



PRELIMINARY FUNCTIONAL SERVICING REPORT AND STORMWATER MANAGEMENT REPORT

STELLAR ESTATES SUBDIVISION PHASE 2

REPORT PREPARED FOR:

STELLAR HOMES INC.
125 Don Hillock Drive, Unit 8B
Aurora, Ontario
L4G 0H8

REPORT PREPARED BY:

Ecometrix Incorporated, an Egis Group Company
www.egis-group.com
Mississauga, ON

April 7, 2026
Ref. 22-3001

TOWN OF CALEDON
PLANNING
RECEIVED

04/14/2026

TABLE OF CONTENTS

- 1.0 INTRODUCTION.....1.1**
- 2.0 STUDY AREA.....2.1**
 - 2.1 General 2.1
 - 2.2 Physiography and Landform 2.1
 - 2.3 Topography 2.1
 - 2.4 Pre-Development Land Use and Drainage Patterns 2.2
 - 2.5 Surficial Soils 2.3
 - 2.6 Surficial Geology 2.4
 - 2.7 Hydrogeology and Groundwater 2.4
- 3.0 STORMWATER MANAGEMENT3.1**
 - 3.1 General 3.1
 - 3.2 Stormwater Management Criteria 3.1
 - 3.3 Stormwater Management Strategy 3.1
 - 3.4 Stormwater Management Assessment – Quantity Control 3.2
 - 3.4.1 Hydrologic Modelling Approach 3.2
 - 3.4.2 Peak Flow Rate Estimates..... 3.2
 - 3.4.3 Existing East Stormwater Management Pond Operational Characteristics..... 3.3
 - 3.5 Stormwater Management Assessment – Quality Control 3.5
 - 3.6 Stormwater Management Assessment – Water Balance..... 3.6
 - 3.7 Review and Discussion of Low Impact Development (LID) Options..... 3.7
- 4.0 MINOR AND MAJOR DRAINAGE SYSTEM DESIGN4.1**
- 5.0 DRAINAGE SYSTEM OPERATION AND MAINTENANCE CONSIDERATIONS .5.1**
 - 5.1 General 5.1
 - 5.2 Town of Caledon Consolidated Linear Infrastructure Environmental Compliance Approval..... 5.2
- 6.0 SANITARY AND WATER SERVICING PLAN6.1**
 - 6.1 Sanitary Servicing Plan..... 6.1
 - 6.2 Water Servicing Plan 6.2

6.2.1 Water Demand 6.2

6.2.2 Water Supply and Distribution 6.3

6.2.3 Water Services 6.3

6.2.4 Fire Flow 6.3

7.0 ROADWAY AND GRADING..... 7.1

7.1 General Description and Location..... 7.1

7.2 Road Design..... 7.1

8.0 EROSION AND SEDIMENT CONTROL..... 8.1

8.1 General 8.1

8.2 Emergency Contact Information..... 8.2

9.0 UTILITY SERVICES 9.1

10.0 SUMMARY 10.1

11.0 REFERENCES 11.1

APPENDIX A FIGURES AND MAPS A.1

APPENDIX B STORMWATER MANAGEMENT CALCULATIONS B.1

APPENDIX C ENGINEERING DRAWINGS C.1

1.0 Introduction

Ecometrix Incorporated, an Egis Group Company, has been retained by Stellar Homes Inc. to prepare a Preliminary Functional Servicing and Stormwater Management Report for the proposed second phase of the Stellar Estates Subdivision (Phase 2). This report is supporting documentation for the Draft Plan of Subdivision application for Phase 2.

The site is in the Palgrave Estates area of the Town of Caledon on Mulloy Court. Mulloy Court is west of Mount Pleasant Road between Old Church Road and Castleberg Side Road. The site is bounded by Mount Pleasant Road to the east, Mulloy Court and existing estate residential development to the north and west (Stellar Estates Subdivision herein denoted as Phase 1; Registered Plan 43M-1994), and agricultural land to the south. The legal description of the property is Part of Lot 18, Concession 8, former Township of Albion, Town of Caledon, Regional Municipality of Peel.

The Phase 2 site comprises approximately 4.10 hectares or 10.13 acres. It is proposed to develop the site with 5 estate residential lots using private septic systems for sewage disposal systems and municipal water. All 5 lots would front on to Mulloy Court. Mulloy Court was constructed in 2013/2014 with an urban road cross-section and comprises 10 estate residential lots serviced with private septic systems and municipal water. The Stellar Estates Subdivision Phase 1 (Registered Plan 43M-1994) has not been assumed as of the writing of this report. Currently, the 10 lots associated with the Stellar Estates Subdivision Phase 1 have either constructed and occupied dwellings or dwellings under construction. Drainage and stormwater for the proposed Phase 2 site would be managed with existing infrastructure and application of Low Impact Development (LID) practices.

The objective of this report is to describe proposed sanitary and water servicing, drainage and stormwater management, site grading, and other proposed servicing infrastructure. Also addressed in this report are applicable review comments made during the Draft Plan of Subdivision application submission and review process. This report is associated with the Fourth Submission and is an update to the Preliminary Functional Servicing and Stormwater Management Report dated January 17, 2025.

2.0 Study Area

2.1 General

The site is in the Palgrave Estates area of the Town of Caledon on Mulloy Court. Mulloy Court is west of Mount Pleasant Road between Old Church Road and Castleberg Side Road. The site is bounded by Mount Pleasant Road to the east, Mulloy Court and existing estate residential development to the north and west (Stellar Estates Subdivision herein denoted as Phase 1; Registered Plan 43M-1994), and agricultural land to the south. The legal description of the property is Part of Lot 18, Concession 8, former Township of Albion, Town of Caledon, Regional Municipality of Peel.

Illustrated on the Site Plan in Appendix A is the proposed lot pattern. Access to all five lots would be from Mulloy Court.

2.2 Physiography and Landform

The Phase 2 site is located within the physiographic region referred to as the Oak Ridges Moraine (ORM). The ORM encompasses a stretch of about 160 kilometres from the Trent River to the east to the Niagara Escarpment to the west, and typically varies from 2 to 11 kilometres in width. The moraine was created as glaciers receded and deposited layers of sand and gravel that are separated by clay and till soils. The ORM comprises smaller landforms, including Palgrave Morane, within which the site is located (Chapman and Putnam, 1984). The Palgrave Moraine is an ice-contact stratified area of sands, gravels, and silts that originated as kame outwash deposits, and consists of a strip of hummocky topography 5 to 7 kilometers in width extending from Caledon East to the Palgrave and Mount Wolfe area, and then east to King City (White, 1975).

2.3 Topography

The site and surrounding area is characterized by gently sloping terrain with moderate to shallow slopes. Elevation tends to gradually decrease moving from north to south across the site. Surface water from the site drains to a tributary of the Humber River. Thus, the site falls under jurisdiction of the Toronto and Region Conservation Authority. Specifically, the site is part of the Cold Creek subwatershed, which drains to the main branch of the Humber River.

The highest elevation within the site occurs at the top of a small ridge located along the north property limit at approximate elevation 269 metres and the lowest elevation occurs in the southwest corner of the site and along Mount Pleasant Road at approximate elevation 264 metres.

The Palgrave Estates Residential Community Secondary Plan (PERCSP) contains policies for development within the Palgrave Estates area which apply to the proposed subdivision. Specific references to topography and slopes within the secondary plan are discussed below.

Section 7.1.9.11 of the PERSCP specifies that structure envelopes will generally be restricted to areas with slopes of 10 per cent or less and may include areas with 11 to 15 per cent slope and occasionally greater than a 15 percent slope to permit the advantageous siting of a house designed for steep slopes. Additionally, all structure envelopes must include a well-drained area with slopes of 10 percent or less for a sewage disposal system. Consistent with this policy, all proposed lots have an appropriate area for a sewage disposal system (discussed further in Section 6.1 of this report) and generally include gentler slopes within the structure envelope.

Section 7.1.9.23 of the PERSCP specifies that the continuity and integrity of the lowland open space system must be maintained in estate residential plans of subdivision. The proposed subdivision is in general conformance with this policy based on the siting of lot structure envelopes away from the lowland areas, and Key Natural Heritage Feature and associated minimum vegetation protection zone in the southwest corner of the site..

Section 7.1.9.40 of the PERSCP specifies that roads in estate residential developments should follow the topography of the site and Section 7.1.9.41 specifies that the depth of cut for local streets and structure envelopes in future estate residential plans of subdivision will normally be restricted to 1 to 2 metres. Mulloy Court is an existing road and the conceptual grading for lots 1 to 5 does not result in a cut greater than 2 metres from the existing ground surface.

2.4 Pre-Development Land Use and Drainage Patterns

The land was historically cleared and farmed. Currently, portions of the lands are planted with agricultural crops. The remaining areas are either cultural meadows or wetland and hedgerow features. There are no existing buildings or structures on the property.

The site is located within the headwater reaches of Cold Creek, a tributary of Humber River Watershed. Surface flow on the site is typically via sheet flow to topographic lows. The site falls within the jurisdictional boundary of the Toronto and Region Conservation Authority and partially regulated based on review of available online mapping.

Pre-development drainage patterns are presented on Map 5 in Appendix A. Five sub-catchments have been identified. The respective sub-basins and associated characteristics are summarized in Table 2.1.

