

QC SUMMARY

Method Blank: a blank matrix that is carried through the entire analytical procedure. Used to assess laboratory contamination.

Duplicate: Paired analysis of a separate portion of the same sample that is carried through the entire analytical procedure. Used to evaluate measurement precision.

LCS/Spike Blank: Laboratory control sample or spike blank refer to a blank matrix to which a known amount of analyte has been added. Used to evaluate analyte recovery and laboratory accuracy without sample matrix effects.

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate laboratory accuracy with sample matrix effects.

Reference Material: a material or substance matrix matched to the samples that contains a known amount of the analyte of interest. A reference material may be used in place of a matrix spike.

RL: Reporting limit

RPD: Relative percent difference

AC: Acceptance criteria

Multielement Scan Qualifier: as the number of analytes in a scan increases, so does the chance of a limit exceedance by random chance as opposed to a real method problem. Thus, in multielement scans, for the LCS and matrix spike, up to 10% of the analytes may exceed the quoted limits by up to 10% absolute and the spike is considered acceptable.

Duplicate Qualifier: for duplicates as the measured result approaches the RL, the uncertainty associated with the value increases dramatically, thus duplicate acceptance limits apply only where the average of the two duplicates is greater than five times the RL.

Matrix Spike Qualifier: for matrix spikes, as the concentration of the native analyte increases, the uncertainty of the matrix spike recovery increases. Thus, the matrix spike acceptance limits apply only when the concentration of the matrix spike is greater than or equal to the concentration of the native analyte.

**LEGEND**

FOOTNOTES

NSS Insufficient sample for analysis.
RL Reporting Limit.
 ↑ Reporting limit raised.
 ↓ Reporting limit lowered.
NA The sample was not analysed for this analyte
ND Non Detect

Results relate only to the sample tested.

Data reported represent the sample as submitted to SGS. Solid samples expressed on a dry weight basis.

"Temperature Upon Receipt" is representative of the whole shipment and may not reflect the temperature of individual samples.

Analysis conducted on samples submitted pursuant to or as part of Reg. 153/04, are in accordance to the "Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act and Excess Soil Quality" published by the Ministry and dated March 9, 2004 as amended.

SGS provides criteria information (such as regulatory or guideline limits and summary of limit exceedances) as a service. Every attempt is made to ensure the criteria information in this report is accurate and current, however, it is not guaranteed. Comparison to the most current criteria is the responsibility of the client and SGS assumes no responsibility for the accuracy of the criteria levels indicated.

SGS Canada Inc. statement of conformity decision rule does not consider uncertainty when analytical results are compared to a specified standard or regulation.

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This report supersedes all previous versions.

-- End of Analytical Report --

Request for Laboratory Services and CHAIN OF CUSTODY

No: **029705**

Page **1 of 1**

Laboratory Information Section - Lab use only

Received By: [Signature] Received By (signature): _____
 Received Date: **10/26/22** (mm/dd/yy) Custody Seal Present: Yes No
 Received Time: **12:00** (hr: min) Custody Seal Initialed: Yes No

Cooling Agent Present: Yes No Type: **ICE**
 Temperature Upon Receipt (°C) **9.9.9**

LAB LIMS #: **CA40196-00722**

| REPORT INFORMATION | INVOICE INFORMATION |
|--|------------------------------|
| Company: DS consultants Ltd. | (same as Report Information) |
| Contact: Dorothy Santos | Company: _____ |
| Address: 6221 Hwy -7, Unit-16 Vaughan, ON | Contact: Accounting |
| Phone: 905-264-9393 | Address: _____ |
| Fac: _____ | Phone: _____ |
| Email: dorothy.santos@dsconsultants.ca | Email: _____ |

Quotation #: _____ P.O. #: _____
 Project #: **19-093-100** Site Location/ID: **7675 King St, Bolton**

TURNAROUND TIME (TAT) REQUIRED
 Regular TAT (5-7days) TAT's are quoted in business days (exclude statutory holidays & weekends).
 Samples received after 5pm or on weekends, TAT begins next business day

RUSH TAT (Additional Charges May Apply): 1 Day 2 Days 3 Days 4 Days
PLEASE CONFIRM RUSH FEASIBILITY WITH SGS REPRESENTATIVE PRIOR TO SUBMISSION
 Specify Due Date: _____ ***NOTE: DRINKING (POTABLE) WATER SAMPLES FOR HUMAN CONSUMPTION MUST BE SUBMITTED WITH SGS DRINKING WATER CHAIN OF CUSTODY**

REGULATIONS

| | | | |
|--|---------------------------------------|--|---|
| <input type="checkbox"/> O.Reg 153/04 | <input type="checkbox"/> O.Reg 405/19 | Other Regulations: | Sewer By-Law: |
| <input type="checkbox"/> Table 1 | <input type="checkbox"/> Res/Park | <input type="checkbox"/> Reg 347/551 (3 Day min TAT) | <input checked="" type="checkbox"/> Sanitary |
| <input type="checkbox"/> Table 2 | <input type="checkbox"/> Ind/Com | <input checked="" type="checkbox"/> PWOC | <input checked="" type="checkbox"/> Storm |
| <input type="checkbox"/> Table 3 | <input type="checkbox"/> Agri/Other | <input type="checkbox"/> MMER | Municipality: Peel |
| <input type="checkbox"/> Table _____ | <input type="checkbox"/> Medium/Tric | <input type="checkbox"/> CCME | |
| Soil Volume: <input type="checkbox"/> <350m3 | <input type="checkbox"/> >350m3 | <input type="checkbox"/> MGA | <input type="checkbox"/> DOWS Not Responsible *See note |

ANALYSIS REQUESTED

| M & I | SVOC | PCB | PHC | VOC | Peat | Other (please specify) | SPLP | TCLP |
|---|------------------------------------|--------------------------------|---------------------------------------|------------------------------------|---|---|-----------------------------------|-----------------------------------|
| <input type="checkbox"/> Field Filtered (V/V) | <input type="checkbox"/> PAHs only | <input type="checkbox"/> Total | <input type="checkbox"/> F1-F4 + BTEX | <input type="checkbox"/> VOCs | <input type="checkbox"/> Pesticides | <input type="checkbox"/> _____ | Specify tests: | Specify tests: |
| <input type="checkbox"/> Metals & Inorganics | <input type="checkbox"/> SVOCs | <input type="checkbox"/> PCBs | <input type="checkbox"/> F1-F4 only | <input type="checkbox"/> VOCs | <input checked="" type="checkbox"/> Peel Sanitary/Storm Sewer | <input checked="" type="checkbox"/> PWOC | <input type="checkbox"/> Metals | <input type="checkbox"/> Metals |
| <input type="checkbox"/> Full Metals Suite | <input type="checkbox"/> PAHs only | <input type="checkbox"/> Total | <input type="checkbox"/> BTEX only | <input type="checkbox"/> BTEX only | <input type="checkbox"/> Sewer Use: _____ | <input type="checkbox"/> Water Characterization (Flg) | <input type="checkbox"/> Organics | <input type="checkbox"/> Organics |
| <input type="checkbox"/> ICP Metals only | <input type="checkbox"/> SVOCs | <input type="checkbox"/> Total | <input type="checkbox"/> VOCs | <input type="checkbox"/> BTEX only | <input type="checkbox"/> Pesticides | <input type="checkbox"/> Sewer Use: _____ | <input type="checkbox"/> Organics | <input type="checkbox"/> Organics |
| <input type="checkbox"/> PAHs only | <input type="checkbox"/> SVOCs | <input type="checkbox"/> Total | <input type="checkbox"/> VOCs | <input type="checkbox"/> BTEX only | <input type="checkbox"/> Pesticides | <input type="checkbox"/> Sewer Use: _____ | <input type="checkbox"/> Organics | <input type="checkbox"/> Organics |

COMMENTS:

Non-Filtered sample

RECORD OF SITE CONDITION (RSC) YES NO

| SAMPLE IDENTIFICATION | DATE SAMPLED | TIME SAMPLED | # OF BOTTLES | MATRIX |
|-----------------------|-------------------------------|--------------|--------------|------------|
| BH 22-5 | Oct 26th 22 | PM | 17 | GrW |
| | | | | |
| | | | | |
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| | | | | |

Observations/Comments/Special Instructions

| | | | |
|--|-------------------------------|----------------------------------|---------------------------|
| Sampled By (NAME): Harry Chamberlayne | Signature: <u>[Signature]</u> | Date: 10/26/22 (mm/dd/yy) | Print Copy - Client |
| Retrieved By (NAME): Harry Chamberlayne | Signature: <u>[Signature]</u> | Date: 10/26/22 (mm/dd/yy) | Yellow & White Copy - SGS |

Note: Submission of samples to SGS is acknowledgment that you have been provided direction on sample collection, labeling and transportation of samples. (2) Submission of samples to SGS is considered authorization for completion of work. Signature does not apply to this form or be returned with this form. (3) Results may be sent by email to an unlimited number of addresses for no additional cost. Fee is available upon request. This document is issued by the Company under its General Conditions of Service applicable at the time of issue of this form. http://www.sgs.com/terms_and_conditions.htm (Printed copies are available upon request.) Attention is drawn to the limitation of liability.



FINAL REPORT

CA40196-OCT22 R1

19-093-100, 7675 King St., Bolton

Prepared for

DS Consultants



FINAL REPORT

CA40196-OCT22 R1

First Page

| CLIENT DETAILS | | LABORATORY DETAILS | |
|----------------|-----------------------------------|--------------------|---|
| Client | DS Consultants | Project Specialist | Jill Campbell, B.Sc.,GISAS |
| Address | 6221 Highway 7 Unit 16 | Laboratory | SGS Canada Inc. |
| | Vaughan, Ontario | Address | 185 Concession St., Lakefield ON, K0L 2H0 |
| | L4H 0K8, Canada | | |
| Contact | Dorothy Santos | Telephone | 2165 |
| Telephone | 905-329-2735 | Facsimile | 705-652-6365 |
| Facsimile | 905-264-2685 | Email | jill.campbell@sgs.com |
| Email | dorothy.santos@dsconsultants.ca | SGS Reference | CA40196-OCT22 |
| Project | 19-093-100, 7675 King St., Bolton | Received | 10/26/2022 |
| Order Number | | Approved | 11/03/2022 |
| Samples | Ground Water (1) | Report Number | CA40196-OCT22 R1 |
| | | Date Reported | 11/03/2022 |

COMMENTS

RL - SGS Reporting Limit

Temperature of Sample upon Receipt: 9 degrees C

Cooling Agent Present: Yes

Custody Seal Present: Yes

Chain of Custody Number: 029795

SIGNATORIES

Jill Campbell, B.Sc.,GISAS



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FINAL REPORT

CA40196-OCT22 R1

Client: DS Consultants

Project: 19-093-100, 7675 King St., Bolton

Project Manager: Dorothy Santos

Samplers: Harry/ Chaitemya

MATRIX: WATER

Sample Number 8
Sample Name BH 22-5
Sample Matrix Ground Water
Sample Date 26/10/2022

L1 = PWQQ_L / WATER / - - Table 2 - General - July 1999 PIBS 3303E

| Parameter | Units | RL | L1 | Result |
|----------------------------------|-----------|----------|--------|-----------|
| General Chemistry | | | | |
| Biochemical Oxygen Demand (BOD5) | mg/L | 2 | | 5 |
| Total Suspended Solids | mg/L | 2 | | 94 |
| Total Kjeldahl Nitrogen | as N mg/L | 0.5 | | < 0.5 |
| Metals and Inorganics | | | | |
| Fluoride | mg/L | 0.06 | | 0.27 |
| Cyanide (total) | mg/L | 0.01 | | < 0.01 |
| Sulphate | mg/L | 2 | | 22 |
| Aluminum (total) | mg/L | 0.001 | | 4.96 |
| Antimony (total) | mg/L | 0.0009 | 0.02 | < 0.0009 |
| Arsenic (total) | mg/L | 0.0002 | 0.005 | 0.0061 |
| Cadmium (total) | mg/L | 0.000003 | 0.0001 | 0.000024 |
| Chromium (total) | mg/L | 0.00008 | 0.1 | 0.00591 |
| Copper (total) | mg/L | 0.0002 | 0.001 | 0.0056 |
| Cobalt (total) | mg/L | 0.000004 | 0.0009 | 0.00314 |
| Lead (total) | mg/L | 0.00009 | 0.005 | 0.00155 |
| Manganese (total) | mg/L | 0.00001 | | 0.148 |
| Molybdenum (total) | mg/L | 0.00004 | 0.04 | 0.00761 |
| Nickel (total) | mg/L | 0.0001 | 0.025 | 0.0064 |
| Phosphorus (total) | mg/L | 0.003 | 0.01 | 0.171 |
| Selenium (total) | mg/L | 0.00004 | 0.1 | 0.00023 |
| Silver (total) | mg/L | 0.00005 | 0.0001 | < 0.00005 |
| Tin (total) | mg/L | 0.00006 | | 0.00340 |



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Project Manager: Dorothy Santos

Samplers: Harry/ Chaitemya

MATRIX: WATER

Sample Number 8

Sample Name BH 22-5

Sample Matrix Ground Water

Sample Date 26/10/2022

L1 = PWQQ_L / WATER / - - Table 2 - General - July 1999 PIBS 3303E

| Parameter | Units | RL | L1 | Result |
|--|-----------|---------|------|--------|
| Metals and Inorganics (continued) | | | | |
| Titanium (total) | mg/L | 0.00005 | | 0.0707 |
| Zinc (total) | mg/L | 0.002 | 0.02 | 0.019 |
| Microbiology | | | | |
| E. Coli | cfu/100mL | 0 | 100 | 2 |
| Nonylphenol and Ethoxylates | | | | |
| Nonylphenol | mg/L | 0.001 | | 0.001 |
| Nonylphenol Ethoxylates | mg/L | 0.01 | | < 0.01 |
| Nonylphenol diethoxylate | mg/L | 0.01 | | < 0.01 |
| Nonylphenol monoethoxylate | mg/L | 0.01 | | < 0.01 |
| Oil and Grease | | | | |
| Oil & Grease (total) | mg/L | 2 | | < 2 |
| Oil & Grease (animal/vegetable) | mg/L | 4 | | < 4 |
| Oil & Grease (mineral/synthetic) | mg/L | 4 | | < 4 |



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MATRIX: WATER

Sample Number 8

Sample Name BH 22-5

Sample Matrix Ground Water

Sample Date 26/10/2022

L1 = PWQQ_L / WATER / - - Table 2 - General - July 1999 PIBS 3303E

| Parameter | Units | RL | L1 | Result |
|--|---------|---------|--------|-----------|
| Other (ORP) | | | | |
| pH | No unit | 0.05 | 8.6 | 8.04 |
| Mercury (total) | mg/L | 0.00001 | 0.0002 | < 0.00001 |
| PCBs | | | | |
| Polychlorinated Biphenyls (PCBs) - Total | mg/L | 0.0001 | | < 0.0001 |
| Phenols | | | | |
| 4AAP-Phenolics | mg/L | 0.002 | 0.001 | < 0.002 |
| SVOCs | | | | |
| di-n-Butyl Phthalate | mg/L | 0.002 | | < 0.002 |
| Bis(2-ethylhexyl)phthalate | mg/L | 0.002 | | < 0.002 |
| VOCs | | | | |
| Chloroform | mg/L | 0.0005 | | < 0.0005 |
| 1,2-Dichlorobenzene | mg/L | 0.0005 | | < 0.0005 |
| 1,4-Dichlorobenzene | mg/L | 0.0005 | | < 0.0005 |
| cis-1,2-Dichloroethene | mg/L | 0.0005 | | < 0.0005 |
| trans-1,3-Dichloropropene | mg/L | 0.0005 | | < 0.0005 |
| Methylene Chloride | mg/L | 0.0005 | 0.1 | < 0.0005 |
| 1,1,2,2-Tetrachloroethane | mg/L | 0.0005 | 0.07 | < 0.0005 |
| Methyl ethyl ketone | mg/L | 0.02 | | < 0.02 |
| Styrene | mg/L | 0.0005 | | < 0.0005 |
| Tetrachloroethylene (perchloroethylene) | mg/L | 0.0005 | 0.05 | < 0.0005 |
| Trichloroethylene | mg/L | 0.0005 | 0.02 | < 0.0005 |



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MATRIX: WATER

Sample Number 8

Sample Name BH 22-5

Sample Matrix Ground Water

Sample Date 26/10/2022

L1 = PWQQ_L / WATER / - - Table 2 - General - July 1999 PIBS 3303E

| Parameter | Units | RL | L1 | Result |
|--------------------|-------|--------|--------|----------|
| VOCs - BTEX | | | | |
| Benzene | mg/L | 0.0005 | 0.1 | < 0.0005 |
| Ethylbenzene | mg/L | 0.0005 | 0.008 | < 0.0005 |
| Toluene | mg/L | 0.0005 | 0.0008 | < 0.0005 |
| Xylene (total) | mg/L | 0.0005 | | < 0.0005 |
| m-p-xylene | mg/L | 0.0005 | 0.002 | < 0.0005 |
| o-xylene | mg/L | 0.0005 | 0.04 | < 0.0005 |



EXCEEDANCE SUMMARY

| Parameter | Method | Units | Result | PWQO_L / WATER / - - Table 2 - General - July 1999 PIBS 3303E L1 |
|-----------|--------|-------|--------|--|
|-----------|--------|-------|--------|--|

BH 22-5

| | | | | |
|----------------|-------------------|------|---------|--------|
| Arsenic | SM 3030/EPA 200.8 | mg/L | 0.0061 | 0.005 |
| Cobalt | SM 3030/EPA 200.8 | mg/L | 0.00314 | 0.0009 |
| Copper | SM 3030/EPA 200.8 | mg/L | 0.0056 | 0.001 |
| Phosphorus | SM 3030/EPA 200.8 | mg/L | 0.171 | 0.01 |
| 4AAP-Phenolics | SM 5530B-D | mg/L | < 0.002 | 0.001 |



FINAL REPORT

CA40196-OCT22 R1

QC SUMMARY

Anions by discrete analyzer

Method: US EPA 375.4 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-026

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Sulphate | DIO5002-NOV22 | mg/L | 2 | <2 | ND | 20 | 106 | 80 | 120 | 106 | 75 | 125 |

Biochemical Oxygen Demand

Method: SM 5210 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-007

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Biochemical Oxygen Demand (BOD5) | BOD0054-OCT22 | mg/L | 2 | < 2 | 18 | 30 | 99 | 70 | 130 | NV | 70 | 130 |

Cyanide by SFA

Method: SM 4500 | Internal ref.: ME-CA-IENVISFA-LAK-AN-005

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------------|--------------------|-------|------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Cyanide (total) | SKA0285-OCT22 | mg/L | 0.01 | <0.01 | ND | 10 | 98 | 90 | 110 | 101 | 75 | 125 |



FINAL REPORT

CA40196-OCT22 R1

QC SUMMARY

Fluoride by Specific Ion Electrode

Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-014

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------|--------------------|-------|------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Fluoride | EWL0664-OCT22 | mg/L | 0.06 | <0.06 | ND | 10 | 104 | 90 | 110 | 100 | 75 | 125 |

Mercury by CVAAS

Method: EPA 7471A/SM 3112B | Internal ref.: ME-CA-IENVISPE-LAK-AN-004

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------------|--------------------|-------|---------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Mercury (total) | EHG0051-OCT22 | mg/L | 0.00001 | < 0.00001 | 4 | 20 | 115 | 80 | 120 | 106 | 70 | 130 |



FINAL REPORT

CA40196-OCT22 R1

QC SUMMARY

Metals in aqueous samples - ICP-MS

Method: SM 3030/EPA 200.8 | Internal ref.: ME-CA-IENVISPE-LAK-AN-006

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|--------------------|--------------------|-------|----------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Silver (total) | EMS0224-OCT22 | mg/L | 0.00005 | <0.00005 | ND | 20 | 106 | 90 | 110 | 98 | 70 | 130 |
| Aluminum (total) | EMS0224-OCT22 | mg/L | 0.001 | <0.001 | 1 | 20 | 107 | 90 | 110 | 110 | 70 | 130 |
| Arsenic (total) | EMS0224-OCT22 | mg/L | 0.0002 | <0.0002 | 11 | 20 | 109 | 90 | 110 | 105 | 70 | 130 |
| Cadmium (total) | EMS0224-OCT22 | mg/L | 0.000003 | <0.000003 | ND | 20 | 106 | 90 | 110 | 101 | 70 | 130 |
| Cobalt (total) | EMS0224-OCT22 | mg/L | 0.000004 | <0.000004 | 0 | 20 | 106 | 90 | 110 | 93 | 70 | 130 |
| Chromium (total) | EMS0224-OCT22 | mg/L | 0.00008 | <0.00008 | 19 | 20 | 106 | 90 | 110 | 113 | 70 | 130 |
| Copper (total) | EMS0224-OCT22 | mg/L | 0.0002 | <0.0002 | 6 | 20 | 105 | 90 | 110 | 97 | 70 | 130 |
| Manganese (total) | EMS0224-OCT22 | mg/L | 0.00001 | <0.00001 | 1 | 20 | 109 | 90 | 110 | 108 | 70 | 130 |
| Molybdenum (total) | EMS0224-OCT22 | mg/L | 0.00004 | <0.00004 | 5 | 20 | 105 | 90 | 110 | 105 | 70 | 130 |
| Nickel (total) | EMS0224-OCT22 | mg/L | 0.0001 | <0.0001 | 5 | 20 | 102 | 90 | 110 | 94 | 70 | 130 |
| Lead (total) | EMS0224-OCT22 | mg/L | 0.00009 | <0.00001 | 18 | 20 | 106 | 90 | 110 | 95 | 70 | 130 |
| Phosphorus (total) | EMS0224-OCT22 | mg/L | 0.003 | <0.003 | 0 | 20 | 108 | 90 | 110 | NV | 70 | 130 |
| Antimony (total) | EMS0224-OCT22 | mg/L | 0.0009 | <0.0009 | ND | 20 | 101 | 90 | 110 | 94 | 70 | 130 |
| Selenium (total) | EMS0224-OCT22 | mg/L | 0.00004 | <0.00004 | 11 | 20 | 109 | 90 | 110 | 108 | 70 | 130 |
| Tin (total) | EMS0224-OCT22 | mg/L | 0.00006 | <0.00006 | ND | 20 | 104 | 90 | 110 | NV | 70 | 130 |
| Titanium (total) | EMS0224-OCT22 | mg/L | 0.00005 | <0.00005 | 13 | 20 | 106 | 90 | 110 | NV | 70 | 130 |
| Zinc (total) | EMS0224-OCT22 | mg/L | 0.002 | <0.002 | 1 | 20 | 103 | 90 | 110 | 121 | 70 | 130 |



FINAL REPORT

CA40196-OCT22 R1

QC SUMMARY

Microbiology

Method: SM 9222D | Internal ref.: ME-CA-IENVIMIC-LAK-AN-006

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------|--------------------|-----------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| E. Coli | BAC9419-OCT22 | cfu/100mL | - | ACCEPTED | ACCEPTED | | | | | | | |

Nonylphenol and Ethoxylates

Method: ASTM D7065-06 | Internal ref.: ME-CA-IENVIGC-LAK-AN-015

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------------|--------------------|-------|-------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Nonylphenol diethoxylate | GCM0431-OCT22 | mg/L | 0.01 | <0.01 | | | 113 | 55 | 120 | | | |
| Nonylphenol Ethoxylates | GCM0431-OCT22 | mg/L | 0.01 | < 0.01 | | | | | | | | |
| Nonylphenol monoethoxylate | GCM0431-OCT22 | mg/L | 0.01 | <0.01 | | | 115 | 55 | 120 | | | |
| Nonylphenol | GCM0431-OCT22 | mg/L | 0.001 | <0.001 | | | 115 | 55 | 120 | | | |



FINAL REPORT

CA40196-OCT22 R1

QC SUMMARY

Oil & Grease

Method: MOE E3401 | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Oil & Grease (total) | GCM0410-OCT22 | mg/L | 2 | <2 | NSS | 20 | 100 | 75 | 125 | | | |

Oil & Grease-AV/MS

Method: MOE E3401/SM 5520F | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Oil & Grease (animal/vegetable) | GCM0410-OCT22 | mg/L | 4 | < 4 | NSS | 20 | NA | 70 | 130 | | | |
| Oil & Grease (mineral/synthetic) | GCM0410-OCT22 | mg/L | 4 | < 4 | NSS | 20 | NA | 70 | 130 | | | |

pH

Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-006

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------|--------------------|---------|------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| pH | EWL0681-OCT22 | No unit | 0.05 | NA | 0 | | 101 | | | NA | | |



FINAL REPORT

CA40196-OCT22 R1

QC SUMMARY

Phenols by SFA

Method: SM 5530B-D | Internal ref.: ME-CA-IENVISFA-LAK-AN-006

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------|--------------------|-------|-------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| 4AAP-Phenolics | SKA0318-OCT22 | mg/L | 0.002 | <0.002 | ND | 10 | 100 | 80 | 120 | 100 | 75 | 125 |

Polychlorinated Biphenyls

Method: MOE E3400/EPA 8082A | Internal ref.: ME-CA-IENVIGC-LAK-AN-001

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|--|--------------------|-------|--------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Polychlorinated Biphenyls (PCBs) - Total | GCM0377-OCT22 | mg/L | 0.0001 | <0.0001 | NSS | 30 | 84 | 60 | 140 | NSS | 60 | 140 |



FINAL REPORT

CA40196-OCT22 R1

QC SUMMARY

Semi-Volatile Organics

Method: EPA 3510C/8270D | Internal ref.: ME-CA-IENVIGC-LAK-AN-005

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------------|--------------------|-------|-------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Bis(2-ethylhexyl)phthalate | GCM0391-OCT22 | mg/L | 0.002 | < 0.002 | NSS | 30 | 123 | 50 | 140 | NSS | 50 | 140 |
| di-n-Butyl Phthalate | GCM0391-OCT22 | mg/L | 0.002 | < 0.002 | NSS | 30 | 113 | 50 | 140 | NSS | 50 | 140 |

Suspended Solids

Method: SM 2540D | Internal ref.: ME-CA-IENVIEWL-LAK-AN-004

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|------------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Total Suspended Solids | EWL0006-NOV22 | mg/L | 2 | < 2 | 0 | 10 | 93 | 90 | 110 | NA | | |

Total Nitrogen

Method: SM 4500-N C/4500-NO3- F | Internal ref.: ME-CA-IENVISFA-LAK-AN-002

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-------------------------|--------------------|-----------|-----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Total Kjeldahl Nitrogen | SKA0015-NOV22 | as N mg/L | 0.5 | <0.5 | 2 | 10 | 100 | 90 | 110 | 107 | 75 | 125 |



FINAL REPORT

CA40196-OCT22 R1

QC SUMMARY

Volatile Organics

Method: EPA 5030B/8260C | Internal ref.: ME-CA-ENVIGC-LAK-AN-004

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|---|--------------------|-------|--------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| 1,1,2,2-Tetrachloroethane | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 92 | 60 | 130 | 94 | 50 | 140 |
| 1,2-Dichlorobenzene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 95 | 60 | 130 | 98 | 50 | 140 |
| 1,4-Dichlorobenzene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 94 | 60 | 130 | 96 | 50 | 140 |
| Benzene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 100 | 60 | 130 | 102 | 50 | 140 |
| Chloroform | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 98 | 60 | 130 | 100 | 50 | 140 |
| cis-1,2-Dichloroethene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 100 | 60 | 130 | 102 | 50 | 140 |
| Ethylbenzene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 98 | 60 | 130 | 102 | 50 | 140 |
| m-p-xylene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 97 | 60 | 130 | 100 | 50 | 140 |
| Methyl ethyl ketone | GCM0375-OCT22 | mg/L | 0.02 | <0.02 | ND | 30 | 93 | 50 | 140 | 95 | 50 | 140 |
| Methylene Chloride | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 97 | 60 | 130 | 98 | 50 | 140 |
| o-xylene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 98 | 60 | 130 | 102 | 50 | 140 |
| Styrene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 98 | 60 | 130 | 101 | 50 | 140 |
| Tetrachloroethylene (perchloroethylene) | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 96 | 60 | 130 | 100 | 50 | 140 |
| Toluene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 97 | 60 | 130 | 99 | 50 | 140 |
| trans-1,3-Dichloropropene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 96 | 60 | 130 | 97 | 50 | 140 |
| Trichloroethylene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 97 | 60 | 130 | 99 | 50 | 140 |

QC SUMMARY

Method Blank: a blank matrix that is carried through the entire analytical procedure. Used to assess laboratory contamination.

Duplicate: Paired analysis of a separate portion of the same sample that is carried through the entire analytical procedure. Used to evaluate measurement precision.

LCS/Spike Blank: Laboratory control sample or spike blank refer to a blank matrix to which a known amount of analyte has been added. Used to evaluate analyte recovery and laboratory accuracy without sample matrix effects.

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate laboratory accuracy with sample matrix effects.

Reference Material: a material or substance matrix matched to the samples that contains a known amount of the analyte of interest. A reference material may be used in place of a matrix spike.

RL: Reporting limit

RPD: Relative percent difference

AC: Acceptance criteria

Multielement Scan Qualifier: as the number of analytes in a scan increases, so does the chance of a limit exceedance by random chance as opposed to a real method problem. Thus, in multielement scans, for the LCS and matrix spike, up to 10% of the analytes may exceed the quoted limits by up to 10% absolute and the spike is considered acceptable.

Duplicate Qualifier: for duplicates as the measured result approaches the RL, the uncertainty associated with the value increases dramatically, thus duplicate acceptance limits apply only where the average of the two duplicates is greater than five times the RL.

Matrix Spike Qualifier: for matrix spikes, as the concentration of the native analyte increases, the uncertainty of the matrix spike recovery increases. Thus, the matrix spike acceptance limits apply only when the concentration of the matrix spike is greater than or equal to the concentration of the native analyte.

**LEGEND**

FOOTNOTES

NSS Insufficient sample for analysis.
RL Reporting Limit.
 ↑ Reporting limit raised.
 ↓ Reporting limit lowered.
NA The sample was not analysed for this analyte
ND Non Detect

Results relate only to the sample tested.

Data reported represent the sample as submitted to SGS. Solid samples expressed on a dry weight basis.

"Temperature Upon Receipt" is representative of the whole shipment and may not reflect the temperature of individual samples.

Analysis conducted on samples submitted pursuant to or as part of Reg. 153/04, are in accordance to the "Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act and Excess Soil Quality" published by the Ministry and dated March 9, 2004 as amended.

SGS provides criteria information (such as regulatory or guideline limits and summary of limit exceedances) as a service. Every attempt is made to ensure the criteria information in this report is accurate and current, however, it is not guaranteed. Comparison to the most current criteria is the responsibility of the client and SGS assumes no responsibility for the accuracy of the criteria levels indicated.

SGS Canada Inc. statement of conformity decision rule does not consider uncertainty when analytical results are compared to a specified standard or regulation.

This document is issued, on the Client's behalf, by the Company under its General Conditions of Service available on request and accessible at http://www.sgs.com/terms_and_conditions.htm.

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This report supersedes all previous versions.

-- End of Analytical Report --

Request for Laboratory Services and CHAIN OF CUSTODY

Laboratory Information Section - Lab use only

Received By: [Signature] Received By (signature): _____
 Received Date: 10/26/22 (mm/dd/yy) Custody Seal Present: Yes No Cooling Agent Present: Yes No Type: ICE
 Received Time: 12:00 (hr./min) Custody Seal Intact: Yes No Temperature Upon Receipt (°C): 9.9.9 LAB LIMS #: CA40196-0022

REPORT INFORMATION
 Company: DS consultants Ltd. (same as Report Information)
 Contact: Dorothy Santos
 Address: 6221 Hwy-7, Unit 10
Vaughan, ON
 Phone: 905-264-9393
 Fax: _____
 Email: dorothy.santos@dsconsultants.ca

INVOICE INFORMATION
 Company: _____
 Contact: Accounting
 Address: _____
 Phone: _____
 Email: _____

Quotation #: _____ P.O. #: _____
 Project #: 19-093-100 Site Location/ID: 7675 King St, Bolton
TURNAROUND TIME (TAT) REQUIRED
 Regular TAT (5-7days) TAT's are quoted in business days (exclude statutory holidays & weekends).
 Samples received after 6pm or on weekends; TAT begins next business day.
 RUSH TAT (Additional Charges May Apply): 1 Day 2 Days 3 Days 4 Days
 PLEASE CONFIRM RUSH FEASIBILITY WITH SGS REPRESENTATIVE PRIOR TO SUBMISSION
 Specify Due Date: _____ *NOTE: DRINKING (POTABLE) WATER SAMPLES FOR HUMAN CONSUMPTION MUST BE SUBMITTED WITH SGS DRINKING WATER CHAIN OF CUSTODY

REGULATIONS
 O.Reg 153/04 O.Reg 405/19
 Table 1 Res/Pans Soil Texture
 Table 2 Ind/Com Coarse
 Table 3 Agri/Other Medium/Fine
 Table _____ Appx. _____
 Soil Volume: <350m3 >350m3
 Other Regulations: Reg 347/551 (3 Day min TAT) P/NOC NMBR
 CCME Other: _____
 MGA DOWS Not Responsible *See note
 Sower By-Law: Sanitary Storm
 Municipality: Peel

ANALYSIS REQUESTED

| M & I | SVOC | PCB | PHC | VOC | Peat | Other (please specify) | SPLP | TCLP | COMMENTS: |
|---------------------------------------|-------------------------------|--|-------------------------------------|---|-------------------------------------|---|--|--|----------------------------|
| Field Filtered (V/VN) | PAHs only | PCBs Total <input type="checkbox"/> Aroclor <input type="checkbox"/> | F1-F4 + BTEX | VOCs <input type="checkbox"/> BTEX only | Pesticides <input type="checkbox"/> | Peel Sanitary/Storm Sewer <input checked="" type="checkbox"/> | <input type="checkbox"/> Sewer Use: <input type="checkbox"/> Surface <input type="checkbox"/> Ground | <input type="checkbox"/> Sewer Use: <input type="checkbox"/> Surface <input type="checkbox"/> Ground | <u>Non-Filtered sample</u> |
| Metals & Inorganics (ICP Metals only) | SVOCs (Total PAHs, PCBs, CPs) | PCBs | F1-F4 only <input type="checkbox"/> | VOCs <input type="checkbox"/> BTEX only | Pesticides (Specify/Identify) | Peel Sanitary/Storm Sewer <input checked="" type="checkbox"/> | <input type="checkbox"/> Sewer Use: <input type="checkbox"/> Surface <input type="checkbox"/> Ground | <input type="checkbox"/> Sewer Use: <input type="checkbox"/> Surface <input type="checkbox"/> Ground | |
| Full Metals Suite (ICP Metals only) | PAHs only | PCBs Total <input type="checkbox"/> Aroclor <input type="checkbox"/> | F1-F4 + BTEX | VOCs <input type="checkbox"/> BTEX only | Pesticides (Specify/Identify) | Peel Sanitary/Storm Sewer <input checked="" type="checkbox"/> | <input type="checkbox"/> Sewer Use: <input type="checkbox"/> Surface <input type="checkbox"/> Ground | <input type="checkbox"/> Sewer Use: <input type="checkbox"/> Surface <input type="checkbox"/> Ground | |
| ICP Metals only (ICP Metals only) | PAHs only | PCBs Total <input type="checkbox"/> Aroclor <input type="checkbox"/> | F1-F4 + BTEX | VOCs <input type="checkbox"/> BTEX only | Pesticides (Specify/Identify) | Peel Sanitary/Storm Sewer <input checked="" type="checkbox"/> | <input type="checkbox"/> Sewer Use: <input type="checkbox"/> Surface <input type="checkbox"/> Ground | <input type="checkbox"/> Sewer Use: <input type="checkbox"/> Surface <input type="checkbox"/> Ground | |

RECORD OF SITE CONDITION (RSC) YES NO

| SAMPLE IDENTIFICATION | DATE SAMPLED | TIME SAMPLED | # OF BOTTLES | MATRIX |
|-----------------------|----------------------------|--------------|--------------|------------|
| <u>BH 22-5</u> | <u>Oct 26th</u> | <u>12 PM</u> | <u>17</u> | <u>GrW</u> |
| | | | | |
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Observations/Comments/Special Instructions: _____

Sampled By (NAME): Harry Charbonneau Signature: [Signature] Date: 10/26/22 (mm/dd/yy) Pink Copy - Client
 Retrievished by (NAME): [Signature] Signature: [Signature] Date: 10/26/22 (mm/dd/yy) Yellow & White Copy - SGS

Note: Submission of samples to SGS is acknowledgment that you have been provided direction on sample collection, sealing and transportation of samples. (2) Submission of samples to SGS is considered authorization for verification of work. Signatures may appear on this form or be returned on file in the contract, or in an alternative format (e.g. e-mailing photos). (3) Results may be sent by email to an unlimited number of addresses for no additional cost. Fax is available upon request. This document is issued by the Company under its General Conditions of Service applicable at the time of issue of this form. http://www.sgs.com/terms_and_conditions.html (Printed copies are available upon request.) Attention is drawn to the limitation of liability.



FINAL REPORT

CA40197-OCT22 R1

19-093-100, 7675 King St, Bolton

Prepared for

DS Consultants



FINAL REPORT

CA40197-OCT22 R1

First Page

| CLIENT DETAILS | | LABORATORY DETAILS | |
|----------------|----------------------------------|--------------------|---|
| Client | DS Consultants | Project Specialist | Jill Campbell, B.Sc.,GISAS |
| Address | 6221 Highway 7 Unit 16 | Laboratory | SGS Canada Inc. |
| | Vaughan, Ontario | Address | 185 Concession St., Lakefield ON, K0L 2H0 |
| | L4H 0K8, Canada | | |
| Contact | Dorothy Santos | Telephone | 2165 |
| Telephone | 905-329-2735 | Facsimile | 705-652-6365 |
| Facsimile | 905-264-2685 | Email | jill.campbell@sgs.com |
| Email | dorothy.santos@dsconsultants.ca | SGS Reference | CA40197-OCT22 |
| Project | 19-093-100, 7675 King St, Bolton | Received | 10/26/2022 |
| Order Number | | Approved | 11/03/2022 |
| Samples | Ground Water (1) | Report Number | CA40197-OCT22 R1 |
| | | Date Reported | 11/03/2022 |

COMMENTS

RL - SGS Reporting Limit

Temperature of Sample upon Receipt: 9 degrees C

Cooling Agent Present: Yes

Custody Seal Present: Yes

Chain of Custody Number: 029796

Note: Elevated E coli reporting limit due to excessive growth of bacteria at higher volumes.

