filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\f63a0b64-1c13-43f1-ab8d-9b771eedc5ba\scenar

Summary filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\f63a0b64-1c13-43f1-ab8d-9b771eedc5ba\scenar

DATE: 06/29/2022

TIME: 12:14:26

USER:

COMMENTS: _____

 ** SIMULATION : 03 - 10yr Chicago **

 | CHICAGO STORM |
Ptotal= 51.68 mm

IDF curve parameters: A= 667.963
 B= 1.500
 C= 0.719

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
 Storm time step = 10.00 min
 Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.17	4.14	1.17	22.67	2.17	8.53	3.17	4.81
0.33	4.65	1.33	115.37	2.33	7.46	3.33	4.51
0.50	5.35	1.50	28.60	2.50	6.67	3.50	4.26
0.67	6.36	1.67	16.77	2.67	6.05	3.67	4.04
0.83	7.99	1.83	12.41	2.83	5.56	3.83	3.84
1.00	11.21	2.00	10.04	3.00	5.15	4.00	3.66

 | CALIB |
 | NASHYD (0201) |
ID= 1 DT= 5.0 min

Area (ha)= 12.44 Curve Number (CN)= 58.1
 Ia (mm)= 8.04 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 0.39

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	4.14	1.083	22.67	2.083	8.53	3.08	4.81
0.167	4.14	1.167	22.67	2.167	8.53	3.17	4.81
0.250	4.65	1.250	115.37	2.250	7.46	3.25	4.51
0.333	4.65	1.333	115.37	2.333	7.46	3.33	4.51
0.417	5.35	1.417	28.60	2.417	6.67	3.42	4.26
0.500	5.35	1.500	28.60	2.500	6.67	3.50	4.26
0.583	6.36	1.583	16.77	2.583	6.05	3.58	4.04
0.667	6.36	1.667	16.77	2.667	6.05	3.67	4.04
0.750	7.99	1.750	12.41	2.750	5.56	3.75	3.84

0.833	7.99	1.833	12.41	2.833	5.56	3.83	3.84
0.917	11.21	1.917	10.04	2.917	5.15	3.92	3.66
1.000	11.21	2.000	10.04	3.000	5.15	4.00	3.66

Unit Hyd Qpeak (cms)= 1.218

PEAK FLOW (cms)= 0.174 (i)
 TIME TO PEAK (hrs)= 1.833
 RUNOFF VOLUME (mm)= 8.396
 TOTAL RAINFALL (mm)= 51.682
 RUNOFF COEFFICIENT = 0.162

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
NASHYD (0203)	Area (ha)=	0.07	Curve Number (CN)= 61.0
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.10	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	4.14	1.083	22.67	2.083	8.53	3.08	4.81
0.167	4.14	1.167	22.67	2.167	8.53	3.17	4.81
0.250	4.65	1.250	115.37	2.250	7.46	3.25	4.51
0.333	4.65	1.333	115.37	2.333	7.46	3.33	4.51
0.417	5.35	1.417	28.60	2.417	6.67	3.42	4.26
0.500	5.35	1.500	28.60	2.500	6.67	3.50	4.26
0.583	6.36	1.583	16.77	2.583	6.05	3.58	4.04
0.667	6.36	1.667	16.77	2.667	6.05	3.67	4.04
0.750	7.99	1.750	12.41	2.750	5.56	3.75	3.84
0.833	7.99	1.833	12.41	2.833	5.56	3.83	3.84
0.917	11.21	1.917	10.04	2.917	5.15	3.92	3.66
1.000	11.21	2.000	10.04	3.000	5.15	4.00	3.66

Unit Hyd Qpeak (cms)= 0.027

PEAK FLOW (cms)= 0.003 (i)
 TIME TO PEAK (hrs)= 1.333
 RUNOFF VOLUME (mm)= 10.148
 TOTAL RAINFALL (mm)= 51.682
 RUNOFF COEFFICIENT = 0.196

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.


```

-----
| CALIB |
| NASHYD ( 0202) | Area (ha)= 3.50 Curve Number (CN)= 65.8
| ID= 1 DT= 5.0 min | Ia (mm)= 4.61 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.18

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	4.14	1.083	22.67	2.083	8.53	3.08	4.81
0.167	4.14	1.167	22.67	2.167	8.53	3.17	4.81
0.250	4.65	1.250	115.37	2.250	7.46	3.25	4.51
0.333	4.65	1.333	115.37	2.333	7.46	3.33	4.51
0.417	5.35	1.417	28.60	2.417	6.67	3.42	4.26
0.500	5.35	1.500	28.60	2.500	6.67	3.50	4.26
0.583	6.36	1.583	16.77	2.583	6.05	3.58	4.04
0.667	6.36	1.667	16.77	2.667	6.05	3.67	4.04
0.750	7.99	1.750	12.41	2.750	5.56	3.75	3.84
0.833	7.99	1.833	12.41	2.833	5.56	3.83	3.84
0.917	11.21	1.917	10.04	2.917	5.15	3.92	3.66
1.000	11.21	2.000	10.04	3.000	5.15	4.00	3.66

Unit Hyd Qpeak (cms)= 0.743

PEAK FLOW (cms)= 0.124 (i)
 TIME TO PEAK (hrs)= 1.500
 RUNOFF VOLUME (mm)= 12.337
 TOTAL RAINFALL (mm)= 51.682
 RUNOFF COEFFICIENT = 0.239

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR( 0050) | OVERFLOW IS OFF
| IN= 2---> OUT= 1 |
| DT= 5.0 min |
-----
| OUTFLOW STORAGE | OUTFLOW STORAGE
| (cms) (ha.m.) | (cms) (ha.m.)
|
| **** WARNING : FIRST OUTFLOW IS NOT ZERO.
| 0.0016 0.0000 | 1.0000 0.0450
| 0.0016 0.0449 | 0.0000 0.0000
|
| AREA QPEAK TPEAK R.V.
| (ha) (cms) (hrs) (mm)
|
| INFLOW : ID= 2 ( 0202) 3.500 0.124 1.50 12.34
| OUTFLOW: ID= 1 ( 0050) 3.500 0.002 1.08 12.34

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 1.26
 TIME SHIFT OF PEAK FLOW (min)=-25.00
 MAXIMUM STORAGE USED (ha.m.)= 0.0412

CALIB			
STANDHYD (0204)	Area (ha)=	1.39	
ID= 1 DT= 5.0 min	Total Imp(%)=	20.00	Dir. Conn.(%)= 1.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	0.28	1.11
Dep. Storage	(mm)=	2.00	2.00
Average Slope	(%)=	1.50	2.00
Length	(m)=	20.00	25.00
Mannings n	=	0.013	0.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	4.14	1.083	22.67	2.083	8.53	3.08	4.81
0.167	4.14	1.167	22.67	2.167	8.53	3.17	4.81
0.250	4.65	1.250	115.37	2.250	7.46	3.25	4.51
0.333	4.65	1.333	115.37	2.333	7.46	3.33	4.51
0.417	5.35	1.417	28.60	2.417	6.67	3.42	4.26
0.500	5.35	1.500	28.60	2.500	6.67	3.50	4.26
0.583	6.36	1.583	16.77	2.583	6.05	3.58	4.04
0.667	6.36	1.667	16.77	2.667	6.05	3.67	4.04
0.750	7.99	1.750	12.41	2.750	5.56	3.75	3.84
0.833	7.99	1.833	12.41	2.833	5.56	3.83	3.84
0.917	11.21	1.917	10.04	2.917	5.15	3.92	3.66
1.000	11.21	2.000	10.04	3.000	5.15	4.00	3.66

Max.Eff.Inten.(mm/hr)=	115.37	32.49
over (min)	5.00	10.00
Storage Coeff. (min)=	0.81 (ii)	9.16 (ii)
Unit Hyd. Tpeak (min)=	5.00	10.00
Unit Hyd. peak (cms)=	0.34	0.12

TOTALS

PEAK FLOW (cms)=	0.00	0.07	0.067 (iii)
TIME TO PEAK (hrs)=	1.33	1.42	1.42
RUNOFF VOLUME (mm)=	49.68	13.83	14.18
TOTAL RAINFALL (mm)=	51.68	51.68	51.68
RUNOFF COEFFICIENT =	0.96	0.27	0.27

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 61.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR( 0051) | OVERFLOW IS OFF
| IN= 2---> OUT= 1 |
| DT= 5.0 min      |
-----
      OUTFLOW   STORAGE | OUTFLOW   STORAGE
      (cms)     (ha.m.) | (cms)     (ha.m.)
**** WARNING : FIRST OUTFLOW IS NOT ZERO.
      0.0010    0.0000 | 1.0000    0.0278
      0.0010    0.0277 | 0.0000    0.0000

                AREA   QPEAK   TPEAK   R.V.
                (ha)   (cms)   (hrs)   (mm)
INFLOW : ID= 2 ( 0204) 1.390   0.067   1.42   14.18
OUTFLOW: ID= 1 ( 0051) 1.390   0.001   0.83   14.19

                PEAK FLOW REDUCTION [Qout/Qin](%)= 1.42
                TIME SHIFT OF PEAK FLOW (min)=-35.00
                MAXIMUM STORAGE USED (ha.m.)= 0.0184
  
