

**TOWN OF CALEDON
PLANNING
RECEIVED**

December 15, 2020



January 15, 2020
27301-19

Shirewood Centre Inc.
472541 County Road 11
Amaranth, Ontario
L9W 0R3

Attention: Gary Grant

Dear Sir:

**Re: Stormwater Brief
1 Victoria Road
Part of Block A, Registered Plan CAL-5
Town of Caledon, Ontario**

Van Harten is pleased to submit this Stormwater Brief to accompany a Lot Grading Plan recently completed for the above referenced site, located on King Street between Agnes Street and Victoria Street in the Village of Alton, as indicated on the Key Map of Appendix A. This work was authorized by Mr. Gary Grant of Shirewood Centre Inc.

The project involves the proposed severance of an existing property into three individual lots. The existing privately serviced single family home is to be demolished in order to facilitate the construction of three single family dwellings. The purpose of this letter is to outline the grading and stormwater management approach taken in the design and to discuss existing and proposed drainage patterns.

The pre- and post- development conditions were analyzed in order to observe the effect the proposed construction will have on the stormwater runoff characteristics at the subject property. Runoff coefficients for the site were derived as a weighted average referencing Town of Caledon Standard Drawing 103. Runoff coefficients for all impervious areas were calculated assuming $C = 0.90$ and all pervious areas as $C = 0.25$. The intensity of the 2-, 5-, 25- and 100-year design storms were generated using the rational method with IDF curves obtained from Town of Caledon Standard Drawing 103. Inlet times are assumed to be 10 minutes. These parameters are summarized in the following table:

Parameter	2-Year Storm	5-Year Storm	25-Year Storm	100-Year Storm
a	1070	1593	3158	4688
b	7.85	11	15	17
c	0.8759	0.8789	0.9335	0.9624

572 Weber Street North, Unit 7
Waterloo ON N2L 5C6
519-742-8371

Elmira, ON:
519-669-5070

423 Woolwich Street
Guelph, ON N1H 3X3
519-821-2763

660 Riddell Road, Unit 1
Orangeville, ON L9W 5G5
519-940-4110

Collingwood, ON:
249-499-8359

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Referring to Appendix B, the site as it currently exists is divided into two catchments, referred to here as Catchment 1 and Catchment 2. Catchment 1 comprises of the northwest portion of the property that currently drains towards Agnes Street. Catchment 2 will comprise the south east portion of the property, draining towards Victoria Street.

As illustrated in the Post-Development Catchment Sketch found in Appendix B, the site will continue to generally act as two catchments, referred to here as Catchment 101 and Catchment 102. Catchment 101 comprises Lot 1 and approximately half of Lot 2, and will drain towards Agnes Street, similar to the existing conditions noted in Catchment 1. Catchment 102 will comprise Lot 3 and the remainder of Lot 2 and will drain towards Victoria Street as per the existing conditions noted in Catchment 2. Details of the existing and proposed catchments are as follows:

9 Victoria Street				
Catchment	Area (m ²)	Impervious Area (m ²)	% Impervious	Runoff Coefficient
1	1,000	136	13.6	0.34
2	1,073	147	13.7	0.34
Pre Total	2,073	283	13.7	0.34
101	850	277	32.6	0.46
102	1,223	246	20.1	0.38
Post Total	2,073	523	25.2	0.41

Attached as Appendix C are calculations relating to the runoff characteristics of the site before and following development. A summary of the runoff rates are as follows:

	To Agnes Street (m ³ /sec)		To Victoria Street (m ³ /sec)	
	Pre-Development	Post-Development	Pre-Development	Post-Development
2-Year Storm	0.008	0.009	0.009	0.011
5-Year Storm	0.010	0.012	0.011	0.014
25-Year Storm	0.015	0.017	0.016	0.020
100-Year Storm	0.019	0.022	0.020	0.026

As noted above, a small amount of increased runoff is anticipated following the development of these properties. It is noted the runoff coefficients calculated above are relatively conservative, as it is understood the proposed site plan will require several zoning amendments to allow for development of the dwellings as described. Also, further increase in impervious area through the construction of rear yard patios or pools is unlikely due to the need to service these lots with on-site sewage systems, which will likely encompass most of the rear yard of each lot. Generally speaking, the largest increase in post development runoff in any direction from the subject property will be towards Victoria Street during the 100-year storm. As noted, an increase in the runoff rate from 0.020 to 0.026 m³/second is anticipated



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(approximately 6 L/second, or 30% increased runoff), which is relatively minimal considering the overall catchment area draining to Victoria Street. Overall, the proposed development would appear to have a negligible impact on runoff characteristics from the site directed to the municipal roadways.