SIGNATORIES

Jill Campbell, B.Sc.,GISAS



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FINAL REPORT

CA40197-OCT22 R1

Client: DS Consultants

Project: 19-093-100, 7675 King St, Bolton

Project Manager: Dorothy Santos

Samplers: Harry/Chaitanyo

MATRIX: WATER

Sample Number 8

Sample Name BH 22-1

Sample Matrix Ground Water

Sample Date 26/10/2022

L1 = SANSEW / WATER / - - Peel Table 1 - Sanitary Sewer Discharge - BL_53_2010

L2 = SANSEW / WATER / - - Peel Table 2 - Storm Sewer Discharge - BL_53_2010

| Parameter | Units | RL | L1 | L2 | Result |
|-----------|-------|----|----|----|--------|
|-----------|-------|----|----|----|--------|

General Chemistry

| | | | | | |
|----------------------------------|-----------|-----|-----|----|-------|
| Biochemical Oxygen Demand (BOD5) | mg/L | 2 | 300 | 15 | < 4 † |
| Total Suspended Solids | mg/L | 2 | 350 | 15 | 38300 |
| Total Kjeldahl Nitrogen | as N mg/L | 0.5 | 100 | 1 | < 0.5 |

Metals and Inorganics

| | | | | | |
|--------------------|------|----------|------|-------|----------|
| Fluoride | mg/L | 0.06 | 10 | | 0.14 |
| Cyanide (total) | mg/L | 0.01 | 2 | 0.02 | < 0.01 |
| Sulphate | mg/L | 2 | 1500 | | 24 |
| Aluminum (total) | mg/L | 0.001 | 50 | | 15.7 |
| Antimony (total) | mg/L | 0.0009 | 5 | | < 0.0009 |
| Arsenic (total) | mg/L | 0.0002 | 1 | 0.02 | 0.0072 |
| Cadmium (total) | mg/L | 0.000003 | 0.7 | 0.008 | 0.000178 |
| Chromium (total) | mg/L | 0.00008 | 5 | 0.08 | 0.0326 |
| Copper (total) | mg/L | 0.0002 | 3 | 0.05 | 0.0266 |
| Cobalt (total) | mg/L | 0.000004 | 5 | | 0.0125 |
| Lead (total) | mg/L | 0.00009 | 3 | 0.12 | 0.0180 |
| Manganese (total) | mg/L | 0.00001 | 5 | 0.05 | 2.17 |
| Molybdenum (total) | mg/L | 0.00004 | 5 | | 0.00230 |
| Nickel (total) | mg/L | 0.0001 | 3 | 0.08 | 0.0248 |
| Phosphorus (total) | mg/L | 0.003 | 10 | 0.4 | 3.12 |
| Selenium (total) | mg/L | 0.00004 | 1 | 0.02 | 0.00022 |
| Silver (total) | mg/L | 0.00005 | 5 | 0.12 | 0.00006 |
| Tin (total) | mg/L | 0.00006 | 5 | | 0.00227 |



FINAL REPORT

CA40197-OCT22 R1

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Sample Number 8

Sample Name BH 22-1

Sample Matrix Ground Water

Sample Date 26/10/2022

L1 = SANSEW / WATER / - - Peel Table 1 - Sanitary Sewer Discharge - BL_53_2010

L2 = SANSEW / WATER / - - Peel Table 2 - Storm Sewer Discharge - BL_53_2010

| Parameter | Units | RL | L1 | L2 | Result |
|-----------|-------|----|----|----|--------|
|-----------|-------|----|----|----|--------|

Metals and Inorganics (continued)

| | | | | | |
|------------------|------|---------|---|------|-------|
| Titanium (total) | mg/L | 0.00005 | 5 | | 0.576 |
| Zinc (total) | mg/L | 0.002 | 3 | 0.04 | 0.057 |

Microbiology

| | | | | | |
|---------|-----------|---|--|-----|--------|
| E. Coli | cfu/100mL | 0 | | 200 | < 20 † |
|---------|-----------|---|--|-----|--------|

Nonylphenol and Ethoxylates

| | | | | | |
|----------------------------|------|-------|------|--|---------|
| Nonylphenol | mg/L | 0.001 | 0.02 | | < 0.001 |
| Nonylphenol Ethoxylates | mg/L | 0.01 | 0.2 | | < 0.01 |
| Nonylphenol diethoxylate | mg/L | 0.01 | | | < 0.01 |
| Nonylphenol monoethoxylate | mg/L | 0.01 | | | < 0.01 |

Oil and Grease

| | | | | | |
|----------------------------------|------|---|-----|--|-------|
| Oil & Grease (total) | mg/L | 2 | | | < 4 † |
| Oil & Grease (animal/vegetable) | mg/L | 4 | 150 | | < 4 |
| Oil & Grease (mineral/synthetic) | mg/L | 4 | 15 | | < 4 |



FINAL REPORT

CA40197-OCT22 R1

Client: DS Consultants

Project: 19-093-100, 7675 King St, Bolton

Project Manager: Dorothy Santos

Samplers: Harry/Chaitanyo

MATRIX: WATER

Sample Number 8

Sample Name BH 22-1

Sample Matrix Ground Water

Sample Date 26/10/2022

L1 = SANSEW / WATER / - - Peel Table 1 - Sanitary Sewer Discharge - BL_53_2010

L2 = SANSEW / WATER / - - Peel Table 2 - Storm Sewer Discharge - BL_53_2010

| Parameter | Units | RL | L1 | L2 | Result |
|--|---------|---------|-------|--------|----------|
| Other (ORP) | | | | | |
| pH | No unit | 0.05 | 10 | 9 | 7.72 |
| Mercury (total) | mg/L | 0.00001 | 0.01 | 0.0004 | 0.00002 |
| PCBs | | | | | |
| Polychlorinated Biphenyls (PCBs) - Total | mg/L | 0.0001 | 0.001 | 0.0004 | < 0.0001 |
| Phenols | | | | | |
| 4AAP-Phenolics | mg/L | 0.002 | 1 | 0.008 | < 0.002 |
| SVOCs | | | | | |
| di-n-Butyl Phthalate | mg/L | 0.002 | 0.08 | 0.015 | < 0.002 |
| Bis(2-ethylhexyl)phthalate | mg/L | 0.002 | 0.012 | 0.0088 | < 0.002 |
| VOCs | | | | | |
| Chloroform | mg/L | 0.0005 | 0.04 | 0.002 | < 0.0005 |
| 1,2-Dichlorobenzene | mg/L | 0.0005 | 0.05 | 0.0056 | < 0.0005 |
| 1,4-Dichlorobenzene | mg/L | 0.0005 | 0.08 | 0.0068 | < 0.0005 |
| cis-1,2-Dichloroethene | mg/L | 0.0005 | 4 | 0.0056 | < 0.0005 |
| trans-1,3-Dichloropropene | mg/L | 0.0005 | 0.14 | 0.0056 | < 0.0005 |
| Methylene Chloride | mg/L | 0.0005 | 2 | 0.0052 | < 0.0005 |
| 1,1,2,2-Tetrachloroethane | mg/L | 0.0005 | 1.4 | 0.017 | < 0.0005 |
| Methyl ethyl ketone | mg/L | 0.02 | 8 | | < 0.02 |
| Styrene | mg/L | 0.0005 | 0.2 | | < 0.0005 |
| Tetrachloroethylene (perchloroethylene) | mg/L | 0.0005 | 1 | 0.0044 | < 0.0005 |
| Trichloroethylene | mg/L | 0.0005 | 0.4 | 0.008 | < 0.0005 |



FINAL REPORT

CA40197-OCT22 R1

Client: DS Consultants

Project: 19-093-100, 7675 King St, Bolton

Project Manager: Dorothy Santos

Samplers: Harry/Chaitanyo

MATRIX: WATER

Sample Number 8

Sample Name BH 22-1

Sample Matrix Ground Water

Sample Date 26/10/2022

L1 = SANSEW / WATER / - - Peel Table 1 - Sanitary Sewer Discharge - BL_53_2010

L2 = SANSEW / WATER / - - Peel Table 2 - Storm Sewer Discharge - BL_53_2010

| Parameter | Units | RL | L1 | L2 | Result |
|--------------------|-------|--------|------|--------|----------|
| VOCs - BTEX | | | | | |
| Benzene | mg/L | 0.0005 | 0.01 | 0.002 | < 0.0005 |
| Ethylbenzene | mg/L | 0.0005 | 0.16 | 0.002 | < 0.0005 |
| Toluene | mg/L | 0.0005 | 0.27 | 0.002 | 0.0005 |
| Xylene (total) | mg/L | 0.0005 | 1.4 | 0.0044 | < 0.0005 |
| m-p-xylene | mg/L | 0.0005 | | | < 0.0005 |
| o-xylene | mg/L | 0.0005 | | | < 0.0005 |



EXCEEDANCE SUMMARY

| Parameter | Method | Units | Result | SANSEW / WATER | SANSEW / WATER |
|-----------|--------|-------|--------|---|--|
| | | | | / - - Peel Table 1 - Sanitary Sewer Discharge - BL_53_2010 L1 | / - - Peel Table 2 - Storm Sewer Discharge - BL_53_2010 L2 |

BH 22-1

| | | | | | |
|------------------------|-------------------|------|-------|-----|------|
| Total Suspended Solids | SM 2540D | mg/L | 38300 | 350 | 15 |
| Manganese | SM 3030/EPA 200.8 | mg/L | 2.17 | | 0.05 |
| Phosphorus | SM 3030/EPA 200.8 | mg/L | 3.12 | | 0.4 |
| Zinc | SM 3030/EPA 200.8 | mg/L | 0.057 | | 0.04 |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Anions by discrete analyzer

Method: US EPA 375.4 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-026

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Sulphate | DIO5002-NOV22 | mg/L | 2 | <2 | ND | 20 | 106 | 80 | 120 | 106 | 75 | 125 |

Biochemical Oxygen Demand

Method: SM 5210 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-007

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Biochemical Oxygen Demand (BOD5) | BOD0054-OCT22 | mg/L | 2 | < 2 | 18 | 30 | 99 | 70 | 130 | NV | 70 | 130 |

Cyanide by SFA

Method: SM 4500 | Internal ref.: ME-CA-IENVISFA-LAK-AN-005

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------------|--------------------|-------|------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Cyanide (total) | SKA0285-OCT22 | mg/L | 0.01 | <0.01 | ND | 10 | 98 | 90 | 110 | 101 | 75 | 125 |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Fluoride by Specific Ion Electrode

Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-014

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------|--------------------|-------|------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Fluoride | EWL0664-OCT22 | mg/L | 0.06 | <0.06 | ND | 10 | 104 | 90 | 110 | 100 | 75 | 125 |

Mercury by CVAAS

Method: EPA 7471A/SM 3112B | Internal ref.: ME-CA-IENVISPE-LAK-AN-004

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------------|--------------------|-------|---------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Mercury (total) | EHG0051-OCT22 | mg/L | 0.00001 | < 0.00001 | 4 | 20 | 115 | 80 | 120 | 106 | 70 | 130 |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Metals in aqueous samples - ICP-MS

Method: SM 3030/EPA 200.8 | Internal ref.: ME-CA-IENVISPE-LAK-AN-006

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|--------------------|--------------------|-------|----------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Silver (total) | EMS0217-OCT22 | mg/L | 0.00005 | <0.00005 | ND | 20 | 104 | 90 | 110 | 102 | 70 | 130 |
| Aluminum (total) | EMS0217-OCT22 | mg/L | 0.001 | <0.001 | 3 | 20 | 103 | 90 | 110 | 107 | 70 | 130 |
| Arsenic (total) | EMS0217-OCT22 | mg/L | 0.0002 | <0.0002 | ND | 20 | 110 | 90 | 110 | 106 | 70 | 130 |
| Cadmium (total) | EMS0217-OCT22 | mg/L | 0.000003 | <0.000003 | ND | 20 | 103 | 90 | 110 | 102 | 70 | 130 |
| Cobalt (total) | EMS0217-OCT22 | mg/L | 0.000004 | <0.000004 | 2 | 20 | 104 | 90 | 110 | 99 | 70 | 130 |
| Chromium (total) | EMS0217-OCT22 | mg/L | 0.00008 | <0.00008 | 4 | 20 | 105 | 90 | 110 | 104 | 70 | 130 |
| Copper (total) | EMS0217-OCT22 | mg/L | 0.0002 | <0.0002 | 5 | 20 | 105 | 90 | 110 | 92 | 70 | 130 |
| Manganese (total) | EMS0217-OCT22 | mg/L | 0.00001 | <0.00001 | ND | 20 | 107 | 90 | 110 | 83 | 70 | 130 |
| Molybdenum (total) | EMS0217-OCT22 | mg/L | 0.00004 | <0.00004 | ND | 20 | 105 | 90 | 110 | 105 | 70 | 130 |
| Nickel (total) | EMS0217-OCT22 | mg/L | 0.0001 | <0.0001 | ND | 20 | 105 | 90 | 110 | 90 | 70 | 130 |
| Lead (total) | EMS0217-OCT22 | mg/L | 0.00009 | <0.00001 | 3 | 20 | 103 | 90 | 110 | 93 | 70 | 130 |
| Phosphorus (total) | EMS0217-OCT22 | mg/L | 0.003 | <0.003 | ND | 20 | 97 | 90 | 110 | NV | 70 | 130 |
| Antimony (total) | EMS0217-OCT22 | mg/L | 0.0009 | <0.0009 | ND | 20 | 103 | 90 | 110 | 106 | 70 | 130 |
| Selenium (total) | EMS0217-OCT22 | mg/L | 0.00004 | <0.00004 | ND | 20 | 110 | 90 | 110 | 100 | 70 | 130 |
| Tin (total) | EMS0217-OCT22 | mg/L | 0.00006 | <0.00006 | ND | 20 | 106 | 90 | 110 | NV | 70 | 130 |
| Titanium (total) | EMS0217-OCT22 | mg/L | 0.00005 | <0.00005 | ND | 20 | 105 | 90 | 110 | NV | 70 | 130 |
| Zinc (total) | EMS0217-OCT22 | mg/L | 0.002 | <0.002 | 1 | 20 | 102 | 90 | 110 | 104 | 70 | 130 |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Microbiology

Method: SM 9222D | Internal ref.: ME-CA-IENVIMIC-LAK-AN-006

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------|--------------------|-----------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| E. Coli | BAC9419-OCT22 | cfu/100mL | - | ACCEPTED | ACCEPTED | | | | | | | |

Nonylphenol and Ethoxylates

Method: ASTM D7065-06 | Internal ref.: ME-CA-IENVIGC-LAK-AN-015

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------------|--------------------|-------|-------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Nonylphenol diethoxylate | GCM0431-OCT22 | mg/L | 0.01 | <0.01 | | | 113 | 55 | 120 | | | |
| Nonylphenol Ethoxylates | GCM0431-OCT22 | mg/L | 0.01 | < 0.01 | | | | | | | | |
| Nonylphenol monoethoxylate | GCM0431-OCT22 | mg/L | 0.01 | <0.01 | | | 115 | 55 | 120 | | | |
| Nonylphenol | GCM0431-OCT22 | mg/L | 0.001 | <0.001 | | | 115 | 55 | 120 | | | |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Oil & Grease

Method: MOE E3401 | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Oil & Grease (total) | GCM0410-OCT22 | mg/L | 2 | <2 | NSS | 20 | 100 | 75 | 125 | | | |

Oil & Grease-AV/MS

Method: MOE E3401/SM 5520F | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Oil & Grease (animal/vegetable) | GCM0410-OCT22 | mg/L | 4 | < 4 | NSS | 20 | NA | 70 | 130 | | | |
| Oil & Grease (mineral/synthetic) | GCM0410-OCT22 | mg/L | 4 | < 4 | NSS | 20 | NA | 70 | 130 | | | |

pH

Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-006

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------|--------------------|---------|------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| pH | EWL0681-OCT22 | No unit | 0.05 | NA | 0 | | 101 | | | NA | | |



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CA40197-OCT22 R1

QC SUMMARY

Phenols by SFA

Method: SM 5530B-D | Internal ref.: ME-CA-IENVISFA-LAK-AN-006

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------|--------------------|-------|-------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| 4AAP-Phenolics | SKA0318-OCT22 | mg/L | 0.002 | <0.002 | ND | 10 | 100 | 80 | 120 | 100 | 75 | 125 |

Polychlorinated Biphenyls

Method: MOE E3400/EPA 8082A | Internal ref.: ME-CA-IENVIGC-LAK-AN-001

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|--|--------------------|-------|--------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Polychlorinated Biphenyls (PCBs) - Total | GCM0377-OCT22 | mg/L | 0.0001 | <0.0001 | NSS | 30 | 84 | 60 | 140 | NSS | 60 | 140 |



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CA40197-OCT22 R1

QC SUMMARY

Semi-Volatile Organics

Method: EPA 3510C/8270D | Internal ref.: ME-CA-IENVIGC-LAK-AN-005

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------------|--------------------|-------|-------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Bis(2-ethylhexyl)phthalate | GCM0391-OCT22 | mg/L | 0.002 | < 0.002 | NSS | 30 | 123 | 50 | 140 | NSS | 50 | 140 |
| di-n-Butyl Phthalate | GCM0391-OCT22 | mg/L | 0.002 | < 0.002 | NSS | 30 | 113 | 50 | 140 | NSS | 50 | 140 |

Suspended Solids

Method: SM 2540D | Internal ref.: ME-CA-IENVIEWL-LAK-AN-004

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|------------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Total Suspended Solids | EWL0006-NOV22 | mg/L | 2 | < 2 | 0 | 10 | 93 | 90 | 110 | NA | | |

Total Nitrogen

Method: SM 4500-N C/4500-NO3- F | Internal ref.: ME-CA-IENVISFA-LAK-AN-002

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-------------------------|--------------------|-----------|-----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Total Kjeldahl Nitrogen | SKA0004-NOV22 | as N mg/L | 0.5 | <0.5 | 2 | 10 | 98 | 90 | 110 | 106 | 75 | 125 |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Volatile Organics

Method: EPA 5030B/8260C | Internal ref.: ME-CA-ENVIGC-LAK-AN-004

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|---|--------------------|-------|--------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| 1,1,2,2-Tetrachloroethane | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 92 | 60 | 130 | 94 | 50 | 140 |
| 1,2-Dichlorobenzene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 95 | 60 | 130 | 98 | 50 | 140 |
| 1,4-Dichlorobenzene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 94 | 60 | 130 | 96 | 50 | 140 |
| Benzene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 100 | 60 | 130 | 102 | 50 | 140 |
| Chloroform | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 98 | 60 | 130 | 100 | 50 | 140 |
| cis-1,2-Dichloroethene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 100 | 60 | 130 | 102 | 50 | 140 |
| Ethylbenzene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 98 | 60 | 130 | 102 | 50 | 140 |
| m-p-xylene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 97 | 60 | 130 | 100 | 50 | 140 |
| Methyl ethyl ketone | GCM0375-OCT22 | mg/L | 0.02 | <0.02 | ND | 30 | 93 | 50 | 140 | 95 | 50 | 140 |
| Methylene Chloride | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 97 | 60 | 130 | 98 | 50 | 140 |
| o-xylene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 98 | 60 | 130 | 102 | 50 | 140 |
| Styrene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 98 | 60 | 130 | 101 | 50 | 140 |
| Tetrachloroethylene (perchloroethylene) | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 96 | 60 | 130 | 100 | 50 | 140 |
| Toluene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 97 | 60 | 130 | 99 | 50 | 140 |
| trans-1,3-Dichloropropene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 96 | 60 | 130 | 97 | 50 | 140 |
| Trichloroethylene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 97 | 60 | 130 | 99 | 50 | 140 |

QC SUMMARY

Method Blank: a blank matrix that is carried through the entire analytical procedure. Used to assess laboratory contamination.

Duplicate: Paired analysis of a separate portion of the same sample that is carried through the entire analytical procedure. Used to evaluate measurement precision.

LCS/Spike Blank: Laboratory control sample or spike blank refer to a blank matrix to which a known amount of analyte has been added. Used to evaluate analyte recovery and laboratory accuracy without sample matrix effects.

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate laboratory accuracy with sample matrix effects.

Reference Material: a material or substance matrix matched to the samples that contains a known amount of the analyte of interest. A reference material may be used in place of a matrix spike.

RL: Reporting limit

RPD: Relative percent difference

AC: Acceptance criteria

Multielement Scan Qualifier: as the number of analytes in a scan increases, so does the chance of a limit exceedance by random chance as opposed to a real method problem. Thus, in multielement scans, for the LCS and matrix spike, up to 10% of the analytes may exceed the quoted limits by up to 10% absolute and the spike is considered acceptable.

Duplicate Qualifier: for duplicates as the measured result approaches the RL, the uncertainty associated with the value increases dramatically, thus duplicate acceptance limits apply only where the average of the two duplicates is greater than five times the RL.

Matrix Spike Qualifier: for matrix spikes, as the concentration of the native analyte increases, the uncertainty of the matrix spike recovery increases. Thus, the matrix spike acceptance limits apply only when the concentration of the matrix spike is greater than or equal to the concentration of the native analyte.



LEGEND

FOOTNOTES

- NSS** Insufficient sample for analysis.
- RL** Reporting Limit.
 - ↑ Reporting limit raised.
 - ↓ Reporting limit lowered.
- NA** The sample was not analysed for this analyte
- ND** Non Detect

Results relate only to the sample tested.

Data reported represent the sample as submitted to SGS. Solid samples expressed on a dry weight basis.

"Temperature Upon Receipt" is representative of the whole shipment and may not reflect the temperature of individual samples.

Analysis conducted on samples submitted pursuant to or as part of Reg. 153/04, are in accordance to the "Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act and Excess Soil Quality" published by the Ministry and dated March 9, 2004 as amended.

SGS provides criteria information (such as regulatory or guideline limits and summary of limit exceedances) as a service. Every attempt is made to ensure the criteria information in this report is accurate and current, however, it is not guaranteed. Comparison to the most current criteria is the responsibility of the client and SGS assumes no responsibility for the accuracy of the criteria levels indicated.

SGS Canada Inc. statement of conformity decision rule does not consider uncertainty when analytical results are compared to a specified standard or regulation.

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This report supersedes all previous versions.

-- End of Analytical Report --



Request for Laboratory Services and CHAIN OF CUSTODY

No: 029796

Page 1 of 1

Laboratory Information Section - Lab use only

Received By: [Signature]
 Received Date: 10/26/22 (month/day)
 Received Time: 17:50 (hr./min)

Received By (signature): [Signature]
 Custody Seal Present: Yes No
 Custody Seal Intact: Yes No
 Cooling Agent Present: Yes No Type: Ice
 Temperature Upon Receipt (°C): 9.2/3

LAB LIMS # CA40197-001
22

| REPORT INFORMATION | INVOICE INFORMATION |
|---|--|
| Company: <u>DS Consultants</u> | <input checked="" type="checkbox"/> (same as Report Information) |
| Contact: <u>Dorothy Santos</u> | Company: _____ |
| Address: <u>6221 Hwy 7, Unit 16 Vaughan, ON</u> | Contact: <u>Accounting</u> |
| Phone: <u>905 329 2735</u> | Address: _____ |
| Fax: _____ | Phone: _____ |
| Email: <u>dorothy.santos@dsconsultants.com</u> | Email: _____ |

Quotation #: _____ P.O. #: _____
 Project #: 19-093-100 Site Location/ID: 7675 King St. Bolton

TURNAROUND TIME (TAT) REQUIRED
 Regular TAT (5-7 days) TATs are quoted in business days (exclude statutory holidays & weekends). Samples received after 5pm or on weekends, TAT begins next business day.
 1 Day 2 Days 3 Days 4 Days
RUSH TAT (Additional Charges May Apply):
 PLEASE CONFIRM RUSH FEASIBILITY WITH SGS REPRESENTATIVE PRIOR TO SUBMISSION

Specify Due Date: _____ *NOTE: DRINKING (POTABLE) WATER SAMPLES FOR HUMAN CONSUMPTION MUST BE SUBMITTED WITH SGS DRINKING WATER CHAIN OF CUSTODY

REGULATIONS

O.Reg 153/04 O.Reg 405/19

Other Regulations:
 Reg 347/553 (3 Day min TAT)
 P/VOC MMR
 CCME Other: _____
 MSA
 DOWS Not Responsible *See note

Sewer By-Law:
 Sanyal
 Storm
 Municipality: PCCL

| M & I | SVOC | PCB | PHC | VOC | Post | Other (please specify) | SPLP | TCLP |
|--------------------|-----------|--|--------------|---|-------------------------------------|------------------------|---------------|---------------|
| Field Filled (Y/N) | PAHs only | PCBs Total <input type="checkbox"/> Aroclor <input type="checkbox"/> | F1-F4 + BTEX | VOCs <input type="checkbox"/> BTEX only | Pesticides <input type="checkbox"/> | Other (please specify) | Specify tests | Specify tests |

RECORD OF SITE CONDITION (RSC) YES NO

| SAMPLE IDENTIFICATION | DATE SAMPLED | TIME SAMPLED | # OF BOTTLES | MATRIX |
|-----------------------|-------------------|--------------|--------------|-----------|
| 1 <u>BH 22-1</u> | <u>Oct 26, 22</u> | <u>PM</u> | <u>17</u> | <u>GW</u> |
| 2 | | | | |
| 3 | | | | |
| 4 | | | | |
| 5 | | | | |
| 6 | | | | |
| 7 | | | | |
| 8 | | | | |
| 9 | | | | |
| 10 | | | | |
| 11 | | | | |
| 12 | | | | |

| Metals & Inorganics | Full Metals Suite | ICP Metals only | PAHs only | SVOCs | PCBs | F1-F4 + BTEX | F1-F4 only | VOCs | BTEX only | Pesticides | Other (please specify) | SPLP | TCLP |
|---------------------|-------------------|-----------------|-----------|-------|------|--------------|------------|------|-----------|------------|------------------------|------|------|
| | | | | | | | | | | | | | |

COMMENTS:

Non Filtered Sample

Observed/Comments/Special Instructions: _____

Sampled By (NAME): Hony Chaitanya Signature: [Signature] Date: 10/26/22 (month/day)
 Requisitioned by (NAME): [Signature] Signature: [Signature] Date: 10/26/22 (month/day)



FINAL REPORT

CA40197-OCT22 R1

19-093-100, 7675 King St, Bolton

Prepared for

DS Consultants



FINAL REPORT

CA40197-OCT22 R1

First Page

| CLIENT DETAILS | | LABORATORY DETAILS | |
|----------------|----------------------------------|--------------------|---|
| Client | DS Consultants | Project Specialist | Jill Campbell, B.Sc.,GISAS |
| Address | 6221 Highway 7 Unit 16 | Laboratory | SGS Canada Inc. |
| | Vaughan, Ontario | Address | 185 Concession St., Lakefield ON, K0L 2H0 |
| | L4H 0K8, Canada | | |
| Contact | Dorothy Santos | Telephone | 2165 |
| Telephone | 905-329-2735 | Facsimile | 705-652-6365 |
| Facsimile | 905-264-2685 | Email | jill.campbell@sgs.com |
| Email | dorothy.santos@dsconsultants.ca | SGS Reference | CA40197-OCT22 |
| Project | 19-093-100, 7675 King St, Bolton | Received | 10/26/2022 |
| Order Number | | Approved | 11/03/2022 |
| Samples | Ground Water (1) | Report Number | CA40197-OCT22 R1 |
| | | Date Reported | 11/03/2022 |

COMMENTS

RL - SGS Reporting Limit

Temperature of Sample upon Receipt: 9 degrees C

Cooling Agent Present: Yes

Custody Seal Present: Yes

Chain of Custody Number: 029796

Note: Elevated E coli reporting limit due to excessive growth of bacteria at higher volumes.

SIGNATORIES

Jill Campbell, B.Sc.,GISAS



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FINAL REPORT

CA40197-OCT22 R1

Client: DS Consultants

Project: 19-093-100, 7675 King St, Bolton

Project Manager: Dorothy Santos

Samplers: Harry/Chaitanyo

MATRIX: WATER

Sample Number 8

Sample Name BH 22-1

Sample Matrix Ground Water

Sample Date 26/10/2022

L1 = PWQQ_L / WATER / - - Table 2 - General - July 1999 PIBS 3303E

| Parameter | Units | RL | L1 | Result |
|----------------------------------|-----------|----------|--------|----------|
| General Chemistry | | | | |
| Biochemical Oxygen Demand (BOD5) | mg/L | 2 | | < 4 † |
| Total Suspended Solids | mg/L | 2 | | 38300 |
| Total Kjeldahl Nitrogen | as N mg/L | 0.5 | | < 0.5 |
| Metals and Inorganics | | | | |
| Fluoride | mg/L | 0.06 | | 0.14 |
| Cyanide (total) | mg/L | 0.01 | | < 0.01 |
| Sulphate | mg/L | 2 | | 24 |
| Aluminum (total) | mg/L | 0.001 | | 15.7 |
| Antimony (total) | mg/L | 0.0009 | 0.02 | < 0.0009 |
| Arsenic (total) | mg/L | 0.0002 | 0.005 | 0.0072 |
| Cadmium (total) | mg/L | 0.000003 | 0.0001 | 0.000178 |
| Chromium (total) | mg/L | 0.00008 | 0.1 | 0.0326 |
| Copper (total) | mg/L | 0.0002 | 0.001 | 0.0266 |
| Cobalt (total) | mg/L | 0.000004 | 0.0009 | 0.0125 |
| Lead (total) | mg/L | 0.00009 | 0.005 | 0.0180 |
| Manganese (total) | mg/L | 0.00001 | | 2.17 |
| Molybdenum (total) | mg/L | 0.00004 | 0.04 | 0.00230 |
| Nickel (total) | mg/L | 0.0001 | 0.025 | 0.0248 |
| Phosphorus (total) | mg/L | 0.003 | 0.01 | 3.12 |
| Selenium (total) | mg/L | 0.00004 | 0.1 | 0.00022 |
| Silver (total) | mg/L | 0.00005 | 0.0001 | 0.00006 |
| Tin (total) | mg/L | 0.00006 | | 0.00227 |



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Sample Number 8

Sample Name BH 22-1

Sample Matrix Ground Water

Sample Date 26/10/2022

L1 = PWQQ_L / WATER / - - Table 2 - General - July 1999 PIBS 3303E

| Parameter | Units | RL | L1 | Result |
|--|-----------|---------|------|---------|
| Metals and Inorganics (continued) | | | | |
| Titanium (total) | mg/L | 0.00005 | | 0.576 |
| Zinc (total) | mg/L | 0.002 | 0.02 | 0.057 |
| Microbiology | | | | |
| E. Coli | cfu/100mL | 0 | 100 | < 20 † |
| Nonylphenol and Ethoxylates | | | | |
| Nonylphenol | mg/L | 0.001 | | < 0.001 |
| Nonylphenol Ethoxylates | mg/L | 0.01 | | < 0.01 |
| Nonylphenol diethoxylate | mg/L | 0.01 | | < 0.01 |
| Nonylphenol monoethoxylate | mg/L | 0.01 | | < 0.01 |
| Oil and Grease | | | | |
| Oil & Grease (total) | mg/L | 2 | | < 4 † |
| Oil & Grease (animal/vegetable) | mg/L | 4 | | < 4 |
| Oil & Grease (mineral/synthetic) | mg/L | 4 | | < 4 |



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MATRIX: WATER

Sample Number 8

Sample Name BH 22-1

Sample Matrix Ground Water

Sample Date 26/10/2022

L1 = PWQQ_L / WATER / - - Table 2 - General - July 1999 PIBS 3303E

| Parameter | Units | RL | L1 | Result |
|--|---------|---------|--------|----------|
| Other (ORP) | | | | |
| pH | No unit | 0.05 | 8.6 | 7.72 |
| Mercury (total) | mg/L | 0.00001 | 0.0002 | 0.00002 |
| PCBs | | | | |
| Polychlorinated Biphenyls (PCBs) - Total | mg/L | 0.0001 | | < 0.0001 |
| Phenols | | | | |
| 4AAP-Phenolics | mg/L | 0.002 | 0.001 | < 0.002 |
| SVOCs | | | | |
| di-n-Butyl Phthalate | mg/L | 0.002 | | < 0.002 |
| Bis(2-ethylhexyl)phthalate | mg/L | 0.002 | | < 0.002 |
| VOCs | | | | |
| Chloroform | mg/L | 0.0005 | | < 0.0005 |
| 1,2-Dichlorobenzene | mg/L | 0.0005 | | < 0.0005 |
| 1,4-Dichlorobenzene | mg/L | 0.0005 | | < 0.0005 |
| cis-1,2-Dichloroethene | mg/L | 0.0005 | | < 0.0005 |
| trans-1,3-Dichloropropene | mg/L | 0.0005 | | < 0.0005 |
| Methylene Chloride | mg/L | 0.0005 | 0.1 | < 0.0005 |
| 1,1,2,2-Tetrachloroethane | mg/L | 0.0005 | 0.07 | < 0.0005 |
| Methyl ethyl ketone | mg/L | 0.02 | | < 0.02 |
| Styrene | mg/L | 0.0005 | | < 0.0005 |
| Tetrachloroethylene (perchloroethylene) | mg/L | 0.0005 | 0.05 | < 0.0005 |
| Trichloroethylene | mg/L | 0.0005 | 0.02 | < 0.0005 |



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MATRIX: WATER

Sample Number 8

Sample Name BH 22-1

Sample Matrix Ground Water

Sample Date 26/10/2022

L1 = PWQQ_L / WATER / - - Table 2 - General - July 1999 PIBS 3303E

| Parameter | Units | RL | L1 | Result |
|--------------------|-------|--------|--------|----------|
| VOCs - BTEX | | | | |
| Benzene | mg/L | 0.0005 | 0.1 | < 0.0005 |
| Ethylbenzene | mg/L | 0.0005 | 0.008 | < 0.0005 |
| Toluene | mg/L | 0.0005 | 0.0008 | 0.0005 |
| Xylene (total) | mg/L | 0.0005 | | < 0.0005 |
| m-p-xylene | mg/L | 0.0005 | 0.002 | < 0.0005 |
| o-xylene | mg/L | 0.0005 | 0.04 | < 0.0005 |



EXCEEDANCE SUMMARY

| Parameter | Method | Units | Result | PWQO_L / WATER / - - Table 2 - General - July 1999 PIBS 3303E L1 |
|-----------|--------|-------|--------|--|
|-----------|--------|-------|--------|--|

BH 22-1

| | | | | |
|----------------|-------------------|------|----------|--------|
| Arsenic | SM 3030/EPA 200.8 | mg/L | 0.0072 | 0.005 |
| Cadmium | SM 3030/EPA 200.8 | mg/L | 0.000178 | 0.0001 |
| Cobalt | SM 3030/EPA 200.8 | mg/L | 0.0125 | 0.0009 |
| Copper | SM 3030/EPA 200.8 | mg/L | 0.0266 | 0.001 |
| Lead | SM 3030/EPA 200.8 | mg/L | 0.0180 | 0.005 |
| Phosphorus | SM 3030/EPA 200.8 | mg/L | 3.12 | 0.01 |
| Zinc | SM 3030/EPA 200.8 | mg/L | 0.057 | 0.02 |
| 4AAP-Phenolics | SM 5530B-D | mg/L | < 0.002 | 0.001 |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Anions by discrete analyzer

Method: US EPA 375.4 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-026

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Sulphate | DIO5002-NOV22 | mg/L | 2 | <2 | ND | 20 | 106 | 80 | 120 | 106 | 75 | 125 |

Biochemical Oxygen Demand

Method: SM 5210 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-007

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Biochemical Oxygen Demand (BOD5) | BOD0054-OCT22 | mg/L | 2 | < 2 | 18 | 30 | 99 | 70 | 130 | NV | 70 | 130 |

Cyanide by SFA

Method: SM 4500 | Internal ref.: ME-CA-IENVISFA-LAK-AN-005

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------------|--------------------|-------|------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Cyanide (total) | SKA0285-OCT22 | mg/L | 0.01 | <0.01 | ND | 10 | 98 | 90 | 110 | 101 | 75 | 125 |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Fluoride by Specific Ion Electrode

Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-014

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------|--------------------|-------|------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Fluoride | EWL0664-OCT22 | mg/L | 0.06 | <0.06 | ND | 10 | 104 | 90 | 110 | 100 | 75 | 125 |

Mercury by CVAAS

Method: EPA 7471A/SM 3112B | Internal ref.: ME-CA-IENVISPE-LAK-AN-004

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------------|--------------------|-------|---------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Mercury (total) | EHG0051-OCT22 | mg/L | 0.00001 | < 0.00001 | 4 | 20 | 115 | 80 | 120 | 106 | 70 | 130 |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Metals in aqueous samples - ICP-MS

Method: SM 3030/EPA 200.8 | Internal ref.: ME-CA-IENVISPE-LAK-AN-006

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|--------------------|--------------------|-------|----------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Silver (total) | EMS0217-OCT22 | mg/L | 0.00005 | <0.00005 | ND | 20 | 104 | 90 | 110 | 102 | 70 | 130 |
| Aluminum (total) | EMS0217-OCT22 | mg/L | 0.001 | <0.001 | 3 | 20 | 103 | 90 | 110 | 107 | 70 | 130 |
| Arsenic (total) | EMS0217-OCT22 | mg/L | 0.0002 | <0.0002 | ND | 20 | 110 | 90 | 110 | 106 | 70 | 130 |
| Cadmium (total) | EMS0217-OCT22 | mg/L | 0.000003 | <0.000003 | ND | 20 | 103 | 90 | 110 | 102 | 70 | 130 |
| Cobalt (total) | EMS0217-OCT22 | mg/L | 0.000004 | <0.000004 | 2 | 20 | 104 | 90 | 110 | 99 | 70 | 130 |
| Chromium (total) | EMS0217-OCT22 | mg/L | 0.00008 | <0.00008 | 4 | 20 | 105 | 90 | 110 | 104 | 70 | 130 |
| Copper (total) | EMS0217-OCT22 | mg/L | 0.0002 | <0.0002 | 5 | 20 | 105 | 90 | 110 | 92 | 70 | 130 |
| Manganese (total) | EMS0217-OCT22 | mg/L | 0.00001 | <0.00001 | ND | 20 | 107 | 90 | 110 | 83 | 70 | 130 |
| Molybdenum (total) | EMS0217-OCT22 | mg/L | 0.00004 | <0.00004 | ND | 20 | 105 | 90 | 110 | 105 | 70 | 130 |
| Nickel (total) | EMS0217-OCT22 | mg/L | 0.0001 | <0.0001 | ND | 20 | 105 | 90 | 110 | 90 | 70 | 130 |
| Lead (total) | EMS0217-OCT22 | mg/L | 0.00009 | <0.00001 | 3 | 20 | 103 | 90 | 110 | 93 | 70 | 130 |
| Phosphorus (total) | EMS0217-OCT22 | mg/L | 0.003 | <0.003 | ND | 20 | 97 | 90 | 110 | NV | 70 | 130 |
| Antimony (total) | EMS0217-OCT22 | mg/L | 0.0009 | <0.0009 | ND | 20 | 103 | 90 | 110 | 106 | 70 | 130 |
| Selenium (total) | EMS0217-OCT22 | mg/L | 0.00004 | <0.00004 | ND | 20 | 110 | 90 | 110 | 100 | 70 | 130 |
| Tin (total) | EMS0217-OCT22 | mg/L | 0.00006 | <0.00006 | ND | 20 | 106 | 90 | 110 | NV | 70 | 130 |
| Titanium (total) | EMS0217-OCT22 | mg/L | 0.00005 | <0.00005 | ND | 20 | 105 | 90 | 110 | NV | 70 | 130 |
| Zinc (total) | EMS0217-OCT22 | mg/L | 0.002 | <0.002 | 1 | 20 | 102 | 90 | 110 | 104 | 70 | 130 |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Microbiology

Method: SM 9222D | Internal ref.: ME-CA-IENVIMIC-LAK-AN-006

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------|--------------------|-----------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| E. Coli | BAC9419-OCT22 | cfu/100mL | - | ACCEPTED | ACCEPTED | | | | | | | |

Nonylphenol and Ethoxylates

Method: ASTM D7065-06 | Internal ref.: ME-CA-IENVIGC-LAK-AN-015

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------------|--------------------|-------|-------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Nonylphenol diethoxylate | GCM0431-OCT22 | mg/L | 0.01 | <0.01 | | | 113 | 55 | 120 | | | |
| Nonylphenol Ethoxylates | GCM0431-OCT22 | mg/L | 0.01 | < 0.01 | | | | | | | | |
| Nonylphenol monoethoxylate | GCM0431-OCT22 | mg/L | 0.01 | <0.01 | | | 115 | 55 | 120 | | | |
| Nonylphenol | GCM0431-OCT22 | mg/L | 0.001 | <0.001 | | | 115 | 55 | 120 | | | |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Oil & Grease

Method: MOE E3401 | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Oil & Grease (total) | GCM0410-OCT22 | mg/L | 2 | <2 | NSS | 20 | 100 | 75 | 125 | | | |

Oil & Grease-AV/MS

Method: MOE E3401/SM 5520F | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Oil & Grease (animal/vegetable) | GCM0410-OCT22 | mg/L | 4 | < 4 | NSS | 20 | NA | 70 | 130 | | | |
| Oil & Grease (mineral/synthetic) | GCM0410-OCT22 | mg/L | 4 | < 4 | NSS | 20 | NA | 70 | 130 | | | |

pH

Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-006

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-----------|--------------------|---------|------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| pH | EWL0681-OCT22 | No unit | 0.05 | NA | 0 | | 101 | | | NA | | |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Phenols by SFA

Method: SM 5530B-D | Internal ref.: ME-CA-IENVISFA-LAK-AN-006

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------|--------------------|-------|-------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| 4AAP-Phenolics | SKA0318-OCT22 | mg/L | 0.002 | <0.002 | ND | 10 | 100 | 80 | 120 | 100 | 75 | 125 |

Polychlorinated Biphenyls

Method: MOE E3400/EPA 8082A | Internal ref.: ME-CA-IENVIGC-LAK-AN-001

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|--|--------------------|-------|--------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Polychlorinated Biphenyls (PCBs) - Total | GCM0377-OCT22 | mg/L | 0.0001 | <0.0001 | NSS | 30 | 84 | 60 | 140 | NSS | 60 | 140 |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Semi-Volatile Organics

Method: EPA 3510C/8270D | Internal ref.: ME-CA-IENVIGC-LAK-AN-005

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|----------------------------|--------------------|-------|-------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Bis(2-ethylhexyl)phthalate | GCM0391-OCT22 | mg/L | 0.002 | < 0.002 | NSS | 30 | 123 | 50 | 140 | NSS | 50 | 140 |
| di-n-Butyl Phthalate | GCM0391-OCT22 | mg/L | 0.002 | < 0.002 | NSS | 30 | 113 | 50 | 140 | NSS | 50 | 140 |

Suspended Solids

Method: SM 2540D | Internal ref.: ME-CA-IENVIEWL-LAK-AN-004

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|------------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Total Suspended Solids | EWL0006-NOV22 | mg/L | 2 | < 2 | 0 | 10 | 93 | 90 | 110 | NA | | |

Total Nitrogen

Method: SM 4500-N C/4500-NO3- F | Internal ref.: ME-CA-IENVISFA-LAK-AN-002

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|-------------------------|--------------------|-----------|-----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| Total Kjeldahl Nitrogen | SKA0004-NOV22 | as N mg/L | 0.5 | <0.5 | 2 | 10 | 98 | 90 | 110 | 106 | 75 | 125 |



FINAL REPORT

CA40197-OCT22 R1

QC SUMMARY

Volatile Organics

Method: EPA 5030B/8260C | Internal ref.: ME-CA-ENVIGC-LAK-AN-004

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate | | LCS/Spike Blank | | | Matrix Spike / Ref. | | |
|---|--------------------|-------|--------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
| | | | | | RPD | AC (%) | Spike Recovery (%) | Recovery Limits (%) | | Spike Recovery (%) | Recovery Limits (%) | |
| | | | | | | | | Low | High | | Low | High |
| 1,1,2,2-Tetrachloroethane | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 92 | 60 | 130 | 94 | 50 | 140 |
| 1,2-Dichlorobenzene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 95 | 60 | 130 | 98 | 50 | 140 |
| 1,4-Dichlorobenzene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 94 | 60 | 130 | 96 | 50 | 140 |
| Benzene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 100 | 60 | 130 | 102 | 50 | 140 |
| Chloroform | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 98 | 60 | 130 | 100 | 50 | 140 |
| cis-1,2-Dichloroethene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 100 | 60 | 130 | 102 | 50 | 140 |
| Ethylbenzene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 98 | 60 | 130 | 102 | 50 | 140 |
| m-p-xylene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 97 | 60 | 130 | 100 | 50 | 140 |
| Methyl ethyl ketone | GCM0375-OCT22 | mg/L | 0.02 | <0.02 | ND | 30 | 93 | 50 | 140 | 95 | 50 | 140 |
| Methylene Chloride | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 97 | 60 | 130 | 98 | 50 | 140 |
| o-xylene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 98 | 60 | 130 | 102 | 50 | 140 |
| Styrene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 98 | 60 | 130 | 101 | 50 | 140 |
| Tetrachloroethylene (perchloroethylene) | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 96 | 60 | 130 | 100 | 50 | 140 |
| Toluene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 97 | 60 | 130 | 99 | 50 | 140 |
| trans-1,3-Dichloropropene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 96 | 60 | 130 | 97 | 50 | 140 |
| Trichloroethylene | GCM0375-OCT22 | mg/L | 0.0005 | <0.0005 | ND | 30 | 97 | 60 | 130 | 99 | 50 | 140 |

QC SUMMARY

Method Blank: a blank matrix that is carried through the entire analytical procedure. Used to assess laboratory contamination.