```

```

-----
| ADD HYD ( 0001) |
| 1 + 2 = 3       |
-----
      AREA   QPEAK   TPEAK   R.V.
      (ha)   (cms)   (hrs)   (mm)
      ID1= 1 ( 0201): 12.44  0.174   1.83   8.40
+ ID2= 2 ( 0203):   0.07  0.003   1.33  10.15
=====
      ID = 3 ( 0001): 12.51  0.175   1.83   8.41
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0001) |
| 3 + 2 = 1       |
-----
      AREA   QPEAK   TPEAK   R.V.
      (ha)   (cms)   (hrs)   (mm)
      ID1= 3 ( 0001): 12.51  0.175   1.83   8.41
+ ID2= 2 ( 0050):   3.50  0.002   1.08  12.34
=====
      ID = 1 ( 0001): 16.01  0.177   1.83   9.27
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0001)				
1 + 2 = 3				
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0001):	16.01	0.177	1.83	9.27
+ ID2= 2 (0051):	1.39	0.001	0.83	14.19
=====				
ID = 3 (0001):	17.40	0.178	1.83	9.66

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB			
NASHYD (0205)			
ID= 1 DT= 5.0 min	Area (ha)=	0.83	Curve Number (CN)= 65.9
	Ia (mm)=	4.60	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.14	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	4.14	1.083	22.67	2.083	8.53	3.08	4.81
0.167	4.14	1.167	22.67	2.167	8.53	3.17	4.81
0.250	4.65	1.250	115.37	2.250	7.46	3.25	4.51
0.333	4.65	1.333	115.37	2.333	7.46	3.33	4.51
0.417	5.35	1.417	28.60	2.417	6.67	3.42	4.26
0.500	5.35	1.500	28.60	2.500	6.67	3.50	4.26
0.583	6.36	1.583	16.77	2.583	6.05	3.58	4.04
0.667	6.36	1.667	16.77	2.667	6.05	3.67	4.04
0.750	7.99	1.750	12.41	2.750	5.56	3.75	3.84
0.833	7.99	1.833	12.41	2.833	5.56	3.83	3.84
0.917	11.21	1.917	10.04	2.917	5.15	3.92	3.66
1.000	11.21	2.000	10.04	3.000	5.15	4.00	3.66

Unit Hyd Qpeak (cms)= 0.226

PEAK FLOW (cms)= 0.034 (i)

TIME TO PEAK (hrs)= 1.417

RUNOFF VOLUME (mm)= 12.324

TOTAL RAINFALL (mm)= 51.682

RUNOFF COEFFICIENT = 0.238

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR( 0052) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min      |
-----

```

OVERFLOW IS OFF

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
0.0005	0.0000	1.0000	0.0156
0.0005	0.0155	0.0000	0.0000

**** WARNING : FIRST OUTFLOW IS NOT ZERO.

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0205)	0.830	0.034	1.42	12.32
OUTFLOW: ID= 1 (0052)	0.830	0.001	1.08	12.33

PEAK FLOW REDUCTION [Qout/Qin](%)= 1.57
 TIME SHIFT OF PEAK FLOW (min)=-20.00
 MAXIMUM STORAGE USED (ha.m.)= 0.0096

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-----
| CALIB          |
| NASHYD ( 0206) |
| ID= 1 DT= 5.0 min |
-----

```

Area (ha)= 2.15 Curve Number (CN)= 58.4
 Ia (mm)= 7.15 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 0.12

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.083	4.14	1.083	22.67	2.083	8.53	3.08	4.81
0.167	4.14	1.167	22.67	2.167	8.53	3.17	4.81
0.250	4.65	1.250	115.37	2.250	7.46	3.25	4.51
0.333	4.65	1.333	115.37	2.333	7.46	3.33	4.51
0.417	5.35	1.417	28.60	2.417	6.67	3.42	4.26
0.500	5.35	1.500	28.60	2.500	6.67	3.50	4.26
0.583	6.36	1.583	16.77	2.583	6.05	3.58	4.04
0.667	6.36	1.667	16.77	2.667	6.05	3.67	4.04
0.750	7.99	1.750	12.41	2.750	5.56	3.75	3.84
0.833	7.99	1.833	12.41	2.833	5.56	3.83	3.84
0.917	11.21	1.917	10.04	2.917	5.15	3.92	3.66
1.000	11.21	2.000	10.04	3.000	5.15	4.00	3.66

Unit Hyd Qpeak (cms)= 0.684
 PEAK FLOW (cms)= 0.062 (i)
 TIME TO PEAK (hrs)= 1.417
 RUNOFF VOLUME (mm)= 8.678

TOTAL RAINFALL (mm)= 51.682
 RUNOFF COEFFICIENT = 0.168

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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```

ADD HYD (0002)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0206):	2.15	0.062	1.42	8.68
+ ID2= 2 (0052):	0.83	0.001	1.08	12.33
=====				
ID = 3 (0002):	2.98	0.063	1.42	9.69

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

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V  V  I  SSSSS  U  U  A  L          (v 6.2.2005)
V  V  I  SS    U  U  A  A  L
V  V  I  SS    U  U  AAAAA  L
V  V  I  SS    U  U  A  A  L
  VV   I  SSSSS  UUUUU  A  A  LLLLL

```

```

000  TTTTT  TTTTT  H  H  Y  Y  M  M  000  TM
O  O  T    T  H  H  Y  Y  MM MM  O  O
O  O  T    T  H  H  Y  M  M  O  O
000  T    T  H  H  Y  M  M  000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\V02\voin.dat

Output filename:

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 25-5bc7-4f3a-908e-a89f55dbd791\scenar

Summary filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\c7ca6125-5bc7-4f3a-908e-a89f55dbd791\scenar

DATE: 06/29/2022

TIME: 12:14:26

USER:

COMMENTS: _____

** SIMULATION : 04 - 25yr Chicago **

| CHICAGO STORM |
Ptotal= 61.16 mm

IDF curve parameters: A= 786.108
B= 1.500
C= 0.718

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
Storm time step = 10.00 min
Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.17	4.92	1.17	26.84	2.17	10.11	3.17	5.70
0.33	5.52	1.33	136.11	2.33	8.85	3.33	5.36
0.50	6.35	1.50	33.84	2.50	7.91	3.50	5.05
0.67	7.54	1.67	19.87	2.67	7.18	3.67	4.79
0.83	9.47	1.83	14.70	2.83	6.60	3.83	4.56
1.00	13.29	2.00	11.90	3.00	6.11	4.00	4.35

| CALIB |
| NASHYD (0201) |
ID= 1 DT= 5.0 min

Area (ha)= 12.44 Curve Number (CN)= 58.1
Ia (mm)= 8.04 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 0.39

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	4.92	1.083	26.84	2.083	10.11	3.08	5.70
0.167	4.92	1.167	26.84	2.167	10.11	3.17	5.70
0.250	5.52	1.250	136.11	2.250	8.85	3.25	5.36
0.333	5.52	1.333	136.11	2.333	8.85	3.33	5.36
0.417	6.35	1.417	33.84	2.417	7.91	3.42	5.05
0.500	6.35	1.500	33.84	2.500	7.91	3.50	5.05
0.583	7.54	1.583	19.87	2.583	7.18	3.58	4.79
0.667	7.54	1.667	19.87	2.667	7.18	3.67	4.79
0.750	9.47	1.750	14.70	2.750	6.60	3.75	4.56
0.833	9.47	1.833	14.70	2.833	6.60	3.83	4.56
0.917	13.29	1.917	11.90	2.917	6.11	3.92	4.35
1.000	13.29	2.000	11.90	3.000	6.11	4.00	4.35

Unit Hyd Qpeak (cms)= 1.218

PEAK FLOW (cms)= 0.254 (i)
 TIME TO PEAK (hrs)= 1.750
 RUNOFF VOLUME (mm)= 11.939
 TOTAL RAINFALL (mm)= 61.157
 RUNOFF COEFFICIENT = 0.195

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
NASHYD (0203)	Area (ha)= 0.07	Curve Number (CN)= 61.0	
ID= 1 DT= 5.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= 0.10		

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	4.92	1.083	26.84	2.083	10.11	3.08	5.70
0.167	4.92	1.167	26.84	2.167	10.11	3.17	5.70
0.250	5.52	1.250	136.11	2.250	8.85	3.25	5.36
0.333	5.52	1.333	136.11	2.333	8.85	3.33	5.36
0.417	6.35	1.417	33.84	2.417	7.91	3.42	5.05
0.500	6.35	1.500	33.84	2.500	7.91	3.50	5.05
0.583	7.54	1.583	19.87	2.583	7.18	3.58	4.79
0.667	7.54	1.667	19.87	2.667	7.18	3.67	4.79
0.750	9.47	1.750	14.70	2.750	6.60	3.75	4.56
0.833	9.47	1.833	14.70	2.833	6.60	3.83	4.56
0.917	13.29	1.917	11.90	2.917	6.11	3.92	4.35
1.000	13.29	2.000	11.90	3.000	6.11	4.00	4.35

Unit Hyd Qpeak (cms)= 0.027

PEAK FLOW (cms)= 0.004 (i)
TIME TO PEAK (hrs)= 1.333
RUNOFF VOLUME (mm)= 14.051
TOTAL RAINFALL (mm)= 61.157
RUNOFF COEFFICIENT = 0.230

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB |
| NASHYD (0202) | Area (ha)= 3.50 Curve Number (CN)= 65.8
| ID= 1 DT= 5.0 min | Ia (mm)= 4.61 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= 0.18

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	4.92	1.083	26.84	2.083	10.11	3.08	5.70
0.167	4.92	1.167	26.84	2.167	10.11	3.17	5.70
0.250	5.52	1.250	136.11	2.250	8.85	3.25	5.36
0.333	5.52	1.333	136.11	2.333	8.85	3.33	5.36
0.417	6.35	1.417	33.84	2.417	7.91	3.42	5.05
0.500	6.35	1.500	33.84	2.500	7.91	3.50	5.05
0.583	7.54	1.583	19.87	2.583	7.18	3.58	4.79
0.667	7.54	1.667	19.87	2.667	7.18	3.67	4.79
0.750	9.47	1.750	14.70	2.750	6.60	3.75	4.56
0.833	9.47	1.833	14.70	2.833	6.60	3.83	4.56
0.917	13.29	1.917	11.90	2.917	6.11	3.92	4.35
1.000	13.29	2.000	11.90	3.000	6.11	4.00	4.35

Unit Hyd Qpeak (cms)= 0.743

PEAK FLOW (cms)= 0.173 (i)
TIME TO PEAK (hrs)= 1.500
RUNOFF VOLUME (mm)= 16.909
TOTAL RAINFALL (mm)= 61.157
RUNOFF COEFFICIENT = 0.276

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| RESERVOIR(0050) | OVERFLOW IS OFF

| IN= 2---> OUT= 1 |
 | DT= 5.0 min |

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
0.0016	0.0000	1.0000	0.0450
0.0016	0.0449	0.0000	0.0000

**** WARNING : FIRST OUTFLOW IS NOT ZERO.

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0202)	3.500	0.173	1.50	16.91
OUTFLOW: ID= 1 (0050)	3.500	0.045	2.92	16.91

PEAK FLOW REDUCTION [Qout/Qin](%)= 25.79
 TIME SHIFT OF PEAK FLOW (min)= 85.00
 MAXIMUM STORAGE USED (ha.m.)= 0.0451

 | CALIB |
 | STANDHYD (0204) |
 | ID= 1 DT= 5.0 min |

Area (ha)= 1.39
 Total Imp(%)= 20.00 Dir. Conn.(%)= 1.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.28	1.11
Dep. Storage (mm)=	2.00	2.00
Average Slope (%)=	1.50	2.00
Length (m)=	20.00	25.00
Mannings n =	0.013	0.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.083	4.92	1.083	26.84	2.083	10.11	3.08	5.70
0.167	4.92	1.167	26.84	2.167	10.11	3.17	5.70
0.250	5.52	1.250	136.11	2.250	8.85	3.25	5.36
0.333	5.52	1.333	136.11	2.333	8.85	3.33	5.36
0.417	6.35	1.417	33.84	2.417	7.91	3.42	5.05
0.500	6.35	1.500	33.84	2.500	7.91	3.50	5.05
0.583	7.54	1.583	19.87	2.583	7.18	3.58	4.79
0.667	7.54	1.667	19.87	2.667	7.18	3.67	4.79
0.750	9.47	1.750	14.70	2.750	6.60	3.75	4.56
0.833	9.47	1.833	14.70	2.833	6.60	3.83	4.56
0.917	13.29	1.917	11.90	2.917	6.11	3.92	4.35
1.000	13.29	2.000	11.90	3.000	6.11	4.00	4.35

Max.Eff.Inten.(mm/hr)= 136.11 44.30
 over (min) 5.00 10.00

Storage Coeff. (min)=	0.76 (ii)	8.13 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.34	0.13	
			TOTALS
PEAK FLOW (cms)=	0.01	0.09	0.096 (iii)
TIME TO PEAK (hrs)=	1.33	1.42	1.42
RUNOFF VOLUME (mm)=	59.16	18.58	18.98
TOTAL RAINFALL (mm)=	61.16	61.16	61.16
RUNOFF COEFFICIENT =	0.97	0.30	0.31

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
 ***** WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 61.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----
| RESERVOIR( 0051) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min      |
-----
```