The completed stormwater brief is specific to the subject property based on our knowledge of the proposed development. Please contact our office if you have any questions or require further consultation.

Van Harten Surveying Inc.

Andrew Sumary, EIT
Junior Engineer

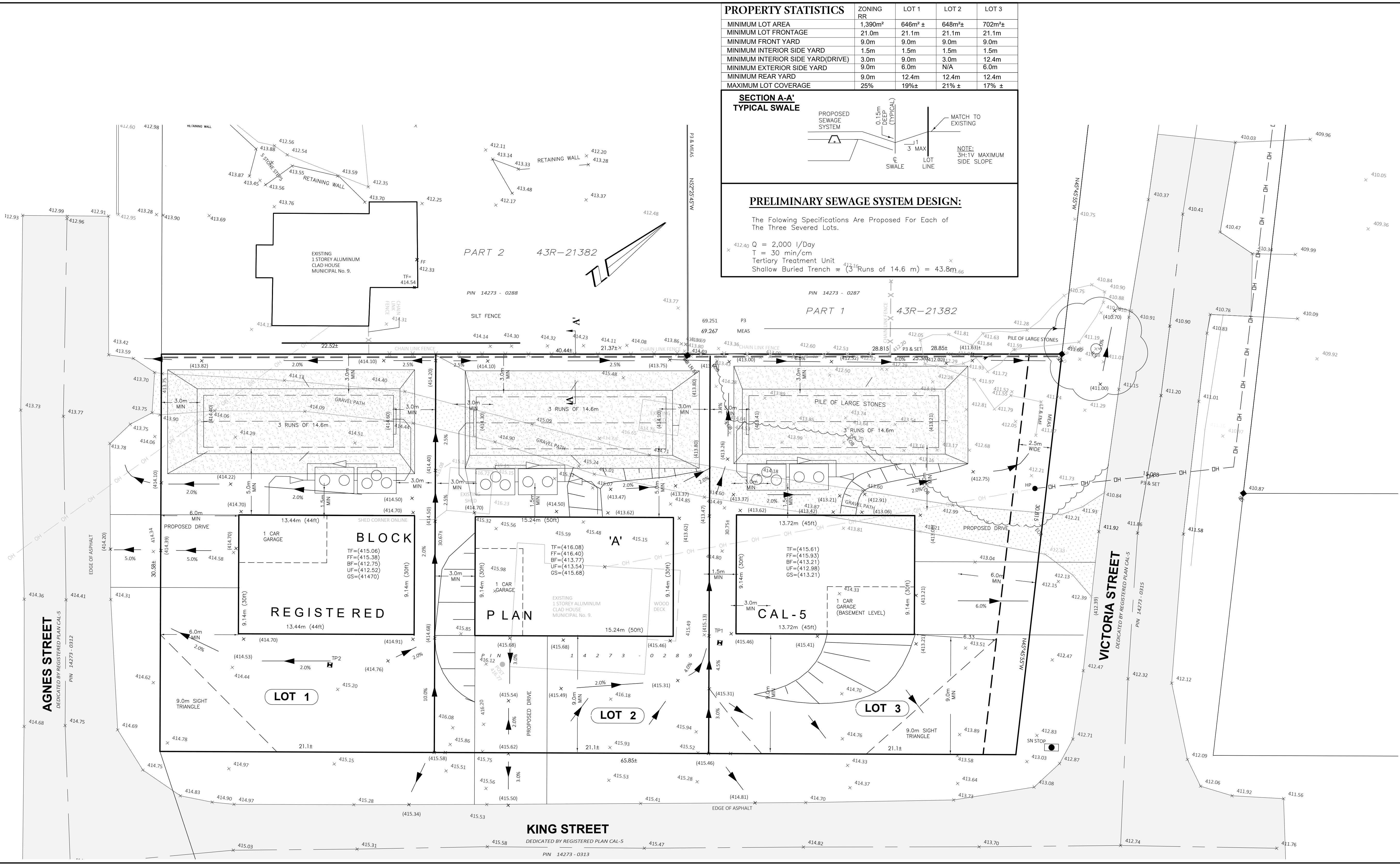
Mike Vaughan, P. Eng.
Professional Engineer