Table 2.1: Summary of Pre-Development Sub-Basin Characteristics

Sub-basin	Drainage Area (ha)	Outlet	Receiver
302a	1.38	Sub-Basin 302a and Node 4 Sub-Basin is external to Phase 2 site and is a vegetated area with a small pond feature. Drainage from this sub-basin is ephemeral.	Cold Creek Tributary, Humber River Watershed
302b	2.09	Node 4 Receives ephemeral drainage from Sub-Basin 302b. Identified natural feature in southwest corner of this sub-basin.	Cold Creek Tributary, Humber River Watershed
303	3.89	Node 1 Drainage is to existing Stellar Estates Subdivision Phase 1 stormwater management facility which discharges to Mount Pleasant Road.	Cold Creek Tributary, Humber River Watershed
304	1.61	Node 2 Overland flow to Mount Pleasant Road	Cold Creek Tributary, Humber River Watershed
305	1.02	Node 1 Major System Drainage is to existing Stellar Estates Subdivision Phase 1 stormwater management facility which discharges to Mount Pleasant Road. The minor system drains west to an existing stormwater management facility at the west end of Mulloy Court.	Cold Creek Tributary, Humber River Watershed
306	0.09	Node 3 Overland flow to south of Phase 2 site	Cold Creek Tributary Humber River Watershed
Total	10.08		

Note:

1. Units: ha – hectares.
2. Refer to Map 5 in Appendix A for sub-basin delineation.

2.5 Surficial Soils

A geotechnical investigation was performed by GeoTerre Limited (2024) comprising 4 boreholes of which three boreholes were extended to a depth of approximately 6.6 metres and 1 borehole was extended to a depth of 15.7. It was reported that shallow overburden materials included 15 to 60 centimetres of topsoil and the sub-surface profile below the surface topsoil within the limits of the entire site appeared to consist primarily of a series of low plasticity silty clay materials interbedded with occasional thin layers of more silt rich soils.

According to the GeoTerre Limited (2024), the soils within the elevated Phase 2 northern part of the Phase 2 site can be described with a firm degree of consistency/loose degree of

compactness above a depth 1.4 metres and very stiff to hard degree of consistency/compact to dense degree of compactness below 1.4 metres. The soils located within the lower lying natural feature in the southwest corner of the have a dominant low plasticity silty clay soils. These soils are characterized by a firm to stiff degree of consistency above a depth 4.4 metres and a very stiff degree of consistency below a depth 4.4 metres.

2.6 Surficial Geology

Surficial geology in the local area where the Site is located is reported to comprise of yellowish brown, loam to silt loam till within the Palgrave Moraine, and is reported to correlate with Halton Till to the south (White and Karrow, 1973; White, 1975). The Site is located near the northern extent of the Halton Till; regional overburden geology transitions to ice contact stratified drift in the direction of Mount Wolfe. The till has been observed to occur as thin layers (1 to 1.5 metres) overlying stratified sediments in places; as well as deeper layers with consistent texture (White, 1975).

Mapping of overburden sediments within the Humber River watershed provided by the Toronto and Region Conservation Authority (2008) indicates that the main stratigraphic units underlying the Halton Till in the vicinity of the site include Oak Ridges Moraine Deposits, Newmarket Till, Thorncliffe Formation, and Sunnybrook Drift.

Oak Ridges Moraine sediments are described as interbedded fine sand and silt deposits with local deposits of coarse sands and heterogeneous gravels (Toronto and Region Conservation Authority, 2008). The Newmarket Till is a consistently dense silty sand diamicton, with interconnected sand and silt lenses; and is underlain by Thorncliffe Formation deposits, which represent glaciofluvial deposition of sand and silty sand (Toronto and Region Conservation Authority, 2008). Sunnybrook Drift sediments consist mostly of clay and silt and is locally present in the vicinity of the Site (Toronto and Region Conservation Authority, 2008).

2.7 Hydrogeology and Groundwater

As part of the Draft Plan of Subdivision application process, a hydrogeologic assessment was completed by Ecometrix Incorporated (2025). The hydrogeologic assessment focused on the nature of interaction between the groundwater system and the surface water system, identified hydrogeological characteristics of the site, including both groundwater flow and groundwater quality, and provided an assessment of potential impacts to groundwater as a result of the proposed development.

It was concluded by Ecometrix Incorporated (2025) that the shallow groundwater table is typically 2.5 to 4 metres below ground surface (mbgs) or less and inferred to flow in a generally southern direction across the site. The groundwater table reflects the topography and the shallow groundwater flow path follows local topography through the low permeability, predominantly silty clay, overburden. The shallow local groundwater flow system discharges to a natural wetland feature in the southern portion of the site during summer months, but this pattern may reverse during snowmelt or after rain events when surface water rises in the

wetland feature. Groundwater flow in the deeper confined aquifer(s) and regional groundwater system is generally to the south and southwest towards the Humber River

In addition to the above, the proposed 5 lot estate residential development is not anticipated to have an impact on local groundwater levels, well water quantity, or well water quality. Groundwater levels in the immediate area of the sewage disposal system on each lot are expected to be higher than pre-development levels, but this change is unlikely to materially influence the shallow groundwater flow system. Estimates of potential nitrate loading from the individual on-site sewage disposal systems indicates the downstream nitrate concentration at the property boundary will be less than the Ontario drinking water standard of 10 milligrams per litre (mg/L).

Groundwater levels on the site have been monitored since August 2022.

3.0 Stormwater Management

3.1 General

Storm water from the site is proposed to be managed using both conventional stormwater management techniques and Low Impact Development (LID) practices.

3.2 Stormwater Management Criteria

Stormwater management criteria are proposed that are consistent with the Provincial Policy Statement (2014), ORMCP (Ontario Regulation 140/02), and current municipal and Conservation Authority criteria and guidelines, and are intended to avoid impacts to site natural features and local surface and groundwater resources.

Per the Town of Caledon Development Standards Manual (2019), Town of Caledon Consolidated Linear Infrastructure Environmental Compliance Approval (ECA), and the Draft Plan of Subdivision application submission and review process, the following stormwater management criteria are applicable:

- Quantity Control – peak flows are controlled to pre-development levels;
- Quality Control – water quality treatment in conformance with Provincial requirements as outlined in the Stormwater Management Planning and Design Manual (Ministry of the Environment, 2003);
- Water Balance – implementation of Low Impact Development (LID) measures sufficient to control 5 millimetres of runoff; and
- Erosion Control – erosion protection be provided in accordance with policies of the Toronto and Region Conservation Authority.

Further to the above-noted water balance criteria, the Town of Caledon has noted that as the proposed project in an infill development, the water balance requirements can be lowered to controlling 5 millimetres of runoff rather than 27 millimetres of runoff associated with the 90th percentile rainfall event. The Town of Caledon Consolidated Linear Infrastructure ECA requirements require that LID's be located within lands owned by the Town of Caledon.

In addition, Toronto and Region Conservation Authority stormwater management criteria applicable are control of 2 to 100-year post-development peak flows to pre-development peak flows and control of 5 millimetres of runoff for water balance and erosion control considerations.

3.3 Stormwater Management Strategy

Consistent with Section 7.10.6.9.2 of the Town of Caledon Official Plan, the proposed stormwater management strategy comprises a "treatment train" approach utilizing a combination of lot level controls, Low Impact Development (LID) measures, and conventional stormwater management techniques to minimize potential increases in peak flows and runoff volume, maintain water

quality, and provide, as far as practical, a natural hydrologic response. Measures are proposed to be undertaken at the source, and conveyance and end of pipe locations, and are as follows:

- recharge of residential roof and driveway storm water by direction to grassed and naturalized areas to promote filtering and natural infiltration and evapotranspiration;
- discharge of foundation drain water to rear and side lot areas;
- by lot grading, as far as practical, direction of structure envelope drainage, via sheet flow, towards grassed and naturalized areas versus the municipal road right of way;
- application of Low Impact Development practices in the boulevards such as bioswales;
- use of an oil/grit separator where drainage is to a stormwater management pond; and
- use of an existing stormwater management pond to temporarily detain and slowly release storm water to meet applicable stormwater management criteria.

The existing stormwater management pond is in the northeast corner of the Stellar Estates Subdivision Phase 1 and drains to Mount Pleasant Road. Pre-treatment of flow to the stormwater management facility is with use of an oil/grit separator. The existing oil/grit separator installed in Phase 1 will be upgraded to a larger model sized to accommodate the increase in drainage area to the existing stormwater management facility.

3.4 Stormwater Management Assessment – Quantity Control

3.4.1 Hydrologic Modelling Approach

A hydrologic modelling approach was used to determine and evaluate measures for quantity (peak flow) control. A hydrologic model (SWMHYMO Version 4.07 dated July 1999) was set up to reflect the existing (pre-development) condition shown on Map 5 (Appendix A) and post-development condition shown on Map 6 (Appendix A). Available soils, land use, and topographic information was used to calculate SWMHYMO parameters, including curve number (CN), time to peak (tp), and catchment slope. Due to the estate residential nature of the subdivision, the catchments typically had a total imperviousness (TIMP) of less than 20% and were modeled using the Calibrate NASHYD command under post-development conditions. The time to peak was calculated using the Airport formula. The Atmospheric Environment Service (AES) 6-hour and 12-hour duration storms were used with the hydrologic model to determine the critical storm duration. Based on this analysis, the AES 6-hour duration storm was determined to be the critical design storm and applied to estimate peak flows.

3.4.2 Peak Flow Rate Estimates

Peak flows were estimated at four locations where surface water discharges from the site. These locations have been denoted as nodes 1, 2, 3 and 4, and are shown on Map 5 and Map 6 in Appendix A. The peak flow estimates for post-development conditions include the storage effect of the existing stormwater management pond. Summarized in Table 3.1a are estimated pre-development and post-development peak flows at nodes 1, 2, 3, and 4. As shown in Table 3.1a, peak flows can be controlled to pre-development levels with the proposed stormwater

management approach. A summary of model parameters and SWMHYMO input and output files are provided in Appendix B.

3.4.3 Existing East Stormwater Management Pond Operational Characteristics

The existing stormwater management pond is in the northeast corner of the Stellar Estates Subdivision Phase 1 and drains to Mount Pleasant Road. The reference node for the stormwater management pond outlet is Flow Node 1: refer to Map 6 in Appendix A. Summarized in Table 3.1b are operational characteristics of the respective stormwater management pond under the proposed post-development condition.