OVERFLOW IS OFF

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
------------------	--------------------	------------------	--------------------

**** WARNING : FIRST OUTFLOW IS NOT ZERO.

0.0010	0.0000	1.0000	0.0278
0.0010	0.0277	0.0000	0.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0204)	1.390	0.096	1.42	18.98
OUTFLOW: ID= 1 (0051)	1.390	0.001	0.75	18.99

PEAK FLOW REDUCTION [Qout/Qin](%)= 1.00
 TIME SHIFT OF PEAK FLOW (min)=-40.00
 MAXIMUM STORAGE USED (ha.m.)= 0.0250

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-----
| ADD HYD ( 0001) |
| 1 + 2 = 3      |
-----
```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0201):	12.44	0.254	1.75	11.94
+ ID2= 2 (0203):	0.07	0.004	1.33	14.05
=====				
ID = 3 (0001):	12.51	0.255	1.75	11.95

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0001)		AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1		(ha)	(cms)	(hrs)	(mm)
ID1= 3 (0001):		12.51	0.255	1.75	11.95
+ ID2= 2 (0050):		3.50	0.045	2.92	16.91
=====					
ID = 1 (0001):		16.01	0.257	1.75	13.04

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0001)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0001):		16.01	0.257	1.75	13.04
+ ID2= 2 (0051):		1.39	0.001	0.75	18.99
=====					
ID = 3 (0001):		17.40	0.258	1.75	13.51

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB		Area	(ha)=	0.83	Curve Number	(CN)=	65.9
NASHYD (0205)		Ia	(mm)=	4.60	# of Linear Res.(N)=	3.00	
ID= 1 DT= 5.0 min		U.H. Tp(hrs)=		0.14			

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	4.92	1.083	26.84	2.083	10.11	3.08	5.70
0.167	4.92	1.167	26.84	2.167	10.11	3.17	5.70
0.250	5.52	1.250	136.11	2.250	8.85	3.25	5.36
0.333	5.52	1.333	136.11	2.333	8.85	3.33	5.36
0.417	6.35	1.417	33.84	2.417	7.91	3.42	5.05
0.500	6.35	1.500	33.84	2.500	7.91	3.50	5.05
0.583	7.54	1.583	19.87	2.583	7.18	3.58	4.79
0.667	7.54	1.667	19.87	2.667	7.18	3.67	4.79
0.750	9.47	1.750	14.70	2.750	6.60	3.75	4.56
0.833	9.47	1.833	14.70	2.833	6.60	3.83	4.56
0.917	13.29	1.917	11.90	2.917	6.11	3.92	4.35
1.000	13.29	2.000	11.90	3.000	6.11	4.00	4.35

Unit Hyd Qpeak (cms)= 0.226

PEAK FLOW (cms)= 0.048 (i)
TIME TO PEAK (hrs)= 1.417
RUNOFF VOLUME (mm)= 16.888
TOTAL RAINFALL (mm)= 61.157
RUNOFF COEFFICIENT = 0.276

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----  
-----  
| RESERVOIR( 0052) | OVERFLOW IS OFF  
| IN= 2---> OUT= 1 |  
| DT= 5.0 min |  
-----  
***** WARNING : FIRST OUTFLOW IS NOT ZERO.  
          OUTFLOW STORAGE | OUTFLOW STORAGE  
          (cms) (ha.m.) | (cms) (ha.m.)  
          0.0005 0.0000 | 1.0000 0.0156  
          0.0005 0.0155 | 0.0000 0.0000  
  
          AREA QPEAK TPEAK R.V.  
          (ha) (cms) (hrs) (mm)  
INFLOW : ID= 2 ( 0205) 0.830 0.048 1.42 16.89  
OUTFLOW: ID= 1 ( 0052) 0.830 0.001 1.00 16.89  
  
PEAK FLOW REDUCTION [Qout/Qin](%)= 1.12  
TIME SHIFT OF PEAK FLOW (min)=-25.00  
MAXIMUM STORAGE USED (ha.m.)= 0.0133  
-----
```

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-----  
-----  
| CALIB |  
| NASHYD ( 0206) | Area (ha)= 2.15 Curve Number (CN)= 58.4  
| ID= 1 DT= 5.0 min | Ia (mm)= 7.15 # of Linear Res.(N)= 3.00  
-----  
U.H. Tp(hrs)= 0.12
```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```
----- TRANSFORMED HYETOGRAPH -----  
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN  
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr  
0.083 4.92 | 1.083 26.84 | 2.083 10.11 | 3.08 5.70  
0.167 4.92 | 1.167 26.84 | 2.167 10.11 | 3.17 5.70  
0.250 5.52 | 1.250 136.11 | 2.250 8.85 | 3.25 5.36  
0.333 5.52 | 1.333 136.11 | 2.333 8.85 | 3.33 5.36  
0.417 6.35 | 1.417 33.84 | 2.417 7.91 | 3.42 5.05  
0.500 6.35 | 1.500 33.84 | 2.500 7.91 | 3.50 5.05  
0.583 7.54 | 1.583 19.87 | 2.583 7.18 | 3.58 4.79
```

0.667	7.54	1.667	19.87	2.667	7.18	3.67	4.79
0.750	9.47	1.750	14.70	2.750	6.60	3.75	4.56
0.833	9.47	1.833	14.70	2.833	6.60	3.83	4.56
0.917	13.29	1.917	11.90	2.917	6.11	3.92	4.35
1.000	13.29	2.000	11.90	3.000	6.11	4.00	4.35

Unit Hyd Qpeak (cms)= 0.684

PEAK FLOW (cms)= 0.091 (i)

TIME TO PEAK (hrs)= 1.417

RUNOFF VOLUME (mm)= 12.249

TOTAL RAINFALL (mm)= 61.157

RUNOFF COEFFICIENT = 0.200

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 0002) |
| 1 + 2 = 3 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0206):	2.15	0.091	1.42	12.25
+ ID2= 2 (0052):	0.83	0.001	1.00	16.89
=====				
ID = 3 (0002):	2.98	0.091	1.42	13.54

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

V V I SSSSS U U A L (v 6.2.2005)
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

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000 TTTTT TTTTT H H Y Y M M 000 TM
O O T T H H Y Y MM MM O O
O O T T H H Y M M O O
000 T T H H Y M M 000

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\V02\voin.dat

Output filename:

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Summary filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\6eb48f37-ef04-465d-8581-1aa731dd2087\scenar

DATE: 06/29/2022

TIME: 12:14:26

USER:

COMMENTS: _____

** SIMULATION : 05 - 50yr Chicago **

| CHICAGO STORM |
Ptotal= 68.33 mm

IDF curve parameters: A= 878.307
B= 1.500
C= 0.718

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
Storm time step = 10.00 min
Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.17	5.49	1.17	29.99	2.17	11.30	3.17	6.37
0.33	6.17	1.33	152.08	2.33	9.89	3.33	5.98
0.50	7.09	1.50	37.81	2.50	8.84	3.50	5.65
0.67	8.43	1.67	22.20	2.67	8.03	3.67	5.35
0.83	10.58	1.83	16.43	2.83	7.37	3.83	5.09
1.00	14.85	2.00	13.30	3.00	6.83	4.00	4.86

| CALIB |
| NASHYD (0201) |
| ID= 1 DT= 5.0 min |

Area (ha)= 12.44 Curve Number (CN)= 58.1
Ia (mm)= 8.04 # of Linear Res.(N)= 3.00

----- U.H. Tp(hrs)= 0.39

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	5.49	1.083	29.99	2.083	11.30	3.08	6.37
0.167	5.49	1.167	29.99	2.167	11.30	3.17	6.37
0.250	6.17	1.250	152.08	2.250	9.89	3.25	5.98
0.333	6.17	1.333	152.08	2.333	9.89	3.33	5.98
0.417	7.09	1.417	37.81	2.417	8.84	3.42	5.65
0.500	7.09	1.500	37.81	2.500	8.84	3.50	5.65
0.583	8.43	1.583	22.20	2.583	8.03	3.58	5.35
0.667	8.43	1.667	22.20	2.667	8.03	3.67	5.35
0.750	10.58	1.750	16.43	2.750	7.37	3.75	5.09
0.833	10.58	1.833	16.43	2.833	7.37	3.83	5.09
0.917	14.85	1.917	13.30	2.917	6.83	3.92	4.86
1.000	14.85	2.000	13.30	3.000	6.83	4.00	4.86