Duplicate: Paired analysis of a separate portion of the same sample that is carried through the entire analytical procedure. Used to evaluate measurement precision.

LCS/Spike Blank: Laboratory control sample or spike blank refer to a blank matrix to which a known amount of analyte has been added. Used to evaluate analyte recovery and laboratory accuracy without sample matrix effects.

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate laboratory accuracy with sample matrix effects.

Reference Material: a material or substance matrix matched to the samples that contains a known amount of the analyte of interest. A reference material may be used in place of a matrix spike.

RL: Reporting limit

RPD: Relative percent difference

AC: Acceptance criteria

Multielement Scan Qualifier: as the number of analytes in a scan increases, so does the chance of a limit exceedance by random chance as opposed to a real method problem. Thus, in multielement scans, for the LCS and matrix spike, up to 10% of the analytes may exceed the quoted limits by up to 10% absolute and the spike is considered acceptable.

Duplicate Qualifier: for duplicates as the measured result approaches the RL, the uncertainty associated with the value increases dramatically, thus duplicate acceptance limits apply only where the average of the two duplicates is greater than five times the RL.

Matrix Spike Qualifier: for matrix spikes, as the concentration of the native analyte increases, the uncertainty of the matrix spike recovery increases. Thus, the matrix spike acceptance limits apply only when the concentration of the matrix spike is greater than or equal to the concentration of the native analyte.



LEGEND

FOOTNOTES

- NSS** Insufficient sample for analysis.
- RL** Reporting Limit.
 - ↑ Reporting limit raised.
 - ↓ Reporting limit lowered.
- NA** The sample was not analysed for this analyte
- ND** Non Detect

Results relate only to the sample tested.

Data reported represent the sample as submitted to SGS. Solid samples expressed on a dry weight basis.

"Temperature Upon Receipt" is representative of the whole shipment and may not reflect the temperature of individual samples.

Analysis conducted on samples submitted pursuant to or as part of Reg. 153/04, are in accordance to the "Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act and Excess Soil Quality" published by the Ministry and dated March 9, 2004 as amended.

SGS provides criteria information (such as regulatory or guideline limits and summary of limit exceedances) as a service. Every attempt is made to ensure the criteria information in this report is accurate and current, however, it is not guaranteed. Comparison to the most current criteria is the responsibility of the client and SGS assumes no responsibility for the accuracy of the criteria levels indicated.

SGS Canada Inc. statement of conformity decision rule does not consider uncertainty when analytical results are compared to a specified standard or regulation.

This document is issued, on the Client's behalf, by the Company under its General Conditions of Service available on request and accessible at http://www.sgs.com/terms_and_conditions.htm.

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This report supersedes all previous versions.

-- End of Analytical Report --



Request for Laboratory Services and CHAIN OF CUSTODY

No: 029796

Page 1 of 1

Laboratory Information Section - Lab use only

Received By: [Signature]
 Received Date: 10/26/22 (mm/dd/yy)
 Received Time: 17:50 (hr:min)

Received By (signature): [Signature]
 Custody Seal Present: Yes No
 Custody Seal Intact: Yes No
 Cooling Agent Present: Yes No Type: Ice
 Temperature Upon Receipt (°C): 9.2/3

LAB LIMS # CA40197-001
22

| REPORT INFORMATION | INVOICE INFORMATION |
|---|--|
| Company: <u>DS Consultants</u> | <input checked="" type="checkbox"/> (same as Report Information) |
| Contact: <u>Dorothy Santos</u> | Company: |
| Address: <u>6221 Hwy 7, Unit 16 Vaughan, ON</u> | Contact: <u>Accounting</u> |
| Phone: <u>905 329 2735</u> | Address: |
| Fax: | Phone: |
| Email: <u>dorothy.santos@dsconsultants.com</u> | Email: |

Quotation #: _____ P.O. #: _____
 Project #: 19-093-100 Site Location/ID: 7675 King St. Bolton

TURNAROUND TIME (TAT) REQUIRED
 Regular TAT (5-7 days) TATs are quoted in business days (exclude statutory holidays & weekends). Samples received after 5pm or on weekends, TAT begins next business day.
 1 Day 2 Days 3 Days 4 Days
RUSH TAT (Additional Charges May Apply):
 PLEASE CONFIRM RUSH FEASIBILITY WITH SGS REPRESENTATIVE PRIOR TO SUBMISSION

Specify Due Date: _____ *NOTE: DRINKING (POTABLE) WATER SAMPLES FOR HUMAN CONSUMPTION MUST BE SUBMITTED WITH SGS DRINKING WATER CHAIN OF CUSTODY

REGULATIONS

O.Reg 153/04 O.Reg 405/19

Other Regulations:
 Reg 347/553 (3 Day min TAT)
 P/VOC MMR
 CCME Other:
 MSA

Sewer By-Law:
 Sanyary
 Storm
 Municipality: PCCL

| M & I | SVOC | PCB | PHC | VOC | Post | Other (please specify) | SPLP | TCLP |
|--------------------|-----------|--|--------------|---|-------------------------------------|------------------------|---------------|---------------|
| Field Filled (Y/N) | PAHs only | PCBs Total <input type="checkbox"/> Aroclor <input type="checkbox"/> | F1-F4 + BTEX | VOCs <input type="checkbox"/> BTEX only | Pesticides <input type="checkbox"/> | | Specify tests | Specify tests |

RECORD OF SITE CONDITION (RSC) YES NO

| SAMPLE IDENTIFICATION | DATE SAMPLED | TIME SAMPLED | # OF BOTTLES | MATRIX |
|-----------------------|-------------------|--------------|--------------|-----------|
| <u>BH 22-1</u> | <u>Oct 26, 22</u> | <u>PM</u> | <u>17</u> | <u>GW</u> |
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| Water Characterization (Pkg) | Sewer Use: | Other (please specify) |
|-------------------------------------|-------------------------------------|-----------------------------|
| <input type="checkbox"/> General | <input type="checkbox"/> Sewer | <u>Water from and Sewer</u> |
| <input type="checkbox"/> Industrial | <input type="checkbox"/> Cooling | <u>CPWQO</u> |
| <input type="checkbox"/> Domestic | <input type="checkbox"/> Irrigation | |
| <input type="checkbox"/> Other | <input type="checkbox"/> Other | |

COMMENTS:

Non Filtered Sample

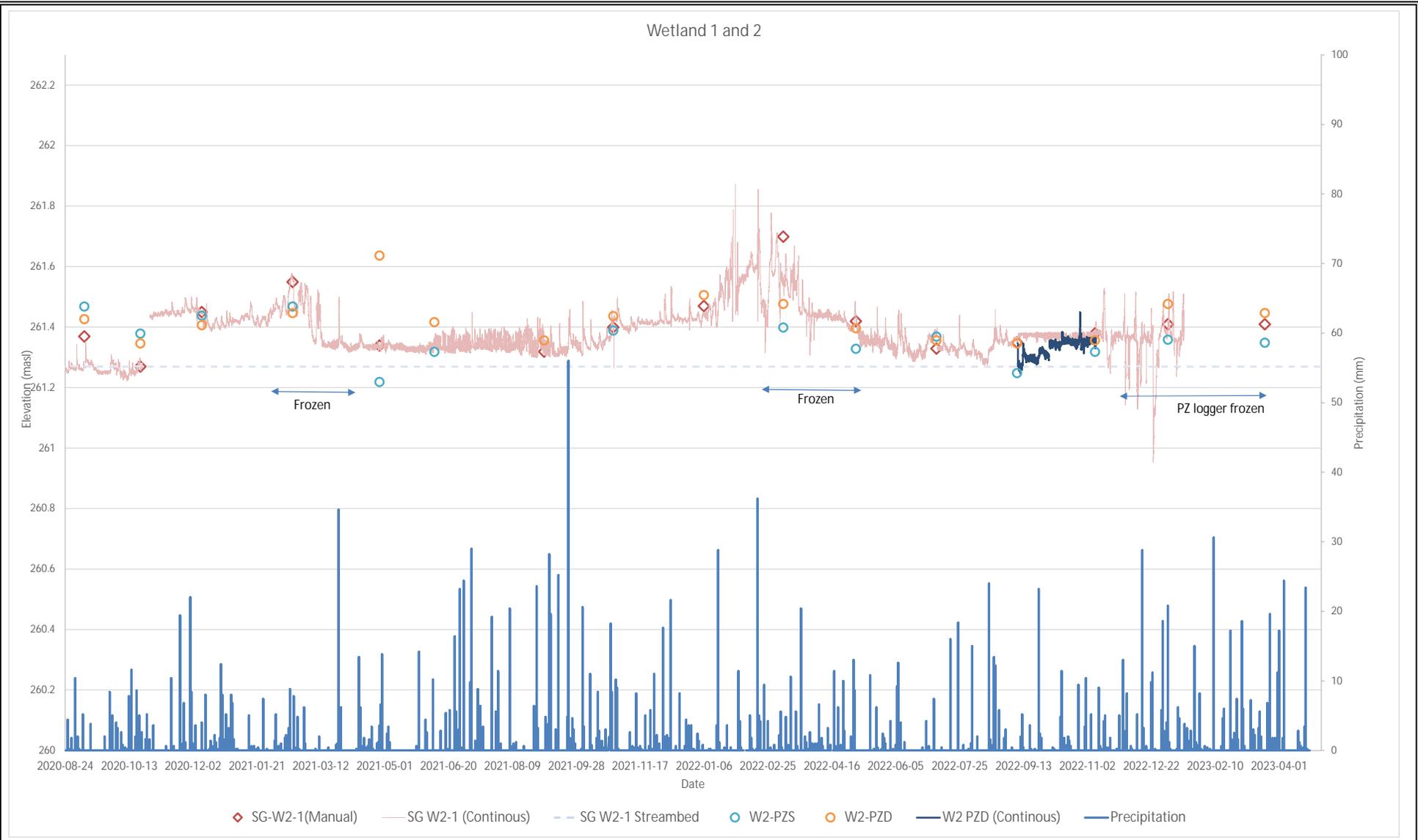
Observed/Comments/Special Instructions

Sampled By (NAME): Hony Chaitanya Signature: [Signature] Date: 10/26/22 (mm/dd/yy) Print Only - Client
 Requisitioned by (NAME): [Signature] Signature: [Signature] Date: 10/26/22 (mm/dd/yy) Yellow & White Copy - S

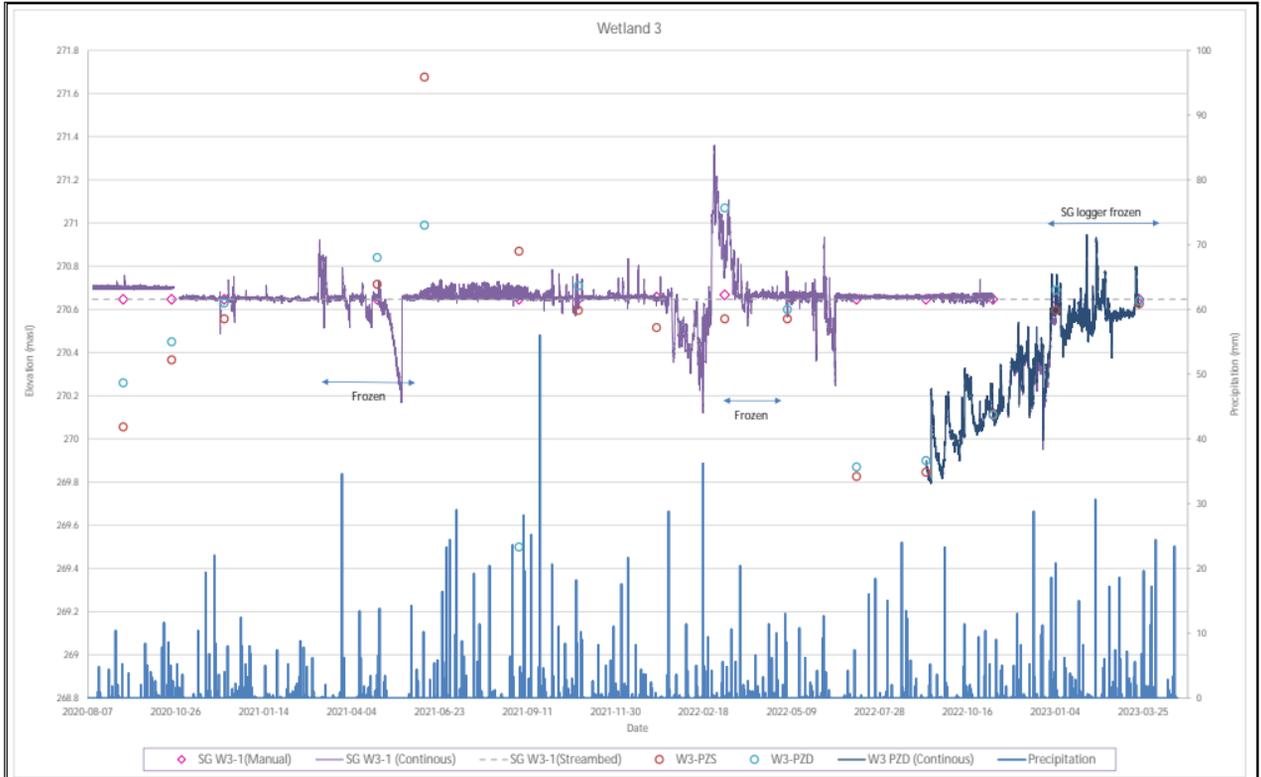


Appendix F

WATER LEVEL HYDROGRAPH



WATER LEVEL HYDROGRAPH



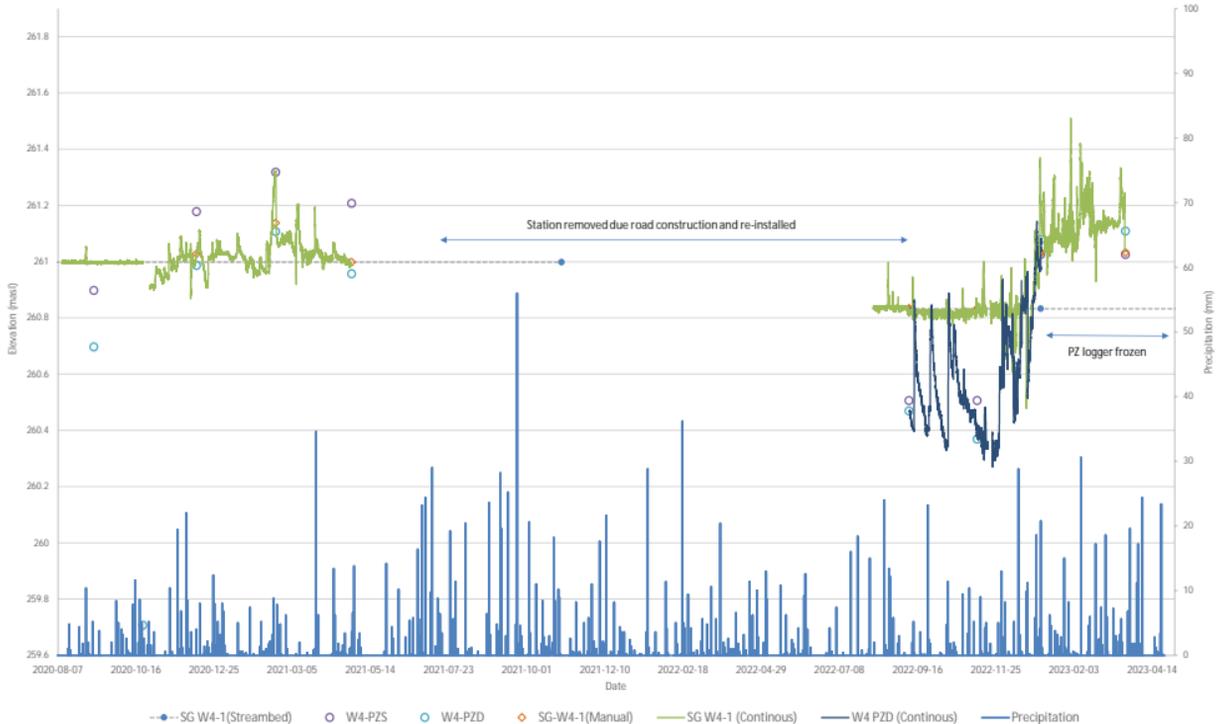
DS CONSULTANTS LTD.
Geotechnical • Environmental • Water • Hydrology

Caledon Station
 WETLAND 3 HYDROGRAPH

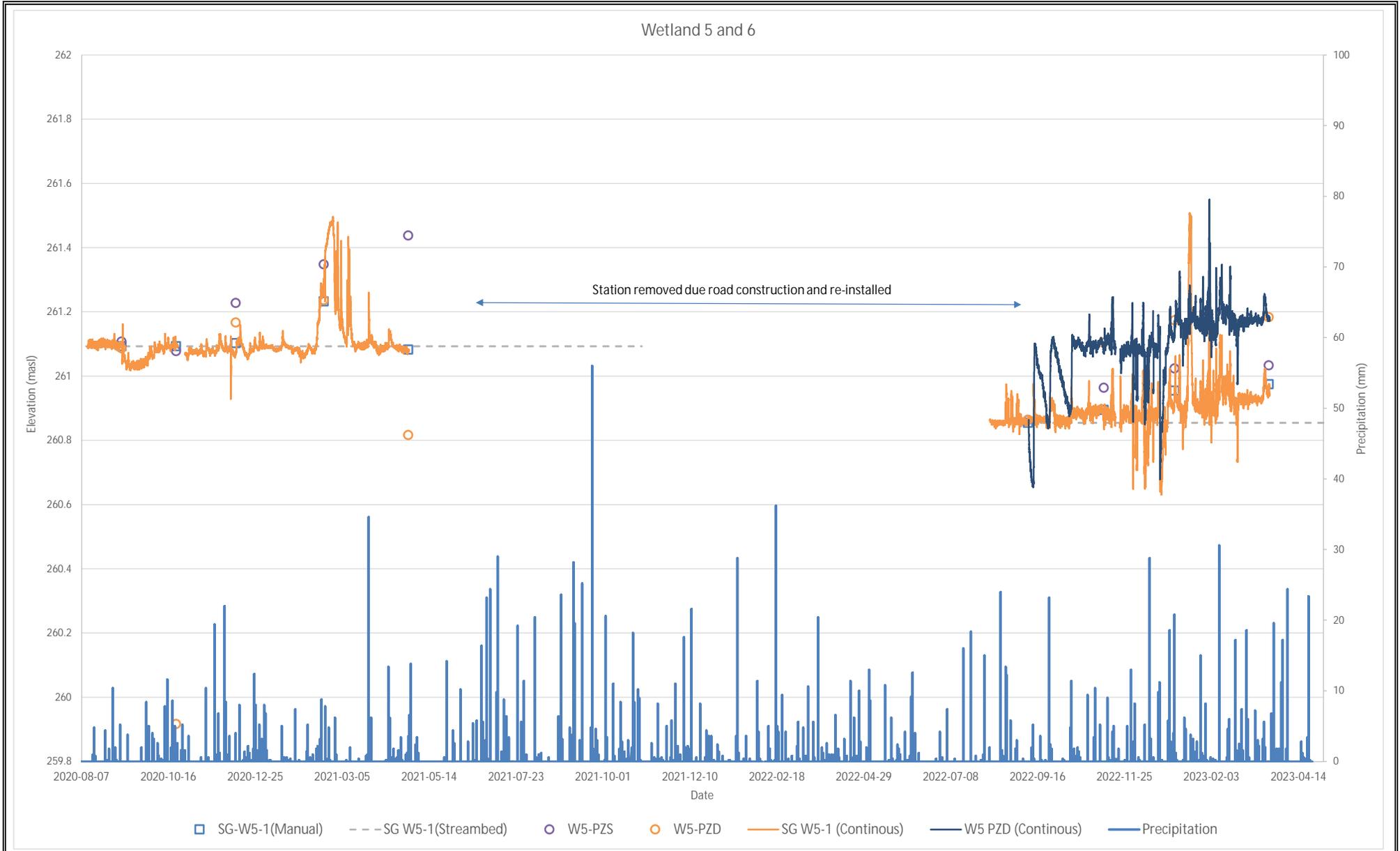
August 2020 - April 2023

WATER LEVEL HYDROGRAPH

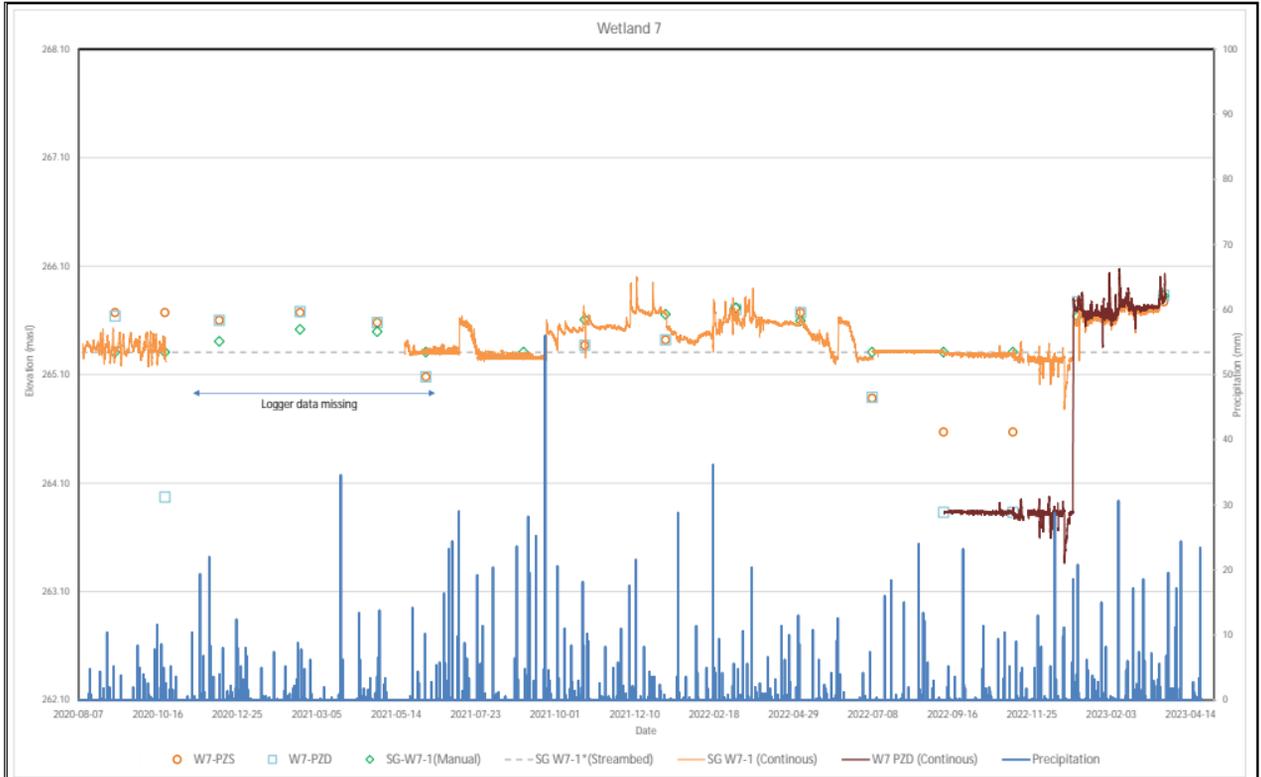
Wetland 4



WATER LEVEL HYDROGRAPH



WATER LEVEL HYDROGRAPH



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WETLAND 7 HYDROGRAPH

August 2020 - April 2023

F6

WATER LEVEL HYDROGRAPH



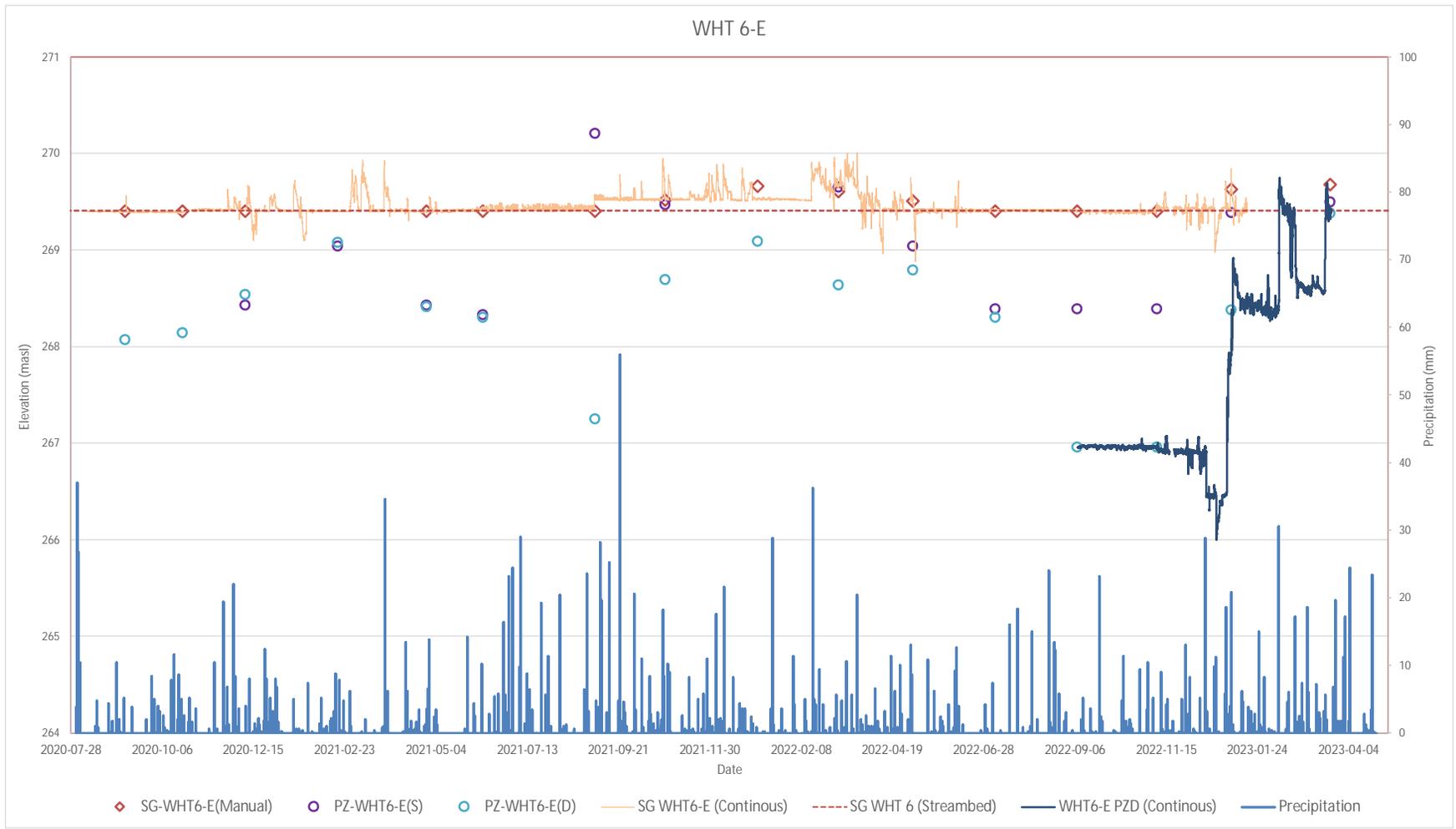
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WETLAND 8 HYDROGRAPH

August 2020 - April 2023

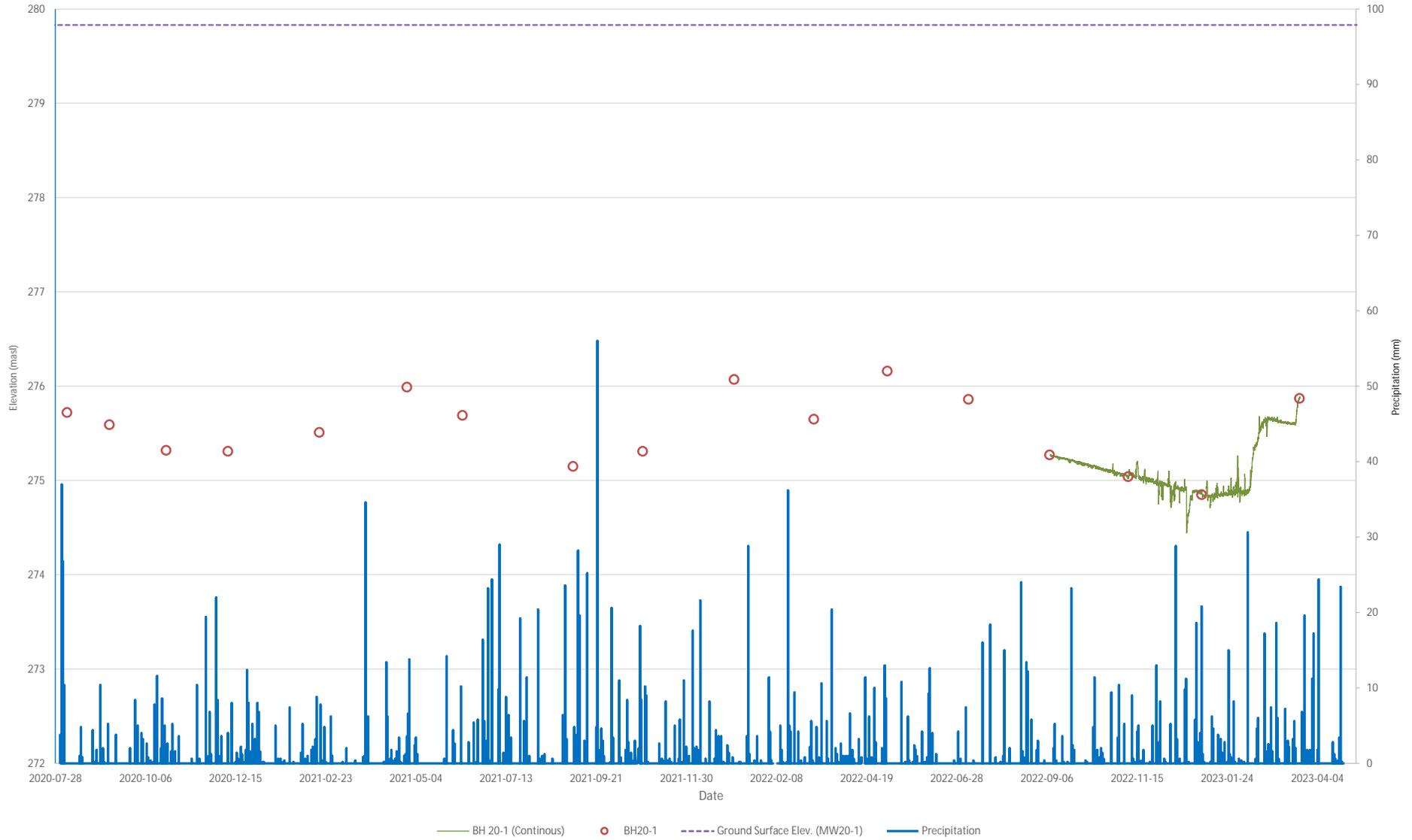
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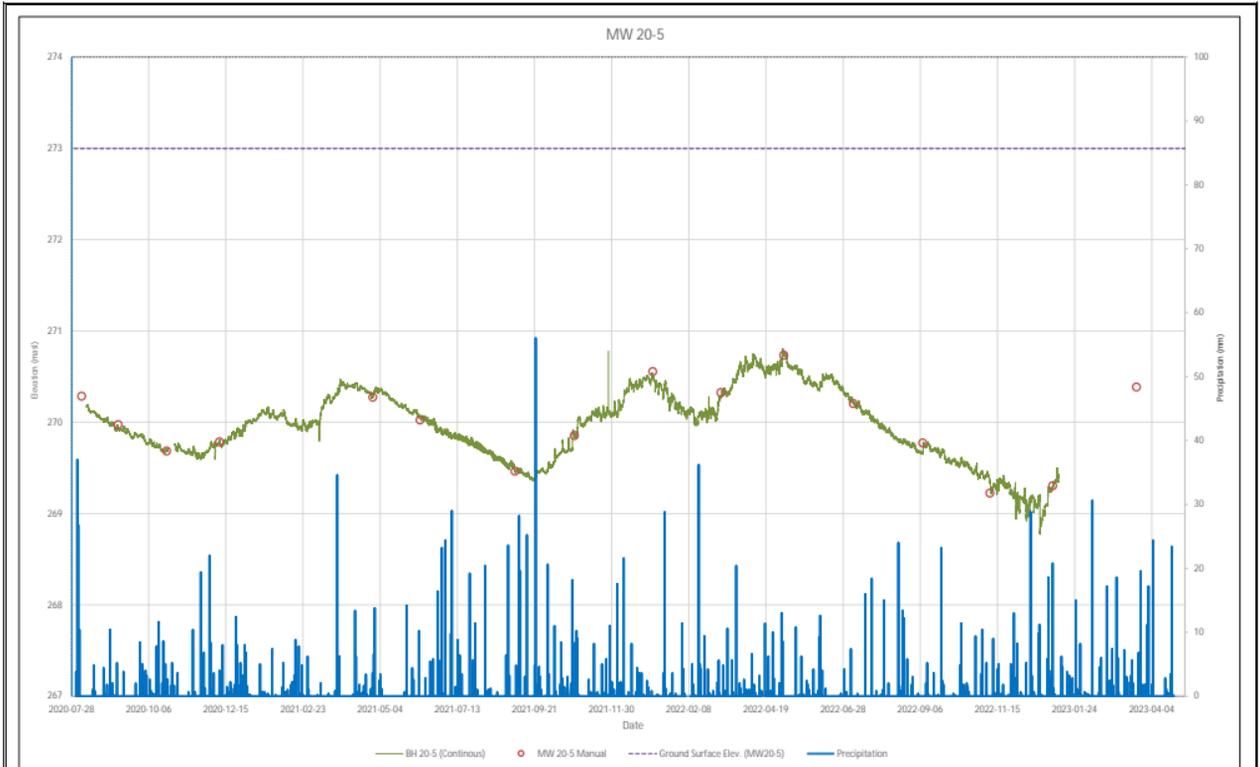


WATER LEVEL HYDROGRAPH

MW 20-1



WATER LEVEL HYDROGRAPH



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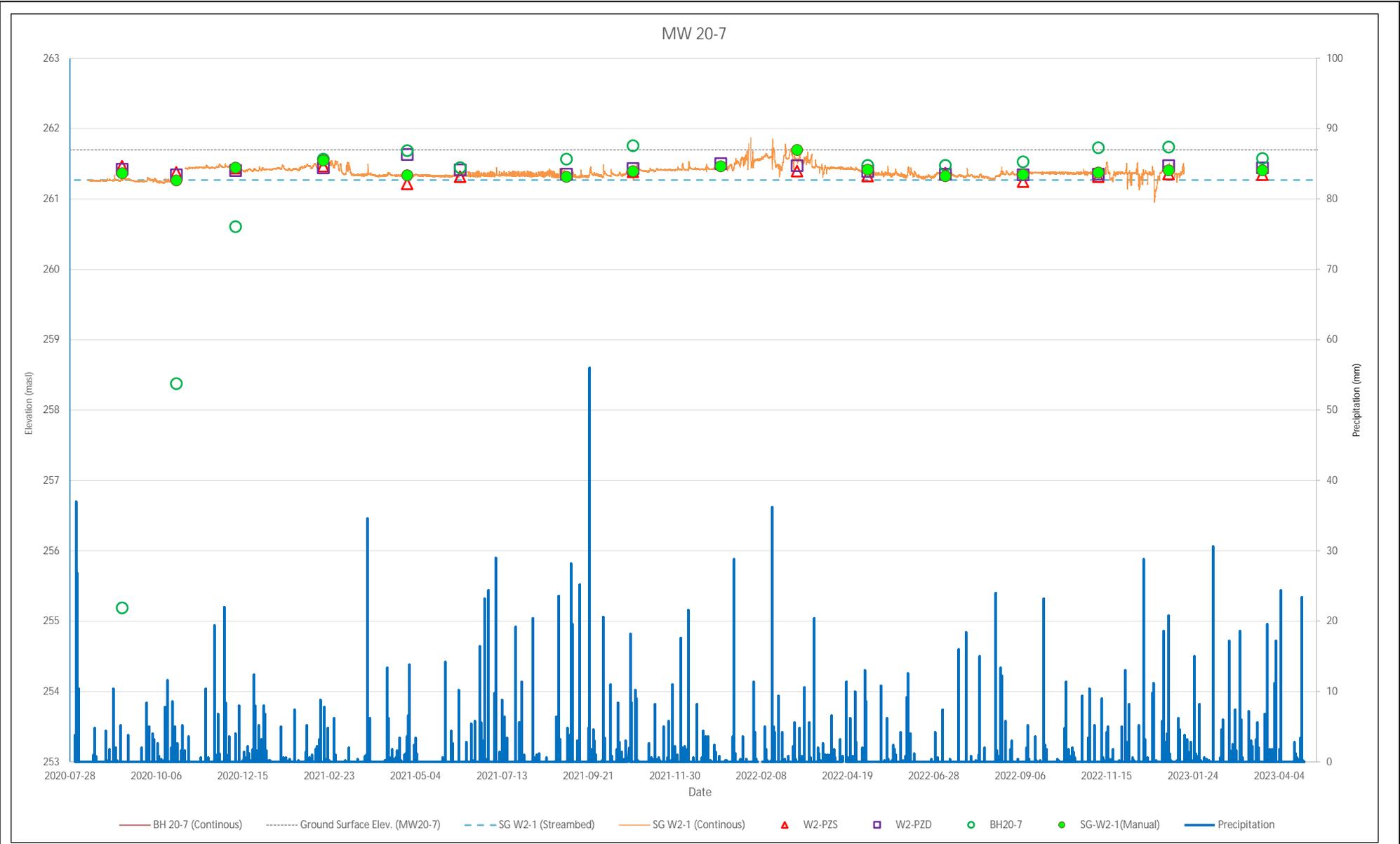
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MW 20-5 HYDROGRAPH