Table 3.1a: Summary of Estimated Peak Flows from the Project Site

Node and Return Period	Pre-Development Peak Flow (cms)	Post-Development Peak Flow (cms)
2-Year Return Period		
1	0.069	0.010
2	0.033	0.012
3	0.003	0.002
4	0.051	0.046
5-Year Return Period		
1	0.136	0.065
2	0.065	0.024
3	0.005	0.004
4	0.103	0.093
10-Year Return Period		
1	0.188	0.096
2	0.088	0.033
3	0.006	0.005
4	0.143	0.130
25-Year Return Period		
1	0.258	0.128
2	0.120	0.045
3	0.009	0.007
4	0.198	0.181
50-Year Return Period		
1	0.313	0.148
2	0.145	0.055
3	0.010	0.008
4	0.243	0.223

Node and Return Period	Pre-Development Peak Flow (cms)	Post-Development Peak Flow (cms)
100-Year Return Period		
1	0.369	0.193
2	0.171	0.065
3	0.012	0.010
4	0.288	0.265

Note:

1. Units: cms – cubic metres per second.
2. Refer to Map 5 and Map 6 in Appendix A for location of flow nodes.
3. Pre-development peak flows are based on hydrologic modelling using SWMHYMO.

Table 3.1b: Existing East Stormwater Management Pond Operational Characteristics

Flow Node	Return Period	Estimated Peak Flow In (cms)	Estimated Peak Flow Out (cms)	Volume Required (cu.m)	Equivalent High Water Level (m)
1	2-Year	0.085	0.010	328.1	264.20
1	5-Year	0.168	0.065	432.2	264.33
1	10-Year	0.232	0.096	525.6	264.44
1	25-Year	0.318	0.128	680.3	264.61
1	50-Year	0.386	0.148	818.8	264.75
1	100-Year	0.455	0.193	944.6	264.86

Note:

1. Units: cms – cubic metres per second cu.m – cubic metres; m – metres.
2. Refer to Map 6 in Appendix A for location of stormwater management facility and Flow Node 1.

3.5 Stormwater Management Assessment – Quality Control

The stormwater management criteria for quality control is to achieve an enhanced level of treatment (Level 1) consistent with the Stormwater Management Planning and Design Manual (Ministry of the Environment, 2003). Typically, Total Suspended Solids (TSS) is used as the parameter to evaluate water quality and the long-term average removal rate to achieve an enhanced level of treatment (Level 1) is 80%.

A “desk-top” accounting approach was used to calculate a nominal average annual TSS removal over the site. This approach was used to account for the various “treatment train” elements. The site was partitioned according to surface condition and an effective average annual TSS removal rate assumed for each surface condition based on flow path and “treatment train” component(s). The effective average annual TSS removal rate was assumed based on information provided in the Low Impact Development Stormwater Management Planning and Design Guide (Credit Valley Conservation and Toronto and Region Conservation, 2010) and Wet Weather Flow Management Guidelines (City of Toronto, 2006). With this approach, each TSS removal value is multiplied by respective percent of site total area to determine the TSS removal rate for each surface condition. The sum of all TSS removal rates for each surface condition is equal to the TSS removal over the site.

Summarized in Table 3.2 are the various treatment train components and assumed average annual TSS removal rate. Provided in Table 3.3 are computations for the site average annual TSS removal. For instance, Node 1 would include treatment train components 4 and 5 per Table 3.2 resulting in an effective TSS removal of 80.0%. Based on this approach, the calculated average annual TSS removal rate for the site is 80.0%. This indicates an enhanced level of treatment can be achieved with the proposed stormwater management approach.

Table 3.2: Summary of Treatment Train Components and Assumed Average Annual TSS Removal Rate

Treatment Train Component	Treatment Train Type No.	Average Annual TSS Removal Rate
In-line Filter System	1	40%
Grassed Swale	2	80%
Roadside Ditch	3	30%
Oil/Grit Separator	4	50%
Dry Stormwater Management Pond	5	60%

Note:

1. TSS – Total Suspended Solids.
2. For assumed average annual TSS removal rates, refer to Table 5 in the Wet Weather Flow Management Guidelines (City of Toronto, 2006).
3. The “In-line Filter System” represents presence a vegetated buffer strip between the lot(s) and natural feature(s).

Table 3.3: Estimation of Site Average Annual TSS Removal

Node	Treatment Train Components	Drainage Area (ha)	Percent of Site Area	Effective TSS Removal	Overall TSS Removal
1	4,5	1.34	33.5%	80%	26.8%
2	2	0.64	16.0%	80%	12.8%
3	na	na	na	na	na
4	2	2.02	50.5%	80%	40.4%
Total	-	4.00	100%		80.0%

Note:

1. Units: ha – hectares.
2. TSS – Total Suspended Solids.
3. na – not applicable.
4. The above calculations only include the Phase 2 site. No values are included for Node 3 as this sub-basin will not be subject to development, and the area is outside of lot structure envelopes.

3.6 Stormwater Management Assessment – Water Balance

The Town of Caledon has noted that as the proposed project in an infill development, the water balance requirements can be lowered to controlling 5 millimetres (mm) of runoff rather than 27 millimetres of runoff associated with the 90th percentile rainfall event. The Town of Caledon Consolidated Linear Infrastructure ECA requirements require that LID’s be located within lands owned by the Town of Caledon. Therefore, the water balance related stormwater management criterion is retention of 5 millimetres of storm runoff on the site through infiltration/filtration, evapotranspiration, and/or reuse, and this is proposed to be achieved using Low Impact Development (LID) measures in the boulevards.

The estimated impervious area of the Phase 2 site is 3,530 square metres. This represents the driveway and roof areas of the respective proposed 5 lots. A five (5) mm depth of storm water over this area represents 17.6 cubic metres.

Two 30 metre in length bioswales with amended topsoil, filter media, and subdrain are proposed to be provided in the boulevards on Mulloy Court near the intersection with Mount Pleasant Road. Approximately 55.8 cubic metres of storage will be provided in respective bioswales. With the proposed bioswales, the retention of 5 mm of storm water on the site can be met and water balance target achieved. Design assumptions and summary computations are provided in Appendix B. Potential location and preliminary design of the LID measures are shown on the engineering drawings provided in Appendix C. The LID measures shown are preliminary and subject to detailed design at the engineering approval stage.

In addition, as far as practical, storm water from the lots will be separated from storm water from the road(s) and directed via grading and sheet flow to grassed and naturalized areas. It is recommended that grass swales, as shown on the engineering plans, be implemented in the rear lot areas draining to the wetland features in the southwest corner of the site. This is recommended for wetland water balance considerations.

In support of the project, a wetland water balance risk evaluation was completed by Ecometrix Incorporated (2026). It was identified in the wetland water balance risk evaluation that there is a low risk the proposed project would have a substantial impact on wetland hydrology (i.e., wetland feature located in the southwest corner of the property). In addition, a Design Mitigation Plan was outlined to maintain wetland water levels and water balance, and maintain wetland water quality.

3.7 Review and Discussion of Low Impact Development (LID) Options

A review was completed of Low Impact Development (LID) options for the proposed Stellar Estates Subdivision Phase 2 and opportunities for integration with the stormwater management planning. A comprehensive discussion of LID's has been provided by Credit Valley Conservation and Toronto and Region Conservation (2010) in the Low Impact Development Stormwater Management Planning and Design Guide.

The proposed stormwater management plan for the Stellar Estates Subdivision Phase 2 incorporates the following transport/conveyance controls and end-of-pipe management techniques:

- bioswales
- grassed swales
- oil/grit separator
- dry stormwater management pond

With respect to lot level controls, as far as practical, preliminary lot grading designs have directed storm water over grassed areas to adjacent open space areas versus the road network.

In general, due to the presence of low permeability soils on the site (i.e., soils with an infiltration rate less than 15 millimetres per hour), the application of infiltration type LID's is limited (i.e., soak-away pits, infiltration trenches). Applicable LID's include bioswales, grassed swales and lengthening of flow paths, vegetated filter strips, and encouragement of rainwater harvesting and application of rain gardens and soft versus hard landscaping (i.e., permeable pavers).

In addition, the re-vegetation of agricultural areas, specifically the restoration of the MVPZ area and lot areas outside of the structure envelopes, and provision of a dense vegetation cover will result in localized areas on the project site with increased infiltration and evapotranspiration (relative to existing conditions). Where storm water from the lots is directed to MVPZ areas and lots areas outside of the structure envelopes, implicitly, these respective areas will act as vegetated filter strips.

For lot level controls, from a planning and implementation perspective, there are limitations on lot coverage and percent imperviousness that is/will be enacted by Town of Caledon Official Plan zoning provisions, the zoning by-law for the project, and the ORMCP. It will be important also, during the Site Plan/Building Permit application stage, that intent of lot grading, as shown of the grading plans, is retained and LID's measures such as grassed swales and vegetated filter strips are incorporated where applicable.

4.0 Minor and Major Drainage System Design

The minor and major drainage systems for the Stellar Estates Subdivision (both Phase 1 and Phase 2) consists of the Mulloy Court existing road system, storm sewers, overland flow paths, and stormwater management facility. The drainage system has been designed to manage storm water for up to the 100-year design storm consistent with Town of Caledon Development Standards Manual (2019). Peak flows up to the 100-year design level would be contained within the municipal road right-of-way and Block 14 associated with the stormwater management pond prior to release to the environment.

The Mulloy Court storm sewer system was designed based on the 2-year design event and collects and conveys storm water to an existing oil/grit separator and subsequently the existing dry stormwater management pond in the northeast corner of the Stellar Estates Subdivision.