Unit Hyd Qpeak (cms)= 1.218

PEAK FLOW (cms)= 0.324 (i)

TIME TO PEAK (hrs)= 1.750

RUNOFF VOLUME (mm)= 14.928

TOTAL RAINFALL (mm)= 68.330

RUNOFF COEFFICIENT = 0.218

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)= 0.07	Curve Number (CN)= 61.0
NASHYD (0203)	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
ID= 1 DT= 5.0 min	U.H. Tp(hrs)= 0.10	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	5.49	1.083	29.99	2.083	11.30	3.08	6.37
0.167	5.49	1.167	29.99	2.167	11.30	3.17	6.37
0.250	6.17	1.250	152.08	2.250	9.89	3.25	5.98
0.333	6.17	1.333	152.08	2.333	9.89	3.33	5.98
0.417	7.09	1.417	37.81	2.417	8.84	3.42	5.65
0.500	7.09	1.500	37.81	2.500	8.84	3.50	5.65

0.583	8.43	1.583	22.20	2.583	8.03	3.58	5.35
0.667	8.43	1.667	22.20	2.667	8.03	3.67	5.35
0.750	10.58	1.750	16.43	2.750	7.37	3.75	5.09
0.833	10.58	1.833	16.43	2.833	7.37	3.83	5.09
0.917	14.85	1.917	13.30	2.917	6.83	3.92	4.86
1.000	14.85	2.000	13.30	3.000	6.83	4.00	4.86

Unit Hyd Qpeak (cms)= 0.027

PEAK FLOW (cms)= 0.005 (i)
 TIME TO PEAK (hrs)= 1.333
 RUNOFF VOLUME (mm)= 17.301
 TOTAL RAINFALL (mm)= 68.330
 RUNOFF COEFFICIENT = 0.253

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD ( 0202) | Area (ha)= 3.50 Curve Number (CN)= 65.8
| ID= 1 DT= 5.0 min | Ia (mm)= 4.61 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.18

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	5.49	1.083	29.99	2.083	11.30	3.08	6.37
0.167	5.49	1.167	29.99	2.167	11.30	3.17	6.37
0.250	6.17	1.250	152.08	2.250	9.89	3.25	5.98
0.333	6.17	1.333	152.08	2.333	9.89	3.33	5.98
0.417	7.09	1.417	37.81	2.417	8.84	3.42	5.65
0.500	7.09	1.500	37.81	2.500	8.84	3.50	5.65
0.583	8.43	1.583	22.20	2.583	8.03	3.58	5.35
0.667	8.43	1.667	22.20	2.667	8.03	3.67	5.35
0.750	10.58	1.750	16.43	2.750	7.37	3.75	5.09
0.833	10.58	1.833	16.43	2.833	7.37	3.83	5.09
0.917	14.85	1.917	13.30	2.917	6.83	3.92	4.86
1.000	14.85	2.000	13.30	3.000	6.83	4.00	4.86

Unit Hyd Qpeak (cms)= 0.743

PEAK FLOW (cms)= 0.214 (i)
 TIME TO PEAK (hrs)= 1.500
 RUNOFF VOLUME (mm)= 20.684
 TOTAL RAINFALL (mm)= 68.330
 RUNOFF COEFFICIENT = 0.303

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR( 0050) | OVERFLOW IS OFF
| IN= 2---> OUT= 1 |
| DT= 5.0 min      |
-----
      OUTFLOW   STORAGE | OUTFLOW   STORAGE
      (cms)     (ha.m.) | (cms)     (ha.m.)
**** WARNING : FIRST OUTFLOW IS NOT ZERO.
      0.0016   0.0000 | 1.0000    0.0450
      0.0016   0.0449 | 0.0000    0.0000

              AREA   QPEAK   TPEAK   R.V.
              (ha)   (cms)   (hrs)   (mm)
INFLOW : ID= 2 ( 0202) 3.500   0.214   1.50    20.68
OUTFLOW: ID= 1 ( 0050) 3.500   0.099   2.25    20.69

      PEAK FLOW REDUCTION [Qout/Qin](%)= 46.17
      TIME SHIFT OF PEAK FLOW (min)= 45.00
      MAXIMUM STORAGE USED (ha.m.)= 0.0468
  
```

```

-----
| CALIB
| STANDHYD ( 0204) | Area (ha)= 1.39
| ID= 1 DT= 5.0 min | Total Imp(%)= 20.00 Dir. Conn.(%)= 1.00
-----
  
```

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.28	1.11
Dep. Storage (mm)=	2.00	2.00
Average Slope (%)=	1.50	2.00
Length (m)=	20.00	25.00
Mannings n =	0.013	0.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	5.49	1.083	29.99	2.083	11.30	3.08	6.37
0.167	5.49	1.167	29.99	2.167	11.30	3.17	6.37
0.250	6.17	1.250	152.08	2.250	9.89	3.25	5.98
0.333	6.17	1.333	152.08	2.333	9.89	3.33	5.98
0.417	7.09	1.417	37.81	2.417	8.84	3.42	5.65
0.500	7.09	1.500	37.81	2.500	8.84	3.50	5.65
0.583	8.43	1.583	22.20	2.583	8.03	3.58	5.35
0.667	8.43	1.667	22.20	2.667	8.03	3.67	5.35
0.750	10.58	1.750	16.43	2.750	7.37	3.75	5.09

0.833	10.58	1.833	16.43	2.833	7.37	3.83	5.09
0.917	14.85	1.917	13.30	2.917	6.83	3.92	4.86
1.000	14.85	2.000	13.30	3.000	6.83	4.00	4.86

Max.Eff.Inten.(mm/hr)=	152.08	54.23	
over (min)	5.00	10.00	
Storage Coeff. (min)=	0.73 (ii)	7.53 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.34	0.13	
			TOTALS
PEAK FLOW (cms)=	0.01	0.12	0.121 (iii)
TIME TO PEAK (hrs)=	1.33	1.42	1.42
RUNOFF VOLUME (mm)=	66.33	22.49	22.92
TOTAL RAINFALL (mm)=	68.33	68.33	68.33
RUNOFF COEFFICIENT =	0.97	0.33	0.34

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
 ***** WARNING:FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
 YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 61.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR( 0051) | OVERFLOW IS OFF
| IN= 2---> OUT= 1 |
| DT= 5.0 min      |
-----
| OUTFLOW          | STORAGE          | OUTFLOW          | STORAGE          |
| (cms)            | (ha.m.)         | (cms)            | (ha.m.)         |
| **** WARNING :  | FIRST OUTFLOW IS NOT ZERO.
| 0.0010          | 0.0000          | 1.0000          | 0.0278          |
| 0.0010          | 0.0277          | 0.0000          | 0.0000          |
  
```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0204)	1.390	0.121	1.42	22.92
OUTFLOW: ID= 1 (0051)	1.390	0.023	3.50	22.93

PEAK FLOW REDUCTION [Qout/Qin](%)= 19.31
 TIME SHIFT OF PEAK FLOW (min)=125.00
 MAXIMUM STORAGE USED (ha.m.)= 0.0279

```

-----
| ADD HYD ( 0001) |
| 1 + 2 = 3      |
| AREA           | QPEAK           | TPEAK           | R.V.           |
  
```

	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0201):	12.44	0.324	1.75	14.93
+ ID2= 2 (0203):	0.07	0.005	1.33	17.30
=====				
ID = 3 (0001):	12.51	0.325	1.75	14.94

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0001)				
3 + 2 = 1				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 (0001):	12.51	0.325	1.75	14.94
+ ID2= 2 (0050):	3.50	0.099	2.25	20.69
=====				
ID = 1 (0001):	16.01	0.333	2.25	16.20

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0001)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0001):	16.01	0.333	2.25	16.20
+ ID2= 2 (0051):	1.39	0.023	3.50	22.93
=====				
ID = 3 (0001):	17.40	0.334	2.25	16.73

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB				
NASHYD (0205)				
ID= 1 DT= 5.0 min				
Area	(ha)=	0.83	Curve Number	(CN)= 65.9
Ia	(mm)=	4.60	# of Linear Res.(N)=	3.00
U.H. Tp	(hrs)=	0.14		

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	5.49	1.083	29.99	2.083	11.30	3.08	6.37
0.167	5.49	1.167	29.99	2.167	11.30	3.17	6.37
0.250	6.17	1.250	152.08	2.250	9.89	3.25	5.98
0.333	6.17	1.333	152.08	2.333	9.89	3.33	5.98
0.417	7.09	1.417	37.81	2.417	8.84	3.42	5.65
0.500	7.09	1.500	37.81	2.500	8.84	3.50	5.65

0.583	8.43	1.583	22.20	2.583	8.03	3.58	5.35
0.667	8.43	1.667	22.20	2.667	8.03	3.67	5.35
0.750	10.58	1.750	16.43	2.750	7.37	3.75	5.09
0.833	10.58	1.833	16.43	2.833	7.37	3.83	5.09
0.917	14.85	1.917	13.30	2.917	6.83	3.92	4.86
1.000	14.85	2.000	13.30	3.000	6.83	4.00	4.86

Unit Hyd Qpeak (cms)= 0.226

PEAK FLOW (cms)= 0.060 (i)
 TIME TO PEAK (hrs)= 1.417
 RUNOFF VOLUME (mm)= 20.655
 TOTAL RAINFALL (mm)= 68.330
 RUNOFF COEFFICIENT = 0.302

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR( 0052) | OVERFLOW IS OFF
| IN= 2----> OUT= 1 |
| DT= 5.0 min      |
-----
| OUTFLOW          | STORAGE          | OUTFLOW          | STORAGE          |
| (cms)            | (ha.m.)         | (cms)            | (ha.m.)         |
| 0.0005          | 0.0000          | 1.0000          | 0.0156          |
| 0.0005          | 0.0155          | 0.0000          | 0.0000          |
|
| AREA            | QPEAK           | TPEAK           | R.V.            |
| (ha)           | (cms)          | (hrs)          | (mm)           |
| INFLOW : ID= 2 ( 0205) | 0.830         | 0.060         | 1.42           | 20.65
| OUTFLOW: ID= 1 ( 0052) | 0.830         | 0.009         | 3.75           | 20.66