August 2020 - April 2023

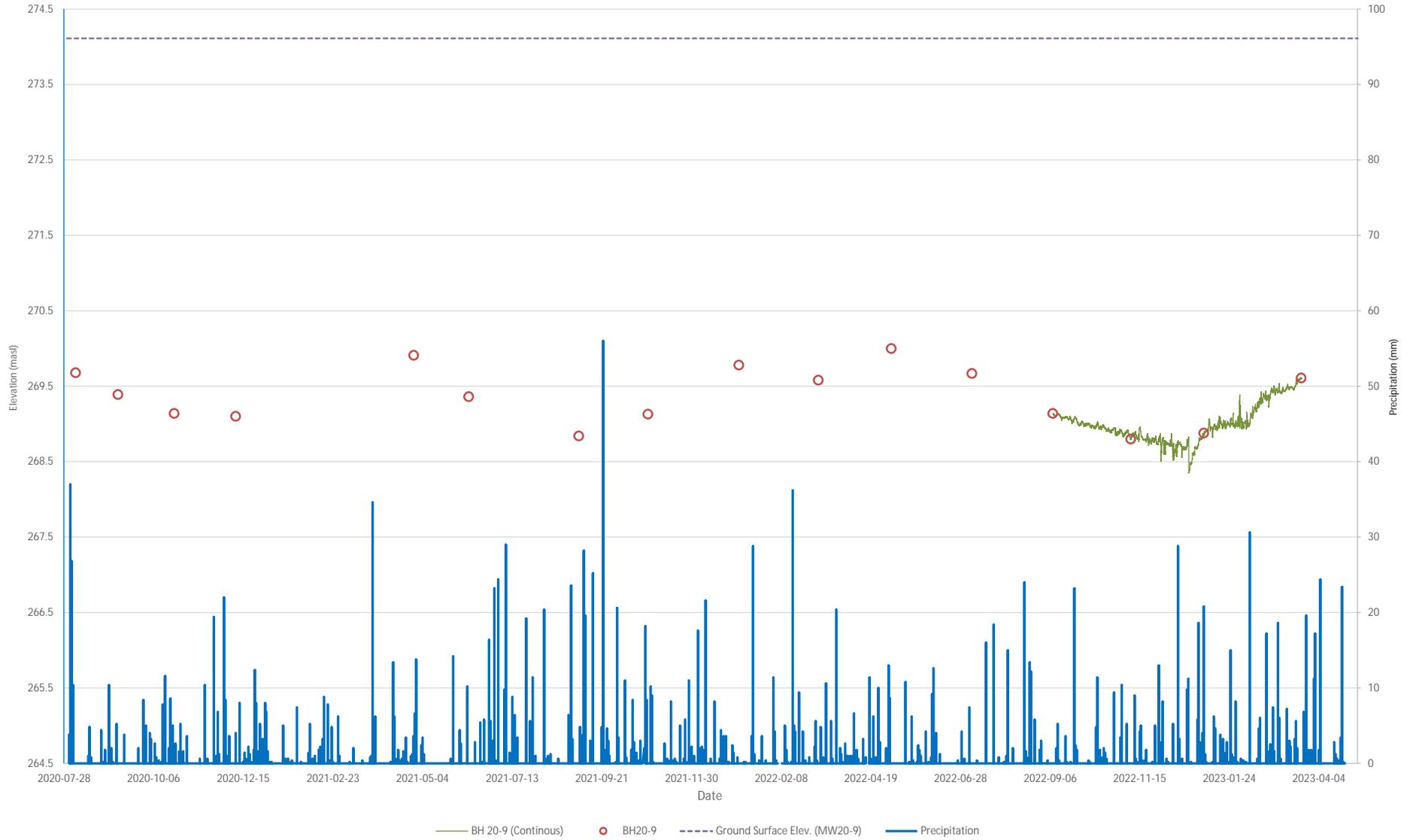
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WATER LEVEL HYDROGRAPH



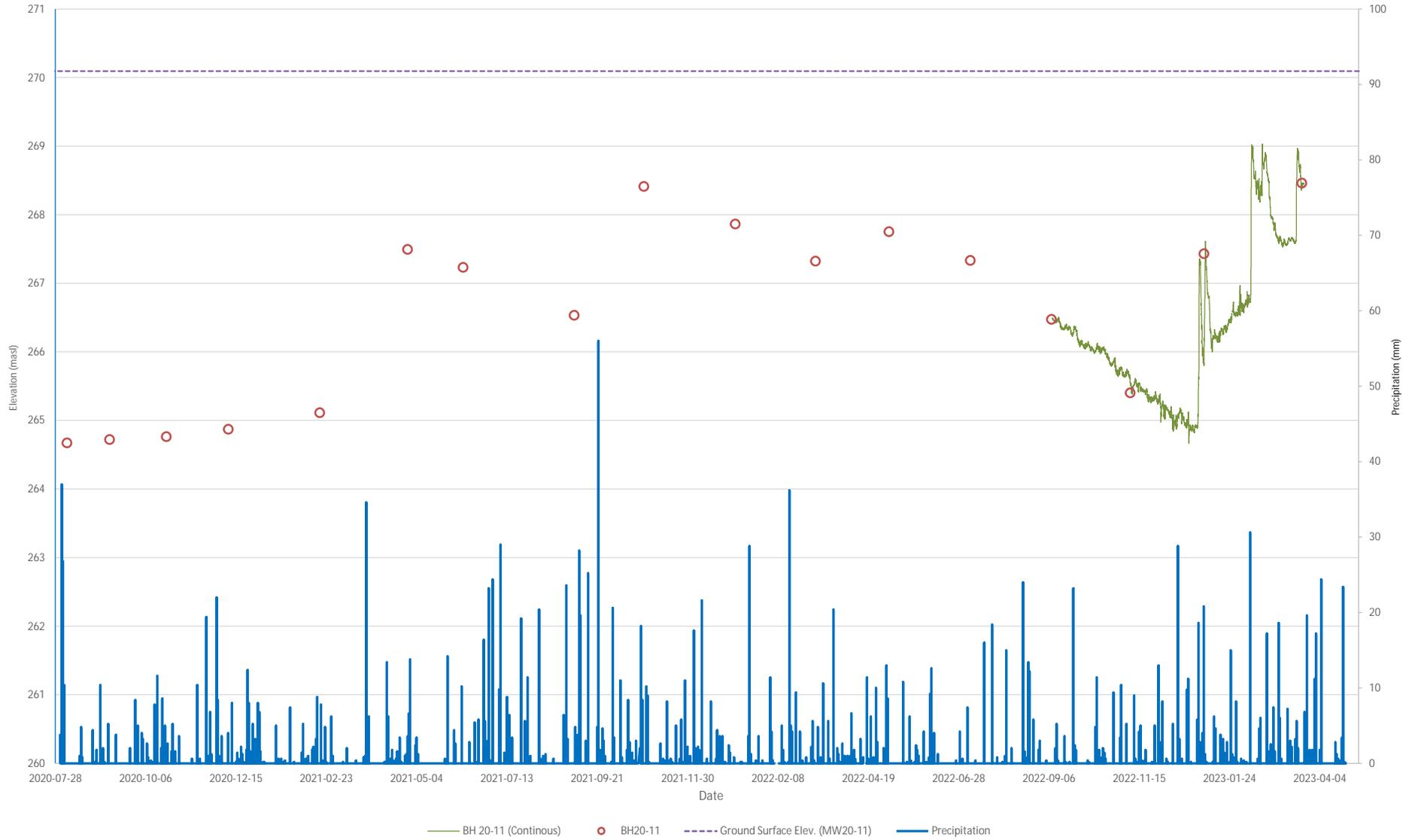
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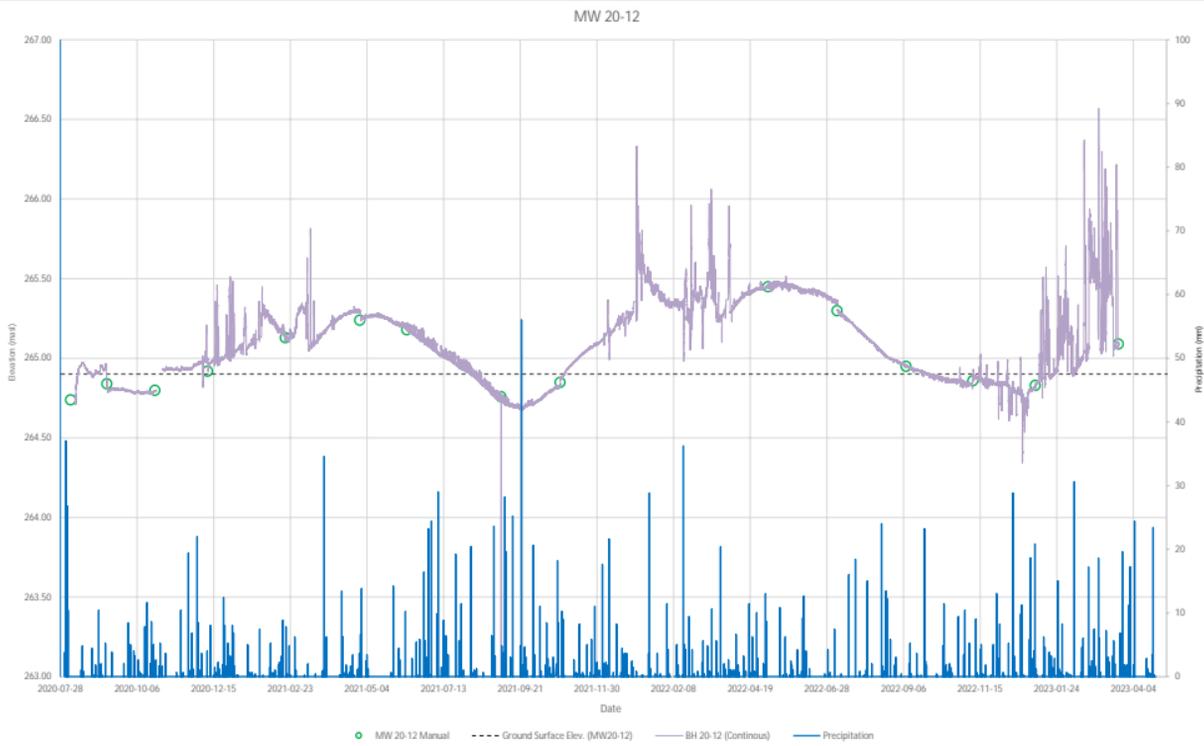


WATER LEVEL HYDROGRAPH

MW 20-11



WATER LEVEL HYDROGRAPH



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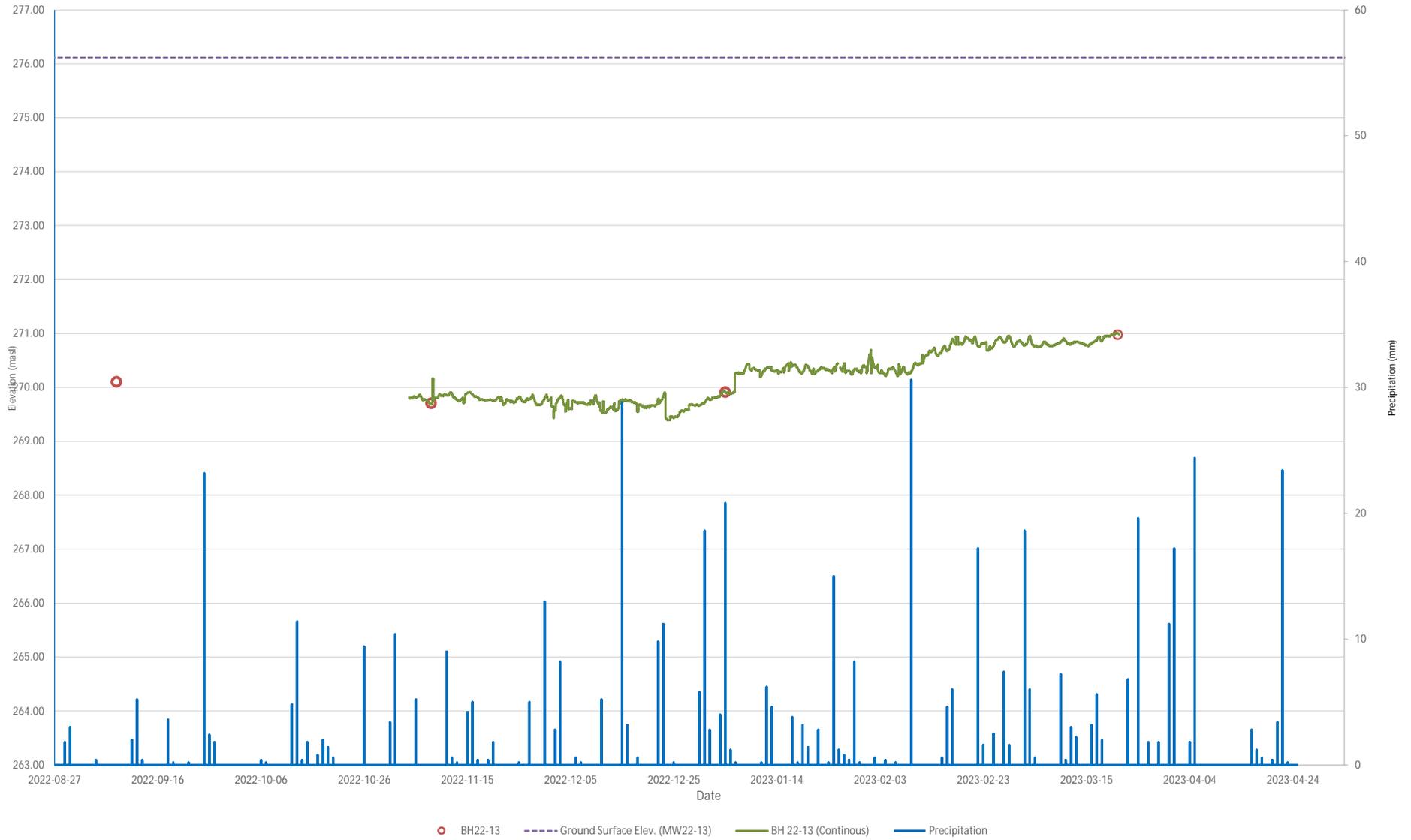
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August 2020 - 2023

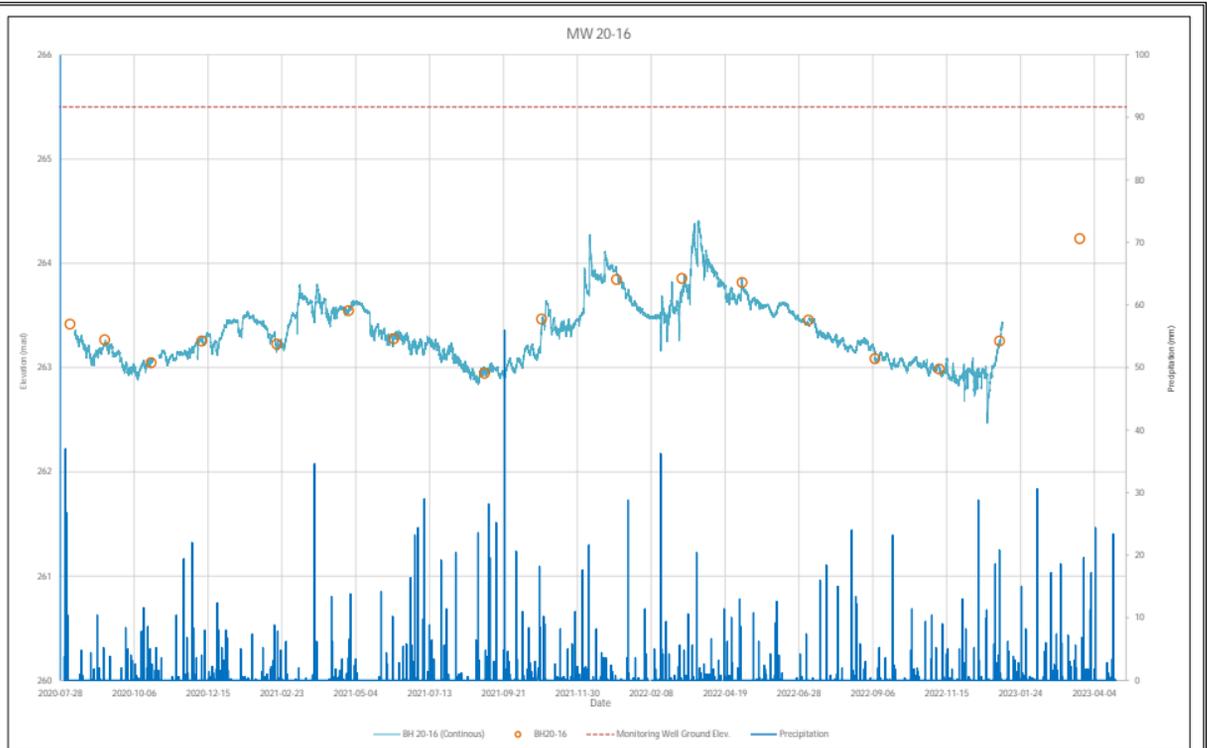
F-13

WATER LEVEL HYDROGRAPH

MW 22-13



WATER LEVEL HYDROGRAPH



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Sustainable Water - Civil & Structural - Water for People - Technology for Growth

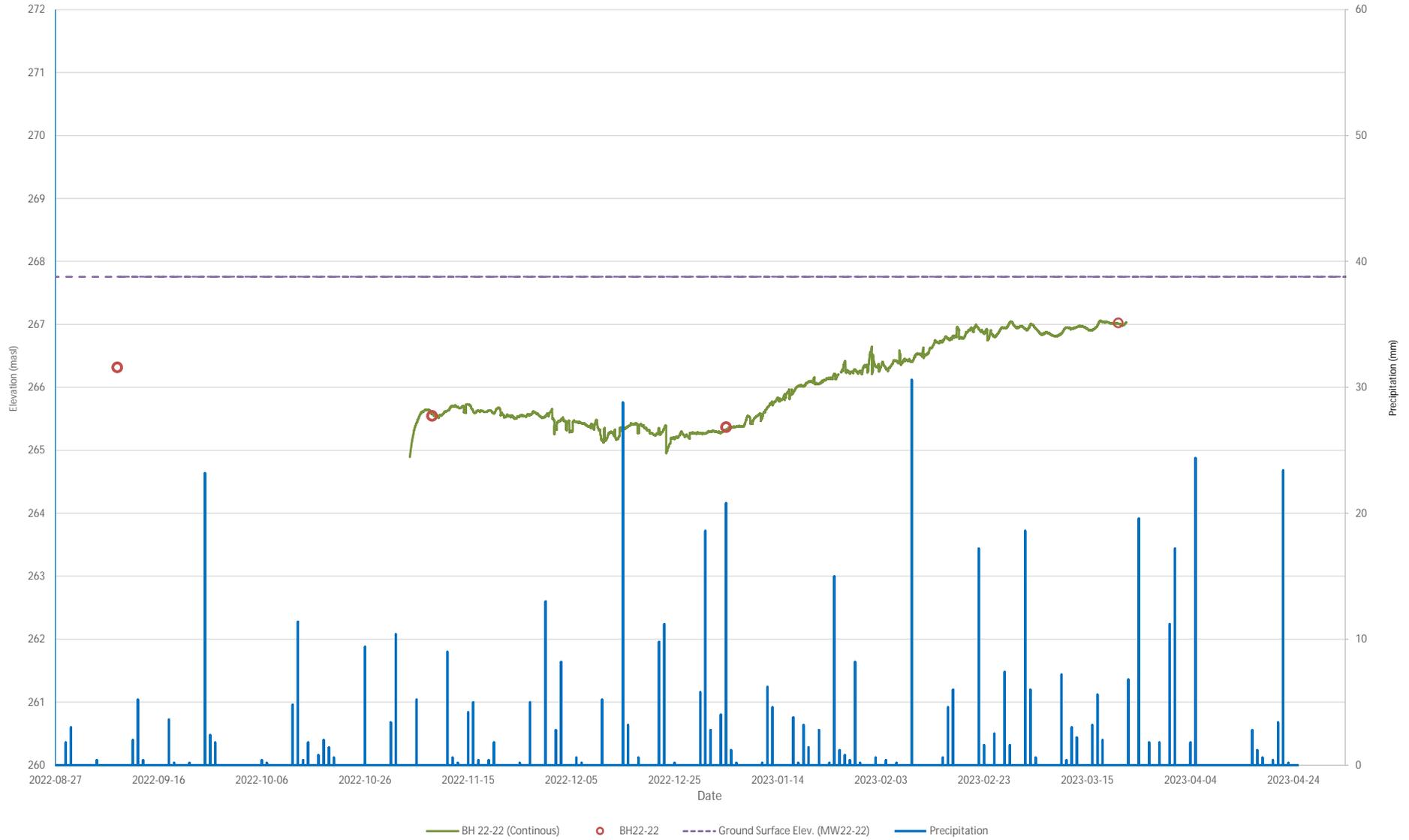
Caledon Station

MW 20-16 HYDROGRAPH

August 2020 - April 2023

WATER LEVEL HYDROGRAPH

MW 22-22



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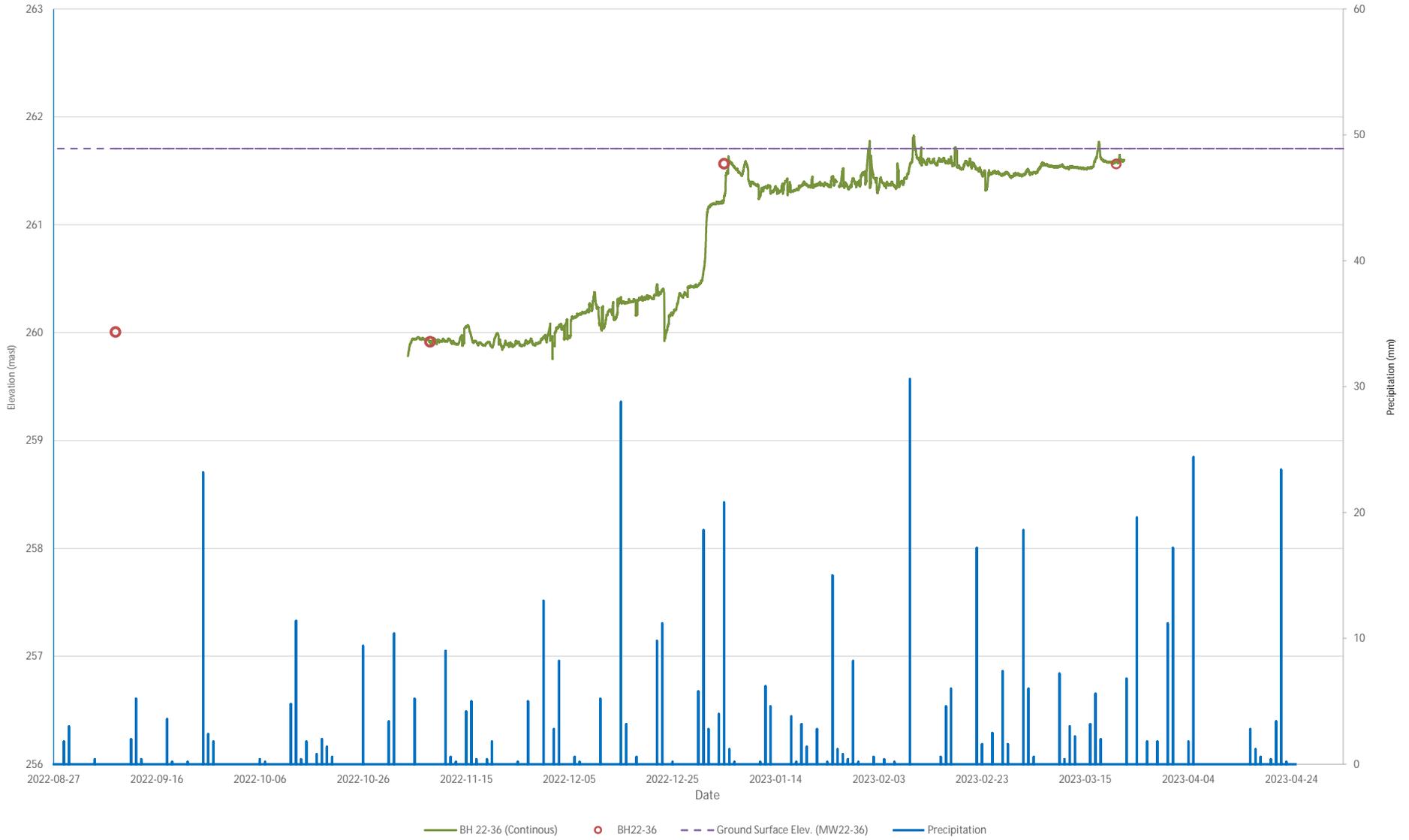
MW 22-22 HYDROGRAPH

August 2022 - April 2023

F-16

WATER LEVEL HYDROGRAPH

MW 22-36



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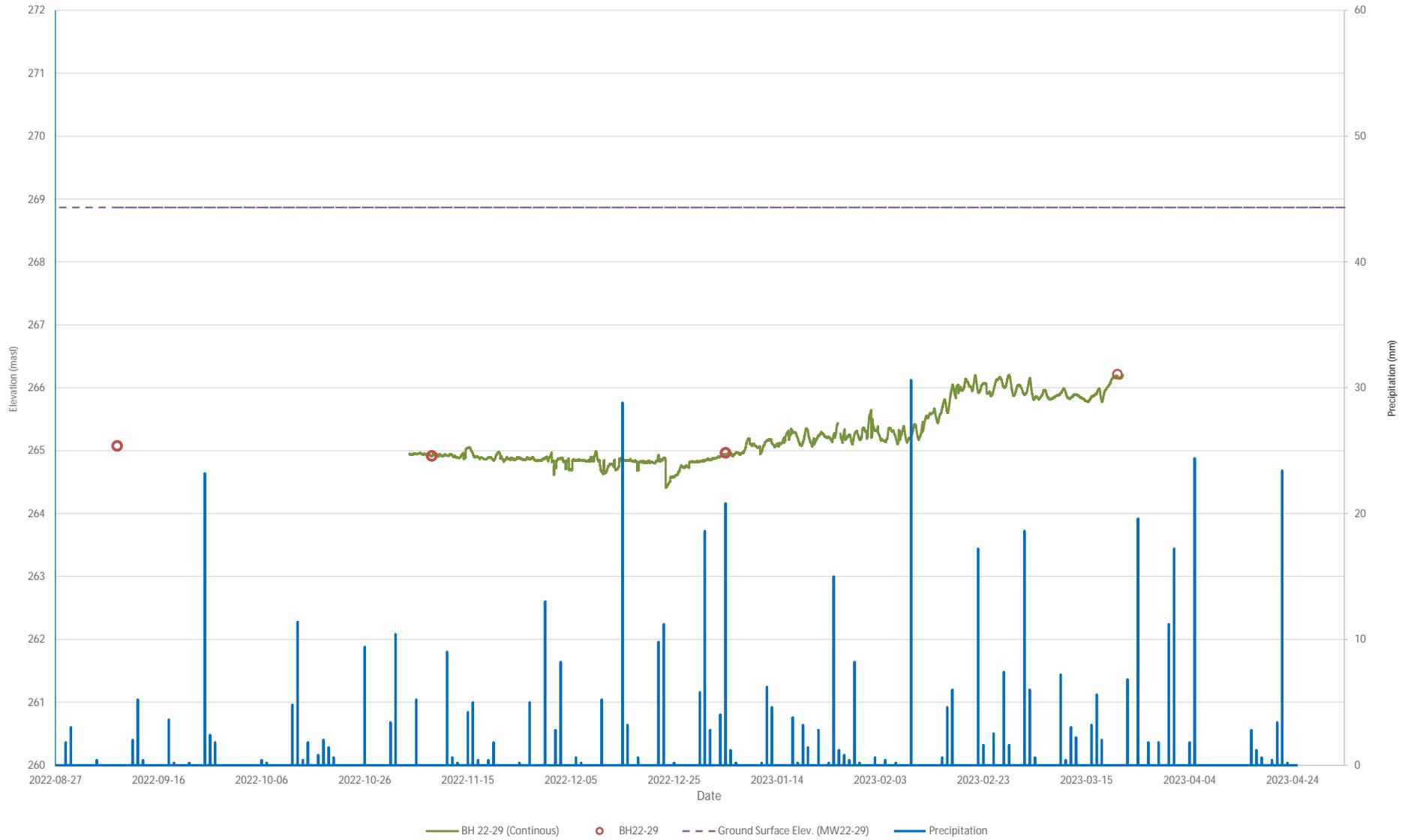
MW 22-36 HYDROGRAPH

August 2022 - April 2023

F-17

WATER LEVEL HYDROGRAPH

MW 22-29



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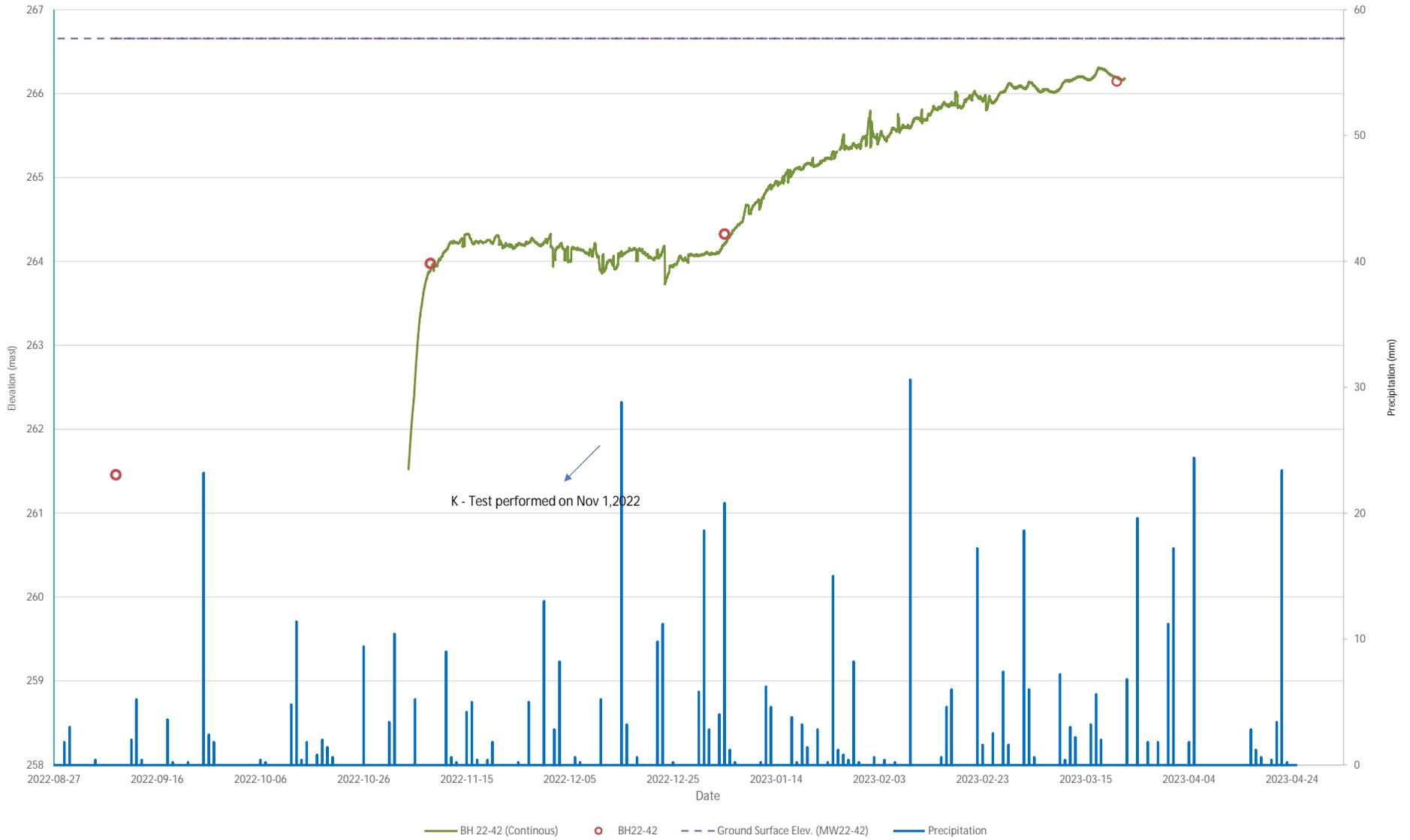
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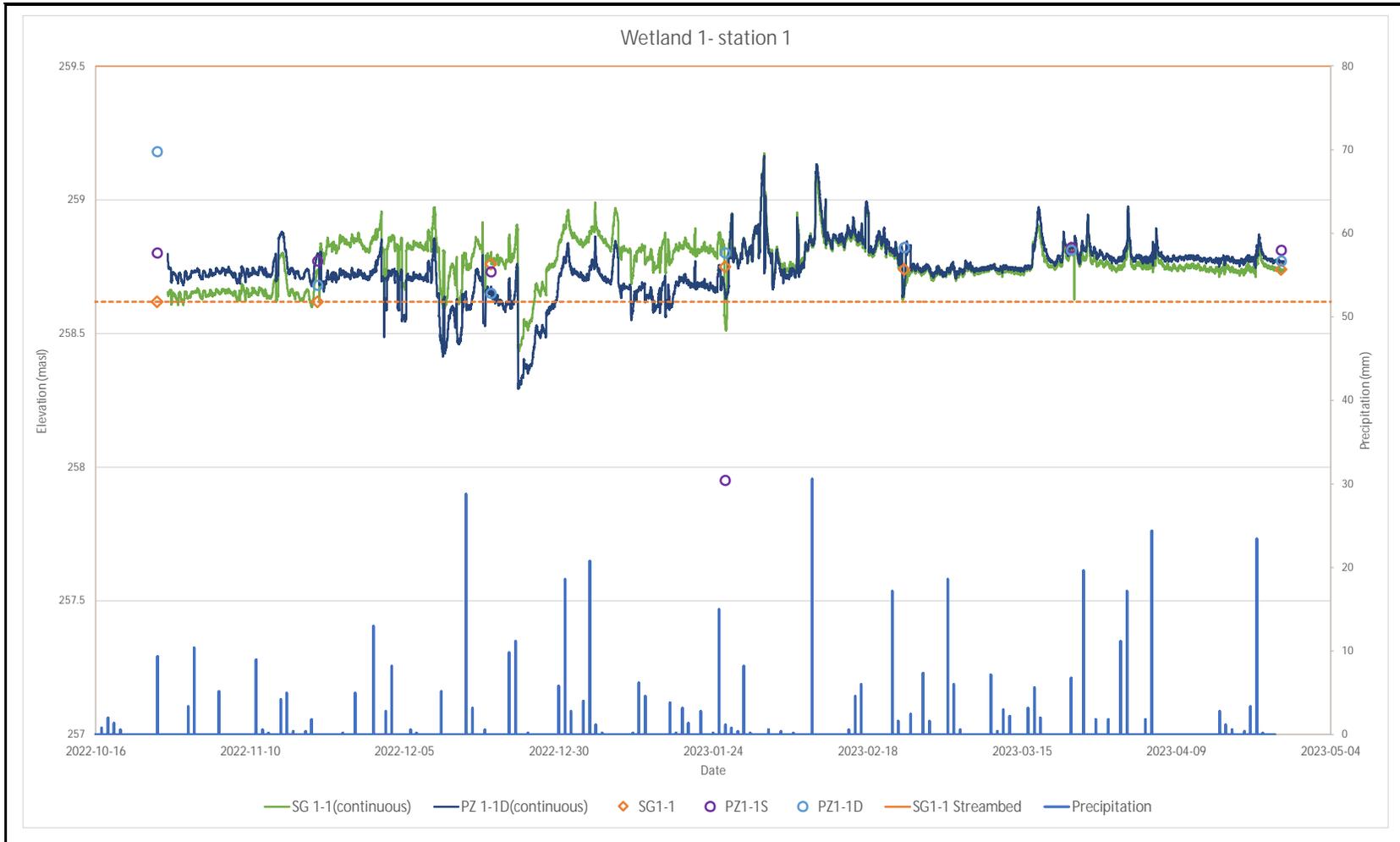
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WATER LEVEL HYDROGRAPH

MW 22-42



WATER LEVEL HYDROGRAPH

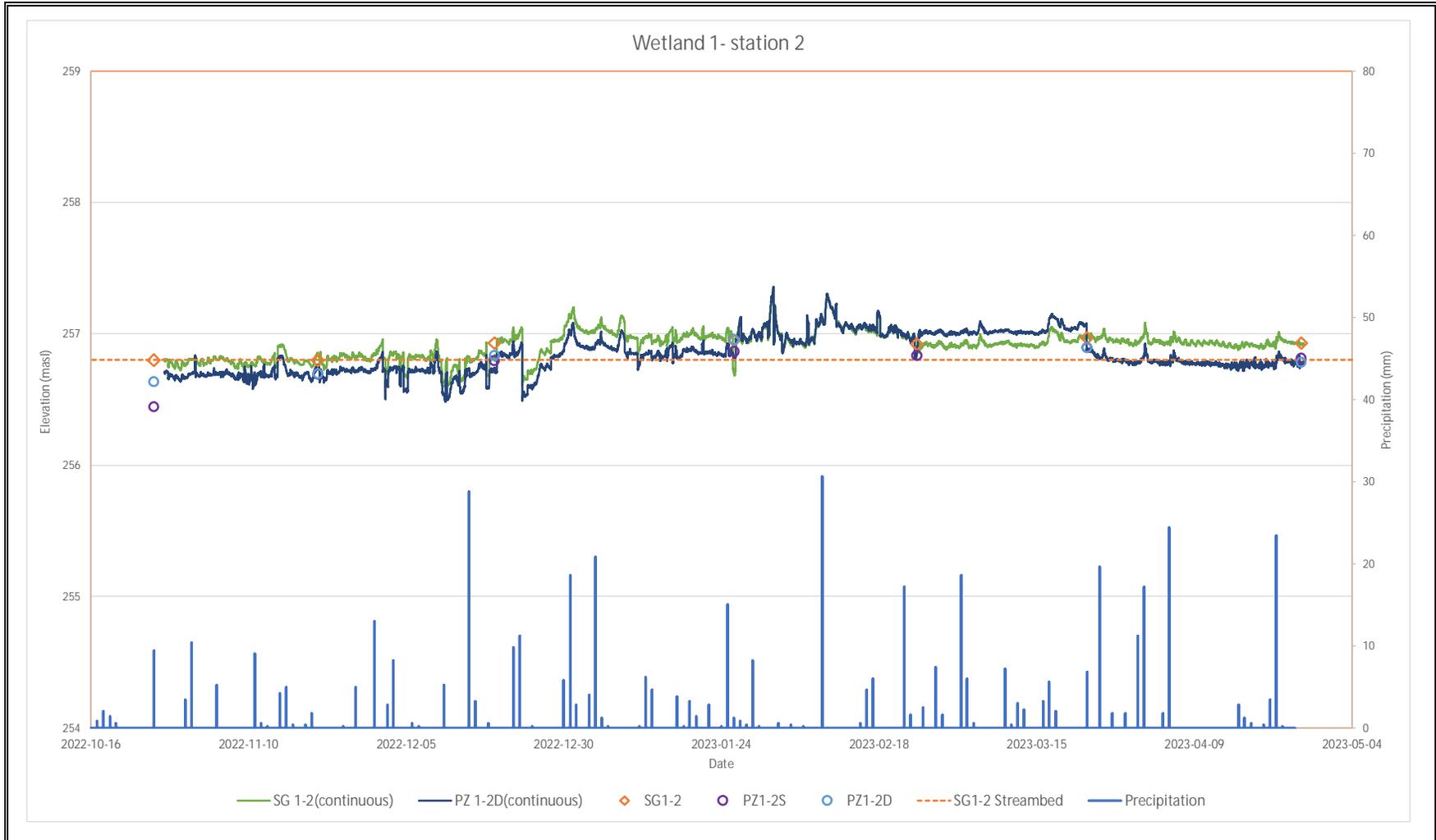


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Argo King I & II
 WETLAND 1 HYDROGRAPH