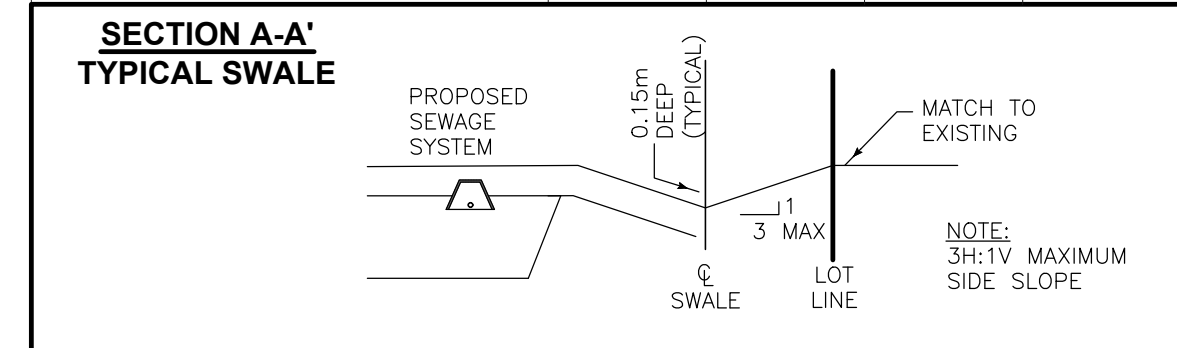
- Encl. Appendix A – Site Grading and Servicing Plan
- Encl. Appendix B – Pre- and Post-Development Catchment Sketches
- Encl. Appendix C – Stormwater Runoff Calculations