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 15.25
 TIME SHIFT OF PEAK FLOW (min)=140.00
 MAXIMUM STORAGE USED (ha.m.)= 0.0156

```

-----
| CALIB
| NASHYD ( 0206) | Area (ha)= 2.15 Curve Number (CN)= 58.4
| ID= 1 DT= 5.0 min | Ia (mm)= 7.15 # of Linear Res.(N)= 3.00
|
| U.H. Tp(hrs)= 0.12

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
| TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN |
| hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr |
| 0.083 5.49 | 1.083 29.99 | 2.083 11.30 | 3.08 6.37 |

```

0.167	5.49	1.167	29.99	2.167	11.30	3.17	6.37
0.250	6.17	1.250	152.08	2.250	9.89	3.25	5.98
0.333	6.17	1.333	152.08	2.333	9.89	3.33	5.98
0.417	7.09	1.417	37.81	2.417	8.84	3.42	5.65
0.500	7.09	1.500	37.81	2.500	8.84	3.50	5.65
0.583	8.43	1.583	22.20	2.583	8.03	3.58	5.35
0.667	8.43	1.667	22.20	2.667	8.03	3.67	5.35
0.750	10.58	1.750	16.43	2.750	7.37	3.75	5.09
0.833	10.58	1.833	16.43	2.833	7.37	3.83	5.09
0.917	14.85	1.917	13.30	2.917	6.83	3.92	4.86
1.000	14.85	2.000	13.30	3.000	6.83	4.00	4.86

Unit Hyd Qpeak (cms)= 0.684

PEAK FLOW (cms)= 0.115 (i)
 TIME TO PEAK (hrs)= 1.417
 RUNOFF VOLUME (mm)= 15.253
 TOTAL RAINFALL (mm)= 68.330
 RUNOFF COEFFICIENT = 0.223

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0002)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0206):	2.15	0.115	1.42	15.25
+ ID2= 2 (0052):	0.83	0.009	3.75	20.66
=====				
ID = 3 (0002):	2.98	0.115	1.42	16.76

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

=====

```

V  V  I  SSSSS  U  U  A  L  (v 6.2.2005)
V  V  I  SS    U  U  A  A  L
V  V  I  SS    U  U  AAAAA  L
V  V  I  SS    U  U  A  A  L
  VV  I  SSSSS  UUUUU  A  A  LLLLL

  000  TTTTT  TTTTT  H  H  Y  Y  M  M  000  TM
  0  0  T  T  H  H  Y  Y  MM  MM  0  0
  0  0  T  T  H  H  Y  M  M  0  0
  000  T  T  H  H  Y  M  M  000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\V02\voin.dat

Output filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\e0b7d654-a50f-4785-b207-c6b7263eadaa\scenar

Summary filename:

C:\Users\bpond\AppData\Local\Civica\XH5\62082276-f617-4be2-807a-c20b5723c417\e0b7d654-a50f-4785-b207-c6b7263eadaa\scenar

DATE: 06/29/2022

TIME: 12:14:26

USER:

COMMENTS: _____

** SIMULATION : 06 - 100yr Chicago **

| CHICAGO STORM |
Ptotal= 75.17 mm

IDF curve parameters: A= 971.524
B= 1.500
C= 0.719

used in: INTENSITY = A / (t + B)^C

Duration of storm = 4.00 hrs
Storm time step = 10.00 min
Time to peak ratio = 0.33

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.17	6.02	1.17	32.97	2.17	12.40	3.17	6.99
0.33	6.77	1.33	167.81	2.33	10.86	3.33	6.56
0.50	7.78	1.50	41.59	2.50	9.70	3.50	6.19
0.67	9.24	1.67	24.40	2.67	8.81	3.67	5.87
0.83	11.62	1.83	18.04	2.83	8.08	3.83	5.58
1.00	16.31	2.00	14.60	3.00	7.49	4.00	5.33

```

-----
| CALIB |
| NASHYD ( 0201) | Area (ha)= 12.44 Curve Number (CN)= 58.1
| ID= 1 DT= 5.0 min | Ia (mm)= 8.04 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.39

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
0.083 6.02 | 1.083 32.97 | 2.083 12.40 | 3.08 6.99
0.167 6.02 | 1.167 32.97 | 2.167 12.40 | 3.17 6.99
0.250 6.77 | 1.250 167.81 | 2.250 10.86 | 3.25 6.56
0.333 6.77 | 1.333 167.81 | 2.333 10.86 | 3.33 6.56
0.417 7.78 | 1.417 41.59 | 2.417 9.70 | 3.42 6.19
0.500 7.78 | 1.500 41.59 | 2.500 9.70 | 3.50 6.19
0.583 9.24 | 1.583 24.40 | 2.583 8.81 | 3.58 5.87
0.667 9.24 | 1.667 24.40 | 2.667 8.81 | 3.67 5.87
0.750 11.62 | 1.750 18.04 | 2.750 8.08 | 3.75 5.58
0.833 11.62 | 1.833 18.04 | 2.833 8.08 | 3.83 5.58
0.917 16.31 | 1.917 14.60 | 2.917 7.49 | 3.92 5.33
1.000 16.31 | 2.000 14.60 | 3.000 7.49 | 4.00 5.33

```

Unit Hyd Qpeak (cms)= 1.218

PEAK FLOW (cms)= 0.397 (i)
 TIME TO PEAK (hrs)= 1.750
 RUNOFF VOLUME (mm)= 18.001
 TOTAL RAINFALL (mm)= 75.169
 RUNOFF COEFFICIENT = 0.239

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| NASHYD ( 0203) | Area (ha)= 0.07 Curve Number (CN)= 61.0
| ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.10

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr

```


0.083	6.02	1.083	32.97	2.083	12.40	3.08	6.99
0.167	6.02	1.167	32.97	2.167	12.40	3.17	6.99
0.250	6.77	1.250	167.81	2.250	10.86	3.25	6.56
0.333	6.77	1.333	167.81	2.333	10.86	3.33	6.56
0.417	7.78	1.417	41.59	2.417	9.70	3.42	6.19
0.500	7.78	1.500	41.59	2.500	9.70	3.50	6.19
0.583	9.24	1.583	24.40	2.583	8.81	3.58	5.87
0.667	9.24	1.667	24.40	2.667	8.81	3.67	5.87
0.750	11.62	1.750	18.04	2.750	8.08	3.75	5.58
0.833	11.62	1.833	18.04	2.833	8.08	3.83	5.58
0.917	16.31	1.917	14.60	2.917	7.49	3.92	5.33
1.000	16.31	2.000	14.60	3.000	7.49	4.00	5.33

Unit Hyd Qpeak (cms)= 0.027

PEAK FLOW (cms)= 0.006 (i)
 TIME TO PEAK (hrs)= 1.333
 RUNOFF VOLUME (mm)= 20.619
 TOTAL RAINFALL (mm)= 75.169
 RUNOFF COEFFICIENT = 0.274

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | CALIB |
 | NASHYD (0202) | Area (ha)= 3.50 Curve Number (CN)= 65.8
 | ID= 1 DT= 5.0 min | Ia (mm)= 4.61 # of Linear Res.(N)= 3.00
 ----- U.H. Tp(hrs)= 0.18

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	6.02	1.083	32.97	2.083	12.40	3.08	6.99
0.167	6.02	1.167	32.97	2.167	12.40	3.17	6.99
0.250	6.77	1.250	167.81	2.250	10.86	3.25	6.56
0.333	6.77	1.333	167.81	2.333	10.86	3.33	6.56
0.417	7.78	1.417	41.59	2.417	9.70	3.42	6.19
0.500	7.78	1.500	41.59	2.500	9.70	3.50	6.19
0.583	9.24	1.583	24.40	2.583	8.81	3.58	5.87
0.667	9.24	1.667	24.40	2.667	8.81	3.67	5.87
0.750	11.62	1.750	18.04	2.750	8.08	3.75	5.58
0.833	11.62	1.833	18.04	2.833	8.08	3.83	5.58
0.917	16.31	1.917	14.60	2.917	7.49	3.92	5.33
1.000	16.31	2.000	14.60	3.000	7.49	4.00	5.33

Unit Hyd Qpeak (cms)= 0.743

PEAK FLOW (cms)= 0.257 (i)
 TIME TO PEAK (hrs)= 1.500
 RUNOFF VOLUME (mm)= 24.506
 TOTAL RAINFALL (mm)= 75.169
 RUNOFF COEFFICIENT = 0.326

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| RESERVOIR( 0050) | OVERFLOW IS OFF
| IN= 2---> OUT= 1 |
| DT= 5.0 min      |
-----
      OUTFLOW   STORAGE | OUTFLOW   STORAGE
      (cms)     (ha.m.) | (cms)     (ha.m.)
**** WARNING : FIRST OUTFLOW IS NOT ZERO.
      0.0016    0.0000 | 1.0000    0.0450
      0.0016    0.0449 | 0.0000    0.0000

      AREA      QPEAK    TPEAK      R.V.
      (ha)      (cms)    (hrs)    (mm)
INFLOW : ID= 2 ( 0202) 3.500    0.257    1.50    24.51
OUTFLOW: ID= 1 ( 0050) 3.500    0.125    2.00    24.51

      PEAK FLOW REDUCTION [Qout/Qin](%)= 48.56
      TIME SHIFT OF PEAK FLOW (min)= 30.00
      MAXIMUM STORAGE USED (ha.m.)= 0.0454
  
```

```

-----
| CALIB
| STANDHYD ( 0204) | Area (ha)= 1.39
| ID= 1 DT= 5.0 min | Total Imp(%)= 20.00 Dir. Conn.(%)= 1.00
-----
  
```

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.28	1.11
Dep. Storage (mm)=	2.00	2.00
Average Slope (%)=	1.50	2.00
Length (m)=	20.00	25.00
Mannings n =	0.013	0.250

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
      TIME    RAIN | TIME    RAIN | TIME    RAIN | TIME    RAIN
      hrs    mm/hr | hrs    mm/hr | hrs    mm/hr | hrs    mm/hr
0.083    6.02 | 1.083   32.97 | 2.083   12.40 | 3.08    6.99
0.167    6.02 | 1.167   32.97 | 2.167   12.40 | 3.17    6.99
0.250    6.77 | 1.250  167.81 | 2.250   10.86 | 3.25    6.56
  