October 2022 - May 2023
 F-20

WATER LEVEL HYDROGRAPH

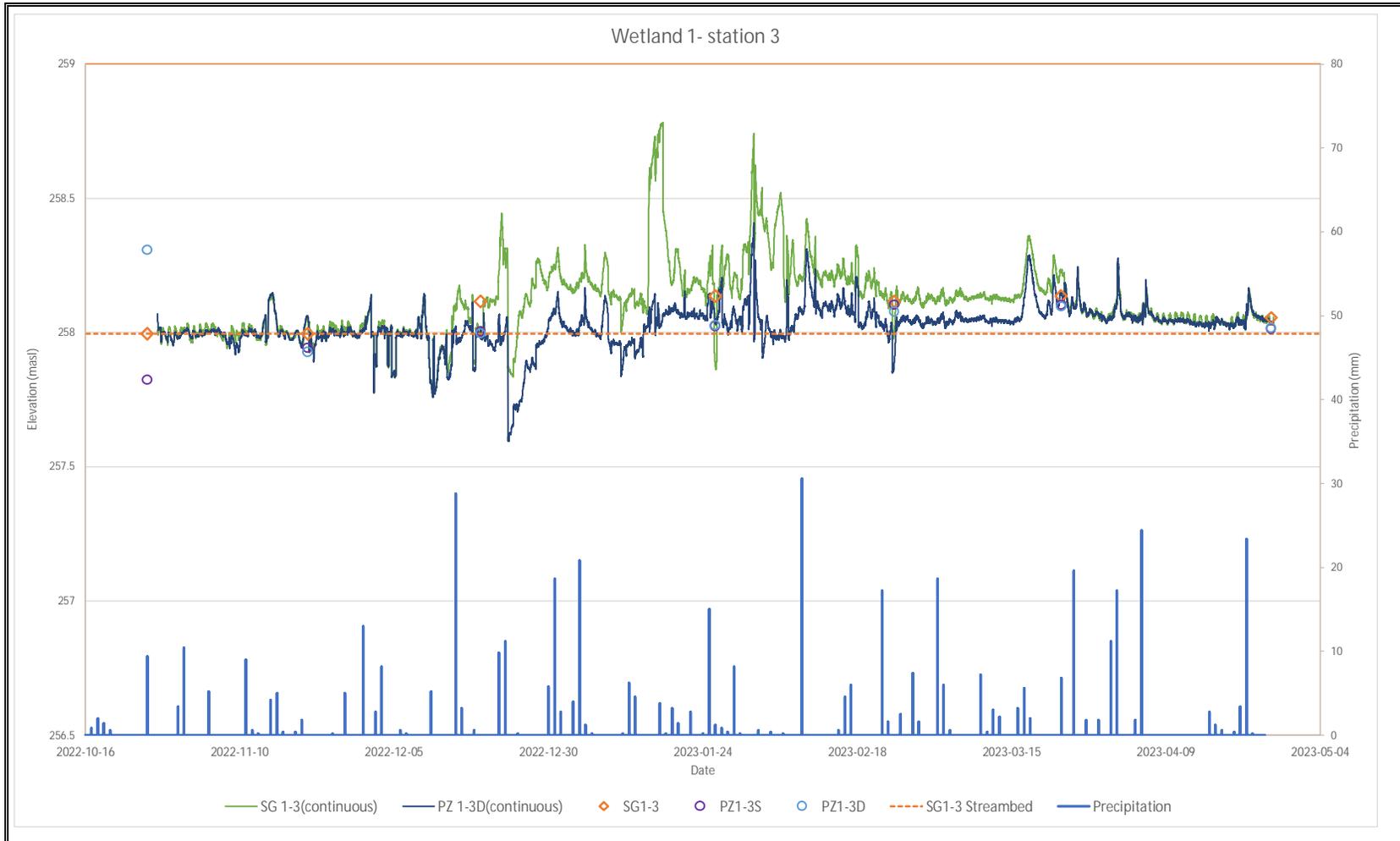


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WATER RESOURCES • ENVIRONMENTAL • GEOTECHNICAL • SURVEYING

Argo King I & II
 WETLAND 1 HYDROGRAPH

October 2022 - May 2022
 F-21

WATER LEVEL HYDROGRAPH



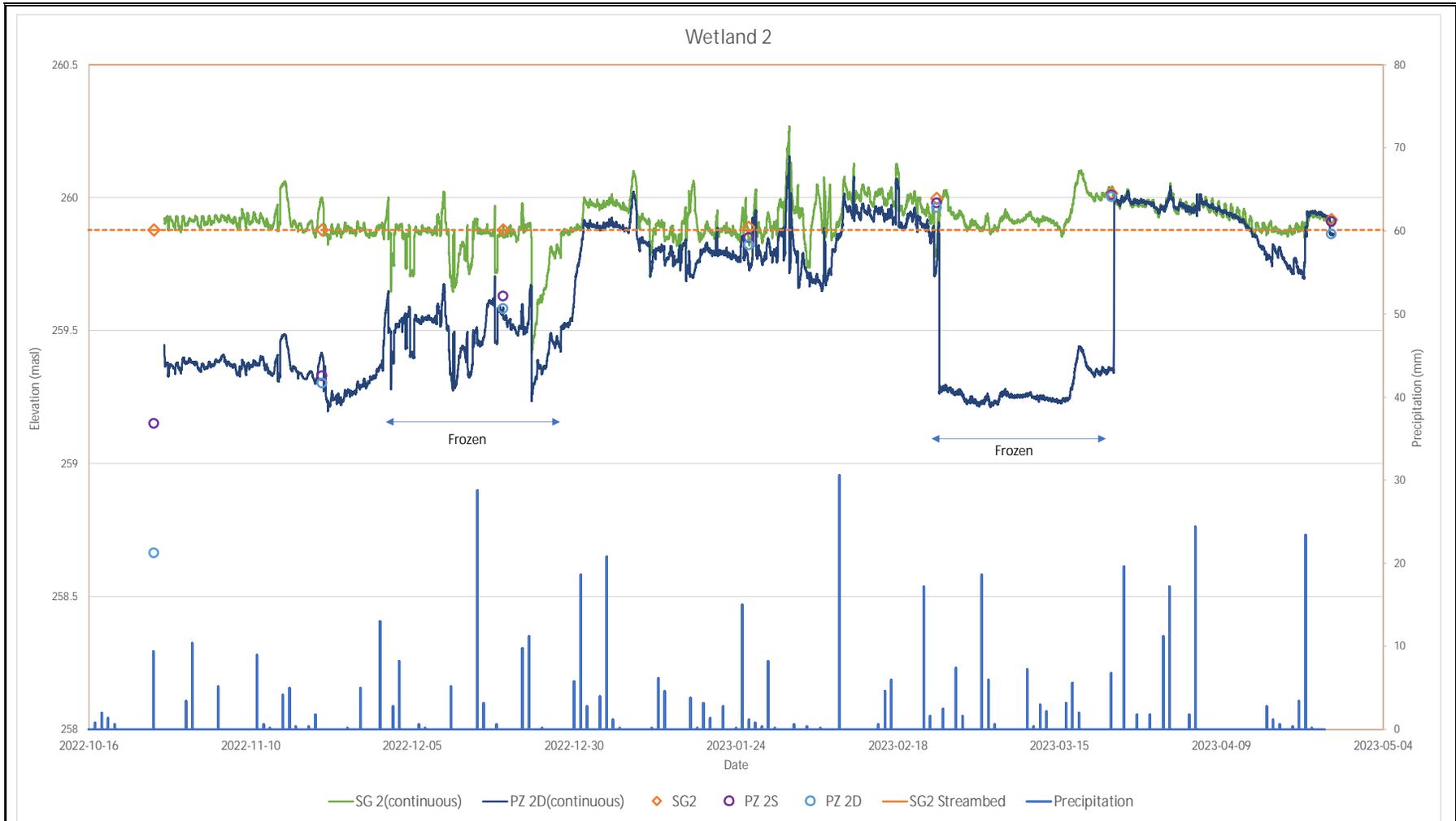
Argo King I & II
WETLAND 1 HYDROGRAPH

October 2022 - May 2022
F-22



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Environmental & Infrastructure Survey, Modelling & Hydrogeology

WATER LEVEL HYDROGRAPH

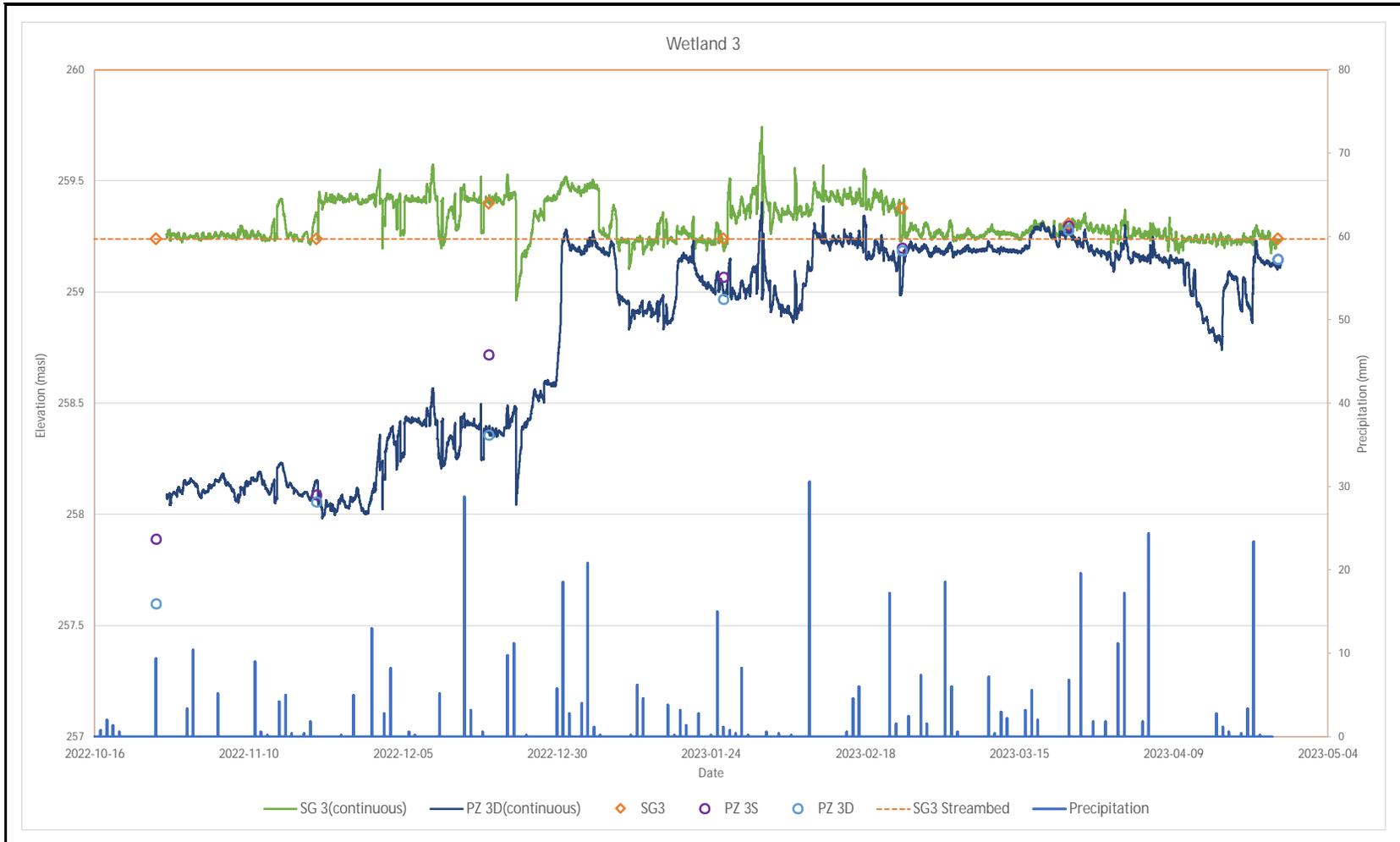


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Спеціалізовані Лічильно-вимірні Станції та Моніторингові Системи

Argo King I & II
 WETLAND 2 HYDROGRAPH

October 2022 - May 2023
 F-23

WATER LEVEL HYDROGRAPH

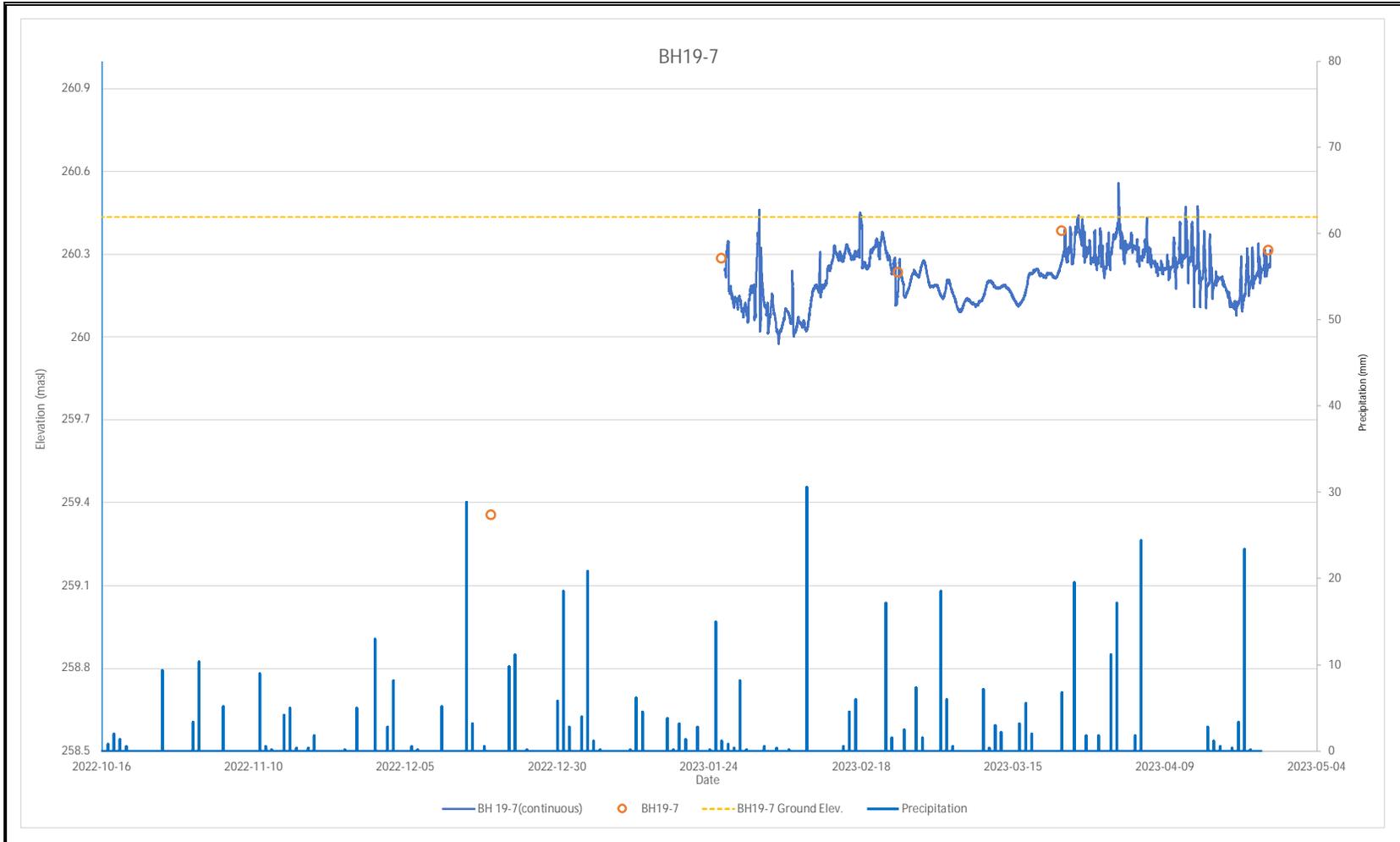


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WETLAND 3 HYDROGRAPH

October 2022 - May 2023
F-24

WATER LEVEL HYDROGRAPH

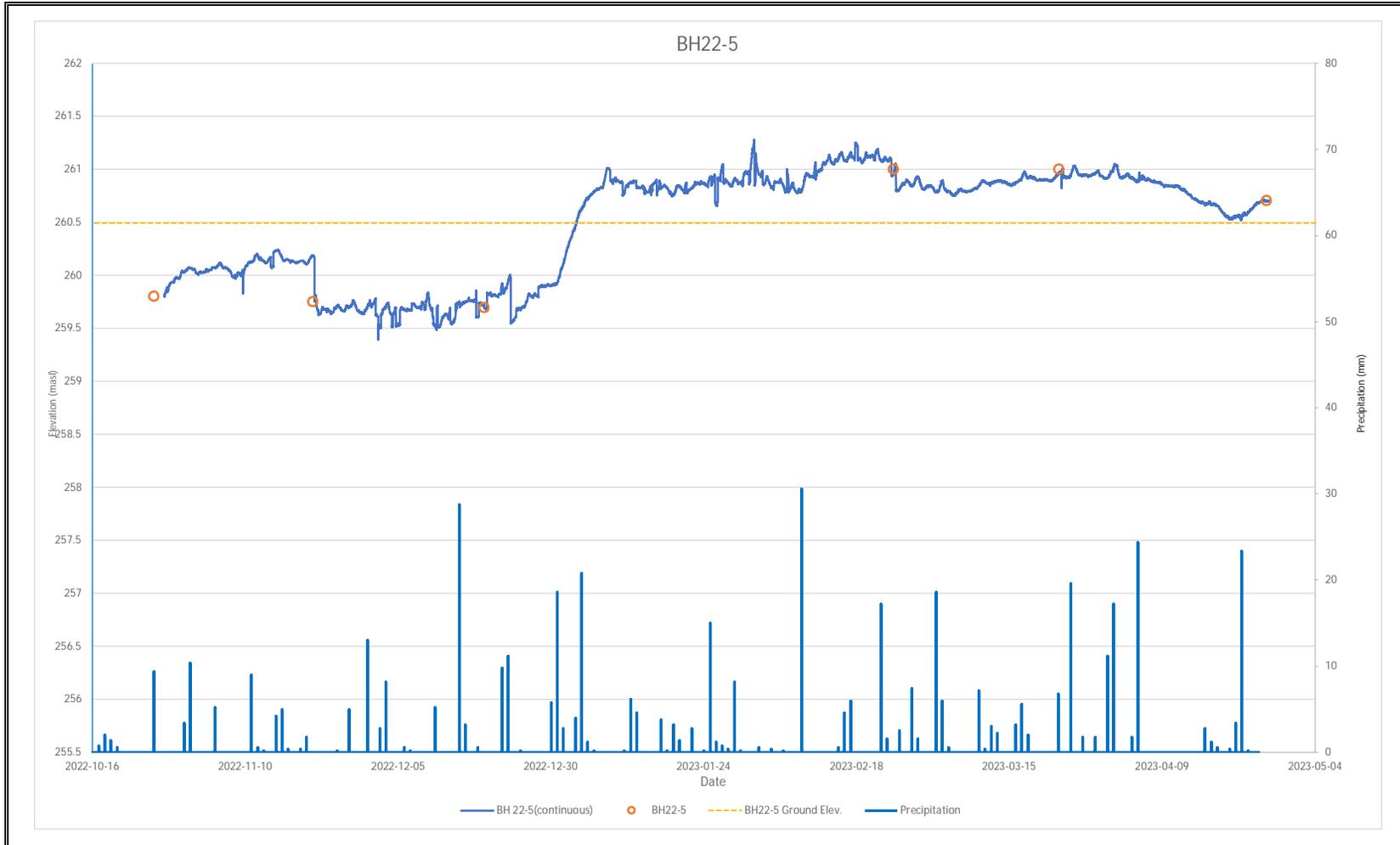


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Argo King I & II
 BH19-7 HYDROGRAPH

October 2022 - May 2023
 F-25

WATER LEVEL HYDROGRAPH

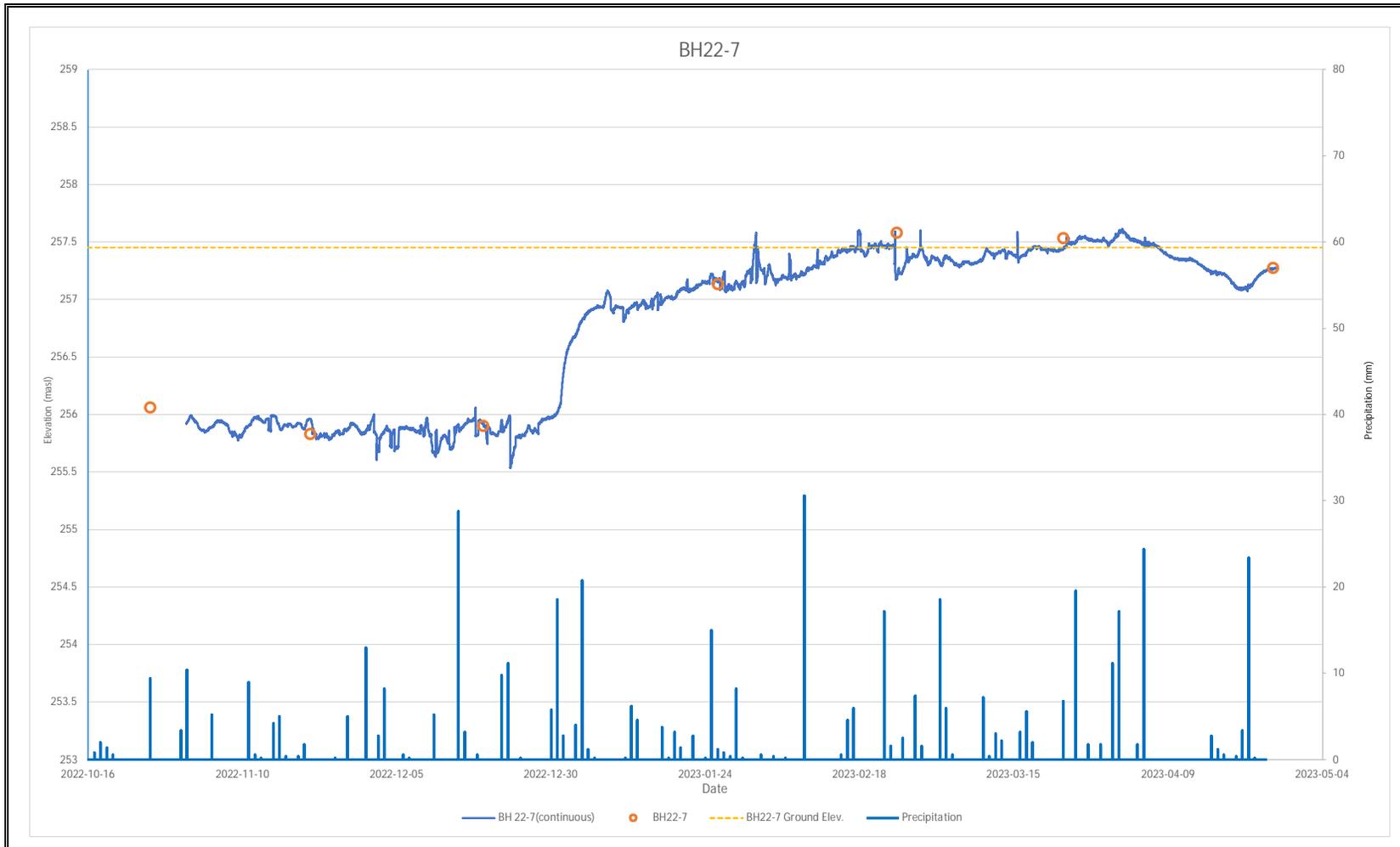


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Argo King I & II
 BH22-5 HYDROGRAPH

October 2022 - May 2023
 F-26

WATER LEVEL HYDROGRAPH



Argo King I & II
BH22-7 HYDROGRAPH

October 2022 - May 2023
F-27



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Water Resources | Environmental | Civil | New Urban | Transportation



Appendix G

TABLE 1
 CLIMATE NORMALS - PERSON CLIMATE STATION
 CALED ON STATION

| Month | Thornthwaite (1948) | | | | | |
|---------------|-----------------------|-------------|--|---------------------------|--|--------------------------|
| | Mean Temperature (°C) | Heat Index | Unadjusted Potential Evapotranspiration (mm) | Daylight Correction Value | Adjusted Potential Evapotranspiration (mm) | Total Precipitation (mm) |
| January | -5.5 | 0.0 | 0.0 | 0.78 | 0.0 | 51.8 |
| February | -4.5 | 0.0 | 0.0 | 0.88 | 0.0 | 47.7 |
| March | 0.1 | 0.0 | 0.2 | 0.99 | 0.2 | 49.8 |
| April | 7.1 | 1.7 | 30.4 | 1.12 | 34.1 | 68.5 |
| May | 13.1 | 4.3 | 60.7 | 1.22 | 74.1 | 74.3 |
| June | 18.6 | 7.3 | 90.2 | 1.28 | 115.4 | 71.5 |
| July | 21.5 | 9.1 | 106.2 | 1.25 | 132.7 | 75.7 |
| August | 20.6 | 8.5 | 101.2 | 1.16 | 117.4 | 78.1 |
| September | 16.2 | 5.9 | 77.2 | 1.04 | 80.2 | 74.5 |
| October | 9.5 | 2.6 | 42.3 | 0.92 | 38.9 | 61.1 |
| November | 3.7 | 0.6 | 14.6 | 0.81 | 11.8 | 75.1 |
| December | -2.2 | 0.0 | 0.0 | 0.75 | 0.0 | 57.9 |
| TOTALS | | 40.1 | 522.9 | | 604.8 | 786.0 |

Notes: Daylight Correction values obtained from Instruction and Tables For Computing Potential Evapotranspiration and The Water Balance (Thornthwaite & Mather, 1957)

TABLE 2
PRE-DEVELOPMENT WATER BALANCE
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total |
|---|--|-----------------|----------|-----------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|----------|-----------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - |
| Soil Moisture Storage (mm) | | 200.00 | 200.00 | 200.00 | 156.09 | 99.08 | 59.83 | 54.09 | 76.31 | 139.58 | 197.48 | 200.00 | 200.00 | - |
| Actual Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 110.59 | 112.07 | 93.70 | 76.14 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 551.60 |
| P-AET (mm) | | 49.55 | 34.41 | 0.22 | -39.09 | -36.37 | -15.60 | -1.64 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -39.09 | -75.46 | -91.05 | -92.69 | -70.47 | -7.19 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 39.09 | 36.37 | 15.60 | 1.64 | -22.22 | -63.28 | -7.19 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 50.71 | 51.80 | 47.70 | 234.40 |
| Infiltration Factor | | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | - |
| Run-Off Coefficient | | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | - |
| Infiltration (mm) | | 19.82 | 13.77 | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 20.28 | 20.72 | 19.08 | 93.76 |
| Run-Off (mm) | | 29.73 | 20.65 | 0.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 30.43 | 31.08 | 28.62 | 140.64 |
| Catchment Area (m ²) = 198234.98 | | Monthly Volumes | | | | | | | | | | | | |
| AET (m ³) | | 48.81 | 6757.08 | 14685.29 | 21922.41 | 22215.71 | 18573.71 | 15092.65 | 7708.02 | 2343.28 | 0.00 | 0.00 | 0.00 | 109346.96 |
| Infiltration (m ³) | | 3929.32 | 2728.81 | 17.43 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4020.99 | 4107.43 | 3782.32 | 18586.29 |
| Run-Off (m ³) | | 5893.97 | 4093.21 | 26.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 6031.49 | 6161.14 | 5673.49 | 27879.44 |
| Soil Moisture Storage (mm) | | 150.00 | 150.00 | 150.00 | 106.09 | 49.08 | 9.83 | 4.09 | 26.31 | 89.58 | 147.48 | 150.00 | 150.00 | - |
| Actual Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 108.98 | 105.19 | 85.81 | 74.77 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 533.86 |
| P-AET (mm) | | 49.55 | 34.41 | 0.22 | -37.48 | -29.49 | -7.71 | -0.27 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -37.48 | -66.97 | -74.68 | -74.94 | -52.73 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 37.48 | 29.49 | 7.71 | 0.27 | -22.22 | -52.73 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 10.55 | 57.90 | 51.80 | 47.70 | 252.14 |
| Infiltration Factor | | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | - |
| Run-Off Coefficient | | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | 0.65 | - |
| Infiltration (mm) | | 17.34 | 12.04 | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.69 | 20.27 | 18.13 | 16.70 | 88.25 |
| Run-Off (mm) | | 32.21 | 22.37 | 0.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 6.86 | 37.64 | 33.67 | 31.01 | 163.89 |
| Catchment Area (m ²) = 1099333.54 | | Monthly Volumes | | | | | | | | | | | | |
| AET (m ³) | | 270.69 | 37472.10 | 81438.87 | 119806.93 | 115636.21 | 94332.64 | 82193.18 | 42745.68 | 12994.90 | 0.00 | 0.00 | 0.00 | 586891.20 |
| Infiltration (m ³) | | 19066.64 | 13241.29 | 84.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4059.96 | 22277.99 | 19930.92 | 18353.37 | 97014.73 |
| Run-Off (m ³) | | 35409.48 | 24590.96 | 157.05 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 7539.92 | 41373.42 | 37014.56 | 34084.84 | 180170.22 |
| Soil Moisture Storage (mm) | | 150.00 | 150.00 | 150.00 | 106.09 | 49.08 | 9.83 | 4.09 | 26.31 | 89.58 | 147.48 | 150.00 | 150.00 | - |
| Actual Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 108.98 | 105.19 | 85.81 | 74.77 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 533.86 |
| P-AET (mm) | | 49.55 | 34.41 | 0.22 | -37.48 | -29.49 | -7.71 | -0.27 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -37.48 | -66.97 | -74.68 | -74.94 | -52.73 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 37.48 | 29.49 | 7.71 | 0.27 | -22.22 | -52.73 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 10.55 | 57.90 | 51.80 | 47.70 | 252.14 |
| Infiltration Factor | | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | - |
| Run-Off Coefficient | | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | - |
| Infiltration (mm) | | 7.43 | 5.16 | 0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.58 | 8.69 | 7.77 | 7.16 | 37.82 |
| Run-Off (mm) | | 42.12 | 29.25 | 0.19 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 8.97 | 49.22 | 44.03 | 40.55 | 214.32 |
| Catchment Area (m ²) = 388529.98 | | Monthly Volumes | | | | | | | | | | | | |
| AET (m ³) | | 95.67 | 13243.51 | 28782.39 | 42342.55 | 40868.52 | 33339.35 | 29048.98 | 15107.32 | 4592.70 | 0.00 | 0.00 | 0.00 | 207420.97 |
| Infiltration (m ³) | | 2887.97 | 2005.62 | 12.81 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 614.95 | 3374.38 | 3018.88 | 2779.93 | 14694.54 |
| Run-Off (m ³) | | 16365.16 | 11365.18 | 72.58 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3484.72 | 19121.50 | 17106.98 | 15752.95 | 83269.06 |
| Soil Moisture Storage (mm) | | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| Actual Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 |
| P-AET (mm) | | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 |
| Infiltration Factor | | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| Infiltration (mm) | | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 |
| Run-Off (mm) | | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 |
| Catchment Area (m ²) = 98770.54 | | Monthly Volumes | | | | | | | | | | | | |
| AET (m ³) | | 24.32 | 3366.71 | 7316.94 | 10129.43 | 8644.07 | 7713.98 | 7358.41 | 3840.52 | 1167.54 | 0.00 | 0.00 | 0.00 | 49561.91 |
| Infiltration (m ³) | | 1468.34 | 1019.72 | 6.51 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1263.01 | 1715.64 | 1534.89 | 1413.41 | 8421.52 |
| Run-Off (m ³) | | 3426.12 | 2379.35 | 15.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2947.01 | 4003.17 | 3581.42 | 3297.95 | 19650.21 |
| Catchment Area (m ²) = 31674.33 | | Monthly Volumes | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | | 236.61 | 325.45 | 353.01 | 339.71 | 359.66 | 371.06 | 353.96 | 290.30 | 356.81 | 275.09 | 246.11 | 226.63 | 3734.40 |
| Run-Off from Imperv. (m ³) - with 15% evap. | | 1340.77 | 1844.24 | 2000.39 | 1925.01 | 2038.08 | 2102.70 | 2005.78 | 1645.01 | 2021.93 | 1558.85 | 1394.62 | 1284.24 | 21161.62 |
| Total Catchment Volumes | | | | | | | | | | | | | | |
| Total ET (m ³) | | 236.61 | 325.45 | 353.01 | 339.71 | 359.66 | 371.06 | 353.96 | 290.30 | 356.81 | 275.09 | 246.11 | 226.63 | 3734.40 |
| Total AET (m ³) | | 439.49 | 60839.40 | 132223.49 | 194201.31 | 187364.50 | 153959.68 | 133693.21 | 69401.55 | 21098.42 | 0.00 | 0.00 | 0.00 | 953221.04 |
| Total Infiltration (m ³) | | 27352.26 | 18995.43 | 121.31 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 5937.91 | 31389.01 | 28592.12 | 26329.04 | 138717.09 |
| Total Runoff (m ³) | | 62435.50 | 44272.94 | 2271.36 | 1925.01 | 2038.08 | 2102.70 | 2005.78 | 1645.01 | 15993.58 | 72088.43 | 65258.72 | 60093.45 | 332130.56 |

NOTES:
1) PET and P Taken from Table 1
2) Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
3) Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
4) Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

TABLE 3
POST-DEVELOPMENT WATER BALANCE
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total |
|---|--|--------------------|---------|---------|---------|---------|---------|-----------|---------|----------|----------|---------|----------|----------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - |
| Soil Moisture Storage (mm) | | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| Actual Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 |
| P-AET (mm) | | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 |
| Infiltration Factor | | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| Infiltration (mm) | | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 |
| Run-Off (mm) | | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 |
| Catchment Area (m ²) 23007.39 | | Imperv coeff. 0.83 | | | | | | | | | | | | |
| | | Monthly Volumes | | | | | | | | | | | | |
| AET (m ³) | | 5.67 | 784.23 | 1704.39 | 2359.53 | 2013.53 | 1796.88 | 1714.05 | 894.60 | 271.96 | 0.00 | 0.00 | 0.00 | 11544.84 |
| Infiltration (m ³) | | 342.03 | 237.53 | 1.52 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 294.20 | 399.64 | 357.53 | 329.24 | 1961.69 |
| Run-Off (m ³) | | 798.07 | 554.24 | 3.54 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 686.47 | 932.49 | 834.25 | 768.22 | 4577.28 |
| Catchment Area (m ²) = 112330.17 | | Monthly Volumes | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | | 839.11 | 1154.19 | 1251.92 | 1204.74 | 1275.51 | 1315.95 | 1255.29 | 1029.51 | 1265.40 | 975.59 | 872.81 | 803.72 | 13243.73 |
| Run-Off from Imperv. (m ³) - with 15% evap. | | 4754.94 | 6540.42 | 7094.21 | 6826.87 | 7227.89 | 7457.04 | 7113.31 | 5833.87 | 7170.60 | 5528.33 | 4945.90 | 4554.43 | 75047.79 |
| Soil Moisture Storage (mm) | | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| Actual Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 |
| P-AET (mm) | | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 | |
| Infiltration Factor | | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| Infiltration (mm) | | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 |
| Run-Off (mm) | | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 |
| Catchment Area (m ²) 9000.00 | | Imperv coeff. 0.90 | | | | | | | | | | | | |
| | | Monthly Volumes | | | | | | | | | | | | |
| AET (m ³) | | 2.22 | 306.78 | 666.72 | 923.00 | 787.65 | 702.90 | 670.50 | 349.95 | 106.39 | 0.00 | 0.00 | 0.00 | 4516.10 |
| Infiltration (m ³) | | 133.80 | 92.92 | 0.59 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 115.09 | 156.33 | 139.86 | 128.79 | 767.37 |
| Run-Off (m ³) | | 312.19 | 216.81 | 1.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 268.53 | 364.77 | 326.34 | 300.51 | 1790.53 |
| Catchment Area (m ²) = 81000.00 | | Monthly Volumes | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | | 605.07 | 832.28 | 902.75 | 868.73 | 919.76 | 948.92 | 905.18 | 742.37 | 912.47 | 703.49 | 629.37 | 579.56 | 9549.90 |
| Run-Off from Imperv. (m ³) - with 15% evap. | | 3428.73 | 4716.23 | 5115.56 | 4922.78 | 5211.95 | 5377.19 | 5129.33 | 4206.74 | 5170.64 | 3986.42 | 3566.43 | 3284.15 | 54116.10 |
| Soil Moisture Storage (mm) | | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| Actual Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 |
| P-AET (mm) | | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 | |
| Infiltration Factor | | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| Infiltration (mm) | | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 |
| Run-Off (mm) | | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 |
| Catchment Area (m ²) 11002.16 | | Imperv coeff. 0.89 | | | | | | | | | | | | |
| | | Monthly Volumes | | | | | | | | | | | | |
| AET (m ³) | | 2.71 | 375.02 | 815.04 | 1128.33 | 962.87 | 859.27 | 819.66 | 427.80 | 130.05 | 0.00 | 0.00 | 0.00 | 5520.76 |
| Infiltration (m ³) | | 163.56 | 113.59 | 0.73 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 140.69 | 191.11 | 170.97 | 157.44 | 938.08 |
| Run-Off (m ³) | | 381.64 | 265.04 | 1.69 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 328.27 | 445.92 | 398.94 | 367.36 | 2188.86 |
| Catchment Area (m ²) = 89017.52 | | Monthly Volumes | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | | 664.96 | 914.65 | 992.10 | 954.71 | 1010.79 | 1042.84 | 994.77 | 815.85 | 1002.78 | 773.12 | 691.67 | 636.92 | 10495.17 |
| Run-Off from Imperv. (m ³) - with 15% evap. | | 3768.11 | 5183.04 | 5621.90 | 5410.04 | 5727.83 | 5909.43 | 5637.03 | 4623.12 | 5682.43 | 4381.00 | 3919.44 | 3609.22 | 59472.60 |

NOTES:

- PET and P Taken from Table 1
- Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
- Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
- Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

TABLE 3
POST-DEVELOPMENT WATER BALANCE
CALDON STATION

| | | | | | | | | | | | | | | | | |
|---|----------------------------------|--------------------------------------|-----------|--------------------|----------|----------|----------|----------|----------|----------|----------|----------|------------------|---------|---------------|--|
| Catchment 104 | Development - Pervious Landscape | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | - | | |
| | | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 | |
| | | P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - | |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - | |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - | |
| | | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 | |
| | | Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - | |
| | | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - | |
| | | Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 | |
| | | Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 | |
| | | Catchment Area (m ²) | 154682.83 | Imperv coeff. 0.78 | | | | | | | | | | | | |
| | | AET (m ³) | 38.09 | 5272.55 | 11458.94 | 15863.52 | 13537.32 | 12080.73 | 11523.87 | 6014.57 | 1828.46 | 0.00 | 0.00 | 0.00 | 77618.05 | |
| | | Infiltration (m ³) | 2299.54 | 1596.97 | 10.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1977.97 | 2686.84 | 2403.77 | 2213.51 | 13188.80 | |
| | | Run-Off (m ³) | 5365.58 | 3726.26 | 23.80 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4615.27 | 6269.29 | 5608.80 | 5164.86 | 30773.86 | |
| | | Catchment Area (m ²) | 548420.93 | Monthly Volumes | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | 4096.70 | 5635.03 | 6112.15 | 5881.81 | 6227.32 | 6424.75 | 6128.60 | 5026.28 | 6177.96 | 4763.04 | 4261.23 | 3923.95 | 64658.83 | | | |
| Run-Off from Imperv. (m ³) - with 15% evap. | 23214.66 | 31931.81 | 34635.52 | 33330.28 | 35288.14 | 36406.92 | 34728.76 | 28482.24 | 35008.45 | 26990.54 | 24146.97 | 22235.73 | 366400.02 | | | |
| Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - | | | |
| Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 | | | |
| P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - | | | |
| Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - | | | |
| Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - | | | |
| Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 | | | |
| Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - | | | |
| Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - | | | |
| Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 | | | |
| Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 | | | |
| Catchment Area (m ²) | 123597.96 | Imperv coeff. 0.64 | | | | | | | | | | | | | | |
| AET (m ³) | 30.43 | 4212.98 | 9156.16 | 12675.60 | 10816.88 | 9653.00 | 9208.05 | 4805.89 | 1461.02 | 0.00 | 0.00 | 0.00 | 62020.02 | | | |
| Infiltration (m ³) | 1837.42 | 1276.04 | 8.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1580.48 | 2146.90 | 1920.71 | 1768.69 | 10538.39 | | | |
| Run-Off (m ³) | 4287.32 | 2977.43 | 19.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3687.79 | 5009.43 | 4481.66 | 4126.94 | 24589.58 | | | |
| Catchment Area (m ²) | 219729.71 | Monthly Volumes | | | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | 1641.38 | 2257.72 | 2448.89 | 2356.60 | 2495.03 | 2574.13 | 2455.48 | 2013.82 | 2475.26 | 1908.35 | 1707.30 | 1572.17 | 25906.13 | | | |
| Run-Off from Imperv. (m ³) - with 15% evap. | 9301.16 | 12793.76 | 13877.03 | 13354.07 | 14138.51 | 14586.76 | 13914.38 | 11411.66 | 14026.45 | 10814.00 | 9674.70 | 8908.94 | 146801.42 | | | |
| Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - | | | |
| Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 | | | |
| P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - | | | |
| Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - | | | |
| Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - | | | |
| Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 | | | |
| Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - | | | |
| Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - | | | |
| Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 | | | |
| Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 | | | |
| Catchment Area (m ²) | 61710.34 | Imperv coeff. 0.78 | | | | | | | | | | | | | | |
| AET (m ³) | 15.19 | 2103.47 | 4571.52 | 6328.71 | 5400.68 | 4819.58 | 4597.42 | 2399.50 | 729.46 | 0.00 | 0.00 | 0.00 | 30965.53 | | | |
| Infiltration (m ³) | 917.39 | 637.11 | 4.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 789.11 | 1071.91 | 958.98 | 883.07 | 5261.64 | | | |
| Run-Off (m ³) | 2140.59 | 1486.58 | 9.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1841.25 | 2501.12 | 2237.62 | 2060.51 | 12277.16 | | | |
| Catchment Area (m ²) | 218791.19 | Monthly Volumes | | | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | 1634.37 | 2248.08 | 2438.43 | 2346.54 | 2484.37 | 2563.14 | 2444.99 | 2005.22 | 2464.68 | 1900.20 | 1700.01 | 1565.45 | 25795.48 | | | |
| Run-Off from Imperv. (m ³) - with 15% evap. | 9261.43 | 12739.12 | 13817.76 | 13297.03 | 14078.12 | 14524.45 | 13854.95 | 11362.92 | 13966.54 | 10767.81 | 9633.38 | 8870.89 | 146174.40 | | | |