APPENDIX A
SITE GRADING AND SERVICING PLAN



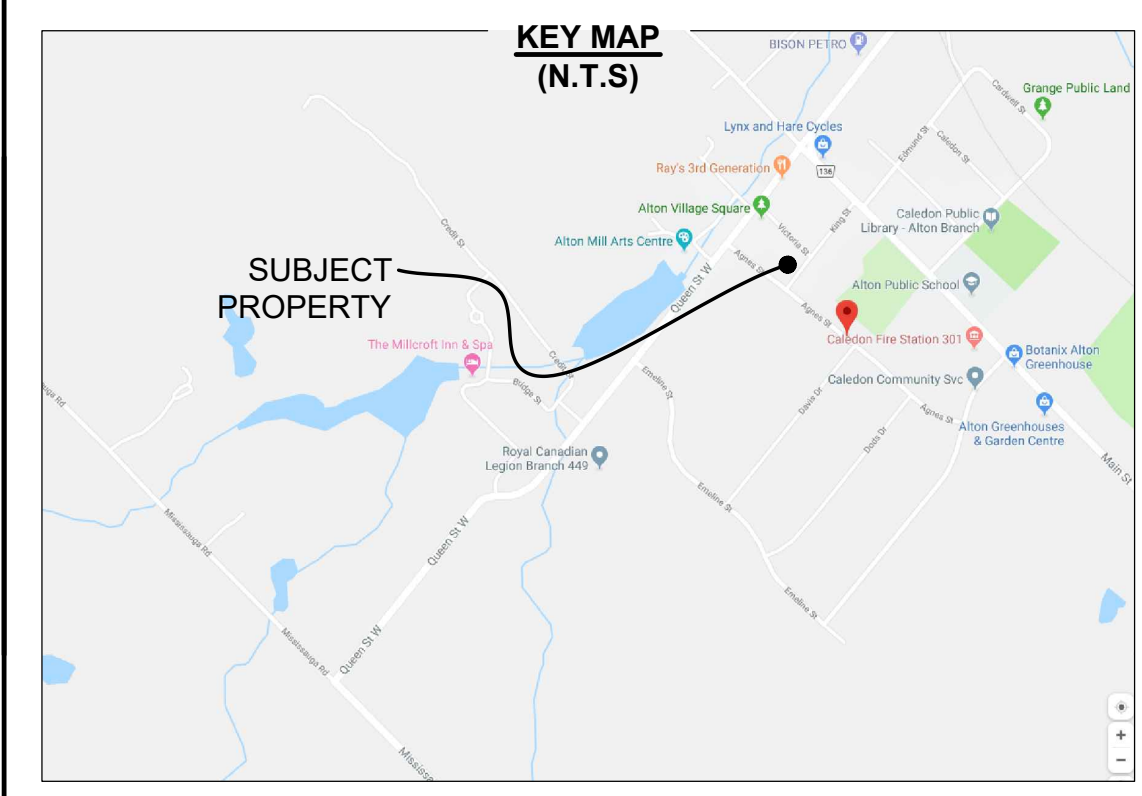
PROPERTY STATISTICS	ZONING RR	LOT 1	LOT 2	LOT 3
MINIMUM LOT AREA	1,390m ²	646m ² ±	648m ² ±	702m ² ±
MINIMUM LOT FRONTAGE	21.0m	21.1m	21.1m	21.1m
MINIMUM FRONT YARD	9.0m	9.0m	9.0m	9.0m
MINIMUM INTERIOR SIDE YARD	1.5m	1.5m	1.5m	1.5m
MINIMUM INTERIOR SIDE YARD(DRIVE)	3.0m	9.0m	3.0m	12.4m
MINIMUM EXTERIOR SIDE YARD	9.0m	6.0m	N/A	6.0m
MINIMUM REAR YARD	9.0m	12.4m	12.4m	12.4m
MAXIMUM LOT COVERAGE	25%	19% ±	21% ±	17% ±



PRELIMINARY SEWAGE SYSTEM DESIGN:

The Following Specifications Are Proposed For Each of The Three Severed Lots.

Q = 2,000 l/Day
 T = 30 min/cm
 Tertiary Treatment Unit
 Shallow Buried Trench = (3 Runs of 14.6 m) = 43.8m_{0.66}



LEGEND:

(395.70)	PROPOSED ELEVATION	---	SILT FENCE
394.82	EXISTING ELEVATION	---	FENCELINE
FF 412.33	EXISTING FINISHED FLOOR ELEVATION	---	OVERHEAD HYDRO
	SLOPE	---	HYDRO POLE
	DIRECTION OF FLOW	---	HP
	TEST PIT	---	TREE LINE
	ASPHALT	---	
	SAND	---	
	GRAVEL	---	

BENCHMARK:

ELEVATIONS ARE BASED ON GPS OBSERVATIONS FROM PERMANENT REFERENCE STATIONS IN THE NAD83 (CSRS-2010) COORDINATE SYSTEM, WITH HEIGHTS CONVERTED TO ORTHOMETRIC ELEVATIONS ON THE CVGD28 DATUM (1978 ADJUSTMENT) WITH GEOID MODEL HTV2.0, AS SUPPLIED BY NATURAL RESOURCES CANADA.

TEMPORARY BENCH MARK: NAIL IN HYDRO POLE 412.43m.