```

0.333	6.77	1.333	167.81	2.333	10.86	3.33	6.56
0.417	7.78	1.417	41.59	2.417	9.70	3.42	6.19
0.500	7.78	1.500	41.59	2.500	9.70	3.50	6.19
0.583	9.24	1.583	24.40	2.583	8.81	3.58	5.87
0.667	9.24	1.667	24.40	2.667	8.81	3.67	5.87
0.750	11.62	1.750	18.04	2.750	8.08	3.75	5.58
0.833	11.62	1.833	18.04	2.833	8.08	3.83	5.58
0.917	16.31	1.917	14.60	2.917	7.49	3.92	5.33
1.000	16.31	2.000	14.60	3.000	7.49	4.00	5.33

Max.Eff.Inten.(mm/hr)= 167.81 64.59
over (min) 5.00 10.00
Storage Coeff. (min)= 0.70 (ii) 7.04 (ii)
Unit Hyd. Tpeak (min)= 5.00 10.00
Unit Hyd. peak (cms)= 0.34 0.14

TOTALS

PEAK FLOW (cms)= 0.01 0.15 0.147 (iii)
TIME TO PEAK (hrs)= 1.33 1.42 1.42
RUNOFF VOLUME (mm)= 73.17 26.42 26.88
TOTAL RAINFALL (mm)= 75.17 75.17 75.17
RUNOFF COEFFICIENT = 0.97 0.35 0.36

***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
***** WARNING: FOR AREAS WITH IMPERVIOUS RATIOS BELOW 20%
YOU SHOULD CONSIDER SPLITTING THE AREA.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 61.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| RESERVOIR(0051) |
| IN= 2---> OUT= 1 |
| DT= 5.0 min |

OVERFLOW IS OFF

OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)

**** WARNING : FIRST OUTFLOW IS NOT ZERO.

0.0010 0.0000 | 1.0000 0.0278
0.0010 0.0277 | 0.0000 0.0000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 (0204)	1.390	0.147	1.42	26.88
OUTFLOW: ID= 1 (0051)	1.390	0.027	2.67	26.89

PEAK FLOW REDUCTION [Qout/Qin](%)= 18.23
TIME SHIFT OF PEAK FLOW (min)= 75.00
MAXIMUM STORAGE USED (ha.m.)= 0.0278

```

-----
| ADD HYD ( 0001) |
| 1 + 2 = 3 |
-----
          AREA      QPEAK      TPEAK      R.V.
          (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 0201):  12.44  0.397  1.75  18.00
+ ID2= 2 ( 0203):   0.07  0.006  1.33  20.62
=====
ID = 3 ( 0001):  12.51  0.399  1.75  18.02

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0001) |
| 3 + 2 = 1 |
-----
          AREA      QPEAK      TPEAK      R.V.
          (ha)      (cms)      (hrs)      (mm)
ID1= 3 ( 0001):  12.51  0.399  1.75  18.02
+ ID2= 2 ( 0050):   3.50  0.125  2.00  24.51
=====
ID = 1 ( 0001):  16.01  0.483  2.00  19.44

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0001) |
| 1 + 2 = 3 |
-----
          AREA      QPEAK      TPEAK      R.V.
          (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 0001):  16.01  0.483  2.00  19.44
+ ID2= 2 ( 0051):   1.39  0.027  2.67  26.89
=====
ID = 3 ( 0001):  17.40  0.484  2.00  20.03

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB
| NASHYD ( 0205) | Area (ha)= 0.83 Curve Number (CN)= 65.9
| ID= 1 DT= 5.0 min | Ia (mm)= 4.60 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= 0.14

```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

```

-----
          ----- TRANSFORMED HYETOGRAPH -----
TIME    RAIN | TIME    RAIN |'  TIME    RAIN | TIME    RAIN
  hrs   mm/hr |  hrs   mm/hr |'  hrs   mm/hr |  hrs   mm/hr

```


----- TRANSFORMED HYETOGRAPH -----

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.083	6.02	1.083	32.97	2.083	12.40	3.08	6.99
0.167	6.02	1.167	32.97	2.167	12.40	3.17	6.99
0.250	6.77	1.250	167.81	2.250	10.86	3.25	6.56
0.333	6.77	1.333	167.81	2.333	10.86	3.33	6.56
0.417	7.78	1.417	41.59	2.417	9.70	3.42	6.19
0.500	7.78	1.500	41.59	2.500	9.70	3.50	6.19
0.583	9.24	1.583	24.40	2.583	8.81	3.58	5.87
0.667	9.24	1.667	24.40	2.667	8.81	3.67	5.87
0.750	11.62	1.750	18.04	2.750	8.08	3.75	5.58
0.833	11.62	1.833	18.04	2.833	8.08	3.83	5.58
0.917	16.31	1.917	14.60	2.917	7.49	3.92	5.33
1.000	16.31	2.000	14.60	3.000	7.49	4.00	5.33

Unit Hyd Qpeak (cms)= 0.684

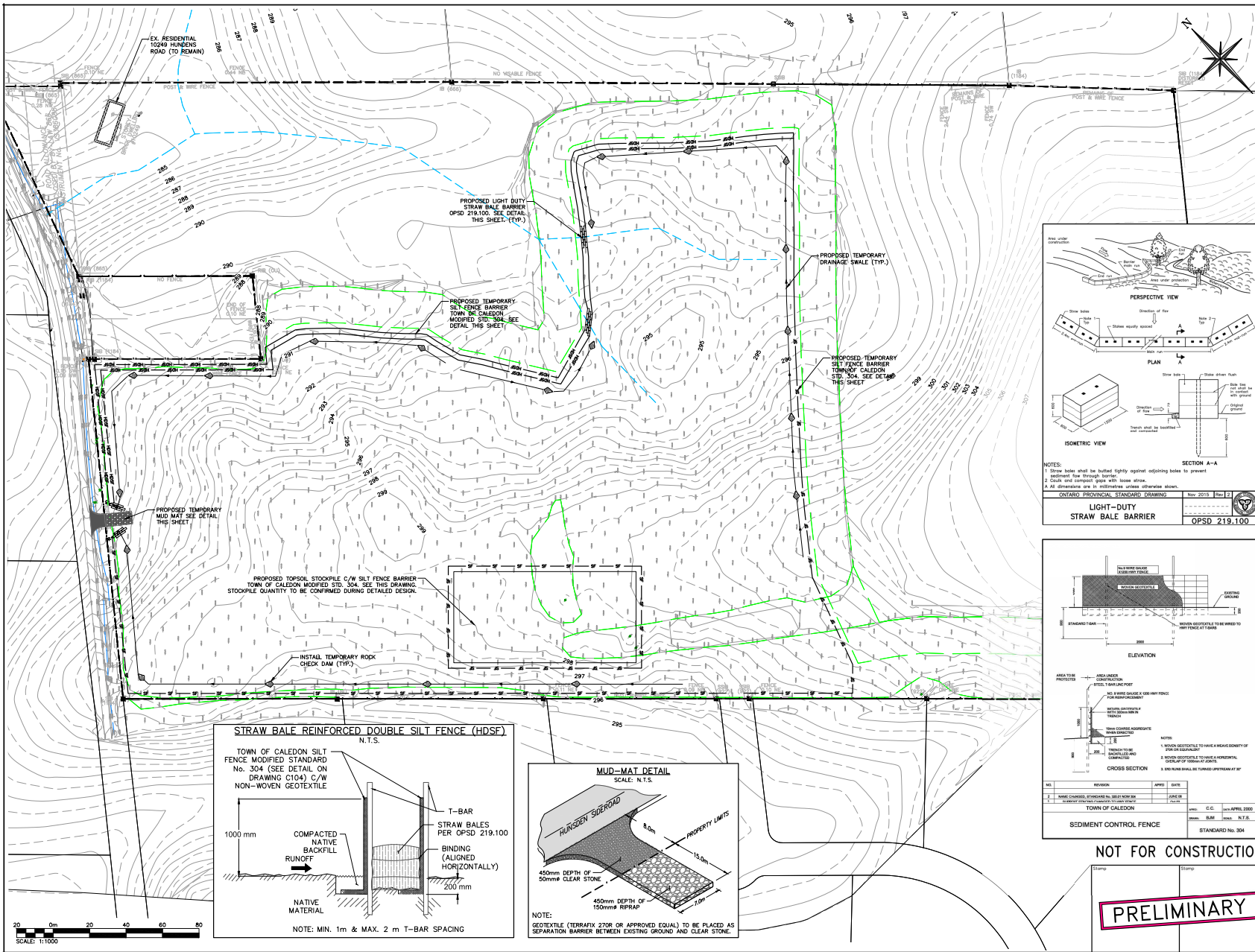
PEAK FLOW (cms)= 0.140 (i)
 TIME TO PEAK (hrs)= 1.417
 RUNOFF VOLUME (mm)= 18.336
 TOTAL RAINFALL (mm)= 75.169
 RUNOFF COEFFICIENT = 0.244

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0002)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0206):		2.15	0.140	1.42	18.34
+ ID2= 2 (0052):		0.83	0.014	2.83	24.47
=====					
ID = 3 (0002):		2.98	0.141	1.42	20.05

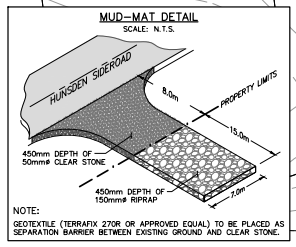
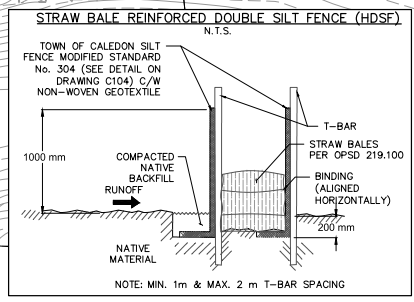
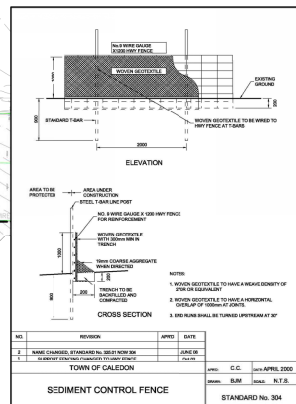
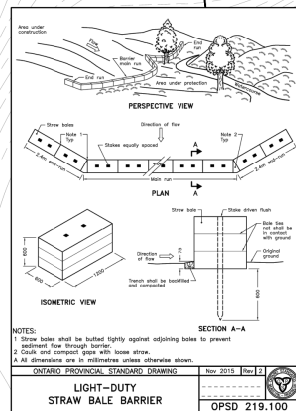
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DRAWINGS