NOTES:

- PET and P Taken from Table 1
- Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
- Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
- Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

TABLE 3
POST-DEVELOPMENT WATER BALANCE
CALDON STATION

| | | | | | | | | | | | | | | | | |
|---|--------------------------------------|---|------------------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------------------|------------------|---------------|--|
| Channel 1 & 2 | Development - Pervious Landscape | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | - | | |
| | | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 | |
| | | P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - | |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - | |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - | |
| | | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 | |
| | | Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - | |
| | | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - | |
| | | Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 | |
| | | Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 | |
| | | Catchment Area (m ²) 26559.05 | Imperv coeff. 0.10 Monthly Volumes | | | | | | | | | | | | | |
| | | AET (m ³) | 6.54 | 905.30 | 1967.50 | 2723.77 | 2324.36 | 2074.26 | 1978.65 | 1032.70 | 313.95 | 0.00 | 0.00 | 0.00 | 13327.03 | |
| | | Infiltration (m ³) | 394.83 | 274.20 | 1.75 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 339.62 | 461.33 | 412.73 | 380.06 | 2264.52 | |
| | | Run-Off (m ³) | 921.27 | 639.80 | 4.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 792.44 | 1076.44 | 963.03 | 886.81 | 5283.87 | |
| | | Catchment Area (m ²) = 2951.01 | Monthly Volumes | | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | 22.04 | 30.32 | 32.89 | 31.65 | 33.51 | 34.57 | 32.98 | 27.05 | 33.24 | 25.63 | 22.93 | 21.11 | 347.92 | | | |
| Run-Off from Imperv. (m ³) - with 15% evap. | 124.92 | 171.82 | 186.37 | 179.35 | 189.88 | 195.90 | 186.87 | 153.26 | 188.38 | 145.23 | 129.93 | 119.65 | 1971.57 | | | |
| Pond 2A | Development - Pervious Landscape | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | - | | |
| | | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 | |
| | | P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - | |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - | |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - | |
| | | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 | |
| | | Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - | |
| | | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - | |
| | | Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 | |
| | | Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 | |
| | | Catchment Area (m ²) 5653.57 | Imperv coeff. 0.85 Monthly Volumes | | | | | | | | | | | | | |
| | | AET (m ³) | 1.39 | 192.71 | 418.82 | 579.80 | 494.78 | 441.54 | 421.19 | 219.83 | 66.83 | 0.00 | 0.00 | 0.00 | 2836.90 | |
| | | Infiltration (m ³) | 84.05 | 58.37 | 0.37 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 72.29 | 98.20 | 87.86 | 80.90 | 482.04 | |
| | | Run-Off (m ³) | 196.11 | 136.19 | 0.87 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 168.69 | 229.14 | 205.00 | 188.77 | 1124.77 | |
| | | Catchment Area (m ²) = 32036.92 | Monthly Volumes | | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | 239.32 | 329.18 | 357.05 | 343.60 | 363.78 | 375.31 | 358.01 | 293.62 | 360.90 | 278.24 | 248.93 | 229.22 | 3777.15 | | | |
| Run-Off from Imperv. (m ³) - with 15% evap. | 1356.12 | 1865.35 | 2023.29 | 1947.04 | 2061.42 | 2126.77 | 2028.74 | 1663.84 | 2045.08 | 1576.70 | 1410.59 | 1298.94 | 21403.86 | | | |
| NHS | Pasture/Shrub, Silty Clay Soils | Soil Moisture Storage (mm) | 200.00 | 200.00 | 200.00 | 156.09 | 99.08 | 59.83 | 54.09 | 76.31 | 75.00 | 132.90 | 135.42 | 135.42 | - | |
| | | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 110.59 | 112.07 | 93.70 | 76.14 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 551.60 | |
| | | P-AET (mm) | 49.55 | 34.41 | 0.22 | -39.09 | -36.37 | -15.60 | -1.64 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - | |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -39.09 | -75.46 | -91.05 | -92.69 | -70.47 | -7.19 | 0.00 | 0.00 | 0.00 | - | |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 39.09 | 36.37 | 15.60 | 1.64 | -22.22 | -63.28 | -7.19 | 0.00 | 0.00 | - | |
| | | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 50.71 | 51.80 | 47.70 | 234.40 | |
| | | Infiltration Factor | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | - | |
| | | Run-Off Coefficient | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | - | |
| | | Infiltration (mm) | 19.82 | 13.77 | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 20.28 | 20.72 | 19.08 | 93.76 | |
| | | Run-Off (mm) | 29.73 | 20.65 | 0.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 30.43 | 31.08 | 28.62 | 140.64 | |
| | | Catchment Area (m ²) 97052.63 | Imperv coeff. 0.00 Monthly Volumes | | | | | | | | | | | | | |
| | | AET (m ³) | 23.90 | 3308.16 | 7189.68 | 10732.86 | 10876.45 | 9093.39 | 7389.12 | 3773.72 | 1147.23 | 0.00 | 0.00 | 0.00 | 53534.50 | |
| | | Infiltration (m ³) | 1923.73 | 1335.98 | 8.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1968.61 | 2010.93 | 1851.76 | 9099.55 | | |
| | | Run-Off (m ³) | 2885.59 | 2003.97 | 12.80 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2952.92 | 3016.40 | 2777.65 | 13649.32 | | |
| | | Catchment Area (m ²) = 0.00 | Monthly Volumes | | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | |
| Run-Off from Imperv. (m ³) - with 15% evap. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | |
| Total Site | Total Catchment Volumes | | | | | | | | | | | | | | | |
| | Total ET (m ³) | 9742.95 | 13401.45 | 14536.17 | 13988.38 | 14810.07 | 15279.61 | 14575.30 | 11953.70 | 14692.69 | 11327.65 | 10134.24 | 9332.11 | 153774.31 | | |
| | Total AET (m ³) | 126.13 | 17461.20 | 37948.77 | 53315.11 | 47214.53 | 41521.55 | 38322.51 | 19918.58 | 6055.35 | 0.00 | 0.00 | 0.00 | 261883.71 | | |
| | Total Infiltration (m ³) | 8096.35 | 5622.70 | 35.91 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 5309.45 | 9180.87 | 8463.35 | 7793.47 | 44502.08 | | |
| Total Runoff (m ³) | 72498.43 | 87947.87 | 82448.32 | 79267.46 | 83923.73 | 86584.46 | 82593.37 | 67737.65 | 95647.26 | 83971.53 | 75499.37 | 69523.55 | 967642.99 | | | |

NOTES:

- PET and P Taken from Table 1
- Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
- Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
- Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

TABLE 4
POST-DEVELOPMENT WATER BALANCE WITH MITIGATION
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total |
|---|--|---------------------------------|---------|---------|---------|---------|---------|-----------|---------|----------|----------|---------|----------|-----------------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - |
| Soil Moisture Storage (mm) | | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| Actual Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 |
| P-AET (mm) | | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 |
| Infiltration Factor | | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| Infiltration (mm) | | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 |
| Run-Off (mm) | | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 |
| Catchment Area (m ²) 12087.39 | | Monthly Volumes | | | | | | | | | | | | |
| AET (m ³) | | 2.98 | 412.01 | 895.44 | 1239.62 | 1057.85 | 944.02 | 900.51 | 470.00 | 142.88 | 0.00 | 0.00 | 0.00 | 6065.31 |
| Infiltration (m ³) | | 179.69 | 124.79 | 0.80 | 0.00 | 0.00 | 0.00 | 0.00 | 154.56 | 209.96 | 187.84 | 172.97 | 1030.61 | 1030.61 |
| Run-Off (m ³) | | 419.28 | 291.18 | 1.86 | 0.00 | 0.00 | 0.00 | 0.00 | 360.65 | 489.90 | 438.29 | 403.60 | 2404.76 | 2404.76 |
| Development - Unconnected Pervious Landscape | | Monthly Volumes | | | | | | | | | | | | |
| Catchment Area (m ²) = 97050.17 | | Imperv coeff. 0.83 | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | | 724.96 | 997.19 | 1081.62 | 1040.86 | 1102.00 | 1136.94 | 1084.54 | 889.46 | 1093.27 | 842.88 | 754.08 | 694.39 | 11442.22 |
| Run-Off from Imperv. (m ³) - with 15% evap. | | 4108.13 | 5650.75 | 6129.20 | 5898.22 | 6244.69 | 6442.68 | 6145.70 | 5040.30 | 6195.20 | 4776.32 | 4273.12 | 3934.90 | 64839.22 |
| P - Total Precipitation plus irrigation (mm) | | 54.50 | 74.97 | 81.32 | 78.25 | 82.85 | 85.48 | 81.54 | 66.87 | 82.19 | 63.37 | 56.69 | 52.21 | - |
| P-PET (mm) | | 54.26 | 40.88 | 7.24 | -37.15 | -49.86 | -31.88 | 1.29 | 27.99 | 70.37 | 63.37 | 56.69 | 52.21 | - |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -37.15 | -87.01 | -118.89 | -117.60 | -89.61 | -19.24 | 0.00 | 0.00 | 0.00 | - |
| Soil Moisture Storage (mm) | | 75.00 | 75.00 | 75.00 | 37.85 | 0.00 | 0.00 | 1.29 | 29.28 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| Actual Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 104.53 | 90.08 | 78.10 | 74.55 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 506.38 |
| P-AET (mm) | | 54.26 | 40.88 | 7.24 | -26.28 | -7.23 | 7.38 | 6.99 | 27.99 | 70.37 | 63.37 | 56.69 | 52.21 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -26.28 | -33.51 | -26.14 | -19.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 26.28 | 7.23 | -7.38 | -6.99 | -19.15 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 54.26 | 40.88 | 7.24 | 0.00 | 0.00 | 0.00 | 0.00 | 8.84 | 70.37 | 63.37 | 56.69 | 52.21 | 353.85 |
| MOECC Infiltration Factor | | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| Infiltration (mm) | | 16.28 | 12.26 | 2.17 | 0.00 | 0.00 | 0.00 | 0.00 | 2.65 | 21.11 | 19.01 | 17.01 | 15.66 | 106.16 |
| Run-Off (mm) | | 37.98 | 28.62 | 5.07 | 0.00 | 0.00 | 0.00 | 0.00 | 6.19 | 49.26 | 44.36 | 39.68 | 36.54 | 247.70 |
| Catchment Area (m ²) 6840.00 | | Monthly Volumes (Pervious Area) | | | | | | | | | | | | |
| AET (m ³) | | 1.68 | 233.15 | 506.71 | 715.00 | 616.17 | 534.20 | 509.92 | 265.96 | 80.85 | 0.00 | 0.00 | 0.00 | 3463.65 |
| Infiltration (m ³) | | 111.34 | 83.89 | 14.85 | 0.00 | 0.00 | 0.00 | 0.00 | 18.13 | 144.40 | 130.03 | 116.33 | 107.12 | 726.10 |
| Run-Off (m ³) | | 259.78 | 195.75 | 34.65 | 0.00 | 0.00 | 0.00 | 0.00 | 42.31 | 336.94 | 303.41 | 271.44 | 249.96 | 1694.24 |
| Mitigation - Connected Pervious Park Area | | Monthly Volumes | | | | | | | | | | | | |
| Catchment Area (m ²) = 760.00 | | Imperv coeff. 0.10 | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | | 5.68 | 7.81 | 8.47 | 8.15 | 8.63 | 8.90 | 8.49 | 6.97 | 8.56 | 6.60 | 5.91 | 5.44 | 89.60 |
| Run-Off Directed to Pervious Area (m ³) | | 32.17 | 44.25 | 48.00 | 46.19 | 48.90 | 50.45 | 48.13 | 39.47 | 48.51 | 37.40 | 33.46 | 30.81 | 507.76 |

NOTES:

- PET and P Taken from Table 1
- Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
- Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
- Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

TABLE 4
POST-DEVELOPMENT WATER BALANCE WITH MITIGATION
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total | |
|---|---|--------------------------------------|-----------------|-----------------|--------|---------|---------|-----------|---------|----------|----------|---------|----------------|----------------|----------------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 | |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 | |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 | |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - | |
| Catchment 1 (continued) | Mitigation - Pervious Park Area to Silva Cells | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| | | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 |
| | | P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - |
| | | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 |
| | | Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| | | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| | | Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 |
| | | Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 |
| | | Catchment Area (m ²) | 3840.00 | Monthly Volumes | | | | | | | | | | | |
| | | AET (m ³) | 0.95 | 130.89 | 284.47 | 393.81 | 336.06 | 299.90 | 286.08 | 149.31 | 45.39 | 0.00 | 0.00 | 0.00 | 1926.87 |
| | Infiltration (m ³) | 57.09 | 39.64 | 0.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 49.10 | 66.70 | 59.67 | 54.95 | 327.41 | |
| | Run-Off Directed to Silva Cells (m ³) | 133.20 | 92.50 | 0.59 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 114.57 | 155.64 | 139.24 | 128.22 | 763.96 | |
| | Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | 133.20 | 92.50 | 0.59 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 114.57 | 155.64 | 139.24 | 128.22 | 763.96 | |
| | Run-Off (m ³) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | Catchment Area (m ²) | 7260.00 | Monthly Volumes | | | | | | | | | | | | |
| | Imperv. coeff. | 0.65 | Monthly Volumes | | | | | | | | | | | | |
| | Evaporation from Imperv. (m ³) - 15% of P. | 54.23 | 74.60 | 80.91 | 77.86 | 82.44 | 85.05 | 81.13 | 66.54 | 81.78 | 63.05 | 56.41 | 51.95 | 855.95 | |
| | Run-Off Directed to Silva Cells (m ³) | 307.32 | 422.71 | 458.51 | 441.23 | 467.14 | 481.96 | 459.74 | 377.05 | 463.44 | 357.30 | 319.66 | 294.36 | 4850.41 | |
| | Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | 307.32 | 422.71 | 458.51 | 441.23 | 467.14 | 481.96 | 459.74 | 377.05 | 463.44 | 357.30 | 319.66 | 294.36 | 4850.41 | |
| | Run-Off (m ³) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | Mitigation - Pervious ROW Area to Silva Cells | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| | | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 |
| | | P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - |
| | | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 |
| | | Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| | | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| Infiltration (mm) | | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 | |
| Run-Off (mm) | | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 | |
| Catchment Area (m ²) | | 2400.00 | Monthly Volumes | | | | | | | | | | | | |
| AET (m ³) | | 0.06 | 8.18 | 17.78 | 24.61 | 21.00 | 18.74 | 17.88 | 9.33 | 2.84 | 0.00 | 0.00 | 0.00 | 120.43 | |
| Infiltration (m ³) | 3.57 | 2.48 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.07 | 4.17 | 3.73 | 3.43 | 20.46 | | |
| Run-Off Directed to Silva Cells (m ³) | 8.33 | 5.78 | 0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 7.16 | 9.73 | 8.70 | 8.01 | 47.75 | | |
| Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | 8.33 | 5.78 | 0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 7.16 | 9.73 | 8.70 | 8.01 | 47.75 | | |
| Run-Off (m ³) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| Catchment Area (m ²) | 7260.00 | Monthly Volumes | | | | | | | | | | | | | |
| Imperv. coeff. | 0.80 | Monthly Volumes | | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | 54.23 | 74.60 | 80.91 | 77.86 | 82.44 | 85.05 | 81.13 | 66.54 | 81.78 | 63.05 | 56.41 | 51.95 | 855.95 | | |
| Run-Off Directed to Silva Cells (m ³) | 307.32 | 422.71 | 458.51 | 441.23 | 467.14 | 481.96 | 459.74 | 377.05 | 463.44 | 357.30 | 319.66 | 294.36 | 4850.41 | | |
| Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | 307.32 | 422.71 | 458.51 | 441.23 | 467.14 | 481.96 | 459.74 | 377.05 | 463.44 | 357.30 | 319.66 | 294.36 | 4850.41 | | |
| Run-Off (m ³) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |

- NOTES:
1) PET and P Taken from Table 1
2) Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
3) Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
4) Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

TABLE 4
POST-DEVELOPMENT WATER BALANCE WITH MITIGATION
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total | | |
|--|---|---|-----------------|--------------------|---------|---------|---------|-----------|---------|----------|----------|---------|----------|---------------|-----------------|-----------------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | | | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 | | |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 | | |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 | | |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - | | |
| Catchment 102 | Development - Pervious Landscape | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - | |
| | | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 | |
| | | P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - | |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - | |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - | |
| | | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 | |
| | | Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - | |
| | | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - | |
| | | Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 | |
| | Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 | | |
| | Catchment Area (m ²) 9000.00 | | Monthly Volumes | | | | | | | | | | | | | |
| | AET (m ³) | | 2.22 | 306.78 | 666.72 | 923.00 | 787.65 | 702.90 | 670.50 | 349.95 | 106.39 | 0.00 | 0.00 | 0.00 | 4516.10 | |
| | Infiltration (m ³) | | 133.80 | 92.92 | 0.59 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 115.09 | 156.33 | 139.86 | 128.79 | 767.37 | |
| | Run-Off (m ³) | | 312.19 | 216.81 | 1.38 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 268.53 | 364.77 | 300.51 | 300.51 | 1790.53 | |
| | Development - Impervious Area | Catchment Area (m ²) = 81000.00 | | Imperv coeff. 0.90 | | | | | | | | | | | | |
| | | | | Monthly Volumes | | | | | | | | | | | | |
| | | Evaporation from Imperv. (m ³) - 15% of P. | | 605.07 | 832.28 | 902.75 | 868.73 | 919.76 | 948.92 | 905.18 | 742.37 | 912.47 | 703.49 | 629.37 | 579.56 | 9549.90 |
| | | Run-Off from Imperv. (m ³) - with 15% evap. | | 3428.73 | 4716.23 | 5115.56 | 4922.78 | 5211.95 | 5377.19 | 5129.33 | 4206.74 | 5170.64 | 3986.42 | 3566.43 | 3284.15 | 54116.10 |
| Catchment 103 | Development - Pervious Landscape | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - | |
| | | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 | |
| | | P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - | |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - | |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - | |
| | | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 | |
| | | Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - | |
| | | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - | |
| | | Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 | |
| | Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 | | |
| | Catchment Area (m ²) 11002.16 | | Monthly Volumes | | | | | | | | | | | | | |
| | AET (m ³) | | 2.71 | 375.02 | 815.04 | 1128.33 | 962.87 | 859.27 | 819.66 | 427.80 | 130.05 | 0.00 | 0.00 | 0.00 | 5520.76 | |
| | Infiltration (m ³) | | 163.56 | 113.59 | 0.73 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 140.69 | 191.11 | 170.97 | 157.44 | 938.08 | |
| | Run-Off (m ³) | | 381.64 | 265.04 | 1.69 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 328.27 | 445.92 | 398.94 | 367.36 | 2188.86 | |
| | Development - Impervious Area | Catchment Area (m ²) = 89017.52 | | Imperv coeff. 0.89 | | | | | | | | | | | | |
| | | | | Monthly Volumes | | | | | | | | | | | | |
| | | Evaporation from Imperv. (m ³) - 15% of P. | | 664.96 | 914.65 | 992.10 | 954.71 | 1010.79 | 1042.84 | 994.77 | 815.85 | 1002.78 | 773.12 | 691.67 | 636.92 | 10495.17 |
| | Run-Off from Imperv. (m ³) - with 15% evap. | | 3768.11 | 5183.04 | 5621.90 | 5410.04 | 5727.83 | 5909.43 | 5637.03 | 4623.12 | 5682.43 | 4381.00 | 3919.44 | 3609.22 | 59472.60 | |

NOTES:

- PET and P Taken from Table 1
- Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
- Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
- Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔS) for a given soil type

TABLE 4
POST-DEVELOPMENT WATER BALANCE WITH MITIGATION
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total |
|---|--|---------------------------------|----------|----------|----------|----------|----------|-----------|----------|----------|----------|----------|----------|------------------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - |
| Soil Moisture Storage (mm) | | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| Actual Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 |
| P-AET (mm) | | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 |
| Infiltration Factor | | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| Infiltration (mm) | | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 |
| Run-Off (mm) | | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 |
| Catchment Area (m ²) 55992.83 | | Monthly Volumes | | | | | | | | | | | | |
| AET (m ³) | | 13.79 | 1908.58 | 4147.96 | 5742.35 | 4900.30 | 4373.04 | 4171.47 | 2177.18 | 661.87 | 0.00 | 0.00 | 0.00 | 28096.55 |
| Infiltration (m ³) | | 832.40 | 578.08 | 3.69 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 972.60 | 870.13 | 801.26 | 801.26 | 4774.14 |
| Run-Off (m ³) | | 1942.26 | 1348.85 | 8.61 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1670.66 | 2269.39 | 2030.30 | 1869.60 | 11139.67 |
| Catchment Area (m ²) = 452310.93 | | Monthly Volumes | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | | 3378.76 | 4647.49 | 5041.01 | 4851.03 | 5135.99 | 5298.82 | 5054.57 | 4145.43 | 5095.28 | 3928.32 | 3514.46 | 3236.28 | 53327.46 |
| Run-Off from Imperv. (m ³) - with 15% evap. | | 19146.32 | 26335.80 | 28565.70 | 27489.20 | 29103.95 | 30026.66 | 28642.59 | 23490.77 | 28873.27 | 22260.48 | 19915.25 | 18338.95 | 302188.93 |
| P - Total Precipitation plus irrigation (mm) | | 54.50 | 74.97 | 81.32 | 78.25 | 82.85 | 85.48 | 81.54 | 66.87 | 82.19 | 63.37 | 56.69 | 52.21 | - |
| P-PET (mm) | | 54.26 | 40.88 | 7.24 | -37.15 | -49.86 | -31.88 | 1.29 | 27.99 | 70.37 | 63.37 | 56.69 | 52.21 | - |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -37.15 | -87.01 | -118.89 | -117.60 | -89.61 | -19.24 | 0.00 | 0.00 | 0.00 | - |
| Soil Moisture Storage (mm) | | 75.00 | 75.00 | 75.00 | 37.85 | 0.00 | 0.00 | 1.29 | 29.28 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| Actual Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 104.53 | 90.08 | 78.10 | 74.55 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 506.38 |
| P-AET (mm) | | 54.26 | 40.88 | 7.24 | -26.28 | -7.23 | 7.38 | 6.99 | 27.99 | 70.37 | 63.37 | 56.69 | 52.21 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -26.28 | -33.51 | -26.14 | -19.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 26.28 | 7.23 | -7.38 | -6.99 | -19.15 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 54.26 | 40.88 | 7.24 | 0.00 | 0.00 | 0.00 | 0.00 | 8.84 | 70.37 | 63.37 | 56.69 | 52.21 | 353.85 |
| MOECC Infiltration Factor | | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| Infiltration (mm) | | 16.28 | 12.26 | 2.17 | 0.00 | 0.00 | 0.00 | 0.00 | 2.65 | 21.11 | 19.01 | 17.01 | 15.66 | 106.16 |
| Run-Off (mm) | | 37.98 | 28.62 | 5.07 | 0.00 | 0.00 | 0.00 | 0.00 | 6.19 | 49.26 | 44.36 | 39.68 | 36.54 | 247.70 |
| Catchment Area (m ²) 15030.00 | | Monthly Volumes (Pervious Area) | | | | | | | | | | | | |
| AET (m ³) | | 3.70 | 512.32 | 1113.43 | 1571.11 | 1353.95 | 1173.84 | 1120.48 | 584.42 | 177.67 | 0.00 | 0.00 | 0.00 | 7610.91 |
| Infiltration (m ³) | | 244.65 | 184.34 | 32.63 | 0.00 | 0.00 | 0.00 | 0.00 | 39.85 | 317.31 | 285.73 | 255.63 | 235.39 | 1595.52 |
| Run-Off (m ³) | | 570.84 | 430.13 | 76.14 | 0.00 | 0.00 | 0.00 | 0.00 | 92.98 | 740.38 | 666.70 | 596.46 | 549.25 | 3722.88 |
| Catchment Area (m ²) = 1670.00 | | Monthly Volumes | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | | 12.47 | 17.16 | 18.61 | 17.91 | 18.96 | 19.56 | 18.66 | 15.31 | 18.81 | 14.50 | 12.98 | 11.95 | 196.89 |
| Run-Off Directed to Pervious Area (m ³) | | 70.69 | 97.24 | 105.47 | 101.49 | 107.46 | 110.86 | 105.75 | 86.73 | 106.60 | 82.19 | 73.53 | 67.71 | 1115.73 |

NOTES:

- PET and P Taken from Table 1
- Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
- Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
- Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

TABLE 4
POST-DEVELOPMENT WATER BALANCE WITH MITIGATION
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total |
|--|--|---------------------------------|---------|---------|---------|---------|---------|-----------|---------|----------|----------|---------|----------|----------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - |
| P - Total Precipitation plus irrigation (mm) | | 92.13 | 126.73 | 137.46 | 132.28 | 140.05 | 144.49 | 137.83 | 113.04 | 138.94 | 107.12 | 95.83 | 88.25 | - |
| P-PET (mm) | | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | 88.25 | - |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Soil Moisture Storage (mm) | | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| Actual Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 |
| P-AET (mm) | | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | 88.25 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | 88.25 | 849.27 |
| MOECC Infiltration Factor | | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| Infiltration (mm) | | 27.57 | 27.79 | 19.01 | 5.06 | 2.20 | 8.14 | 17.28 | 22.25 | 38.13 | 32.13 | 28.75 | 26.47 | 254.78 |
| Run-Off (mm) | | 64.32 | 64.85 | 44.36 | 11.81 | 5.14 | 18.99 | 40.31 | 51.91 | 88.98 | 74.98 | 67.08 | 61.77 | 594.49 |
| Catchment Area (m ²) 27400.00 | | Monthly Volumes (Pervious Area) | | | | | | | | | | | | |
| AET (m ³) | | 6.75 | 933.96 | 2029.80 | 3162.17 | 3636.19 | 3215.52 | 2198.62 | 1065.40 | 323.89 | 0.00 | 0.00 | 0.00 | 16572.29 |
| Infiltration (m ³) | | 755.28 | 761.49 | 520.94 | 138.65 | 60.31 | 223.01 | 473.34 | 609.53 | 1044.88 | 880.49 | 787.72 | 725.37 | 6981.01 |
| Run-Off (m ³) | | 1762.33 | 1776.81 | 1215.53 | 323.51 | 140.73 | 520.36 | 1104.45 | 1422.23 | 2438.05 | 2054.47 | 1838.02 | 1692.54 | 16289.03 |
| Mitigation - Connected Pervious Pond Area | | Monthly Volumes | | | | | | | | | | | | |
| Catchment Area (m ²) = 27400.00 | | Imperv coeff. 0.50 | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | | 204.68 | 281.54 | 305.37 | 293.87 | 311.13 | 320.99 | 306.20 | 251.12 | 308.66 | 237.97 | 212.90 | 196.05 | 3230.96 |
| Run-Off Directed to Pervious Area (m ³) | | 1159.84 | 1595.37 | 1730.45 | 1665.24 | 1763.05 | 1818.95 | 1735.11 | 1423.02 | 1749.08 | 1348.49 | 1206.42 | 1110.93 | 18305.94 |
| P - Total Precipitation plus irrigation (mm) | | 92.13 | 126.73 | 137.46 | 132.28 | 140.05 | 144.49 | 137.83 | 113.04 | 138.94 | 107.12 | 95.83 | 88.25 | - |
| P-PET (mm) | | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | 88.25 | - |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Soil Moisture Storage (mm) | | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| Actual Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 |
| P-AET (mm) | | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | 88.25 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | 88.25 | 849.27 |
| MOECC Infiltration Factor | | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| Infiltration (mm) | | 27.57 | 27.79 | 19.01 | 5.06 | 2.20 | 8.14 | 17.28 | 22.25 | 38.13 | 32.13 | 28.75 | 26.47 | 254.78 |
| Run-Off (mm) | | 64.32 | 64.85 | 44.36 | 11.81 | 5.14 | 18.99 | 40.31 | 51.91 | 88.98 | 74.98 | 67.08 | 61.77 | 594.49 |
| Catchment Area (m ²) 23850.00 | | Monthly Volumes (Pervious Area) | | | | | | | | | | | | |
| AET (m ³) | | 5.87 | 812.96 | 1766.81 | 2752.47 | 3165.08 | 2798.91 | 1913.76 | 927.37 | 281.92 | 0.00 | 0.00 | 0.00 | 14425.15 |
| Infiltration (m ³) | | 657.43 | 662.83 | 453.45 | 120.69 | 52.50 | 194.12 | 412.01 | 530.56 | 909.50 | 766.41 | 685.66 | 631.39 | 6076.54 |
| Run-Off (m ³) | | 1534.00 | 1546.60 | 1058.04 | 281.60 | 122.50 | 452.94 | 961.36 | 1237.96 | 2122.17 | 1788.28 | 1599.88 | 1473.25 | 14178.59 |
| Mitigation - Connected Impervious Roof Area | | Monthly Volumes | | | | | | | | | | | | |
| Catchment Area (m ²) = 23850.00 | | Imperv coeff. 0.50 | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | | 178.16 | 245.06 | 265.81 | 255.79 | 270.82 | 279.40 | 266.52 | 218.59 | 268.67 | 207.14 | 185.31 | 170.65 | 2811.92 |
| Run-Off Directed to Pervious Area (m ³) | | 1009.57 | 1388.67 | 1506.25 | 1449.48 | 1534.63 | 1583.28 | 1510.30 | 1238.65 | 1522.46 | 1173.78 | 1050.12 | 967.00 | 15934.19 |

NOTES:

- PET and P Taken from Table 1
- Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
- Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
- Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (Δ ST) for a given soil type

TABLE 4
POST-DEVELOPMENT WATER BALANCE WITH MITIGATION
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total | | |
|---|---|---|--------------------|---------|---------|---------|---------|-----------|---------|----------|----------|---------|----------|---------|-----------------|--------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | | | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 | | |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 | | |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 | | |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - | | |
| Catchment 104 (continued) | Mitigation - Impervious Park Area to Silva Cells | Catchment Area (m ²) = 27670.00 | Imperv coeff. 0.65 | | | | | | | | | | | | Monthly Volumes | |
| | | Evaporation from Imperv. (m ³) - 15% of P. | 206.69 | 284.31 | 308.38 | 296.76 | 314.19 | 324.15 | 309.21 | 253.60 | 311.70 | 240.31 | 215.00 | 197.98 | 3262.29 | |
| | | Run-Off Directed to Pervious Area (m ³) | 1171.27 | 1611.09 | 1747.50 | 1681.64 | 1780.43 | 1836.87 | 1752.20 | 1437.04 | 1766.31 | 1361.78 | 1218.31 | 1121.88 | 18486.33 | |
| | | Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | 1171.27 | 1611.09 | 1747.50 | 1681.64 | 1780.43 | 1836.87 | 1752.20 | 1437.04 | 1766.31 | 1361.78 | 1218.31 | 1121.88 | 18486.33 | |
| | | Run-Off (m ³) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| | | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 0.00 | 501.79 |
| | | P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 47.70 | - |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 47.70 | 284.21 | |
| | Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - | |
| | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - | |
| | Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 14.31 | 85.26 | |
| | Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 33.39 | 198.95 | |
| | Catchment Area (m ²) 28530.00 | | Monthly Volumes | | | | | | | | | | | | | |
| | AET (m ³) | 7.02 | 972.48 | 2113.51 | 2925.90 | 2496.85 | 2228.19 | 2125.49 | 1109.34 | 337.24 | 0.00 | 0.00 | 0.00 | 0.00 | 14316.02 | |
| | Infiltration (m ³) | 424.13 | 294.55 | 1.88 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 364.82 | 495.57 | 443.36 | 408.26 | 408.26 | 2432.57 | |
| | Run-Off (m ³) | 989.64 | 687.28 | 4.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 851.25 | 1156.32 | 1034.50 | 952.62 | 952.62 | 5675.99 | |
| | Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | 989.64 | 687.28 | 4.39 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 851.25 | 1156.32 | 1034.50 | 952.62 | 952.62 | 5675.99 | |
| | Run-Off (m ³) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | Catchment Area (m ²) 15520.00 | | Imperv coeff. 0.80 | | | | | | | | | | | | Monthly Volumes | |
| | Evaporation from Imperv. (m ³) - 15% of P. | 115.93 | 159.47 | 172.97 | 166.45 | 176.23 | 181.82 | 173.44 | 142.24 | 174.83 | 134.79 | 120.59 | 111.05 | 111.05 | 1829.81 | |
| | Run-Off Directed to Pervious Area (m ³) | 656.96 | 903.65 | 980.17 | 943.23 | 998.63 | 1030.30 | 982.80 | 806.03 | 990.72 | 763.82 | 683.35 | 629.26 | 629.26 | 10368.91 | |
| | Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | 656.96 | 903.65 | 980.17 | 943.23 | 998.63 | 1030.30 | 982.80 | 806.03 | 990.72 | 763.82 | 683.35 | 629.26 | 629.26 | 10368.91 | |
| | Run-Off (m ³) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | - | |
| | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 0.00 | 501.79 | |
| | P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 47.70 | - | |
| | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | |
| | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - | |
| | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 47.70 | 284.21 | |
| | Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - | |
| | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - | |
| | Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 14.31 | 85.26 | |
| | Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 33.39 | 198.95 | |
| | Catchment Area (m ²) 3880.00 | | Monthly Volumes | | | | | | | | | | | | | |
| | AET (m ³) | 0.96 | 132.25 | 287.43 | 397.91 | 339.56 | 303.03 | 289.06 | 150.87 | 45.86 | 0.00 | 0.00 | 0.00 | 0.00 | 1946.94 | |
| | Infiltration (m ³) | 57.68 | 40.06 | 0.26 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 49.61 | 67.40 | 60.30 | 55.52 | 55.52 | 330.82 | |
| | Run-Off (m ³) | 134.59 | 93.47 | 0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 115.77 | 157.26 | 140.69 | 129.55 | 129.55 | 771.92 | |
| Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | 134.59 | 93.47 | 0.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 115.77 | 157.26 | 140.69 | 129.55 | 129.55 | 771.92 | | |
| Run-Off (m ³) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |

NOTES:

- PET and P Taken from Table 1
- Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
- Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
- Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

TABLE 4
POST-DEVELOPMENT WATER BALANCE WITH MITIGATION
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total | |
|--|---|--------------------------------------|---------------------------------|-----------------|----------|----------|----------|-----------|----------|----------|----------|---------|-----------------|------------------|-----------------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 | |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 | |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 | |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - | |
| Catchment 105 | Development - Unconnected Pervious Landscape | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | - | |
| | | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 |
| | | P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - |
| | | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 |
| | | Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| | | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| | | Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 |
| | | Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 |
| | | Catchment Area (m ²) | 39952.96 | Monthly Volumes | | | | | | | | | | | |
| | | AET (m ³) | 9.84 | 1361.84 | 2959.72 | 4097.38 | 3496.55 | 3120.33 | 2976.50 | 1553.50 | 472.27 | 0.00 | 0.00 | 0.00 | 20047.93 |
| | | Infiltration (m ³) | 593.95 | 412.48 | 2.63 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 510.89 | 693.98 | 620.87 | 571.73 | 3406.53 |
| | | Run-Off (m ³) | 1385.87 | 962.45 | 6.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1192.08 | 1619.29 | 1448.69 | 1334.03 | 7948.57 |
| | Catchment Area (m ²) | 194074.71 | Monthly Volumes | | | | | | | | | | | | |
| | Evaporation from Imperv. (m ³) - 15% of P. | 1449.74 | 1994.12 | 2162.96 | 2081.45 | 2203.72 | 2273.59 | 2168.78 | 1778.69 | 2186.25 | 1685.54 | 1507.96 | 1388.60 | 22881.41 | |
| | Run-Off from Imperv. (m ³) - with 15% evap. | 8215.18 | 11300.00 | 12256.79 | 11794.89 | 12487.74 | 12883.65 | 12289.78 | 10079.27 | 12388.76 | 9551.39 | 8545.11 | 7868.76 | 129661.31 | |
| | P - Total Precipitation plus irrigation (mm) | 54.50 | 74.97 | 81.32 | 78.25 | 82.85 | 85.48 | 81.54 | 66.87 | 82.19 | 63.37 | 56.69 | 52.21 | - | |
| | P-PET (mm) | 54.26 | 40.88 | 7.24 | -37.15 | -49.86 | -31.88 | 1.29 | 27.99 | 70.37 | 63.37 | 56.69 | 52.21 | - | |
| | Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -37.15 | -87.01 | -118.89 | -117.60 | -89.61 | -19.24 | 0.00 | 0.00 | 0.00 | - | |
| | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 37.85 | 0.00 | 0.00 | 1.29 | 29.28 | 75.00 | 75.00 | 75.00 | 75.00 | - | |
| | Actual Potential Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 104.53 | 90.08 | 78.10 | 74.55 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 506.38 | |
| | P-AET (mm) | 54.26 | 40.88 | 7.24 | -26.28 | -7.23 | 7.38 | 6.99 | 27.99 | 70.37 | 63.37 | 56.69 | 52.21 | - | |
| | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -26.28 | -33.51 | -26.14 | -19.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | |
| | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 26.28 | 7.23 | -7.38 | -6.99 | -19.15 | 0.00 | 0.00 | 0.00 | 0.00 | - | |
| | Precipitation Surplus (mm) | 54.26 | 40.88 | 7.24 | 0.00 | 0.00 | 0.00 | 0.00 | 8.84 | 70.37 | 63.37 | 56.69 | 52.21 | 353.85 | |
| | MOECC Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - | |
| | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - | |
| | Infiltration (mm) | 16.28 | 12.26 | 2.17 | 0.00 | 0.00 | 0.00 | 0.00 | 2.65 | 21.11 | 19.01 | 17.01 | 15.66 | 106.16 | |
| | Run-Off (mm) | 37.98 | 28.62 | 5.07 | 0.00 | 0.00 | 0.00 | 0.00 | 6.19 | 49.26 | 44.36 | 39.68 | 36.54 | 247.70 | |
| | Catchment Area (m ²) | 67770.00 | Monthly Volumes (Pervious Area) | | | | | | | | | | | | |
| | AET (m ³) | 16.69 | 2310.02 | 5020.42 | 7084.12 | 6104.93 | 5292.84 | 5052.22 | 2635.12 | 801.09 | 0.00 | 0.00 | 0.00 | 34317.44 | |
| | Infiltration (m ³) | 1103.10 | 831.20 | 147.14 | 0.00 | 0.00 | 0.00 | 0.00 | 179.67 | 1430.73 | 1288.34 | 1152.61 | 1061.38 | 7194.17 | |
| Run-Off (m ³) | 2573.90 | 1939.46 | 343.32 | 0.00 | 0.00 | 0.00 | 0.00 | 419.23 | 3338.38 | 3006.13 | 2689.42 | 2476.55 | 16786.40 | | |
| Catchment Area (m ²) | 7530.00 | Monthly Volumes | | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | 56.25 | 77.37 | 83.92 | 80.76 | 85.50 | 88.21 | 84.15 | 69.01 | 84.83 | 65.40 | 58.51 | 53.88 | 887.79 | | |
| Run-Off Directed to Pervious Area (m ³) | 318.74 | 438.43 | 475.56 | 457.64 | 484.52 | 499.88 | 476.84 | 391.07 | 480.68 | 370.59 | 331.55 | 305.30 | 5030.79 | | |