PRELIMINARY GRADING PLAN AND SEVERANCE SKETCH FOR:

**PART OF BLOCK A,
 REGISTERED PLAN CAL-5
 TOWN OF CALEDON
 REGIONAL MUNICIPALITY OF PEEL**

2.	UPDATED DWELLING CONFIGURATION	AS	2020-JAN-15
1.	INITIAL SUBMISSION	AS	2019-SEPT-23
NO.	REVISION	BY	DATE

DRAWING REVISION SCHEDULE

PREPARED FOR: SHIREWOOD CENTRE INC

PROJECT No. 27301-19

DRAWING SCALE: 1:150

CAUTION:

- THIS IS NOT A PLAN OF SURVEY AND SHALL NOT BE USED FOR TRANSACTION OR MORTGAGE PURPOSES
- IT IS THE BUILDER'S RESPONSIBILITY TO ENSURE THE PROPOSED FOOTING ELEVATION AND PLUMBING ALLOWS GRAVITY CONNECTION TO THE SEWAGE SYSTEM.
- THIS LOT MAY CONTAIN STRUCTURAL OR NON-STRUCTURAL FILL PLACED DURING SUBDIVISION GRADING OPERATIONS. SOIL BEARING CAPACITY SHOULD BE VERIFIED AT THE TIME OF CONSTRUCTION.
- THE BUILDER MUST ENSURE A MINIMUM OF 1.22m OF EARTH COVER OVER THE FOOTINGS FOR FROST PROTECTION.
- THIS SKETCH IS PROTECTED BY COPYRIGHT.

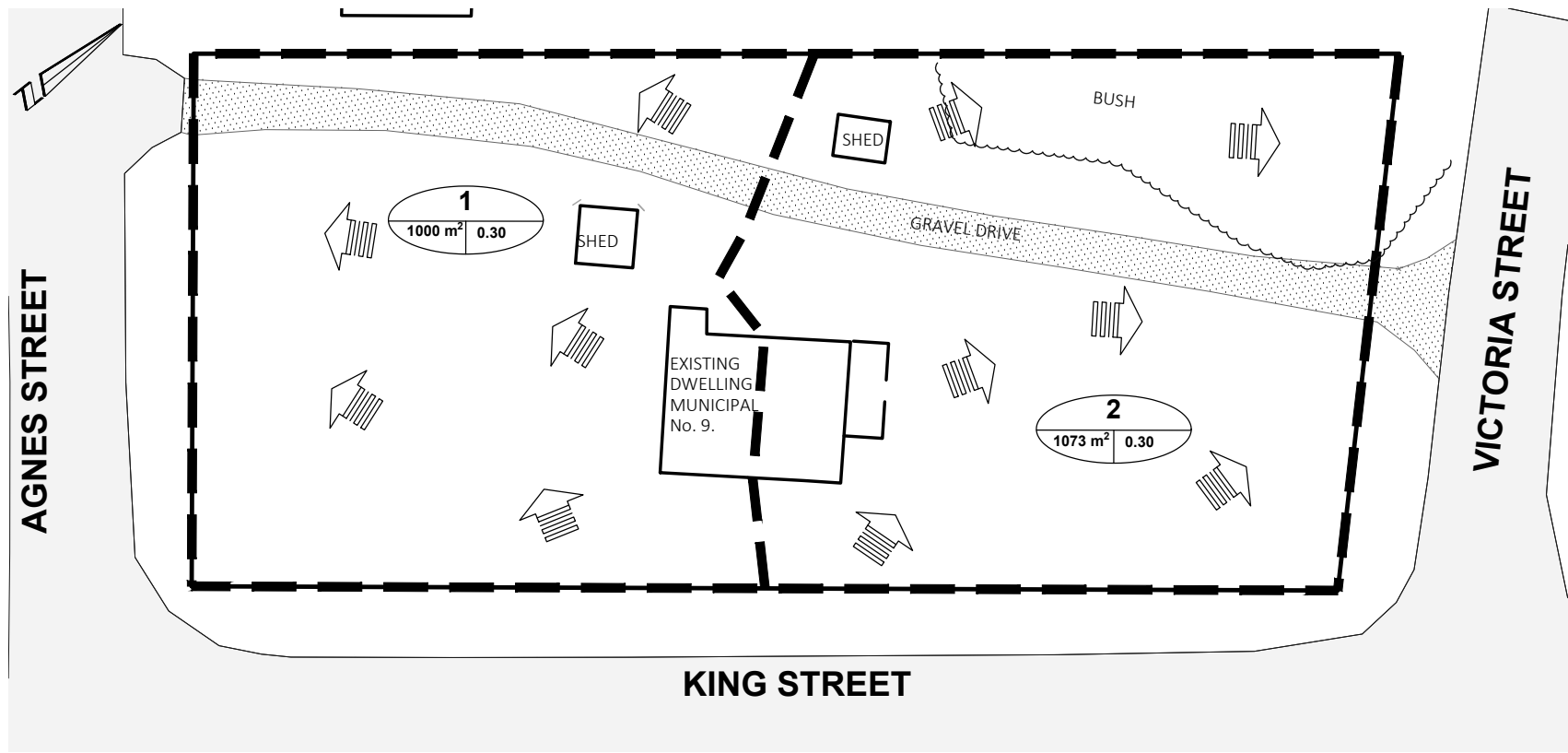
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SURVEYING INC.
LAND SURVEYORS and ENGINEERS