With Stellar Estates Phase 2, the drainage area to the existing minor and major system will increase from 0.8 hectares with a runoff coefficient of 0.40 to 2.14 hectares with a runoff coefficient of 0.34. Design calculations using the Rational Method were completed to evaluate impact on the existing minor and major systems for the 2-year and 100-year design events. The design calculations are provided in Table B.3 and Table B.4 in Appendix B.

For Phase 2, with respect the existing storm sewer system, hydraulic computations were undertaken to determine the hydraulic grade line in the storm sewer system under the 2-year design event. The United States Environmental Protection Agency (US EPA) Stormwater Management Model was setup and applied for this purpose. Results of the hydraulic analysis indicate that the storm sewer system will function under the 2-year design event without surcharging to ground level. Results of the hydraulic calculations are provided in Appendix B.

For Phase 2, due to increased contributing drainage area to the storm sewer system and existing stormwater management facility, it is proposed to replace the existing oil/grit separator with an oil/grit separator sized to accommodate Phase 2. Supporting calculations are provided in Appendix B and preliminary design information is provided on the engineering drawings in Appendix C.

Should the existing storm sewer system surcharge at Maintenance Hole 3 at the eastern end of Mulloy Court and or storm water pond at this location, there is an overland flow path (i.e., channel) to convey flow that exceeds capacity of the storm sewer system to the existing stormwater management facility. Hydraulic calculations were completed to evaluate the existing overland flow path and are provided in Table B.5 in Appendix B. Results of the hydraulic calculations indicate the existing overland flow path can convey the 100-year design event of 316.2 litres per second without exceeding the major system overland flow path (channel) hydraulic capacity of 454.4 litres per second.

Also included in Appendix B are two engineering drawings from the Stellar Estates Phase 1 project illustrating original storm sewer design calculations and design of the existing stormwater management facility and major system overland flow path.

5.0 Drainage System Operation and Maintenance Considerations

5.1 General

Listed below are operation and maintenance considerations for the drainage system and stormwater management features. Construction of the drainage works, specifically Low Impact Development (LID) features, should be scheduled and phased to ensure integrity is not compromised during construction.

1. Drainage works, stormwater management measures, and LID features be inspected on a routine basis to verify they are functioning as intended. This could include periodic inspections after major storm events to determine whether corrective actions are required. For the first two years following construction the LID features should be inspected quarterly and after major storm events. Subsequently, inspections should be conducted in the spring and fall of each year and after major storm events.
2. The drainage works and bioswales be maintained on a routine basis to remove any accumulated trash, mow grass, and remove woody material.
3. The drainage works and bioswales be inspected on a routine basis and any identified erosion, gullies, rills, or bare spots repaired.
4. With respect to the stormwater management pond, summarized in Table 5.1 are suggested routine inspection and maintenance activities, and annual spring inspection and maintenance activities. This information is adapted from Credit Valley Conservation and Toronto and Region Conservation (2010).
5. Signage be posted indicating natural or environmental protection areas, and that they are not to be disturbed or altered without authorization from the Town of Caledon or Toronto Region Conservation Authority.

In addition to the above, operation and maintenance considerations for stormwater management facilities are outlined in the Town of Caledon Development Standards Manual (2019) and Town of Caledon Consolidated Linear Infrastructure Environmental Compliance Approval (see Section 5.2).

Table 5.1: Stormwater Management Pond Inspection and Maintenance Activities

Activity/Inspection Item	Schedule/Corrective Action
Routine Inspection and Maintenance Activities	
Inspect for vegetation density, damage by foot or vehicular traffic, channelization, accumulation of debris, trash and sediment, and structural damage to either inlet or outlet works	After every major storm event, quarterly for first two years, and twice annually thereafter.
Regular watering may be required during the first two years until vegetation established.	As needed for the first two years of operation.
Remove trash and debris on the stormwater management pond surface, and inlets and outlets.	At least twice annually. More frequently if desired for aesthetic reasons.
Remove accumulated sediment from inlet/outlet areas, remove accumulated sediment in stormwater management pond, trim trees and shrubs, replace vegetation and remove invasive growth, repair eroded or sparsely vegetated areas.	Annually or as needed.
Annual Inspection Items and Corrective Actions	
Vegetation health, diversity, and density.	Remove dead and diseased plants, add reinforcement planting to maintain desired vegetation density, prune woody matter, check soil pH for specific vegetation, add mulch to maintain 25 mm layer if applicable.
Sediment build-up and clogging of inlets/outlets.	Remove sand that may accumulate at the inlets/outlets or on the surface following snow melt, examine the contributing drainage area for bare soil and stabilize accordingly, check that pre-treatment device or measures are properly functioning.
Ponding for more than 48 hours.	Check outlet piping for clogging and flush out or remove debris.

5.2 Town of Caledon Consolidated Linear Infrastructure Environmental Compliance Approval

It is specified in the Town of Caledon Consolidated Linear Infrastructure Environmental Compliance Approval that Sewage Works are operated with the objective that the effluent from the Sewage Works is essentially free of floating and settleable solids and does not contain oil or any other substance in amounts sufficient to create a visible film, sheen, foam, or discoloration

on the receiving waters, and the Operator shall evaluate the need for maintenance if the objective is not being met.

In this regard, the Applicant is to ensure that at all times, the Authorized Alteration shall be:

- Operated in accordance with the requirements under the EPA and OWRA; and
- Maintained in a state of good repair.

The Applicant shall develop an Operation and Maintenance Plan as part of Preliminary Acceptance, to be approved by the Town, that will be followed throughout the period from Preliminary Acceptance to Assumption by the Applicant, and will be provided to the Town as part of Assumption. The O&M plan should include the inspections described below: The applicant may be required to undertake the following for stormwater management facilities:

- Inspections of the Authorized Alteration is to be conducted at a frequency of once per month following Preliminary Acceptance and up to Assumption;
- Inspection of the Authorized Alteration are to be conducted prior to all rainfall events greater than and including 10 mm over 12 hours;
- Inspection of the Authorized Alteration are to be conducted within 48 hours following events up to and including 10 mm over 12 hours;
- Inspection of the Authorized Alteration is to be conducted prior to significant snowmelt events;
- Inspection of the Authorized Alteration is to be conducted within 48 hours following significant snowmelt events;
- All stormwater Management Facilities shall be inspected after significant flooding events; and
- Any deficiencies shall be addressed within 48 hours or as soon as possible within reason to the satisfaction of the Town.

In addition to the above, the Applicant or Operator shall maintain records of the results of the inspections, cleaning and maintenance operations undertaken. The records shall include the following:

- Asset ID and name of the Sewage Works;
- Date and results of each inspection, maintenance, or cleaning;
- Name of person who conducted the inspection, maintenance, or the name of the inspecting official, where applicable; and

- As applicable to the type of works, observations resulting from the inspection including, at a minimum:
 - Hydraulic operation of the works (e.g., length of occurrence since the last rainfall event, evidence or occurrence of overflows).
 - Condition of vegetation in and around the work.
 - Occurrence of obstructions at the inlet and outlet of the works.
 - Evidence of spills and/or oil/grease contamination.
 - Presence of trash build-up, and
 - Measurements of other Parameters as required by the monitoring plan

Inspection forms as well as maintenance and cleaning records are to be provided to the Town within 48 hours of having been completed.

6.0 Sanitary and Water Servicing Plan

The proposed Stellar Estates Subdivision Phase 2 will be serviced with municipal water and private on-site sewage disposal systems. Consistent with Section 44 (4) of the Oak Ridges Moraine Conservation Plan (ORMCP), the construction of partial services is permitted within the Palgrave Estates Residential Community. Section 43 of the ORMCP requires that water and sewage services maintain the ecological integrity of hydrological features and key natural heritage features, maintain quantity and quality of groundwater and surface water, maintain stream baseflows, comply with the applicable watershed plan and water budget and conservation plan, that the water use projected for the development will be sustainable, and that water and service trenches be planned designed and constructed so as to keep disruption of natural groundwater flow to a minimum.

The Regional Municipality of Peel Official Plan requires that proposals for water infrastructure within or crossing areas designated as Protected Countryside demonstrate that:

- servicing can be provided in a manner that does not negatively impact ecological features and functions, quality and quantity of ground and surface water, including stream baseflow, and is sufficient to accommodate the proposed use;
- applicable recommendations, standards or targets within watershed plans and water budgets are reflected; and
- any sewage and water servicing installation is planned, designed and constructed to minimize surface and groundwater disruption.

The sanitary and water servicing plan for the proposed Stellar Estates Subdivision Phase 2 is consistent with these policies. For instance, the site water balance has been considered, proposed services are shallow in depth and comprise only water services to proposed dwellings as municipal infrastructure was constructed as part of Phase 1, and the project will not impact the local and regional groundwater regime.

6.1 Sanitary Servicing Plan

Consistent with Section 7.1.8.1 of the Town of Caledon Official Plan, sanitary servicing for the proposed subdivision will be by private individual on-site sewage disposal systems (e.g., septic systems) conforming to the Ontario Building Code. Subject to detailed design at the Building Permit application stage, it is anticipated that on-site sewage disposal systems would comprise a septic tank(s) sized at twice the daily design flow, effluent filter, tertiary treatment unit, dispersal bed, and ancillary piping, pumping system(s), and controls. A tertiary treatment unit is anticipated to be required to fit the respective dispersal bed within the lot structure envelope in conjunction with the dwelling and driveway features. Alternative tertiary treatment units can be found in Supplementary Standard SB-5, Approved Treatment Units, of the Ontario Building Code.