NOTES:

- PET and P Taken from Table 1
- Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
- Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
- Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

TABLE 4
POST-DEVELOPMENT WATER BALANCE WITH MITIGATION
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total | | |
|---|--|--|------------------------------------|--------|--------|---------|---------|-----------|---------|----------|----------|---------|----------|---------|---------|---------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | | | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 | | |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 | | |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 | | |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - | | |
| Catchment 105 (continued) | Mitigation - Connected Pervious Pond Area | P - Total Precipitation plus irrigation (mm) | 92.13 | 126.73 | 137.46 | 132.28 | 140.05 | 144.49 | 137.83 | 113.04 | 138.94 | 107.12 | 95.83 | 88.25 | - | |
| | | P-PET (mm) | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | 88.25 | - | |
| | | Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| | | Actual Potential Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 | |
| | | P-AET (mm) | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | 88.25 | - | |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | | Precipitation Surplus (mm) | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | 88.25 | 88.25 | 849.27 |
| | | MOECC Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| | | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| | | Infiltration (mm) | 27.57 | 27.79 | 19.01 | 5.06 | 2.20 | 8.14 | 17.28 | 22.25 | 38.13 | 32.13 | 28.75 | 26.47 | 26.47 | 254.78 |
| | | Run-Off (mm) | 64.32 | 64.85 | 44.36 | 11.81 | 5.14 | 18.99 | 40.31 | 51.91 | 88.98 | 74.98 | 67.08 | 61.77 | 61.77 | 594.49 |
| | | Catchment Area (m ²) 10700.00 | Monthly Volumes (Pervious Area) | | | | | | | | | | | | | |
| | | AET (m ³) | 2.63 | 364.72 | 792.66 | 1234.86 | 1419.97 | 1255.70 | 858.58 | 416.05 | 126.48 | 0.00 | 0.00 | 0.00 | 0.00 | 6471.66 |
| | Infiltration (m ³) | 294.95 | 297.37 | 203.43 | 54.14 | 23.55 | 87.09 | 184.84 | 238.03 | 408.04 | 343.84 | 307.61 | 283.27 | 283.27 | 2726.16 | |
| | Run-Off (m ³) | 688.21 | 693.86 | 474.68 | 126.34 | 54.96 | 203.20 | 431.30 | 555.40 | 952.09 | 802.29 | 717.77 | 660.96 | 660.96 | 6361.05 | |
| | Mitigation - Connected Impervious Pond Area | Catchment Area (m ²) = 10700.00 | Imperv coeff. 0.50 Monthly Volumes | | | | | | | | | | | | | |
| | | Evaporation from Imperv. (m ³) - 15% of P. | 79.93 | 109.94 | 119.25 | 114.76 | 121.50 | 125.35 | 119.57 | 98.07 | 120.54 | 92.93 | 83.14 | 76.56 | 76.56 | 1261.53 |
| | | Run-Off Directed to Pervious Area (m ³) | 452.93 | 623.01 | 675.76 | 650.29 | 688.49 | 710.32 | 677.58 | 555.70 | 683.03 | 526.60 | 471.12 | 433.83 | 433.83 | 7148.67 |
| | | P - Total Precipitation plus irrigation (mm) | 92.13 | 126.73 | 137.46 | 132.28 | 140.05 | 144.49 | 137.83 | 113.04 | 138.94 | 107.12 | 95.83 | 88.25 | 88.25 | - |
| | | P-PET (mm) | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | 88.25 | 88.25 | - |
| | | Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| | | Actual Potential Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 0.00 | 604.83 |
| | | P-AET (mm) | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | 88.25 | 88.25 | - |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | | Precipitation Surplus (mm) | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | 88.25 | 88.25 | 849.27 |
| | | MOECC Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - | |
| Infiltration (mm) | | 27.57 | 27.79 | 19.01 | 5.06 | 2.20 | 8.14 | 17.28 | 22.25 | 38.13 | 32.13 | 28.75 | 26.47 | 26.47 | 254.78 | |
| Run-Off (mm) | 64.32 | 64.85 | 44.36 | 11.81 | 5.14 | 18.99 | 40.31 | 51.91 | 88.98 | 74.98 | 67.08 | 61.77 | 61.77 | 594.49 | | |
| Catchment Area (m ²) 4250.00 | Monthly Volumes (Pervious Area) | | | | | | | | | | | | | | | |
| AET (m ³) | 1.05 | 144.87 | 314.84 | 490.48 | 564.01 | 498.76 | 341.03 | 165.25 | 50.24 | 0.00 | 0.00 | 0.00 | 0.00 | 2570.52 | | |
| Infiltration (m ³) | 117.15 | 118.11 | 80.80 | 21.51 | 9.36 | 34.59 | 73.42 | 94.54 | 162.07 | 136.57 | 122.18 | 112.51 | 112.51 | 1082.82 | | |
| Run-Off (m ³) | 273.35 | 275.60 | 188.54 | 50.18 | 21.83 | 80.71 | 171.31 | 220.60 | 378.17 | 318.67 | 285.09 | 262.53 | 262.53 | 2526.58 | | |
| Mitigation - Connected Impervious Roof Area | Catchment Area (m ²) = 4250.00 | Monthly Volumes | | | | | | | | | | | | | | |
| | Evaporation from Imperv. (m ³) - 15% of P. | 31.75 | 43.67 | 47.37 | 45.58 | 48.26 | 49.79 | 47.49 | 38.95 | 47.88 | 36.91 | 33.02 | 30.41 | 30.41 | 501.08 | |
| | Run-Off Directed to Pervious Area (m ³) | 179.90 | 247.46 | 268.41 | 258.29 | 273.47 | 282.14 | 269.13 | 220.72 | 271.30 | 209.16 | 187.13 | 172.32 | 172.32 | 2839.43 | |

NOTES:

- PET and P Taken from Table 1
- Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
- Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
- Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

TABLE 4
POST-DEVELOPMENT WATER BALANCE WITH MITIGATION
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total | |
|---|---|---|-----------------|--------|--------|---------|---------|-----------|---------|----------|----------|---------|----------------|---------------|---------------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 | |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 | |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 | |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - | |
| Catchment 105 (continued) | Mitigation - Pervious Park Area to Silva Cells | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | - | |
| | | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 |
| | | P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - |
| | | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 |
| | | Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| | | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| | | Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 |
| | | Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 |
| | | Catchment Area (m ²) 285.00 | Monthly Volumes | | | | | | | | | | | | |
| | | AET (m ³) | 0.07 | 9.71 | 21.11 | 29.23 | 24.94 | 22.26 | 21.23 | 11.08 | 3.37 | 0.00 | 0.00 | 0.00 | 143.01 |
| | Infiltration (m ³) | 4.24 | 2.94 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.64 | 4.95 | 4.43 | 4.08 | 24.30 | |
| | Run-Off (m ³) | 9.89 | 6.87 | 0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 8.50 | 11.55 | 10.33 | 9.52 | 56.70 | |
| | Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | 9.89 | 6.87 | 0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 8.50 | 11.55 | 10.33 | 9.52 | 56.70 | |
| | Run-Off (m ³) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | Catchment Area (m ²) = 615.00 | Imperv coeff. 0.65 | Monthly Volumes | | | | | | | | | | | | |
| | Evaporation from Imperv. (m ³) - 15% of P. | 4.59 | 6.32 | 6.85 | 6.60 | 6.98 | 7.20 | 6.87 | 5.64 | 6.93 | 5.34 | 4.78 | 4.40 | 72.51 | |
| | Run-Off Directed to Pervious Area (m ³) | 26.03 | 35.81 | 38.84 | 37.38 | 39.57 | 40.83 | 38.94 | 31.94 | 39.26 | 30.27 | 27.08 | 24.94 | 410.88 | |
| | Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | 26.03 | 35.81 | 38.84 | 37.38 | 39.57 | 40.83 | 38.94 | 31.94 | 39.26 | 30.27 | 27.08 | 24.94 | 410.88 | |
| | Run-Off (m ³) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - | |
| | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 | |
| | P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - | |
| | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - | |
| | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - | |
| | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 | |
| | Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - | |
| | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - | |
| | Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 | |
| Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 | | |
| Catchment Area (m ²) 640.00 | Monthly Volumes | | | | | | | | | | | | | | |
| AET (m ³) | 0.16 | 21.82 | 47.41 | 65.64 | 56.01 | 49.98 | 47.68 | 24.89 | 7.57 | 0.00 | 0.00 | 0.00 | 321.14 | | |
| Infiltration (m ³) | 9.51 | 6.61 | 0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 8.18 | 11.12 | 9.95 | 9.16 | 54.57 | | |
| Run-Off (m ³) | 22.20 | 15.42 | 0.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 19.10 | 25.94 | 23.21 | 21.37 | 127.33 | | |
| Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | 22.20 | 15.42 | 0.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 19.10 | 25.94 | 23.21 | 21.37 | 127.33 | | |
| Run-Off (m ³) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| Catchment Area (m ²) = 2560.00 | Imperv coeff. 0.80 | Monthly Volumes | | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | 19.12 | 26.30 | 28.53 | 27.46 | 29.07 | 29.99 | 28.61 | 23.46 | 28.84 | 22.23 | 19.89 | 18.32 | 301.82 | | |
| Run-Off Directed to Pervious Area (m ³) | 108.36 | 149.06 | 161.68 | 155.58 | 164.72 | 169.95 | 162.11 | 132.95 | 163.42 | 125.99 | 112.72 | 103.80 | 1710.34 | | |
| Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | 108.36 | 149.06 | 161.68 | 155.58 | 164.72 | 169.95 | 162.11 | 132.95 | 163.42 | 125.99 | 112.72 | 103.80 | 1710.34 | | |
| Run-Off (m ³) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |

- NOTES:
1) PET and P Taken from Table 1
2) Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
3) Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
4) Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

TABLE 4
POST-DEVELOPMENT WATER BALANCE WITH MITIGATION
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total |
|---|--|---------------------------------|----------|----------|----------|----------|----------|-----------|----------|----------|----------|---------|----------|------------------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - |
| Soil Moisture Storage (mm) | | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| Actual Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 |
| P-AET (mm) | | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 |
| Infiltration Factor | | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| Infiltration (mm) | | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 |
| Run-Off (mm) | | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 |
| Catchment Area (m ²) 56130.34 | | Monthly Volumes | | | | | | | | | | | | |
| AET (m ³) | | 13.82 | 1913.27 | 4158.15 | 5756.45 | 4912.34 | 4383.78 | 4181.71 | 2182.53 | 663.50 | 0.00 | 0.00 | 0.00 | 28165.55 |
| Infiltration (m ³) | | 834.44 | 579.50 | 3.70 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 717.75 | 974.98 | 872.27 | 803.23 | 4785.87 |
| Run-Off (m ³) | | 1947.03 | 1352.16 | 8.64 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1674.76 | 2274.96 | 2035.29 | 1874.19 | 11167.02 |
| Catchment Area (m ²) = 209771.19 | | Monthly Volumes | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | | 1566.99 | 2155.40 | 2337.90 | 2249.80 | 2381.95 | 2457.47 | 2344.19 | 1922.55 | 2363.07 | 1821.86 | 1629.92 | 1500.91 | 24732.02 |
| Run-Off from Imperv. (m ³) - with 15% evap. | | 8879.61 | 12213.93 | 13248.10 | 12748.84 | 13497.73 | 13925.66 | 13283.76 | 10894.47 | 13390.74 | 10323.89 | 9236.23 | 8505.17 | 140148.13 |
| P - Total Precipitation plus irrigation (mm) | | 54.50 | 74.97 | 81.32 | 78.25 | 82.85 | 85.48 | 81.54 | 66.87 | 82.19 | 63.37 | 56.69 | 52.21 | - |
| P-PET (mm) | | 54.26 | 40.88 | 7.24 | -37.15 | -49.86 | -31.88 | 1.29 | 27.99 | 70.37 | 63.37 | 56.69 | 52.21 | - |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -37.15 | -87.01 | -118.89 | -117.60 | -89.61 | -19.24 | 0.00 | 0.00 | 0.00 | - |
| Soil Moisture Storage (mm) | | 75.00 | 75.00 | 75.00 | 37.85 | 0.00 | 0.00 | 1.29 | 29.28 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| Actual Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 104.53 | 90.08 | 78.10 | 74.55 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 506.38 |
| P-AET (mm) | | 54.26 | 40.88 | 7.24 | -26.28 | -7.23 | 7.38 | 6.99 | 27.99 | 70.37 | 63.37 | 56.69 | 52.21 | - |
| Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -26.28 | -33.51 | -26.14 | -19.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 26.28 | 7.23 | -7.38 | -6.99 | -19.15 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| Precipitation Surplus (mm) | | 54.26 | 40.88 | 7.24 | 0.00 | 0.00 | 0.00 | 0.00 | 8.84 | 70.37 | 63.37 | 56.69 | 52.21 | 353.85 |
| MOECC Infiltration Factor | | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| Infiltration (mm) | | 16.28 | 12.26 | 2.17 | 0.00 | 0.00 | 0.00 | 0.00 | 2.65 | 21.11 | 19.01 | 17.01 | 15.66 | 106.16 |
| Run-Off (mm) | | 37.98 | 28.62 | 5.07 | 0.00 | 0.00 | 0.00 | 0.00 | 6.19 | 49.26 | 44.36 | 39.68 | 36.54 | 247.70 |
| Catchment Area (m ²) 3420.00 | | Monthly Volumes (Pervious Area) | | | | | | | | | | | | |
| AET (m ³) | | 0.84 | 116.57 | 253.35 | 357.50 | 308.08 | 267.10 | 254.96 | 132.98 | 40.43 | 0.00 | 0.00 | 0.00 | 1731.82 |
| Infiltration (m ³) | | 55.67 | 41.95 | 7.43 | 0.00 | 0.00 | 0.00 | 0.00 | 9.07 | 72.20 | 65.02 | 58.17 | 53.56 | 363.05 |
| Run-Off (m ³) | | 129.89 | 97.87 | 17.33 | 0.00 | 0.00 | 0.00 | 0.00 | 21.16 | 168.47 | 151.70 | 135.72 | 124.98 | 847.12 |
| Catchment Area (m ²) = 380.00 | | Monthly Volumes | | | | | | | | | | | | |
| Evaporation from Imperv. (m ³) - 15% of P. | | 2.84 | 3.90 | 4.24 | 4.08 | 4.31 | 4.45 | 4.25 | 3.48 | 4.28 | 3.30 | 2.95 | 2.72 | 44.80 |
| Run-Off Directed to Pervious Area (m ³) | | 16.09 | 22.13 | 24.00 | 23.09 | 24.45 | 25.23 | 24.06 | 19.74 | 24.26 | 18.70 | 16.73 | 15.41 | 253.88 |

NOTES:

- PET and P Taken from Table 1
- Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
- Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
- Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

TABLE 4
POST-DEVELOPMENT WATER BALANCE WITH MITIGATION
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total | | |
|---|---|--|-----------------|---------------------------------|---------|---------|---------|-----------|---------|----------|----------|---------|----------|---------|----------|--------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | | | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 | | |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 | | |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 | | |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - | | |
| Catchment 106 (continued) | Mitigation - Pervious ROW Area to Silva Cells | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 31.09 | 0.00 | 0.00 | 0.00 | 22.22 | 75.00 | 75.00 | 75.00 | 75.00 | - | |
| | | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 102.56 | 87.52 | 78.10 | 74.50 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 501.79 | |
| | | P-AET (mm) | 49.55 | 34.41 | 0.22 | -31.06 | -11.82 | 0.00 | 0.00 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - | |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | -31.06 | -42.87 | -42.87 | -42.87 | -20.66 | 0.00 | 0.00 | 0.00 | 0.00 | - | |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 31.06 | 11.82 | 0.00 | 0.00 | -22.22 | -20.66 | 0.00 | 0.00 | 0.00 | - | |
| | | Precipitation Surplus (mm) | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 42.62 | 57.90 | 51.80 | 47.70 | 284.21 | |
| | | Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| | | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| | | Infiltration (mm) | 14.87 | 10.32 | 0.07 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 12.79 | 17.37 | 15.54 | 14.31 | 85.26 | |
| | | Run-Off (mm) | 34.69 | 24.09 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 29.84 | 40.53 | 36.26 | 33.39 | 198.95 | |
| | Catchment Area (m ²) 2160.00 | | Monthly Volumes | | | | | | | | | | | | | |
| | AET (m ³) | 0.53 | 73.63 | 160.01 | 221.52 | 189.04 | 168.70 | 160.92 | 83.99 | 25.53 | 0.00 | 0.00 | 0.00 | 1083.86 | | |
| | Infiltration (m ³) | 32.11 | 22.30 | 0.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 27.62 | 37.52 | 33.57 | 30.91 | 184.17 | | |
| | Run-Off (m ³) | 74.93 | 52.03 | 0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 64.45 | 87.54 | 78.32 | 72.12 | 429.73 | | |
| | Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | 74.93 | 52.03 | 0.33 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 64.45 | 87.54 | 78.32 | 72.12 | 429.73 | | |
| | Run-Off (m ³) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| | Catchment Area (m ²) = 8640.00 | | Monthly Volumes | | | | | | | | | | | | | |
| | Imperv coeff. 0.80 | | | | | | | | | | | | | | | |
| | Evaporation from Imperv. (m ³) - 15% of P. | | 64.54 | 88.78 | 96.29 | 92.66 | 98.11 | 101.22 | 96.55 | 79.19 | 97.33 | 75.04 | 67.13 | 61.82 | 1018.66 | |
| | Run-Off Directed to Pervious Area (m ³) | | 365.73 | 503.06 | 545.66 | 525.10 | 555.94 | 573.57 | 547.13 | 448.72 | 551.53 | 425.22 | 380.42 | 350.31 | 5772.38 | |
| Infiltration via Silva Cells (Sized for 25mm capture) (m ³) | | 365.73 | 503.06 | 545.66 | 525.10 | 555.94 | 573.57 | 547.13 | 448.72 | 551.53 | 425.22 | 380.42 | 350.31 | 5772.38 | | |
| Run-Off (m ³) | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| Channels | Mitigation - Impervious ROW Area to Silva Cells | Catchment Area (m ²) = 2951.01 | | Monthly Volumes | | | | | | | | | | | | |
| | | Imperv coeff. 0.10 | | | | | | | | | | | | | | |
| | | Evaporation from Imperv. (m ³) - 15% of P. | | 22.04 | 30.32 | 32.89 | 31.65 | 33.51 | 34.57 | 32.98 | 27.05 | 33.24 | 25.63 | 22.93 | 21.11 | 347.92 |
| | Run-Off Directed to Pervious Area (m ³) | | 124.92 | 171.82 | 186.37 | 179.35 | 189.88 | 195.90 | 186.87 | 153.26 | 188.38 | 145.23 | 129.93 | 119.65 | 1971.57 | |
| | Mitigation - Connected Pervious Area | P - Total Precipitation plus irrigation (mm) | | 54.50 | 74.97 | 81.32 | 78.25 | 82.85 | 85.48 | 81.54 | 66.87 | 82.19 | 63.37 | 56.69 | 52.21 | - |
| | | P-PET (mm) | | 54.26 | 40.88 | 7.24 | -37.15 | -49.86 | -31.88 | 1.29 | 27.99 | 70.37 | 63.37 | 56.69 | 52.21 | - |
| | | Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -37.15 | -87.01 | -118.89 | -117.60 | -89.61 | -19.24 | 0.00 | 0.00 | 0.00 | - |
| | | Soil Moisture Storage (mm) | | 75.00 | 75.00 | 75.00 | 37.85 | 0.00 | 0.00 | 1.29 | 29.28 | 75.00 | 75.00 | 75.00 | 75.00 | - |
| | | Actual Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 104.53 | 90.08 | 78.10 | 74.55 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 506.38 |
| | | P-AET (mm) | | 54.26 | 40.88 | 7.24 | -26.28 | -7.23 | 7.38 | 6.99 | 27.99 | 70.37 | 63.37 | 56.69 | 52.21 | - |
| | | Actual Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -26.28 | -33.51 | -26.14 | -19.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | | Change in Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | 26.28 | 7.23 | -7.38 | -6.99 | -19.15 | 0.00 | 0.00 | 0.00 | 0.00 | - |
| | | Precipitation Surplus (mm) | | 54.26 | 40.88 | 7.24 | 0.00 | 0.00 | 0.00 | 0.00 | 8.84 | 70.37 | 63.37 | 56.69 | 52.21 | 353.85 |
| | | MOECC Infiltration Factor | | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | - |
| | | Run-Off Coefficient | | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | - |
| | | Infiltration (mm) | | 16.28 | 12.26 | 2.17 | 0.00 | 0.00 | 0.00 | 0.00 | 2.65 | 21.11 | 19.01 | 17.01 | 15.66 | 106.16 |
| | | Run-Off (mm) | | 37.98 | 28.62 | 5.07 | 0.00 | 0.00 | 0.00 | 0.00 | 6.19 | 49.26 | 44.36 | 39.68 | 36.54 | 247.70 |
| | | Catchment Area (m ²) 26559.05 | | Monthly Volumes (Pervious Area) | | | | | | | | | | | | |
| | | AET (m ³) | 6.54 | 905.30 | 1967.50 | 2776.27 | 2392.52 | 2074.26 | 1979.97 | 1032.70 | 313.95 | 0.00 | 0.00 | 0.00 | 13449.00 | |
| Infiltration (m ³) | | 432.31 | 325.75 | 57.66 | 0.00 | 0.00 | 0.00 | 0.00 | 70.41 | 560.70 | 504.90 | 451.71 | 415.95 | 2819.39 | | |
| Run-Off (m ³) | 1008.71 | 760.07 | 134.55 | 0.00 | 0.00 | 0.00 | 0.00 | 164.30 | 1308.31 | 1178.10 | 1053.98 | 970.56 | 6578.59 | | | |

NOTES:

- PET and P Taken from Table 1
- Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
- Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
- Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

TABLE 4
POST-DEVELOPMENT WATER BALANCE WITH MITIGATION
CALDON STATION

| Catchments and Hydrologic Components | | Month | | | | | | | | | | | | Total | | | |
|--|--|---|---|-----------------|----------|----------|----------|-----------|----------|----------|----------|----------|----------|-----------|----------|----------|--------|
| | | March | April | May | June | July | August | September | October | November | December | January | February | | | | |
| PET - Adjusted Potential Evapotranspiration (mm) | | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | 0.00 | 604.83 | | | |
| P - Total Precipitation (mm) | | 49.80 | 68.50 | 74.30 | 71.50 | 75.70 | 78.10 | 74.50 | 61.10 | 75.10 | 57.90 | 51.80 | 47.70 | 786.00 | | | |
| P-PET (mm) | | 49.55 | 34.41 | 0.22 | -43.91 | -57.01 | -39.25 | -5.74 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | 181.17 | | | |
| Soil Moisture Deficit (mm) | | 0.00 | 0.00 | 0.00 | -43.91 | -100.92 | -140.17 | -145.91 | -123.69 | -60.42 | -2.52 | 0.00 | 0.00 | - | | | |
| Ponds | Mitigation - Connected Impervious Area | Catchment Area (m ²) = 18845.25 | | | | | | | | | | | | Total | | | |
| | | Imperv coeff. 0.50 | | | | | | | | | | | | | | | |
| | | Monthly Volumes | | | | | | | | | | | | | | | |
| | | Evaporation from Imperv. (m ³) - 15% of P. | 140.77 | 193.63 | 210.03 | 202.12 | 213.99 | 220.77 | 210.60 | 172.72 | 212.29 | 163.67 | 146.43 | | 134.84 | 2221.85 | |
| | | Run-Off from Imperv. (m ³) - with 15% evap. | 797.72 | 1097.26 | 1190.17 | 1145.32 | 1212.60 | 1251.04 | 1193.38 | 978.73 | 1202.99 | 927.47 | 829.76 | | 764.08 | 12590.51 | |
| | | P - Total Precipitation plus irrigation (mm) | 92.13 | 126.73 | 137.46 | 132.28 | 140.05 | 144.49 | 137.83 | 113.04 | 138.94 | 107.12 | 95.83 | | 88.25 | - | |
| | | P-PET (mm) | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | | 88.25 | - | |
| | | Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | 0.00 | - | |
| | | Soil Moisture Storage (mm) | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | 75.00 | | 75.00 | - | |
| | | Actual Potential Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 115.41 | 132.71 | 117.35 | 80.24 | 38.88 | 11.82 | 0.00 | 0.00 | | 0.00 | 604.83 | |
| | | P-AET (mm) | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | | 88.25 | - | |
| | | Actual Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | 0.00 | - | |
| | | Change in Soil Moisture Deficit (mm) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | 0.00 | - | |
| | | Precipitation Surplus (mm) | 91.88 | 92.64 | 63.37 | 16.87 | 7.34 | 27.13 | 57.58 | 74.15 | 127.11 | 107.12 | 95.83 | | 88.25 | 849.27 | |
| | | MOECC Infiltration Factor | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | | 0.30 | - | |
| | | Run-Off Coefficient | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | | 0.70 | - | |
| | | Infiltration (mm) | 27.57 | 27.79 | 19.01 | 5.06 | 2.20 | 8.14 | 17.28 | 22.25 | 38.13 | 32.13 | 28.75 | | 26.47 | 254.78 | |
| | | Run-Off (mm) | 64.32 | 64.85 | 44.36 | 11.81 | 5.14 | 18.99 | 40.31 | 51.91 | 88.98 | 74.98 | 67.08 | | 61.77 | 594.49 | |
| | | Catchment Area (m ²) 18845.25 | Monthly Volumes (Pervious Area) | | | | | | | | | | | | | | |
| | | AET (m ³) | 4.64 | 642.36 | 1396.06 | 2174.89 | 2500.91 | 2211.58 | 1512.17 | 732.76 | 222.76 | 0.00 | 0.00 | | 0.00 | 11398.14 | |
| | | Infiltration (m ³) | 519.47 | 523.74 | 358.29 | 95.36 | 41.48 | 153.38 | 325.55 | 419.22 | 718.65 | 605.58 | 541.78 | | 498.90 | 4801.42 | |
| | | Run-Off (m ³) | 1212.10 | 1222.06 | 836.02 | 222.51 | 96.79 | 357.89 | 759.62 | 978.19 | 1676.85 | 1413.03 | 1264.16 | | 1164.10 | 11203.31 | |
| | NHS | Development - Pervious Landscape | Soil Moisture Storage (mm) | 200.00 | 200.00 | 200.00 | 156.09 | 99.08 | 59.83 | 54.09 | 76.31 | 75.00 | 132.90 | | 135.42 | 135.42 | - |
| | | | Actual Evapotranspiration (mm) | 0.25 | 34.09 | 74.08 | 110.59 | 112.07 | 93.70 | 76.14 | 38.88 | 11.82 | 0.00 | | 0.00 | 0.00 | 551.60 |
| P-AET (mm) | | | 49.55 | 34.41 | 0.22 | -39.09 | -36.37 | -15.60 | -1.64 | 22.22 | 63.28 | 57.90 | 51.80 | 47.70 | - | | |
| Actual Soil Moisture Deficit (mm) | | | 0.00 | 0.00 | 0.00 | -39.09 | -75.46 | -91.05 | -92.69 | -70.47 | -7.19 | 0.00 | 0.00 | 0.00 | - | | |
| Change in Soil Moisture Deficit (mm) | | | 0.00 | 0.00 | 0.00 | 39.09 | 36.37 | 15.60 | 1.64 | -22.22 | -63.28 | -7.19 | 0.00 | 0.00 | - | | |
| Precipitation Surplus (mm) | | | 49.55 | 34.41 | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 50.71 | 51.80 | 47.70 | 234.40 | | |
| Infiltration Factor | | | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | - | | |
| Run-Off Coefficient | | | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | 0.60 | - | | |
| Infiltration (mm) | | | 19.82 | 13.77 | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 20.28 | 20.72 | 19.08 | 93.76 | | |
| Run-Off (mm) | | | 29.73 | 20.65 | 0.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 30.43 | 31.08 | 28.62 | 140.64 | | |
| | | | Catchment Area (m ²) 97052.63 | Monthly Volumes | | | | | | | | | | | | | |
| | | | AET (m ³) | 23.90 | 3308.16 | 7189.68 | 10732.86 | 10876.45 | 9093.39 | 7389.12 | 3773.72 | 1147.23 | 0.00 | 0.00 | 0.00 | 53534.50 | |
| | | Infiltration (m ³) | 1923.73 | 1335.98 | 8.53 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1968.61 | 2010.93 | 1851.76 | 9099.55 | | |
| | | Run-Off (m ³) | 2885.59 | 2003.97 | 12.80 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2952.92 | 3016.40 | 2777.65 | 13649.32 | | |
| | | Development - Impervious Area | Catchment Area (m ²) = 0.00 | | | | | | | | | | | | | | |
| | | | Monthly Volumes | | | | | | | | | | | | | | |
| | | Evaporation from Imperv. (m ³) - 15% of P. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| | | Run-Off from Imperv. (m ³) - with 15% evap. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | |
| Total Site | Total Catchment Volumes | | | | | | | | | | | | | | | | |
| | Total ET (m ³) | 9644.41 | 13265.91 | 14389.15 | 13846.89 | 14660.28 | 15125.07 | 14427.88 | 11832.80 | 14544.08 | 11213.08 | 10031.74 | 9237.72 | 152219.01 | | | |
| | Total AET (m ³) | 129.38 | 17910.85 | 38926.02 | 55997.48 | 52519.28 | 45890.25 | 39799.50 | 20431.51 | 6211.28 | 0.00 | 0.00 | 0.00 | 277815.55 | | | |
| | Total Infiltration (m ³) | 13856.98 | 12478.02 | 6296.85 | 4655.73 | 4660.79 | 5307.60 | 5871.83 | 5819.79 | 14248.45 | 15887.54 | 14463.44 | 13318.65 | 116865.68 | | | |
| | Total Runoff (m ³) | 66833.08 | 80778.44 | 75357.16 | 69268.11 | 72710.69 | 76180.36 | 74556.24 | 63489.02 | 90655.80 | 77379.42 | 69601.77 | 64092.75 | 880902.84 | | | |

NOTES:

- PET and P Taken from Table 1
- Soil Moisture Deficit (mm) is a function of P-Pet, once there is a shortage of P to satisfy PET
- Water Holding Capacity (mm) of soils types taken from Table 3.1, SWM Planning & Design Manual (MOE, March 2003) and applied to March
- Actual Evapotranspiration (AET) is a function of Adjusted Potential Evapotranspiration (PET) and change in Groundwater Storage (ΔST) for a given soil type

APPENDIX 6

Wastewater

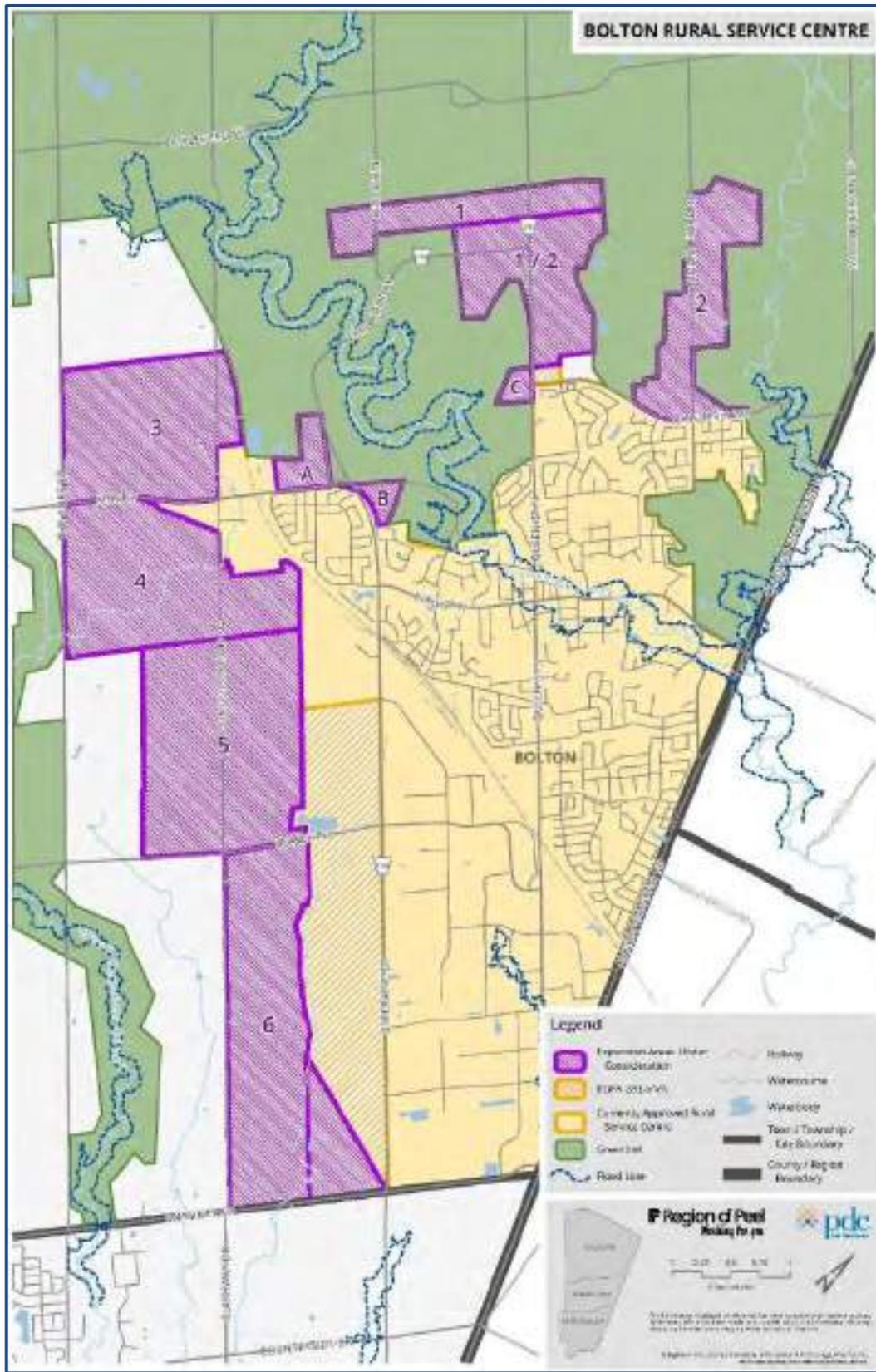


FIGURE 1 BOLTON RESIDENTIAL EXPANSION AREA OPTIONS

4.4.2.6 Option 3

Option 3 is located at the northwest corner of Humber Station Road and King Street. The ground elevations range between 265 m and 280 m.

Wastewater servicing of Option 3 requires an extension of the existing system towards the existing Coleraine Trunk Sewer, which presently conveys all of Bolton's wastewater flow to the lake-based system. Twinning of a section of the Coleraine Trunk sewer will be required. A high level analysis was performed on the ground elevation of the area and it was determined that it can be serviced by gravity in its entirety, therefore eliminating the need for a pumping station.

It is also important to note that the new infrastructure required minimizes the need to work through the urban core, thus lowering the potential for conflict with existing utilities and social impact.

The projects required as part of the wastewater servicing strategy for Option 3 are presented in Table 17.

TABLE 17 WASTEWATER PROJECTS FOR SERVICING OPTION 3

| BRES ID | Description | Size/Capacity | Length (m) |
|------------|--|---------------|------------|
| Opt3 - WW1 | New gravity sewer on King & Coleraine from Option 3 to ex. Coleraine Trunk Sewer south of rail | 450 mm | 2624 |
| Opt3 - WW2 | Twinning of Coleraine Trunk Sewer from south of rail to 700 m north of George Bolton Pkwy | 525 mm | 2908 |

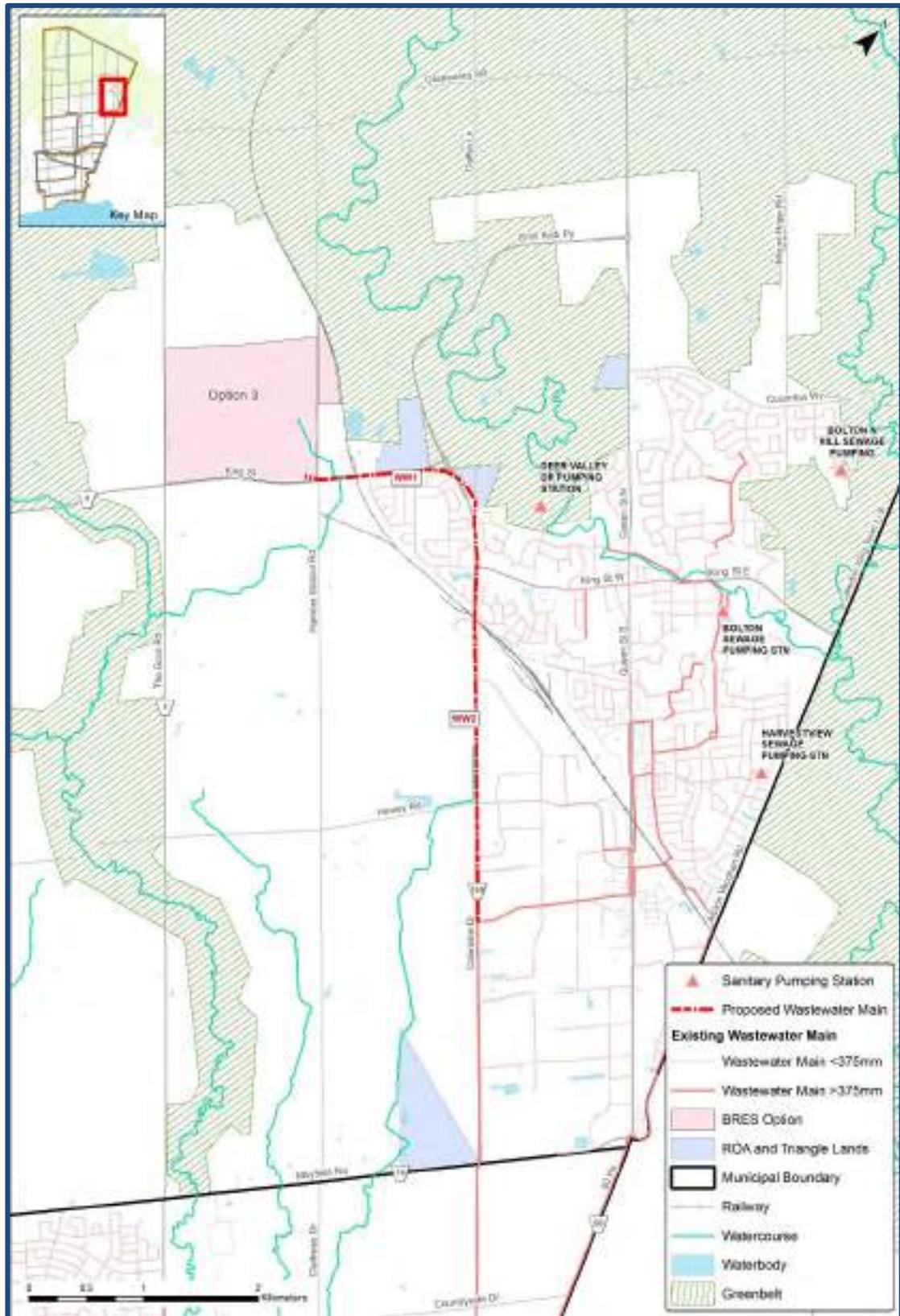


FIGURE 14 WASTEWATER SERVICING OPTION 3

4.4.2.7 Option 4

Option 4 is located at the southeast corner of King St. and The Gore Rd. Ground elevations range between 252 m and 262 m, with a topography allowing for a gravity system without any pumping requirements.

Option 4 can be serviced through a new wastewater gravity sewer on Humber Station Road to the future Holland extension, and then east on the Holland extension to Coleraine Drive. The first section of sewer will need to be more than 5 m deep, further downstream it can be shallower as it approaches Healey Road and the existing sewer on Coleraine. This Option also requires twinning of the Coleraine Trunk sewer to the extension of McEwan Drive.

This servicing strategy minimizes the need to work through the urban core, thus lowering the potential for conflict with existing utilities and social impact.