Kitchener Ph: 519-742-8371		Guelph Ph: 519-821-2763		Orangeville Ph: 519-940-4110	
www.vanharten.com		info@vanharten.com			
DRAWN BY: FCF	DESIGN BY: AS	CHECKED BY: MAMV			

Jan 15, 2020-12:50pm
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**APPENDIX B
PRE- AND POST- DEVELOPMENT
CATCHMENT SKETCHES**



SCALE 1 : 400
 0 5 10 20 metres
 VAN HARTEN SURVEYING INC.

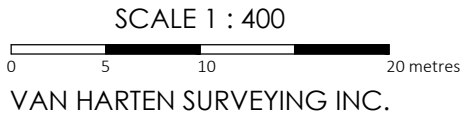
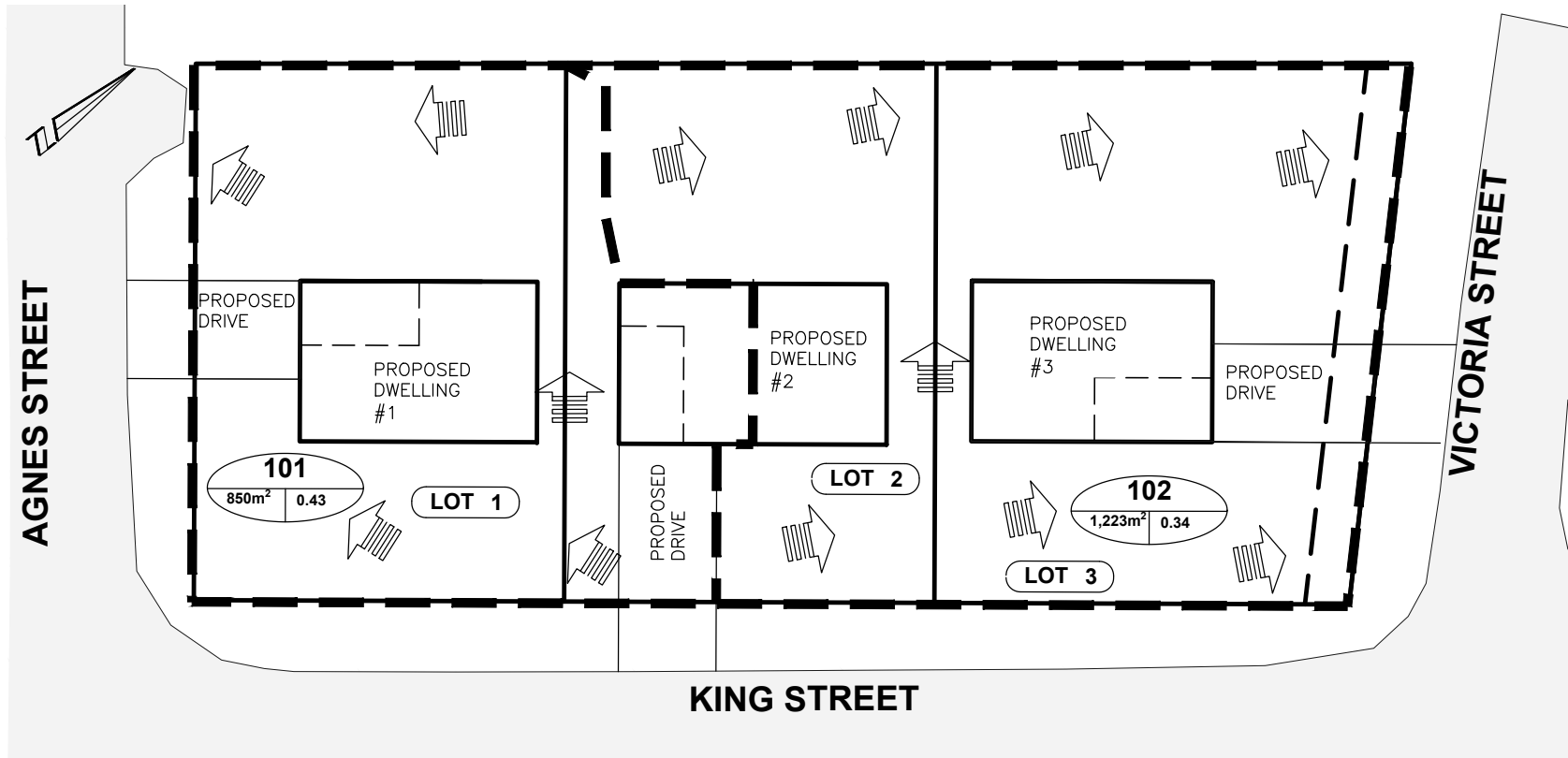
**PRE DEVELOPMENT SKETCH
 PART OF BLOCK A,
 REGISTERED PLAN CAL-5
 TOWN OF CALEDON**