Provided in Appendix C is a grading plan for the Phase 2 site with preliminary sitings of the dwellings and dispersal beds. As shown, the dispersal beds have been sited on lands within

structure envelopes where the slope is less than 10% consistent with Section 7.1.9.11 of the Town of Caledon Official Plan. It should be noted that the maximum slope for siting of dispersal or leaching beds, per the Ontario Building Code, is 25% (i.e., 4 horizontal to 1 vertical). Section 7.1.9.32 of the PERCSP identifies that sewage disposal systems will be normally located a minimum of 30 metres from any pond or stream to minimize nutrient enrichment. Proposed preliminary sitings for dispersal beds associated with sewage disposal systems are consistent with this policy. Supporting nutrient loading computations have been provided by Ecometrix Incorporated (2025).

The septic system dispersal bed sizes shown on the grading plan is based on the following assumptions:

- the lots will be serviced with a dispersal bed contact area of 500 square metres or less (an area of 500 square metres is shown on the engineering plans provided in Appendix E); and
- in-situ soil percolation rate or `T` time is greater than 50 minutes per centimeter.

With a typical tertiary treatment system, a dispersal bed with a contact area of 500 square metres and in-situ soil percolation rate or `T` time of greater than 50 minutes per centimeter can accommodate a maximum daily design flow of 4,000 litres per day.

By way of example, a maximum daily design flow of 4,000 litres per day is representative of an approximately 400 square metre (4,306 square foot) home with four bedrooms. This is consistent with the size of homes anticipated for the proposed subdivision.

Detailed engineering design of the on-site sewage disposal will be undertaken at the Building Permit application stage and reflect site specific soil conditions and house designs. Detailed design of the on-site sewage disposal systems would be in general conformance with the Ontario Building Code.

6.2 Water Servicing Plan

6.2.1 Water Demand

The proposed subdivision comprises 5 estate residential lots. The estimated water demand is summarized in Table 6.1.

Table 6.1: Estimated Water Demand for the Stellar Estates Subdivision Phase 2

Population Type	Number of Units	Population Density (per Unit)	Average Consumption Rate (L/cap/day)	Subdivision Average Day Consumption (L/day)	Subdivision Max. Day Consumption (L/day)	Subdivision Peak Hour Consumption (L/day)
Residential	5	4.202	280	6,160	12,320	18,480

Note:

1. Units: L/cap/day – litres per capita per day; L/day – litres per day.
2. Consumption values determined by rounding the total subdivision population to 22 people.
3. Maximum Day Consumption based on a maximum day factor of 2.0 multiplied by Average Day Consumption.
4. Peak Hour Consumption based on a peak hour factor of 3.0 multiplied by Average Day Consumption.

6.2.2 Water Supply and Distribution

The Stellar Estates Subdivision Phase 2 will be serviced by municipal water. There is an existing 200-millimetre diameter watermain located on the north side of Mulloy Court. The 200-millimetre diameter watermain on Mulloy Court is connected to a 300-millimetre watermain on Mount Pleasant Road and located in Region of Peel Water Pressure Zone PG8. The proposed 5 lots would be serviced by connection to the existing 200-millimetre diameter watermain on Mulloy Court.

6.2.3 Water Services

All water services will be single service connections that are supplied and installed in general conformance with the Region of Peel Public Works Design, Specifications and Procedures Manual, Linear Infrastructure, Watermain Design Criteria (2010). The proposed water service size is 38 millimetres: a minimum 25-millimetre (mm) water service is required per Region of Peel design criteria for lots exceeding 500 square metres in area.

6.2.4 Fire Flow

The fire flow was estimated using “Water Supply for Public Fire Protection” prepared by the Fire Underwriters Survey (1999) and based on the assumption of a single-family dwelling with a gross floor area of 400 square metres and assumption of two adjacent dwellings at a horizontal separation distance of 15 metres.

The required fire flow associated with the Phase 2 development was estimated to be 95.3 litres per second (L/s). Supporting calculations are provided in Appendix B.

7.0 Roadway and Grading

7.1 General Description and Location

The proposed five lots will front on to and have driveway access from Mulloy Court. Mulloy Court is accessed from Mount Pleasant Road. The respective driveways will be designed and sited in general conformance with the Town of Caledon Development Standards Manual (2019) and applicable zoning bylaws.

7.2 Road Design

At the time of writing of this report, Mulloy Court has been constructed to base course asphalt and has not been assumed by the Town of Caledon. The Phase 1 construction of Mulloy Court included the curbs along the Phase 2 site.

8.0 Erosion and Sediment Control

8.1 General

At the engineering approval stage, erosion and sediment control plans will be prepared consistent with the Town of Caledon Development Standards Manual (2019), Town of Caledon Consolidated Linear Infrastructure Environmental Compliance Approval, and the Erosion & Sediment Control Guideline for Urban Construction prepared by the Toronto and Region Conservation Authority (2019). At this stage, a preliminary Erosion and Sediment Control Plan has been prepared and is provided in Appendix C. For project construction, the key items will be limiting construction activities to defined working areas, managing water from dewatering activities, and managing surface runoff. Summarized in Table 8.1 are general procedures and mitigation measures to be implemented to avoid impacts.

In addition to the above, supporting studies and reports will be provided at the detailed design stage related to erosion and sediment control and topsoil management, such as:

- Erosion and Sediment Control Report
- Topsoil and Soils Management Plan

The Topsoil and Soils Management Plan would include requirements for pedologist soil analysis for all soils to be stored on site, including nutrient, contaminants and composition.

Table 8.1: General Procedures and Mitigation Measures for Erosion and Sediment Control

Principle No.	Description
1	Install temporary sediment controls prior to the start of construction per the typical details on the Erosion and Sediment Control Plan.
2	Delineate the working area prior to the start of construction and confine operations to the defined area.
3	Enclose temporary topsoil and soil material stockpile areas with sediment control fence.
4	Maintain construction accesses, working areas, and temporary material storage areas in good repair.
5	Operate machinery in a manner that minimizes disturbance to the environment: <ul style="list-style-type: none"> - protect entrances at machinery access points (e.g., using mud mats/rock pads) - establish single site entry and exit points. - construction equipment and machinery to arrive on site in a clean condition - construction equipment to be maintained free of fluid leaks. - no equipment operation on the streambed and in flowing water - wash, refuel and service machinery in designated areas away from water bodies - store fuel and other materials in designated areas away from water bodies - keep an emergency spill kit on site in case of fluid leaks or spills
6	Inspect, maintain, and repair sediment controls until completion of construction and site restoration.

7	Keep additional erosion and sediment control materials, such as sediment control fencing and clear stone, on-site for emergencies and repairs.
8	Remove and dispose temporary sediment controls following completion of construction and site restoration
9	Vegetate any disturbed areas by planting and seeding preferably with native grasses and cover such areas with mulch to prevent soil erosion and to help seeds germinate. If there is insufficient time remaining in the growing season, the site should be stabilized (e.g., cover exposed areas with mulch, straw, or erosion control blankets to keep the soil in place and prevent erosion) and vegetated the following growing season.

8.2 Emergency Contact Information

As part of the erosion and sediment control planning process, emergency contact numbers would be provided on the project engineering drawings, and a contact list kept on-site and be readily available. An example emergency contact list is provided in Table 8.2. The applicable contacts would be confirmed and updated, as required, at the construction stage.

Table 8.2: Erosion and Sediment Control Plan Emergency Contact List

Name/Agency	Phone Number
Town of Caledon	(905) 584-2272
Toronto and Region Conservation Authority	(416) 661-6600
Ministry of the Environment, Conservation and Parks Spills Reporting	(416) 325-3000 or 1-800-268-6060
Owner – Stellar Homes Inc..	(905) 726-7778
Project Engineer – Ecometrix Incorporated	(905) 794-2325

9.0 Utility Services

It is proposed that gas and communication utilities will be provided for the Stellar Estates Subdivision Phase 2 by connection to existing utilities available either along Mulloy Court or along Mount Pleasant Road.

Electrical power to the site will be provided by connection to existing Hydro One power infrastructure on Mulloy Court. No new street lights will be required for the project.

10.0 Summary

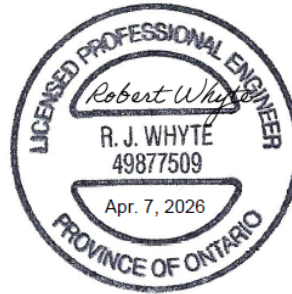
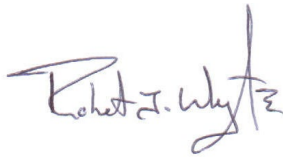
1. Ecometrix Incorporated, an Egis Group company, has been retained by Stellar Homes Inc. to prepare a Preliminary Functional Servicing and Stormwater Management Report for the proposed second phase of the Stellar Estates Subdivision (Phase 2). This report is supporting documentation for the Draft Plan of Subdivision application for Phase 2.
2. The site is in the Palgrave Estates area of the Town of Caledon on Mulloy Court. Mulloy Court is west of Mount Pleasant Road between Old Church Road and Castleberg Side Road. The site is bounded by Mount Pleasant Road to the east, Mulloy Court and existing estate residential development to the north and west (Stellar Estates Subdivision herein denoted as Phase 1; Registered Plan 43M-1994), and agricultural land to the south. The legal description of the property is Part of Lot 18, Concession 8, former Township of Albion, Town of Caledon, Regional Municipality of Peel.
3. The Phase 2 site comprises approximately 4.10 hectares or 10.13 acres. It is proposed to develop the site with 5 estate residential lots using private septic systems for sewage disposal systems and municipal water. All 5 lots would front on to Mulloy Court. Mulloy Court was constructed in 2013/2014 with an urban road cross-section and comprises 10 estate residential lots serviced with private septic systems and municipal water. The Stellar Estates Subdivision Phase 1 (Registered Plan 43M-1994) has not been assumed as of the writing of this report. Currently, the 10 lots associated with the Stellar Estates Subdivision Phase 1 have either constructed and occupied dwellings or dwellings under construction. Drainage and stormwater for the proposed Phase 2 site would be managed with existing infrastructure and application of Low Impact Development (LID) practices.
4. Drainage Storm water from the site is proposed to be managed using both conventional stormwater management techniques and Low Impact Development (LID) practices.
5. Consistent with Section 7.10.6.9.2 of the Town of Caledon Official Plan, the proposed stormwater management strategy comprises a “treatment train” approach utilizing a combination of lot level controls, Low Impact Development (LID) measures, and conventional stormwater management techniques to minimize potential increases in peak flows and runoff volume, maintain water quality, and provide, as far as practical, a natural hydrologic response. Measures are proposed to be undertaken at the source, and conveyance and end of pipe locations, and are as follows:
 - recharge of residential roof and driveway storm water by direction to grassed and naturalized areas to promote filtering and natural infiltration and evapotranspiration;
 - discharge of foundation drain water to rear and side lot areas;