The projects required as part of the wastewater servicing strategy for Option 4 are presented in Table 18.

TABLE 18 WASTEWATER PROJECTS FOR SERVICING OPTION 4

| BRES ID | Description | Size/Capacity | Length (m) |
|------------|--|---------------|------------|
| Opt4 - WW1 | New gravity sewer on Humber Station Rd from 890 m north of Healey Rd to 790 m north of Healey Rd | 450 mm | 790 |
| Opt4 - WW2 | New gravity sewer on Holland Dr extension from Humber Station Rd to 690 m easterly | 450 mm | 690 |
| Opt4 - WW3 | New gravity sewer on Holland Dr extension from Coleraine Dr to 680 m westerly | 450 mm | 680 |
| Opt4 - WW4 | Twinning of Coleraine Trunk Sewer from Holland Dr extension to McEwan Dr | 525 mm | 2080 |

It is anticipated that the new infrastructure will require a few minor creek crossings along Humber Station Road and Healey Road.



FIGURE 15 WASTEWATER SERVICING OPTION 4

| |
|-------------------------------|
| I/c/d |
| I/c/d |
| I/s/ha |
| % |
| <i>down is NOT increased)</i> |

| SANITARY SEWER DESIGN SHEET | |
|-----------------------------|--|
| Macville Argo | |
| Region of Peel | |

| PROJECT DETAILS | DESIGN CRITERIA |
|--|---|
| Project No: 15-458 Date: ##### Designed by: E.L. Checked by: S.H. | Min. Flow = 13 l/s Min Diameter = 200 mm Mannings 'n' = 0.013 Min. Velocity = 0.75 m/s Max. Velocity = 3.00 m/s Factor of Safety = 30 % Daily Per Capital Flow (Residential) = 290.0 l/c/d Daily Per Capital Flow (Non-Residential) = 270.0 l/c/d Extraneous Flows = 0.260 l/s/ha Max. Peaking Factor = 4.00 Min. Peaking Factor = 2.00 |
| NOMINAL PIPE SIZE USED | |

| IPUT | D/S INVERT (m) | MIN DROP @ D/S MH (m) | U/S MH RIM EL. (M) |
|------|----------------|-----------------------|--------------------|
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| STREET | FROM MH | TO MH | RESIDENTIAL | | | | | | | NON-RESIDENTIAL | | | | | FLOW CALCULATIONS | | | | | PIPE DATA | | | | | | | | | | |
|---------------------------|---------|--------|-------------|----------------|-----------|----------------|------------------|-------|-------------|-----------------|----------------|--------------------|------|-------------|------------------------|-------------------|----------------|------------------------|-----------------|----------------------------|-------------------|-----------|---------------|--------------------------|--------------------------|-----------------------|------------------|------|------|-----|
| | | | AREA (ha) | ACC. AREA (ha) | UNITS (#) | DENSITY (P/ha) | DENSITY (P/unit) | POP | ACCUM. POP. | AREA (ha) | ACC. AREA (ha) | EQUIV. POP. (p/ha) | POP. | ACCUM. POP. | EXTRANEIOUS FLOW (l/s) | TOTAL ACCUM. POP. | PEAKING FACTOR | RESIDENTIAL FLOW (l/s) | MIN. FLOW (l/s) | NON RESIDENTIAL FLOW (l/s) | DESIGN FLOW (l/s) | SLOPE (%) | PIPE DIA (mm) | FULL FLOW CAPACITY (l/s) | FULL FLOW VELOCITY (m/s) | ACTUAL VELOCITY (m/s) | PERCENT FULL (%) | | | |
| EXTERNAL LANDS | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BRES-1 LANDS | OPT1 | Emil | 114.70 | 114.70 | | 97 | | | 11126 | 11126 | | | | | | 29.8 | 11,126 | 2.91 | 108.6 | 108.6 | | 138.4 | 0.50 | 450 | 201.6 | 1.27 | 1.33 | 69% | | |
| ROUNDING OUT | Emil | 5 | 22.00 | 136.70 | | 60 | | | 1320 | 12446 | | | | | | 35.5 | 12,446 | 2.86 | 119.5 | 119.5 | | 155.0 | 0.50 | 450 | 201.6 | 1.27 | 1.38 | 77% | | |
| ULTIMATE SAN TRUNK | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| HUMBER STATION RD | 5 | 6C | 100.00 | 369.25 | | 60 | | | 6000 | 43538 | | | | | | 22.85 | 1968 | 101.9 | 45,506 | 2.30 | 336.5 | 336.5 | 14.2 | 452.6 | 0.75 | 675 | 728.0 | 2.03 | 2.10 | 62% |
| HUMBER STATION RD | 6C | 7C | 103.00 | 472.25 | | 60 | | | 6180 | 49718 | | | | | | 22.85 | 1968 | 128.7 | 51,686 | 2.25 | 375.7 | 375.7 | 13.8 | 518.2 | 0.50 | 750 | 787.2 | 1.78 | 1.87 | 66% |
| HUMBER STATION RD | 7C | 8C | 81.00 | 553.25 | | 60 | | | 4860 | 54578 | | | | | | 22.85 | 1968 | 149.8 | 56,546 | 2.22 | 405.8 | 405.8 | 13.6 | 569.2 | 0.50 | 750 | 787.2 | 1.78 | 1.91 | 72% |
| HUMBER STATION RD | 8C | 9C | 81.00 | 634.25 | | 60 | | | 4860 | 59438 | | | | | | 22.85 | 1968 | 170.8 | 61,406 | 2.18 | 435.5 | 435.5 | 13.4 | 619.7 | 1.00 | 750 | 1113.3 | 2.52 | 2.55 | 56% |
| HUMBER STATION RD | 9C | 10C | 81.00 | 715.25 | | 60 | | | 4860 | 64298 | | | | | | 22.85 | 1968 | 191.9 | 66,266 | 2.15 | 464.7 | 464.7 | 13.2 | 669.8 | 0.75 | 750 | 964.1 | 2.18 | 2.29 | 69% |
| HUMBER STATION RD | 10C | EX 1A | | 715.25 | | | | | | 64298 | | | | | | 22.85 | 1968 | 191.9 | 66,266 | 2.15 | 464.7 | 464.7 | 13.2 | 669.8 | 0.75 | 750 | 964.1 | 2.18 | 2.29 | 69% |
| HUMBER STATION RD | EX 1A | EX 2A | | 715.25 | | | | | | 64298 | | | | | | 22.85 | 1968 | 191.9 | 66,266 | 2.15 | 464.7 | 464.7 | 13.2 | 669.8 | 0.30 | 1200 | 2135.4 | 1.89 | 1.64 | 31% |
| COLERAINE ROAD | EXT. | MH 118 | 95.00 | 95.00 | 4000 | | 3.61 | 14440 | 14440 | | | | | | | 24.7 | 14,440 | 2.79 | 135.5 | 135.5 | | 160.2 | 0.30 | 525 | 235.6 | 1.09 | 1.14 | 68% | | |
| WHITE BELT LANDS | WBL | OUT | 120.30 | 120.30 | | 60 | | | 7218 | 7218 | | | | | | 31.3 | 7,218 | 3.09 | 75.0 | 75.0 | | 106.2 | 0.30 | 450 | 156.2 | 0.98 | 1.03 | 68% | | |

APPENDIX 7

R.J. Burnside & Associates Water Modelling

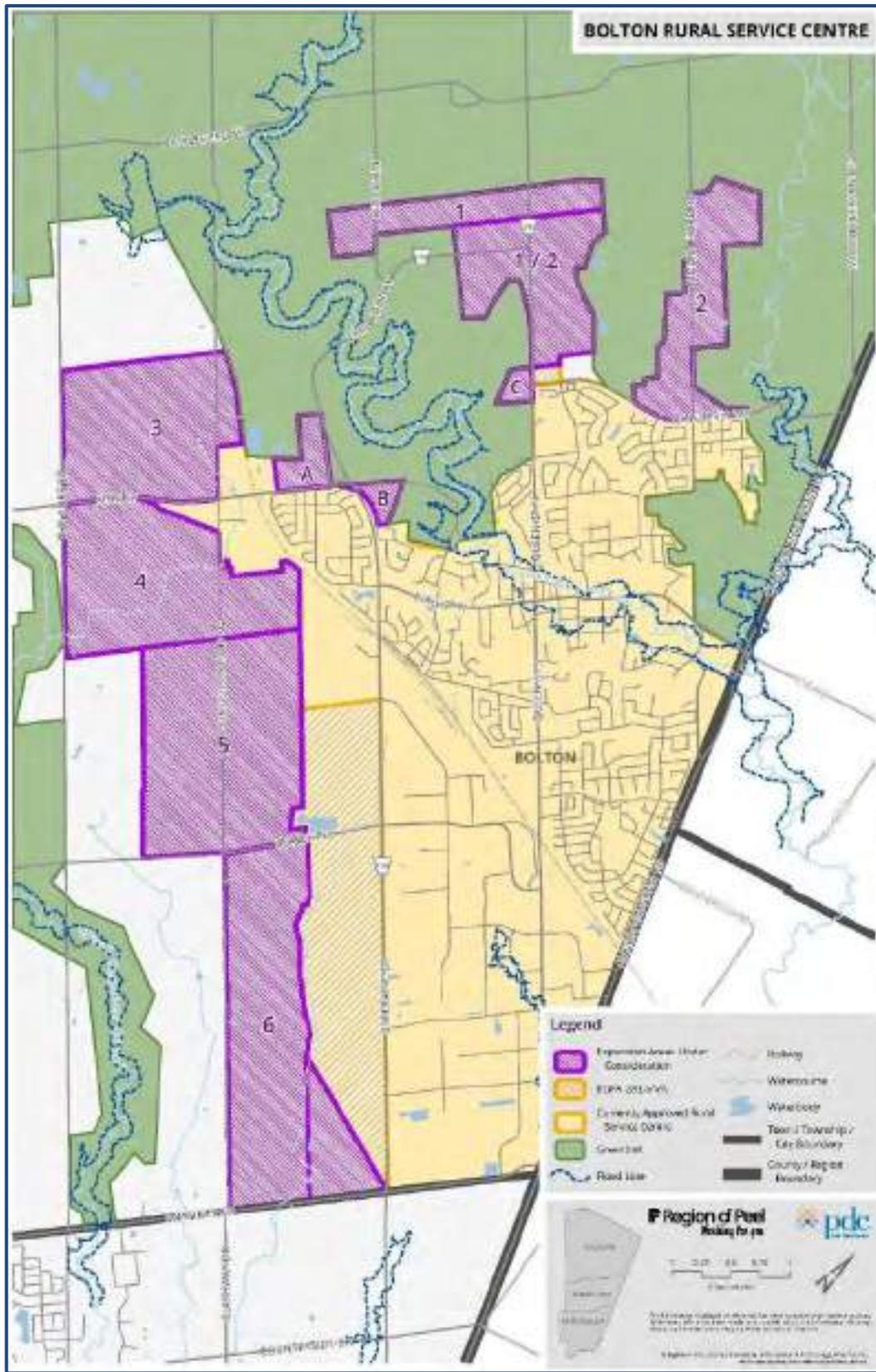


FIGURE 1 BOLTON RESIDENTIAL EXPANSION AREA OPTIONS

3.4.3.6 Option 3

Option 3 is located at the northwest corner of Humber Station Road and King Street. The ground elevations range between 265 m and 280 m, and as such fall in Zone 7. The top water level required to maintain adequate pressures is approximately 328 m.

Water servicing of Option 3 requires the creation of a new pressure zone system due to the range of elevations within the area. To achieve this, a new Zone 7 pumping station is required. Based on previous studies, it was confirmed that the preferred location for a new station is near the intersection of Chickadee Lane and Glasgow Road. An extension of the system through a 400 mm (Zone 6) watermain from the 1050 mm watermain on Coleraine, would provide water to the station, from there, a new 400 mm (Zone 7) feeder main from the proposed Zone 7 pumping station along King Street and Emil Kolb Parkway to the proposed Option 3 storage facility is also required. The proposed location for the elevated tank is a site west of Gore Rd, one which appears to be farm land and has an elevation of 283 m.

A high level evaluation of the storage requirements was undertaken. Based on the ground elevations and environmental features around Option 3, an elevated floating storage facility was selected as the preferred storage servicing strategy. In-ground storage was also considered as an option for provision of storage; however, with a pumped system there must be sufficient pump capacity to supply peak hour demands or maximum day demands plus fire demands. This could result in a larger investment in a pumping facility and larger pipes servicing the area. Furthermore, standby power at the pumping station would also be required. These impacts were considered and it is recognized that elevated floating storage provides a more robust and reliable system and provides a better solution to long term requirements when considering the surrounding areas that could potentially develop.

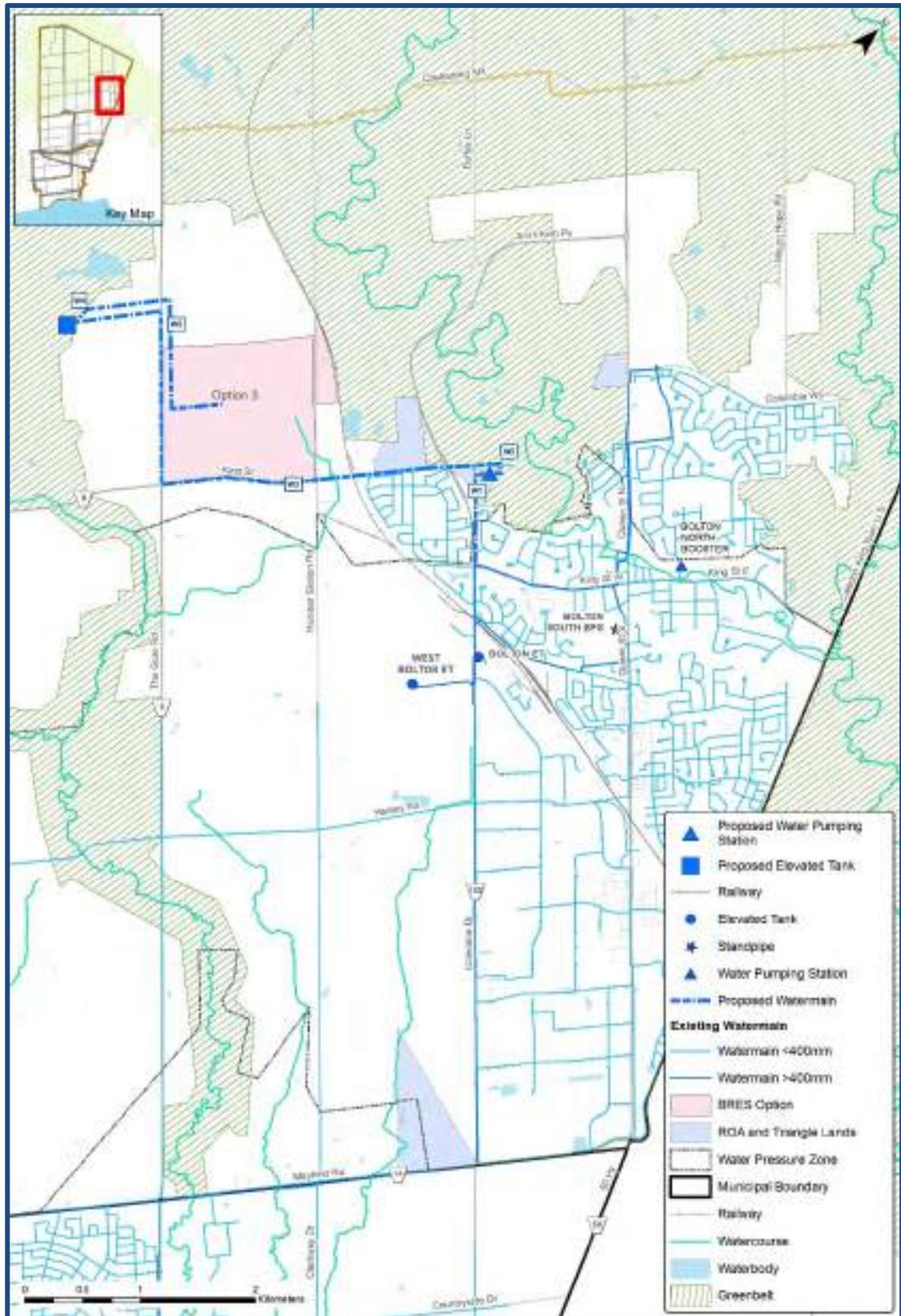


FIGURE 6 WATER SERVICING OPTION 3

The projects required as part of the water servicing strategy for Option 3 are presented in Table 6.

TABLE 6 WATER PROJECTS FOR SERVICING OPTION 3

| BRES ID | Description | Size/Capacity | Length (m) |
|-----------|--|---------------|------------|
| Opt3 - W0 | Class EA for elevated tank and booster station | | |
| Opt3 - W1 | Z6 Feedermain, from ex. 1050 mm at Coleraine King, east to Future Z7 BPS | 400 mm | 1038 |
| Opt3 - W2 | Z7 BPS, at King and Coleraine (greenfield) | 79 L/s | |
| Opt3 - W3 | Z7 Feedermain on King/Gore, from Z7 BPS to E.T. outside | 400 mm | 5176 |
| Opt3 - W4 | E.T. for Option 3 (TWL=327.7m) | 5.1 ML | |
| Opt3 - W5 | Z7 Feedermain, from E.T. to distribution | 400 mm | 2165 |

It is anticipated that the crossing of the Humber River along Emil Kolb Parkway will require either extensive trenchless installation or could potentially be suspended from the future bridge. Either method of installation will incur additional costs for construction and permitting, as this section crosses TRCA lands.

Servicing Option 3 provides an opportunity to service the Rounding Out Areas A and B without additional infrastructure as well as the potential to re-align the pressure zone boundary to shift some of the existing Zone 6 properties which currently experience low pressures to Zone 7. It has been demonstrated that these properties would benefit from an enhanced Zone 7 service.

3.4.3.7 Option 4

Option 4 is located at the southeast corner of King Street and The Gore Road. Ground elevations range between 252 m and 262 m, and as such most of the land falls in Zone 6 with the top part of the area in Zone 7.

Option 4 falls between two zones, therefore the servicing strategy will involve two components:

Zone 6 Servicing of Option 4:

The lower part of Option 4 can be serviced through an extension of the existing Zone 6 infrastructure. A new 300 mm (Zone 6) watermain is required from the proposed 600 mm watermain on Holland Road Extension to Option 4. This watermain is a candidate for oversizing as it could serve as a feedermain to a larger service area in the future.

Zone 7 Servicing of Option 4:



Technical Memorandum

Date: May 15, 2023 **Project No.:** 300034976.0001

Project Name: Bolton Option 3 Lands Preliminary Water Modelling

Client Name: Bolton Option 3 Landowners Group

Submitted To: Ms. Miriam Polga, P.Eng., Region of Peel

Submitted By: Rachel Walton, P.Eng., MAsc.

Reviewed By: Jeff Langlois, P.Eng., MBA

1.0 Introduction

R.J. Burnside & Associates Limited (Burnside) has been retained by the Bolton Option 3 Landowners Group (BO3LG) to complete a preliminary hydraulic water modelling analysis of the proposed Option 3 lands being considered as part of the urban boundary expansion of the Bolton settlement area in the Town of Caledon (Town). The water distribution system in Bolton is part of the Region of Peel (Region) water distribution system.

As dictated by the Ontario Growth Plan, the Region must plan for its share of growth to 2041. The projected growth numbers are dictated by the Province of Ontario and allocated by the Region to the lower tier Municipalities through Regional Council direction and Regional Official Plan Amendment. The Town previously completed the Bolton Residential Expansion Study (BRES) to determine the best approach to meet their urban boundary expansion needs. The BRES examined six different options for expansion of the Bolton settlement area and examined how each area could be serviced. The location of the BRES Option 3 lands is shown in Figure 1.

As determined in the BRES, the Option 3 lands are generally outside of the range of elevations associated with Pressure Zone 6 of the existing water distribution infrastructure in Bolton. As such, development of the Option 3 lands will ultimately require the development of a new pressure Zone 7. Previous studies completed in support of BRES identified a new Zone 7 booster pumping station at King Street and Coleraine Drive. Ultimately, floating storage is proposed in the form of an elevated tank (ET) to provide storage for flow equalization, fire demands and emergencies. The ET is to be situated in the vicinity of the northwest corner of the Option 3 lands.

The purpose of this preliminary modelling exercise and supporting technical memorandum is to determine interim alternative water servicing arrangements, which leverage the existing Zone 6 water supply to allow some portion of the Option 3 lands to be developed prior to the design and construction of the ultimate Zone 7 servicing solution. Water supply to the zone in the interim scenario would be principally through a new Zone 7 booster pumping station. Options investigated included providing water supply to meet fire demands on an interim basis through pumped, as opposed to floating, storage.

2.0 Background Documents

The following reports have been referenced to complete the hydraulic modelling discussed in this memorandum:

- Bolton Residential Expansion Study Infrastructure Report, prepared by GM BluePlan dated June 16, 2014;
- Region of Peel 2013 Water and Wastewater Master Plan for the Lake-Based Systems, Volume III – Water Master Plan, prepared by GM BluePlan and AECOM, dated March 31, 2014;
- Proposed Regional Official Plan Amendment, An Amendment to Establish the Bolton (2031) Residential Expansion Area Planning Justification Report, prepared by Meridian Planning, dated October 2014;
- Region of Peel 2020 Water and Wastewater Master Plan for the Lake Based Systems, prepared by GM BluePlan and Region of Peel, June 2020; and
- Ministry of the Environment, Conservation and Parks (MECP), “Guidelines for the Design of Water Distribution Systems”, 2008.

2.1 System Pressure

As per the Region of Peel 2020 Water and Wastewater Master Plan for the Lake-Based Systems, Volume III – Water Master Plan, prepared by GM BluePlan and Region of Peel, dated June 2020, a minimum operating pressure of 40 psi and a maximum operating pressure of 100 psi shall be maintained within the water distribution system under maximum day demand and a minimum operating pressure of 40 psi shall be maintained under peak hour demand. The allowable operating pressure during fire flow conditions is a minimum of 20 psi.

2.2 Roughness Coefficient (“C” Value)

The friction factors “C” used in the model are based on the Ministry of Environment, Conservation and Parks (MECP) Design Guidelines for Drinking Water Systems (2008), and are as follows:

- 150 mm diameter: C=100
- 200 mm or 250 mm diameter: C=110
- 300 mm to 600 mm diameter: C=120
- > 600 mm diameter: C=130

2.3 Peaking Factor

Peaking factors have been referenced from the 2020 Water and Wastewater Master Plan. The peaking factors used in the modelling are as follows:

- Residential Maximum Day Factor (MDF) = 1.8
- Non-Residential Maximum Day Factor (MDF) = 1.4
- Peak Hour Factor (PHF) = 3

2.4 Water Demand

The population yield for the Option 3 lands is based on the current proposed Block Plan as determined by Urbantech. The proposed Block Plan includes employment and mixed-use lands. The estimated yields are as follows:

- Residential 25,092 persons
- Employment 1,968 jobs

The demands for the Option 3 lands have been calculated based on the following per capita demands:

- Residential 270 L/cap/d
- Employment 250 L/cap/d

These per capita demands are referenced from the 2020 Water and Wastewater Master Plan. Refer to Appendix A for the demand calculations.

The calculated Option 3 lands demands are:

- Average Day Demand (ADD) = 84.1 L/s
- Maximum Day Demand (MDD) = 149.1 L/s
- Peak Hour Demand (PHD) = 252.3 L/s

Given the likelihood of further refinement of the concept plans through the approval process, for preliminary modelling purposes it has been assumed that the demands have an even distribution across the Option 3 lands. Therefore, the residential and employment demands have been divided evenly between each junction in the model.

There are existing areas within Bolton Pressure Zone 6 that have ground elevations within the Pressure Zone 7 servicing range. As such, the development of Bolton Pressure Zone 7 will allow for these existing lands to move into the new Pressure Zone, thereby providing pressure improvements for existing residents.

The existing land area that would be brought into Pressure Zone 7 was estimated based on the existing Pressure Zone 6 elevation boundary of 259.1 m. Using the existing topography, an approximate total land area of 137 ha has been established. Two existing areas have been identified, west of Coleraine Drive, and largely on the south side of King Street and east of

Highway 50, south of Columbia Way. These are areas where the Region has reported complaints by residents of inadequate pressure from time to time. While the Region has made improvements to the system to work towards addressing these concerns, the pressure remains at the lower end of the Region's preferred operating range, primarily due to elevation.

The existing population for these areas was taken from the population target set out in the Population Allocation 2031/2051 Plan (February 2021). A population density of 65 people per hectare was assumed in the allocation plan. An employment density of 25 jobs per hectare was assumed.

The total estimate population yields for the existing lands are as follows:

- Residential West of Coleraine Drive 2,860
- Employment West of Coleraine Drive 500

The calculated existing demands contributing to Option 3 Lands are:

- Average Day Demand (ADD) = 10.4 L/s
- Maximum Day Demand (MDD) = 18.1 L/s
- Peak Hour Demand (PHD) = 31.2 L/s

2.5 Fire Flow

The required fire flow for the Option 3 lands is 220 L/s while maintaining a minimum system operating pressure of 20 psi, as per Bolton Residential Expansion Study Infrastructure Report, prepared by GM BluePlan dated June 16, 2014.

3.0 Existing Water Distribution System

Bolton receives water supply from the Tullamore Pumping Station and Reservoir, through a transmission main along Mayfield Road and Coleraine Drive. Bolton's water distribution system is serviced in two pressure zones, Zone 5 and Zone 6. Zone 5 is serviced through Zone 6 by pressure reducing valves at the Bolton Zone 5 Standpipes. The Standpipes have a high-water level (HWL) of 274.1 m. Storage for Zone 6 is supplied by the Bolton ET and the North Bolton ET. The HWL of both ET's is 297 m. The Zone 6 ET water level ranges from 295 m to 297 m.

The existing ground elevations within the Option 3 lands range from approximately 262 m to 280 m. These elevations fall outside of the range of elevations capable of being serviced by Zone 6 while maintaining adequate operating pressures within the system. The Region of Peel reports operating pressure issues within an existing residential subdivision fronting on King Street in close proximity to the Option 3 lands.

A new pressure Zone 7 with an ET having a HWL of 327.7 m would adequately service all of the Option 3 lands, as well as address existing operating pressure issues for some existing residents.

4.0 Hydraulic Modelling

The hydraulic model was developed using Infowater modelling software. The Option 3 lands water system layout shown in the model is slightly different than the current proposed road network, however these differences are not anticipated to impact the modelling results. The layout of the watermains can be updated as the design progresses.

As identified through previous studies undertaken by the Town of Caledon and Region of Peel, sufficient supply is available to service the domestic and fire flow requirements associated with the Bolton residential expansion. Therefore, supply constraints have not been reviewed. The servicing constraints are based on supply pressure and hydraulic losses, which is dependent on watermain size and ground elevations within the serviced area.

The existing Zone 6 Bolton ET's have been shown schematically in the model as a reservoir and set at a HWL of 297 m during regular operating scenarios. Although the existing elevated tanks and booster pumping station are shown schematically in relatively close proximity to the Option 3 lands, the pipe lengths have been modelled with the actual lengths to properly reflect the friction losses and actual location of the existing and proposed infrastructure.

Several scenarios were developed to simulate operating pressures under Maximum Day Demand and Maximum Day plus Fire Flow. Model outputs are summarized on the attached figures to demonstrate what portion of the lands may be serviced in an interim water servicing situation.

4.1 Maximum Day Demand and Peak Hour Demand Scenarios

Scenario 1 was developed to estimate operating pressures within the Option 3 lands under MDD assuming a supply from Zone 6 without a booster pumping station or Zone 7 ET in place. This scenario would also simulate an emergency situation under an interim condition with no floating storage, and a Zone 7 Booster Pumping Station out of service. Map 1 in Appendix B shows the expected operating pressures under this scenario. The figure shows that only the southern and eastern periphery of the Option 3 Lands can be serviced by Zone 6 while maintaining pressures above 35 psi under MDD conditions. If a smaller area of the Option 3 lands is serviced, the MDD will be reduced, which in turn would reduce the friction losses in the watermain, resulting in potentially higher pressure in the development while being serviced from Zone 6.

Discussion is required with the Region to confirm the range of acceptable operating pressures during an emergency situation with the pumping station out of service until repair of the pumping station could be facilitated. It is proposed that residual operating pressures in the 20 to 30 psi range, consistent with a fire flow scenario would be appropriate on an emergency basis allowing more of the Option 3 lands to be serviced.

Scenario 2 was developed to estimate pressures within the Option 3 lands under MDD assuming a supply from Zone 6 and including a booster pumping station, but without a Zone 7

ET in place. To represent the booster pumping station, a single equivalent pump was input into the model. In reality, the booster pumping station would include several pumps to deliver the range of flows experienced within the zone at acceptable pressures. A typical pumping system arrangement would include a jockey pump, an ADD pump, large domestic service pumps, and if required a fire pump, all with built-in redundancy as per the Region and MECP Drinking Water Guideline requirements. The specific pumping arrangement would be determined during detailed design. Map 2 in Appendix B shows the expected operating pressures under Scenario 2. The equivalent pump was set to deliver the required MDD of 167.2 L/s at a total dynamic head (TDH) of 30.5 m to the Option 3 lands. The system can supply the MDD to the entirety of the Option 3 lands while maintaining system pressures between 40 psi and 100 psi.

4.2 Fire Flow Scenario

In all fire flow scenarios simulated, the Zone 6 ET has been set to the lower HWL limit of 295 m.

Scenario 3 was developed to estimate the fire flows that would be available assuming a fire pump is in place at the proposed Booster Pumping Station. A fire pump was modelled with a capacity of 387.25 L/s (MDD + 220 L/s fire flow) at a TDH of 30.5 m. A single equivalent pump was used to represent the pumping system. The specific pumping arrangement and design points would be determined during detailed design. Map 3 in Appendix B shows available fire flow under Scenario 7. The fire flow in some of the system falls slightly below the 220 L/s requirement while maintaining 20 psi. It is anticipated that the sizing of the internal watermains could be increased to achieve a 220 L/s fire flow. There are some locations of dead end watermains that fall well below the 220 L/s fire flow requirement. The watermains in these locations have been modelled as 200 mm diameter mains. It is not recommended to increase the diameter of a dead-end watermain above 200 mm diameter given concerns around the maintenance of chlorine residual.

Scenario 4 was developed to estimate available fire flows under the ultimate build out scenario for the Option 3 lands and to determine the required internal watermain sizes to deliver 220 L/s while maintaining a system pressure of 20 psi. This scenario assumes that the Zone 7 ET and the Zone 7 Booster Station are engaged in the model, with the HWL of 327.7 m. Map 4 in Appendix B shows the available fire flows under Scenario 4. The figure shows the internal watermain sizing recommended to deliver 220 L/s and maintain a minimum system pressure of 20 psi. These internal sizes are used in all the other scenarios unless otherwise noted.

5.0 Conclusion

A hydraulic model of the proposed water distribution system has been developed for the Option 3 lands. Various scenarios have been modelled to determine how much of the Option 3 lands can be reasonably serviced on an interim basis without the construction of a Zone 7 ET.

Almost the entirety of the Option 3 lands as summarized below can be serviced under all modelling scenarios if a new Booster Pumping Station is constructed in the vicinity of Coleraine Drive and King Street. The Booster Pumping Station will require appropriately sized booster

pumps to provide the ADD, MDD and PHD within the 40 psi to 100 psi pressure range. The Booster Pumping Station will also require a fire pump to provide the Option 3 Lands with 220 L/s of fire flow. The specific arrangement of the Booster Pumping Station would be determined during detailed design.

The MDD scenarios modelled show that the entirety of the Option 3 lands can be serviced within the recommended pressure range of 40 psi to 100 psi with a MDD pump at the Booster Pumping Station.

A fire flow scenario of the ultimate build out of the Option 3 lands, including the Zone 7 ET, was simulated to determine preliminary watermain sizes for the Option 3 lands. These watermain sizes were then used to determine the extent of Option 3 lands that could be serviced on an interim basis with an available fire flow of 220 L/s at 20 psi with no ET in place with a fire pump at the Zone 7 Booster Pumping Station.

Based on the modelling performed, with a fire pump in place at the Zone 7 Booster Pumping Station, the entirety of the Option 3 lands may be serviced, with the exception of a small area in the Northwest portion of the Block Plan which would require oversizing of dead end watermains as highlighted above.

R.J. Burnside & Associates Limited



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Enclosures Appendix A: Demands
 Appendix B: Figures

cc: Mr. Aaron Wisson, Argo Development Corporation (enc.) (Via Email)
 Mr. Dave Leighton, C.E.T., Urbantech Consulting (enc.) (Via Email)

In the preparation of the various instruments of service contained herein, R.J. Burnside & Associates Limited (Burnside) was required to use and rely upon various sources of information (including but not limited to: reports, data, drawings, observations) produced by parties other than Burnside. For its part Burnside has proceeded based on the belief that the third party/parties in question produced this documentation using accepted industry standards and best practices and that all information was therefore accurate, correct and free of errors at the time of consultation. As such, the comments, recommendations and materials presented in this instrument of service reflect our best judgment in light of the information available at the time of preparation. Burnside, its employees, affiliates and subcontractors accept no liability for inaccuracies or errors in the instruments of service provided to the client, arising from deficiencies in the aforementioned third party materials and documents.



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Appendix A

Demands

Bolton Option 3 Zone 7 Demand Calculations

| | |
|--------------|-----------|
| Prepared by: | RW |
| Checked by: | JLL |
| Project No: | 300034976 |
| Date: | 5/10/2023 |

**Assumptions****Water Demands** From the Region of Peel 2020 Water & Wastewater Master Plan for the Lake-Based System

| | | | |
|--------------------|-----------------------------|-----|----------------|
| Residential | Residential Per Capita Flow | 270 | L/person/day |
| | Max Day Factor | 1.8 | |
| | Peak Hour Factor | 3 | |
| Employment | Employment Per Capita Flow | 250 | L/employee/day |
| | Max Day Factor | 1.4 | |
| | Peak Hour Factor | 3 | |

Fire Flow

| | |
|---------|--|
| 220 L/s | From Bolton Residential Expansion Study Infrastructure Report, June 16, 2014 |
|---------|--|

Residential Population 25092**Employment Population** 1968

Population Based on Updated Option 3 Block Plan and Region of Peel Standards (November 2022) Densities

| | Demand (L/s) | | |
|------------|--------------|------------|-------|
| | Residential | Employment | Total |
| ADD | 78.4 | 5.7 | 84.1 |
| MDD | 141.1 | 8.0 | 149.1 |
| PHD | 235.2 | 17.1 | 252.3 |

Bolton Existing Lands Zone 7 Demand Calculations

| | |
|--------------|-----------|
| Prepared by: | RW |
| Checked by: | JLL |
| Project No: | 300034976 |
| Date: | 4/27/2021 |



Assumptions

Water Demands From the Region of Peel 2020 Water & Wastewater Master Plan for the Lake-Based System

| | | | |
|--------------------|-----------------------------|-----|----------------|
| Residential | Residential Per Capita Flow | 270 | L/person/day |
| | Max Day Factor | 1.8 | |
| | Peak Hour Factor | 3 | |
| Employment | Employment Per Capita Flow | 250 | L/employee/day |
| | Max Day Factor | 1.4 | |
| | Peak Hour Factor | 3 | |

Fire Flow

220 L/s From Bolton Residential Expansion Study Infrastructure Report, June 16, 2014

Density

| Unit Type | People Per Unit (ppu)* | People Per Hectare (pp/ha)** |
|-----------------|------------------------|------------------------------|
| Townhomes | 3.1 | 65 |
| Single Detached | 3.7 | 65 |
| Mixed Use | 1.99 | 65 |
| Employment | | 25 |

*from development plan
 ** from BRES Population Allocation 2031-2051 Plan
 BRES assumptions used in absences of a development plan

Demand Allocation

| Unit Type | Total Area (ha)* | # of units | Population | L/ha/s | | | L/s | | |
|---|------------------|------------|-------------|--------|-----|-----|-------------|-------------|-------------|
| | | | | ADD | MDD | PHD | ADD | MDD | PHD |
| Single Detached West of Coleraine Drive | 44 | N/A | 2860 | | | | 8.9 | 16.1 | 26.8 |
| Industrial West of Coleraine Drive | 20 | N/A | 500 | | | | 1.4 | 2.0 | 4.3 |
| Total | 64 | | 3360 | | | | 10.4 | 18.1 | 31.2 |

*area estimated based on existing land area exceeding 259 m, based on existing ground elevation



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Appendix B

Figures

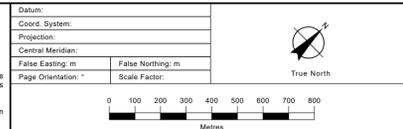
- | | | |
|--------------------------------|---------------------------|-----------------------|
| Junction Pressure (psi) | Pipe Diameter (mm) | Pump Type |
| • less than 20.00 | — 150 | □ Active |
| • 20.00 ~ 40.00 | — 200 | □ Domain |
| • 40.00 ~ 70.00 | — 300 | Reservoir Type |
| • 70.00 ~ 80.00 | — 400 | □ Active |
| • 80.00 ~ 100.00 | — 600 | □ Domain |
| • > 100 | — 1050 | |
| • Domain | — Domain | |



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| | Map Title BOLTON ZONE 7 OPTION 3 OPTION 3 - MDD SERVICED OFF ZONE 6 SCENARIO 1 | | | Map No. 1 |
| | BOLTON OPTION 3 LANDOWNERS GROUP | Drawn: RW Scale: H 1:5000 | Checked: JLL Date: 2023/05/10 Project No: 300034976 | |

| Junction Pressure (psi) | Pipe Diameter (mm) | Pump Type |
|-------------------------|--------------------|----------------|
| • less than 20.00 | — 150 | □ Active |
| • 20.00 ~ 40.00 | — 200 | □ Domain |
| • 40.00 ~ 70.00 | — 300 | |
| • 70.00 ~ 80.00 | — 400 | Reservoir Type |
| • 80.00 ~ 100.00 | — 600 | □ Active |
| • > 100 | — 1050 | □ Domain |
| • Domain | — Domain | |



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True North

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| | BOLTON ZONE 7 OPTION 3 OPTION 3 - MDD WITH BOOSTER PUMPING STATION SCENARIO 2 | | Map No. 2 |
| | Client: BOLTON OPTION 3 LANDOWNERS GROUP | Drawn: RW Checked: JLL Date: 2023/05/15 Scale: H 1:5000 Project No: 300034976 | Map No.: 2 |

- | | | |
|---|---------------------------|-----------------------|
| Junction Hydrant Design Flow (L/s) | Pipe Diameter (mm) | Pump Type |
| • less than 0.0 | — 150 | □ Active |
| • 0.0 ~ 100.0 | — 200 | □ Domain |
| • 100.0 ~ 150.0 | — 300 | Reservoir Type |
| • 150.0 ~ 220.0 | — 400 | ▭ Active |
| • > 220 | — 600 | ▭ Domain |
| • Domain | — 1050 | |
| | — Domain | |



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| | BOLTON ZONE 7 OPTION 3 | | |
| | OPTION 3 - MDD + FIRE FLOW WITH BOOSTER PUMPING STATION SCENARIO 4 | | |
| BOLTON OPTION 3 LANDOWNERS GROUP | Drawn | Checked | Date |
| | RW | JLL | 2023/05/10 |
| | Scale: | Project No. | |
| H 1:5000 | 300034976 | | Map No. 3 |

- Junction Hydrant Design Flow (L/s)**
- less than 0.0
 - 0.0 ~ 100.0
 - 100.0 ~ 150.0
 - 150.0 ~ 220.0
 - > 220
 - Domain
- Pipe Diameter (mm)**
- 150
 - 200
 - 300
 - 400
 - 600
 - 1050
 - Domain

- Pump Type**
- Active
 - Domain
- Reservoir Type**
- Active
 - Domain

Proposed Zone 7 ET
(Location shown schematically)
HWL - 327.7 m



Sources:
1. Ministry of Natural Resources, © Queen's Printer for Ontario
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| Central Meridian: | |
| False Easting: m | False Northing: m |
| Page Orientation: ° | Scale Factor: |

True North

| | | | |
|--|--|---|-------------------|
| | BOLTON ZONE 7 OPTION 3 OPTION 3 - MDD WITH BOOSTER PUMPING STATION SCENARIO 4 | | Map No. 4 |
| | Client: BOLTON OPTION 3 LANDOWNERS GROUP | Drawn: RW Checked: JLL Date: 2023/05/15 Scale: H 1:5000 Project No: 300034976 | Map No.: 4 |

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