LEGEND

- PROPERTY LINE
- - - EXISTING CONTOUR (0.5m)
- - - EXISTING CONTOUR (1.0m)
- - - EXISTING DITCH
- - - EXISTING GRADE
- 215.00 MUD-MAT; SEE DETAIL M00101
- SF SILT FENCE (T.O.C. STD. DWG. No. 304) - SEE DETAIL ON C104
- HDSF HEAVY DUTY SILT FENCE (STRAW BALE REINFORCED DOUBLE SILT FENCE) - SEE DETAIL ON THIS DRAWING
- ROCK FLOW CHECK DAM; OFSD 219.210



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No.	ISSUE / REVISION	YYYY/MM/DD

ELEVATION NOTE:
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SITE BENCHMARKS:
 NB OGD808111 ELEVATION = 286.833m
 NB OGD808113 ELEVATION = 290.087

SURVEY NOTES:
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Project: 10249 HUNSDEN SIDEROAD TOWN OF CALEDON

Drawing: PRELIMINARY EROSION AND SEDIMENT CONTROL PLAN

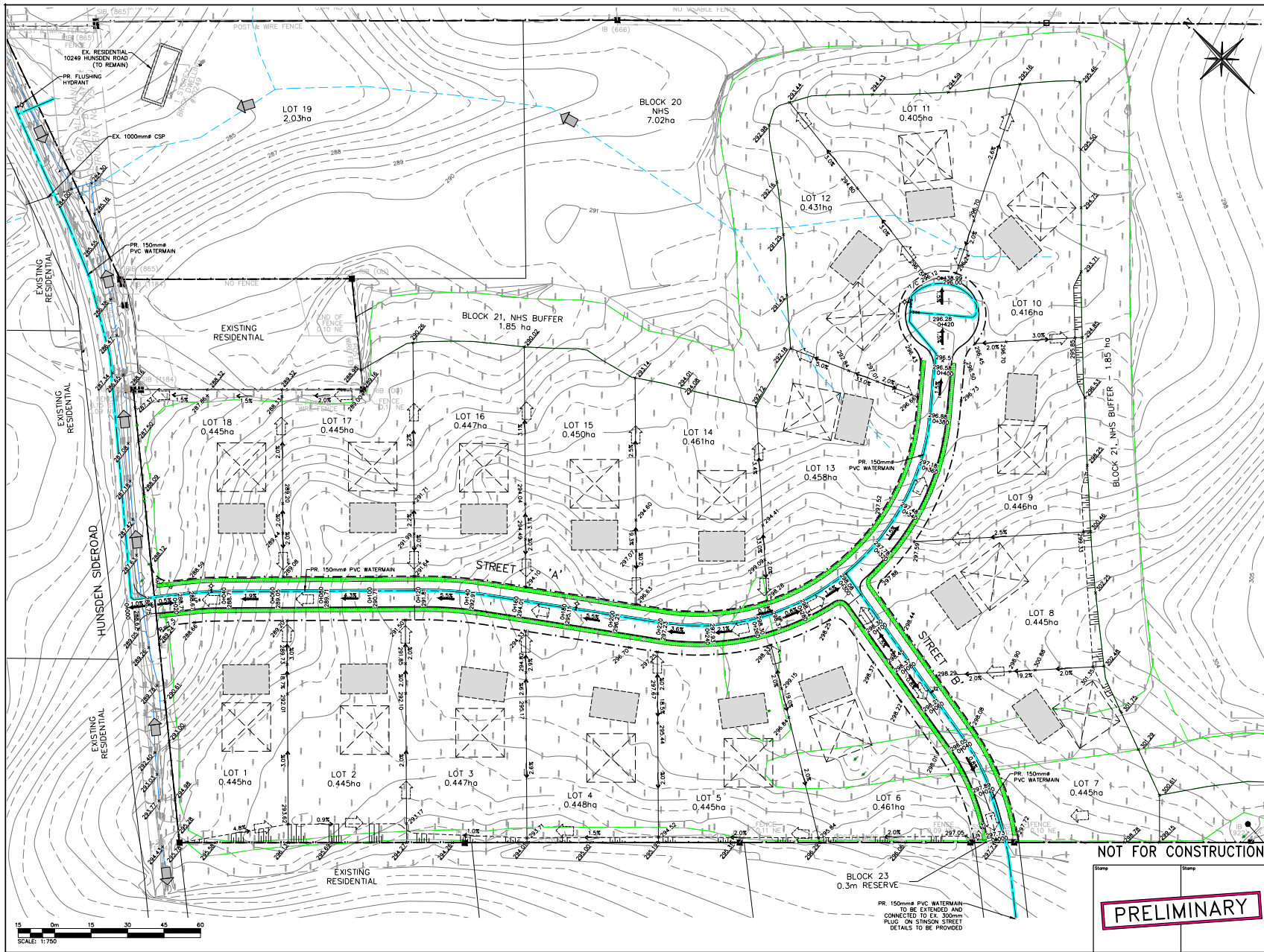
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 MILLTON, ON L0T 1G0
 905-875-0226 T
 905-875-4915 F
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Drawn: M.L.M. Design: P.S. Project No: 952-6305
 Check: S.C. Check: T.E. Date: 1:1000 Page: C101

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PRELIMINARY



LEGEND

- PROPERTY LINE
- EXISTING CONTOUR (0.5m)
- EXISTING CONTOUR (1.0m)
- EXISTING DITCH
- EXISTING FENCE
- EXISTING GRADE
- PROPOSED GRADE
- PROPOSED GRADE (TO MATCH EXISTING)
- PROPOSED MINOR FLOW DIRECTION
- PROPOSED GRASSED SWALE
- PROPOSED SLOPE (3:1 MAX.)
- EXISTING OVERLAND FLOW DIRECTION
- PROPOSED MAJOR OVERLAND FLOW DIRECTION
- PROPOSED FIRE HYDRANT & GATE VALVE
- PROPOSED WATERMAIN & GATE VALVE
- PR. BIOSWALE
- PR. BUILDING ENVELOPE
- SANITARY SEPTIC BED TO BE DESIGNED BY OTHERS

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No	ISSUE / REVISION	YYYY/MM/DD

ELEVATION NOTE:
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SITE BENCHMARKS:
 BM G08050811
 ELEVATION = 286.833m
 BM G08050812
 ELEVATION = 290.087m

SURVEY NOTES:
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Project: 10249 HUNSDEN SIDEROAD
TOWN OF CALEDON

Drawing: PRELIMINARY SITE GRADING & SERVICING PLAN

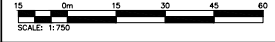
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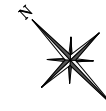
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SUITE 100
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 Check: S.C. Check: T.E. Date: 1:750 Page: C 102

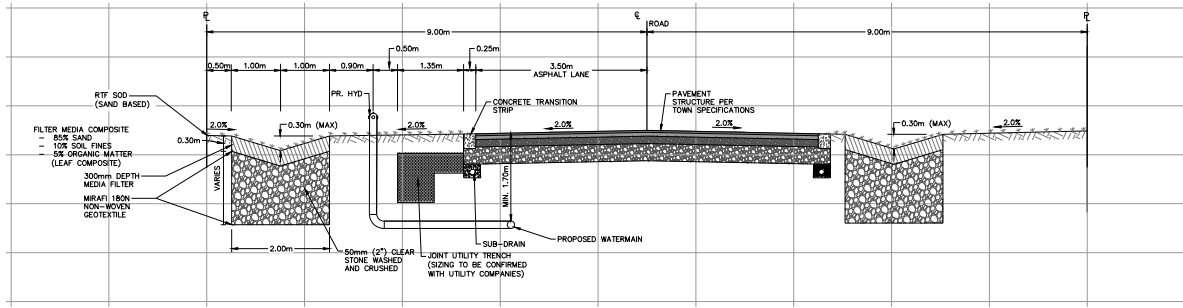


PR 150mm PVC WATERMAIN TO BE EXTENDED AND CONNECTED TO EX. 300mm PUC ON STINSON STREET. DETAILS TO BE PROVIDED.



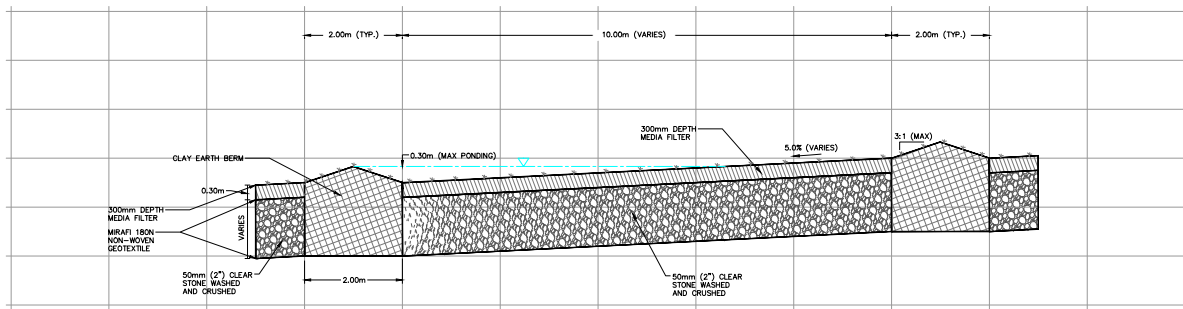
TYPICAL 18.0m R.O.W. ROAD SECTION

SCALE: HOR: 1:50
VER: 1:50



TYPICAL ROADSIDE BIOWALE SECTION

SCALE: HOR: 1:50
VER: 1:50



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ELEVATION NOTE:
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SITE BENCHMARKS:
 N1 026208011
 ELEVATION = 286.833m
 N1 026208013
 ELEVATION = 290.087