- by lot grading, as far as practical, direction of structure envelope drainage, via sheet flow, towards grassed and naturalized areas versus the municipal road right of way;
 - application of Low Impact Development practices both in the boulevards and on the lots such as bioswales and grassed swales;
 - use of an oil/grit separator where road drainage is to a stormwater management pond; and
 - use of an existing dry stormwater management pond to temporarily detain and slowly release storm water to meet applicable stormwater management criteria.
6. Hydrologic modelling and “desk-top” assessments were performed to develop and evaluate the proposed Stormwater Management Plan. Based on the respective technical analyses, proposed stormwater management criteria for quantity control, quality control, erosion control, and water balance can be achieved.
 7. The minor and major drainage system will consist of the existing Mulloy Court road system and storm sewers. The drainage system was designed to manage storm water for up to the 100-year design storm consistent with Town of Caledon Development Standards Manual (2019) and Toronto and Region Conservation stormwater management criteria. Peak flows up to the 100-year design level would be contained within the municipal road right-of-way and stormwater management pond prior to release to the environment. The Mulloy Court storm sewer system was designed based on the 2-year return period event and collects and conveys storm water to an existing oil/grit separator and subsequently the existing dry stormwater management pond.
 8. Sanitary servicing for the proposed subdivision will be by individual on-site sewage disposal systems (e.g., septic systems).
 9. The Stellar Estates Subdivision Phase 2 will be serviced by municipal water. There is an existing 200-millimetre diameter watermain located on the north side of Mulloy Court. The proposed 5 lots would be serviced by connection to the existing 200-millimetre diameter watermain.

10. Considerations are provided for erosion and sediment control planning and erosion and sediment control plans have been prepared for the project. Erosion and sediment control planning would be undertaken consistent with the Town of Caledon Development Standards Manual (2019), Town of Caledon Consolidated Linear Infrastructure Environmental Compliance Approval, and the Erosion & Sediment Control Guideline for Urban Construction prepared by the Toronto and Region Conservation Authority (2019).

Respectfully submitted,

Ecometrix



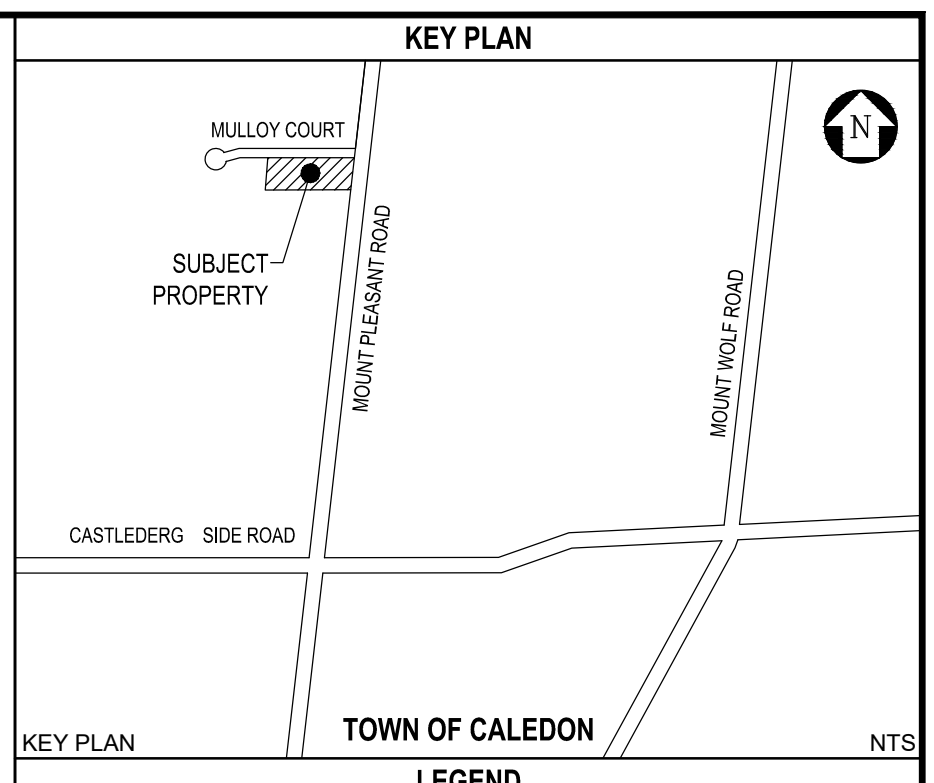
Robert Whyte, M.Sc., P.Eng.
Senior Consultant

11.0 References

- Chapman L.J. and Putnam D.F. 1984. Physiography of Southern Ontario; Ontario Geological Survey, Map P.2715 (coloured). Scale 1: 600 000.
- City of Toronto. 2006. Wet Weather Flow Management Guidelines. November 2006.
- Credit Valley Conservation and Toronto and Region Conservation. 2010. Low Impact Development Stormwater Management Planning and Design Guide. Version 1.0.
- Ecometrix Incorporated. 2025. Hydrogeological Assessment for Stellar Estates Phase 2, Town of Caledon, Ontario. Report prepared for Stellar Homes Inc., January 17, 2025.
- Ecometrix Incorporated. 2026. Wetland Water Balance Risk Evaluation – Hydrologic Screening, Stellar Estates Subdivision Phase 2, 0 Mount Pleasant Road, Town of Caledon, Ontario. Report prepared for Stellar Homes Inc., April 7, 2026.
- Fire Underwriters Survey. 1999. Water Supply For Public Fire Protection.
- GeoTerre Limited. 2024. Geotechnical Investigation Report Proposed Residential Development Stellar Estates – Phase 2 Caledon, Ontario. Report prepared for Ecometrix Incorporated, January 24, 2024
- Ministry of Environment. 2003. Stormwater Management Practices Planning and Design Manual. March 2003.
- Ministry of Municipal Affairs and Housing. 2014. Provincial Policy Statement. Provincial Policy Statement issued under section 3 of the Planning Act, Ministry of Municipal Affairs and Housing, Provincial Planning Policy Branch.
- Ministry of Transportation. 1997. MTO Drainage Management Manual. Drainage and Hydrology Section, Transportation Engineering Branch, Quality and Standards Division.
- Region of Peel. 2010. Public Works Design, Specifications and Procedures Manual, Linear Infrastructure, Watermain Design Criteria. Revised June 2010.
- Toronto and Region Conservation Authority. 2008. Humber River State of the Watershed Report – Geology and Groundwater Resources
- Toronto and Region Conservation Authority. 2022. Humber River.
<https://trca.ca/conservation/watershed-management/humber-river/>. Accessed August 17, 2022.
- Toronto and Region Conservation. 2012. Stormwater Management Criteria. August 2012, Version 1.0.

- Toronto and Region Conservation. 2019. Erosion & Sediment Control Guideline for Urban Construction. 2019.
- Town of Caledon. 2015. Town of Caledon Official Plan. November 2015 Consolidation.
- Town of Caledon. 2019. Development Standards Manual, Town of Caledon. Prepared by the Town of Caledon, Version 5.0.
- White, O.L. 1973. Bedrock topography, Bolton, Southern Ontario. Ministry of Northern Development, Mines, Natural Resources and Forestry. Map M2276, Scale 1:63,360.
- White, O.L. 1975. Quaternary Geology of the Bolton Area, Southern Ontario. Ontario Division of Mines, Geological Report 117.
- White, O.L. and P.F. Karrow. 1973. Quaternary geology, Bolton, Southern Ontario. Ministry of Northern Development, Mines, Natural Resources and Forestry. Map M2275, Scale 1:63,360

Appendix A Figures and Maps



- LEGEND**
- PROPERTY LINES (PROPOSED)
 - PROPERTY LINES (EXISTING)
 - KEY NATURAL HERITAGE FEATURE
 - LIMIT OF PROP. STRUCTURE ENVELOPE
 - PROP. GRASSED SWALE
 - PROP. ENHANCED GRASS SWALE, MIN. 30.0m / LOT
 - MVPZ REHABILITATION PLANTINGS
 - LOT AREA OUTSIDE STRUCTURE ENVELOPE
 - STREETLIGHT POLE
 - ▲ HYDRO ONE TRANSFORMER
 - B#H 2007 BOREHOLES
 - BH22-# 2022 BOREHOLES
 - ① EX. STOP SIGN
 - ② EX. STREET SIGN
 - ③ EX. NO EXIT SIGN
 - MIN. 56 sq.m BACKYARD AMENITY AREA (CONCEPT PLAN)
- REFER TO GENERAL NOTES AND SPECIFICATIONS ON DWG 22-3001-10

LEGAL DESCRIPTION
 PART OF LOT 18, CONCESSION 8 AND BLOCK 15,
 PLAN 43M-1994 (GEOGRAPHIC TOWNSHIP OF ALBION)
 TOWN OF CALEDON
 REGIONAL MUNICIPALITY OF PEEL