LEGEND:

<p>CATCHMENT 101</p> <p>AREA 0.25ha 0.75 RUNOFF COEFFICIENT</p>	<p>— — — — — DRAINAGE AREA BOUNDARY</p>
MAJOR STORM OVERLAND FLOW ROUTE	<div style="display: flex; justify-content: space-around;"> <div style="border: 1px solid black; background-color: #cccccc; padding: 2px;">ASPHALT</div> <div style="border: 1px solid black; background: repeating-linear-gradient(45deg, transparent, transparent 2px, black 2px, black 4px); padding: 2px;">GRAVEL</div> </div> <div style="display: flex; justify-content: center; margin-top: 10px;"> <div style="border: 1px solid black; background: repeating-linear-gradient(-45deg, transparent, transparent 2px, black 2px, black 4px); padding: 2px;">CONCRETE</div> </div>

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 SURVEYING INC.
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Elmira Ph: 519-669-5070	Guelph Ph: 519-821-2763	Orangeville Ph: 519-940-4110
www.vanharten.com		info@vanharten.com
PROJECT NO.: 27301-19	DESIGN BY: AS	CHECKED BY: MMAV
Jan 07, 2020-1:10pm L:\Caledon\Cal-5\BLOCK A\ACAD\LDP.BLOCKA.GARY GRANT(27301-19).dwg		



**POST DEVELOPMENT SKETCH
PART OF BLOCK A,
REGISTERED PLAN CAL-5
TOWN OF CALEDON**

LEGEND:

<p>CATCHMENT</p> <p>AREA RUNOFF COEFFICIENT</p>	<p>— — — — —</p> <p>DRAINAGE AREA BOUNDARY</p>				
<p>MAJOR STORM OVERLAND FLOW ROUTE</p>	<table border="1"> <tr> <td style="background-color: #cccccc;">ASPHALT</td> <td style="background-color: #d3d3d3;">GRAVEL</td> </tr> <tr> <td style="background-color: #d3d3d3;">CONCRETE</td> <td></td> </tr> </table>	ASPHALT	GRAVEL	CONCRETE	
ASPHALT	GRAVEL				
CONCRETE					