SURVEY NOTES:
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Project: 10249 HUNSDEN SIDEROAD
TOWN OF CALEDON

Drawing: SECTIONS AND DETAILS

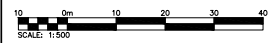
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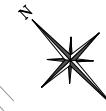
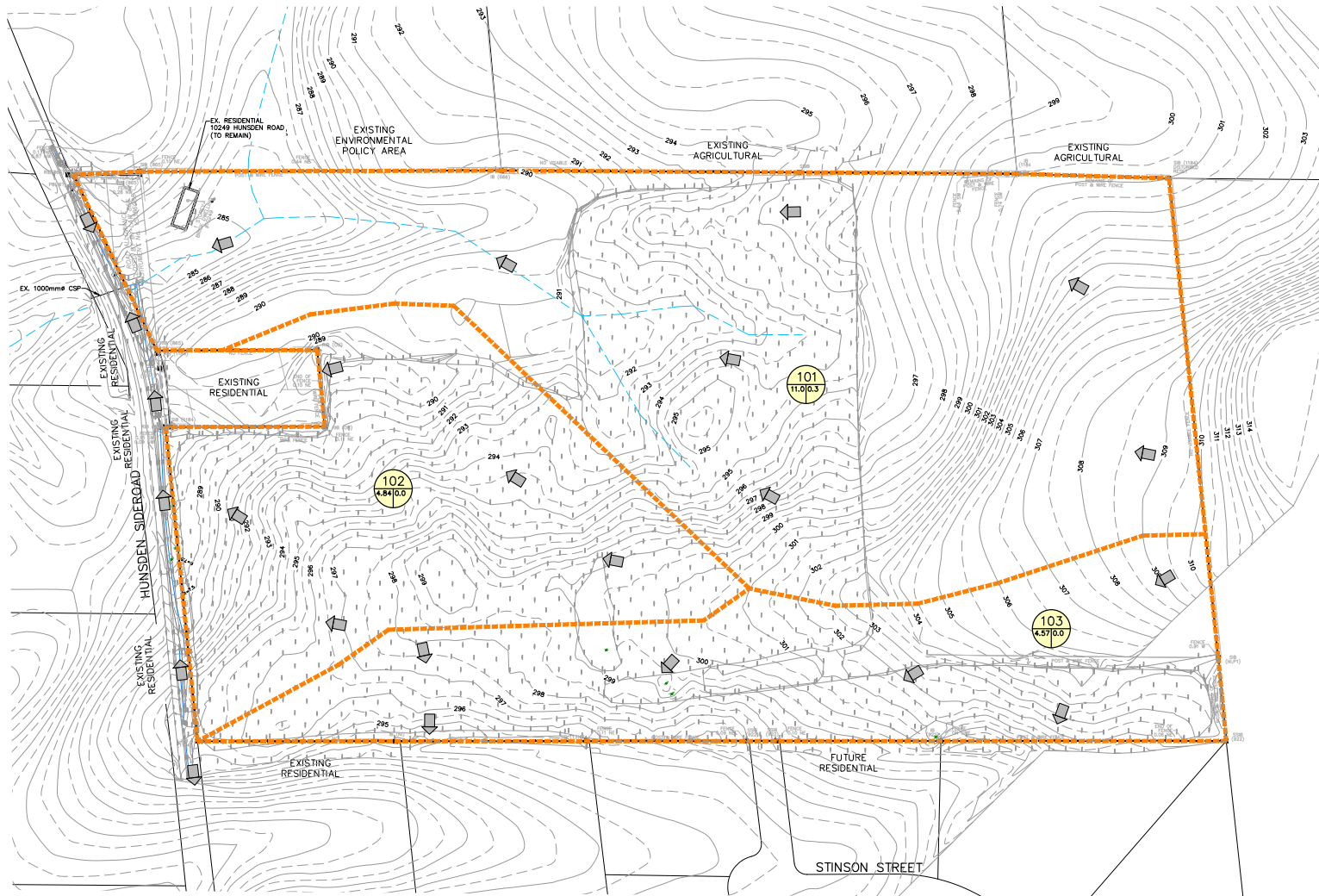


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Drawn	M.L.M.	Design	P.S.	Project No.	952-6305
Check	S.C.	Check	T.E.	Scale AS SHOWN	Sheet C 103



FIGURES



LEGEND	
	PROPERTY LINE
	EXISTING CONTOUR (0.5m)
	EXISTING CONTOUR (1.0m)
	EXISTING DITCH
	EXISTING GRADE
	EXISTING OVERLAND FLOW DIRECTION
	EXISTING STORM DRAINAGE CATCHMENT
	CATCHMENT I.D.
	AREA (ha) PERCENT IMPERVIOUS (%)

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ELEVATION NOTE:
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SITE BENCHMARKS:
 BM 028080811
 ELEVATION = 286.833m
 BM 028080813
 ELEVATION = 290.087

SURVEY NOTES:
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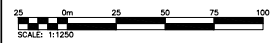
Project: 10249 HUNSDEN SIDEROAD
TOWN OF CALEDON

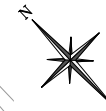
Drawing: PRE-DEVELOPMENT DRAINAGE PLAN

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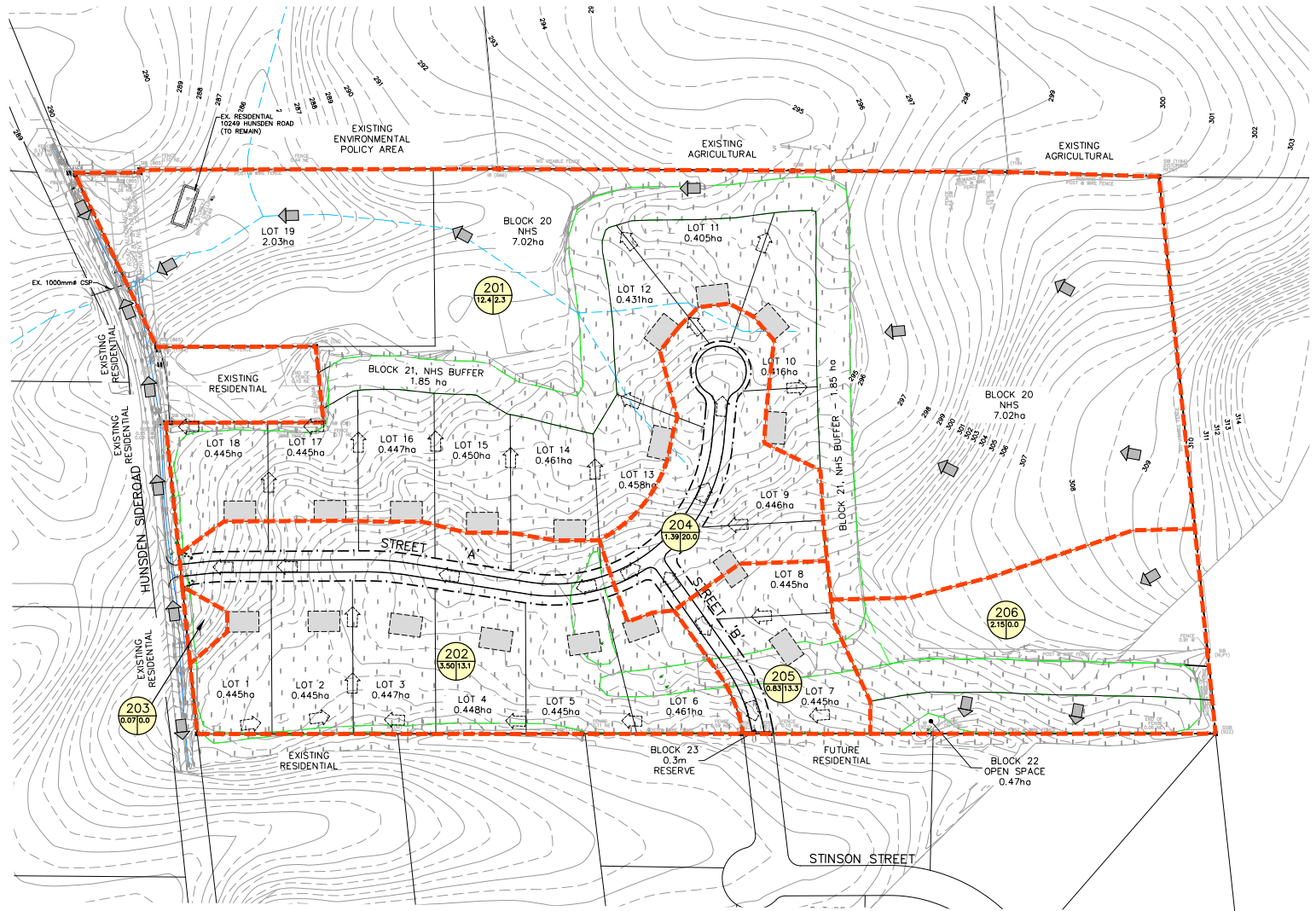
	CROZIER CONSULTING ENGINEERS	2800 High Point Drive Suite 100 Milton, ON L9T 6P4 905-875-0026 T 905-875-4915 F www.crozier.ca
	Draw: M.L.M. Design: P.S. Project No: 952-6305 Check: S.C. Date: T.E. Scale: 1:1250 Page: FIG1	





LEGEND

- PROPERTY LINE
- EXISTING CONTOUR (0.5m)
- EXISTING CONTOUR (1.0m)
- EXISTING DITCH
- EXISTING GRADE
- PROPOSED MAJOR OVERLAND FLOW DIRECTION
- EXISTING MAJOR OVERLAND FLOW DIRECTION
- PROPOSED STORM DRAINAGE CATCHMENT
- CATCHMENT I.D.
- AREA (ha) | PERCENT IMPERVIOUS (%)
- PROPOSED BUILDING ENVELOPE



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ELEVATION NOTE:
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SITE BENCHMARK:
 NB CORNER 0811
 ELEVATION = 286.833m
 NB CORNER 0813
 ELEVATION = 290.087m

SURVEY NOTES:
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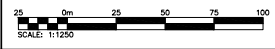
Project: 10249 HUNSDEN SIDEROAD
TOWN OF CALEDON

Drawing: POST DEVELOPMENT
DRAINAGE PLAN

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SUITE 100
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