DESIGNED BY		APPROVED BY	

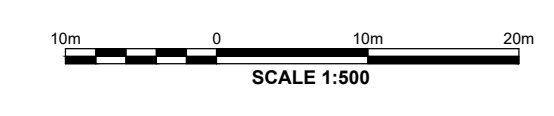
N ^o	Date	Revisions	Dwn.	Dsg'd.	Chk'd.
③	07/APR/2026	FOURTH SUBMISSION	AAF	AAF	RJW
②	21/NOV/2025	THIRD SUBMISSION	AAF	AAF	RJW
①	17/JAN/2025	SECOND SUBMISSION	AAF	AAF	RJW
①	26/JAN/2024	DPA APPLICATION	AAF	AAF	RJW

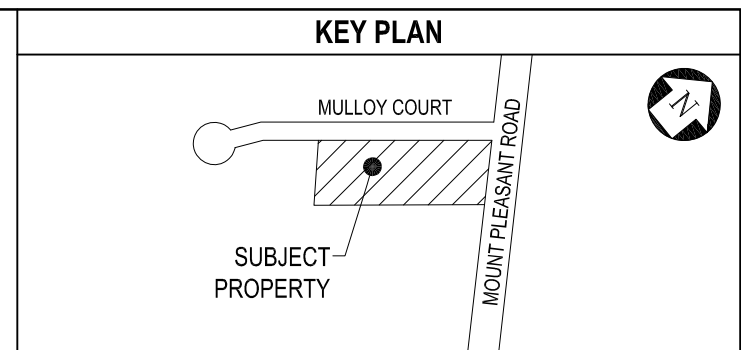
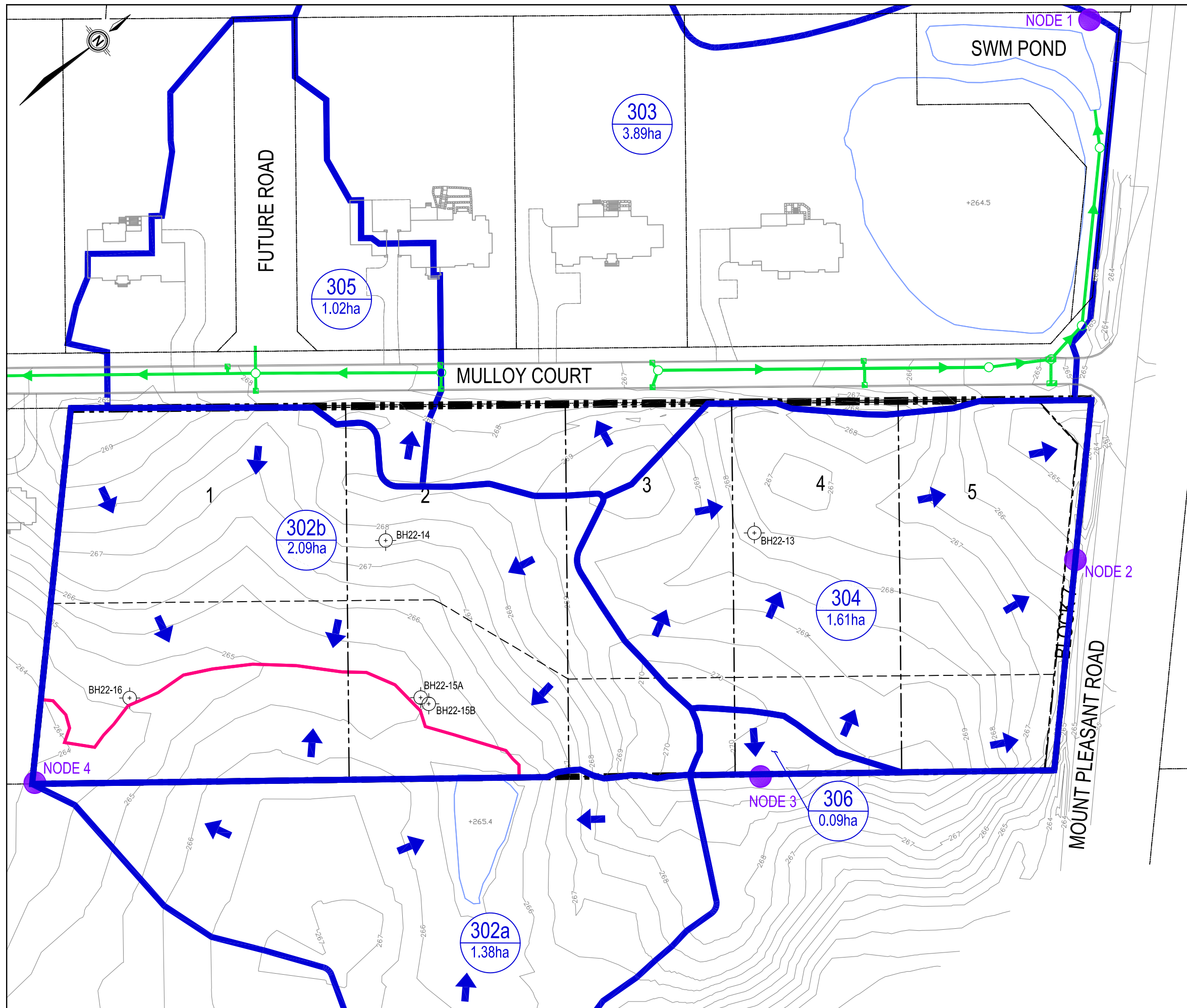
Client: **STELLAR HOMES INC.**

Project Name: **STELLAR ESTATES PHASE 2
MULLOY COURT, TOWN OF CALEDON**

Title Name: **SITE PLAN**

Drawing N^o: **22-3001-01** Sheet N^o: **1 OF 10** Rev. N^o: **3**
 Scale: **1:500**





LEGEND

	SITE BOUNDARY
	ORMCP KEY NATURAL HERITAGE FEATURE
	WATER BODY
	CONTOUR (0.5m INTERVAL)
	MONITORING WELL LOCATION
	DRAINAGE BOUNDARY
	SUB-CATCHMENT ID SUB-CATCHMENT AREA (ha)
	EXISTING STORM SEWER AND FLOW DIRECTION
	MAJOR FLOW DIRECTION
	FLOW NODE
	E2Z AREAS

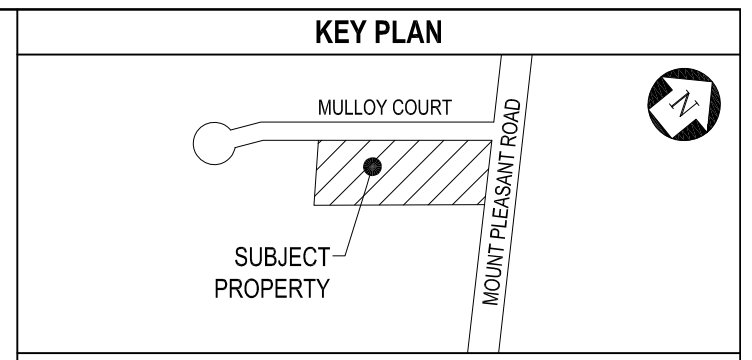
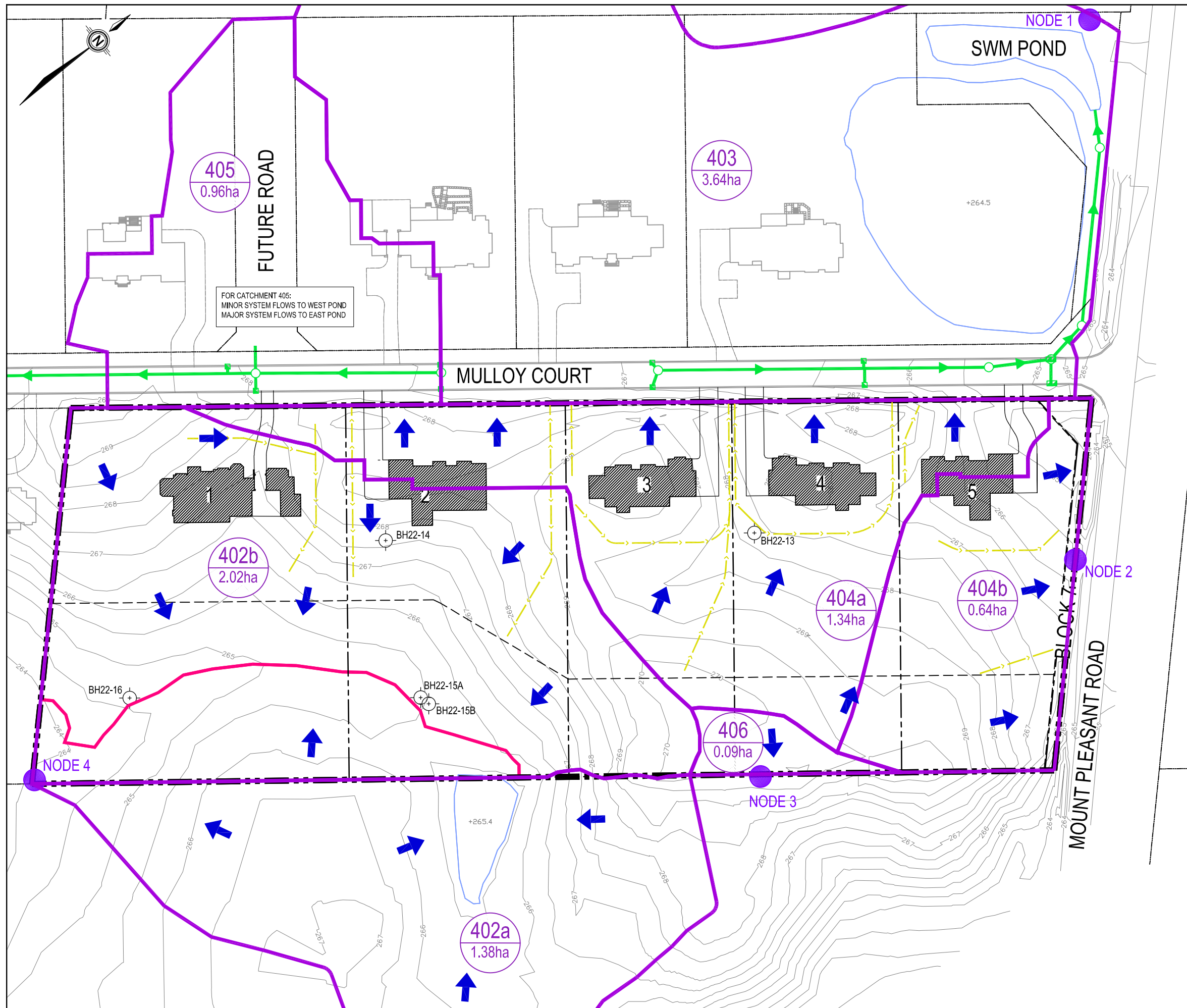
30m 0 30m 60m
SCALE 1:1250