Van Harten
SURVEYING INC.
LAND SURVEYORS and ENGINEERS

Elmira
Ph: 519-669-5070

Guelph
Ph: 519-821-2763

Orangeville
Ph: 519-940-4110

www.vanharten.com

info@vanharten.com

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APPENDIX C STORMWATER RUNOFF CALCULATIONS

2 Year Storm Design							
SHIREWOOD (27301-19)							
Flow Characteristics							
Catchment	Area (m ²)	Impervious Area (m ²)	% Impervious	Runoff Coefficient	Time of Conc. (min)	Intensity (mm/hr)	Flow Rate (m ³ /s)
1	1,000	136	13.6%	0.34	10.00	85.72	0.008
2	1,073	147	13.7%	0.34	10.00	85.72	0.009
Pre total	2,073	283	13.7%	0.34	10.00	85.72	0.017
101	850	277	32.6%	0.46	10.00	85.72	0.009
102	1,223	246	20.1%	0.38	10.00	85.72	0.011
Post Total	2,073	523	25.2%	0.41	10.00	85.72	0.021

2 Year Storm Design Parameters
A= 1070.000
B= 7.850
C= 0.876
Intensity= $A/(t+B)^C$
Q= kCiA
k= 0.0028

Impervious Area C = 0.90

Pervious Area C = 0.25

5 Year Storm Design							
SHIREWOOD (27301-19)							
Flow Characteristics							
Catchment	Area (m ²)	Impervious Area (m ²)	% Impervious	Runoff Coefficient	Time of Conc. (min)	Intensity (mm/hr)	Flow (m ³ /s)
1	1,000	136	13.6%	0.34	10.00	109.68	0.010
2	1,073	147	13.7%	0.34	10.00	109.68	0.011
Pre total	2,073	283	13.7%	0.34	10.00	109.68	0.022
101	850	277	32.6%	0.46	10.00	109.68	0.012
102	1,223	246	20.1%	0.38	10.00	109.68	0.014
Post Total	2,073	523	25.2%	0.41	10.00	109.68	0.026

5 Year Storm Design Parameters
A= 1593.000
B= 11.000
C= 0.879
Intensity= $A/(t+B)^C$
Q= kCiA
k= 0.0028

Impervious Area C = 0.90

Pervious Area C = 0.25

25 Year Storm Design

SHIREWOOD (27301-19)

Flow Characteristics							
Catchment	Area (m ²)	Impervious Area (m ²)	% Impervious	Runoff Coefficient	Time of Conc. (min)	Intensity (mm/hr)	Flow (m ³ /s)
1	1,000	136	13.6%	0.34	10.00	156.47	0.015
2	1,073	147	13.7%	0.34	10.00	156.47	0.016
Pre total	2,073	283	13.7%	0.34	10.00	156.47	0.031
101	850	277	32.6%	0.46	10.00	156.47	0.017
102	1,223	246	20.1%	0.38	10.00	156.47	0.020
Post Total	2,073	523	25.2%	0.41	10.00	156.47	0.038

25 Year Storm Design Parameters

A= 3158.000

B= 15.000

C= 0.934

Intensity= $A/(t+B)^C$

Q= kCiA

k= 0.0028

Impervious Area C = 0.90

Pervious Area C = 0.25

100 Year Storm Design

SHIREWOOD (27301-19)

Flow Characteristics

Catchment	Area (m ²)	Impervious Area (m ²)	% Impervious	Runoff Coefficient	Time of Conc. (min)	Intensity (mm/hr)	Flow (m ³ /s)
1	1,000	136	13.6%	0.34	10.00	196.54	0.019
2	1,073	147	13.7%	0.34	10.00	196.54	0.020
Pre total	2,073	283	13.7%	0.34	10.00	196.54	0.039
101	850	277	32.6%	0.46	10.00	196.54	0.022
102	1,223	246	20.1%	0.38	10.00	196.54	0.026
Post Total	2,073	523	25.2%	0.41	10.00	196.54	0.047

100 Year Storm Design Parameters

A= 4688.000

B= 17.000

C= 0.962

Intensity= $A/(t+B)^C$

Q= kCiA

k= 0.0028

Impervious Area C = 0.90

Pervious Area C = 0.25