- ### NOTES
1. CONTOURS WITHIN PROPERTY LIMITS GENERATED FROM SURVEYED ELEVATIONS BY ECOMETRIX INCORPORATED (2021). CONTOURS SOUTH OF PROPERTY LIMIT FROM FIRST BASE SOLUTIONS. ACTUAL ELEVATIONS MAY VARY FROM THOSE SHOWN.
 2. CONTOUR INTERVAL IS 0.5m.
 3. FEATURE LOCATIONS (e.g. TREELINES, BUILDINGS, ETC.) ARE APPROXIMATE.

Ecometrix | Environmental INTELLIGENCE
www.ecometrix.ca

STELLAR HOMES INC.
STELLAR ESTATES PHASE 2
PART OF LOT 18, CONCESSION 8 (ALBION)
TOWN OF CALEDON, REGION OF PEEL

MAP 5
SURFACE HYDROLOGY MAP



LEGEND

- SITE BOUNDARY
- ORMCP KEY NATURAL HERITAGE FEATURE
- WATER BODY
- CONTOUR (0.5m INTERVAL)
- MONITORING WELL LOCATION
- DRAINAGE BOUNDARY
- SUB-CATCHMENT ID
SUB-CATCHMENT AREA (ha)
- EXISTING STORM SEWER AND FLOW DIRECTION
- MAJOR FLOW DIRECTION
- FLOW NODE
- E2Z AREAS
- PROPOSED GRASS SWALE

30m 0 30m 60m
SCALE 1:1250

- ### NOTES
1. CONTOURS WITHIN PROPERTY LIMITS GENERATED FROM SURVEYED ELEVATIONS BY ECOMETRIX INCORPORATED (2021). CONTOURS SOUTH OF PROPERTY LIMIT FROM FIRST BASE SOLUTIONS. ACTUAL ELEVATIONS MAY VARY FROM THOSE SHOWN.
 2. CONTOUR INTERVAL IS 0.5m.
 3. FEATURE LOCATIONS (e.g. TREELINES, BUILDINGS, ETC.) ARE APPROXIMATE.

Ecometrix | Environmental INTELLIGENCE
www.ecometrix.ca

STELLAR HOMES INC.

STELLAR ESTATES PHASE 2
PART OF LOT 18, CONCESSION 8 (ALBION)
TOWN OF CALEDON, REGION OF PEEL

MAP 6

PROPOSED DRAINAGE BOUNDARY MAP

Appendix B Stormwater Management Calculations

Table B.1
STELLAR HOMES ESTATES PHASE 2, SWMHYMO PARAMETERS
EXISTING CONDITIONS

NASHYD PARAMETERS

Catchment ID	NHYD ID	DT min	Area ha	DWF cms	CN/C Group	Weighted CN	IA mm	N	TP hrs
303	303	1	3.89	0	CD	82	10	3	0.32
305	305	1	1.02	0	CD	84	10	3	0.19
304	304	1	1.61	0	CD	83	10	3	0.23
306	306	1	0.09	0	CD	83	10	3	0.11
302a	302a	1	1.38	0	CD	74	10	3	0.23
302b	302b	1	2.09	0	CD	81	10	3	0.30

Notes:

1. Reference: MTO Design Chart 1.09: Soil/Land Use Curve Numbers
2. Time to Peak (TP) was calculated using Airport Method. TP=2/3 of Time of Concentration.

Table B.2
STELLAR HOMES ESTATES PHASE 2, SWMHYMO PARAMETERS
PROPOSED CONDITIONS:

NASHYD PARAMETERS

Catchment ID	NHYD ID	DT min	Area ha	DWF cms	CN/C Group	Weighted CN	IA mm	N	TP hrs
403	403	1	3.64	0	CD	82	10	3	0.32
405	405	1	0.96	0	CD	84	10	3	0.19
404a	404a	1	1.34	0	CD	83	10	3	0.17
404b	404b	1	0.64	0	CD	80	10	3	0.20
406	406	1	0.09	0	CD	76	10	3	0.11
402a	402a	1	1.38	0	CD	74	10	3	0.23
402b	402b	1	2.02	0	CD	78	10	3	0.30

Notes:

1. Reference: MTO Design Chart 1.09: Soil/Land Use Curve Numbers
2. Time to Peak (TP) was calculated using Airport Method. TP=2/3 of Time of Concentration.

Table B.2A
STELLAR HOMES PHASE 2, WEIGHTED CN VALUES

NASHYD PARAMETERS

EXISTING CONDITIONS:

Catchment	NHYD	total Nashyd area (ha)	Impervious (ha)	Pervious manicured (ha)	Pervious field (ha)	Pervious naturalized (ha)	Pervious woods/bush (ha)	Impervious CN	Pervious manicured CN	Pervious field CN	Pervious naturalized CN
303	303	3.89	0.45	3.44	0.00	0.00	0.00	98	80	83	76
305	305	1.02	0.21	0.81	0.00	0.00	0.00	98	80	83	76
304	304	1.61	0.00	0.00	1.61	0.00	0.00	98	80	83	76
306	306	0.09	0.00	0.00	0.09	0.00	0.00	98	80	83	76
302a	302a	1.38	0.00	0.00	0.00	0.00	1.38	98	80	83	76
302b	302b	2.09	0.00	0.00	1.66	0.00	0.43	98	80	83	76

PROPOSED CONDITIONS:

Catchment	NHYD	total Nashyd area (ha)	Impervious (ha)	Pervious manicured (ha)	Pervious field (ha)	Pervious naturalized (ha)	Pervious woods/bush (ha)	Impervious CN	Pervious manicured CN	Pervious field CN	Pervious naturalized CN
403	403	3.64	0.46	3.18	0.00	0.00	0.00	98	80	83	76
405	405	0.96	0.21	0.75	0.00	0.00	0.00	98	80	83	76
404a	404a	1.34	0.21	1.05	0.00	0.08	0.00	98	80	83	76
404b	404b	0.64	0.03	0.41	0.00	0.20	0.00	98	80	83	76
406	406	0.09	0.00	0.00	0.00	0.09	0.00	98	80	83	76
402a	402a	1.38	0.00	0.00	0.00	0.00	1.38	98	80	83	76
402b	402b	2.02	0.10	0.84	0.00	0.66	0.43	98	80	83	76

Notes:

1. Assumed hydrologic Soils group is CD, legumes or rotation meadows with good drainage, where CN range is = 81 to 85
Reference: MTO Design Chart 1.09: Soil/Land Use Curve Numbers
2. Units: ha-hectares; sq.m-square meters.

**TABLE B.3
2-YEAR STORM SEWER DESIGN SHEET**

Location			Drainage Area				Runoff			Pipe Flow						
Catchment	From MH	To MH	A (ha)	C	A x C	Acc. x C	Tc (min)	I (mm/hr)	Q (L/s)	Pipe Length (m)	Pipe Diameter (m)	Pipe Slope (%)	Full Flow Capacity (L/s)	Full Flow Velocity (m/s)	Time of flow (min.)	% full
A	MH1	MH2	0.6500	0.40	0.26	0.26	15.58	67.55	48.78	108.0	0.300	0.93	93.3	1.32	1.36	52.3%
B + 404a	MH2	CBMH3	1.4900	0.31	0.46	0.72	16.94	64.28	128.90	20.0	0.375	0.30	96.0	0.87	0.38	134.2%
	CBMH3	MH4	0.0000	0.00	0.00	0.72	17.33	63.42	127.18	15.5	0.375	0.30	96.0	0.87	0.30	132.4%
	MH4	MH5	0.0000	0.00	0.00	0.72	17.62	62.77	125.88	58.0	0.375	0.30	96.0	0.87	1.11	131.1%
	MH5	OUTFALL	0.0000	0.00	0.00	0.72	18.74	60.47	121.25	7.0	0.375	0.30	96.0	0.87	0.13	126.3%

Project Notes:
 1. Refer to Phase 1 engineering drawings for Catchment A and Catchment B.
 2. Surcharged flow at CBMH3 to be conveyed by existing major system overflow channel to existing stormwater management facility in Stellar Estates Phase 1 Block 14.
 3. Assumed runoff coefficient for Catchment 404a is 0.30.

Manning's n = 0.013
 Storm Event: 2 year
 where:
 A= 1070
 B= 7.85
 C= 0.8759

$$I = \frac{A}{(t_c + B)^C}$$

PROJECT: Stellar Estates Phase 2, Town of Caledon
 PROJECT No: Ecometrix: 22-3001
 CLIENT: Stellar Homes Inc.



**TABLE B.4
100-YEAR STORM SEWER DESIGN SHEET**

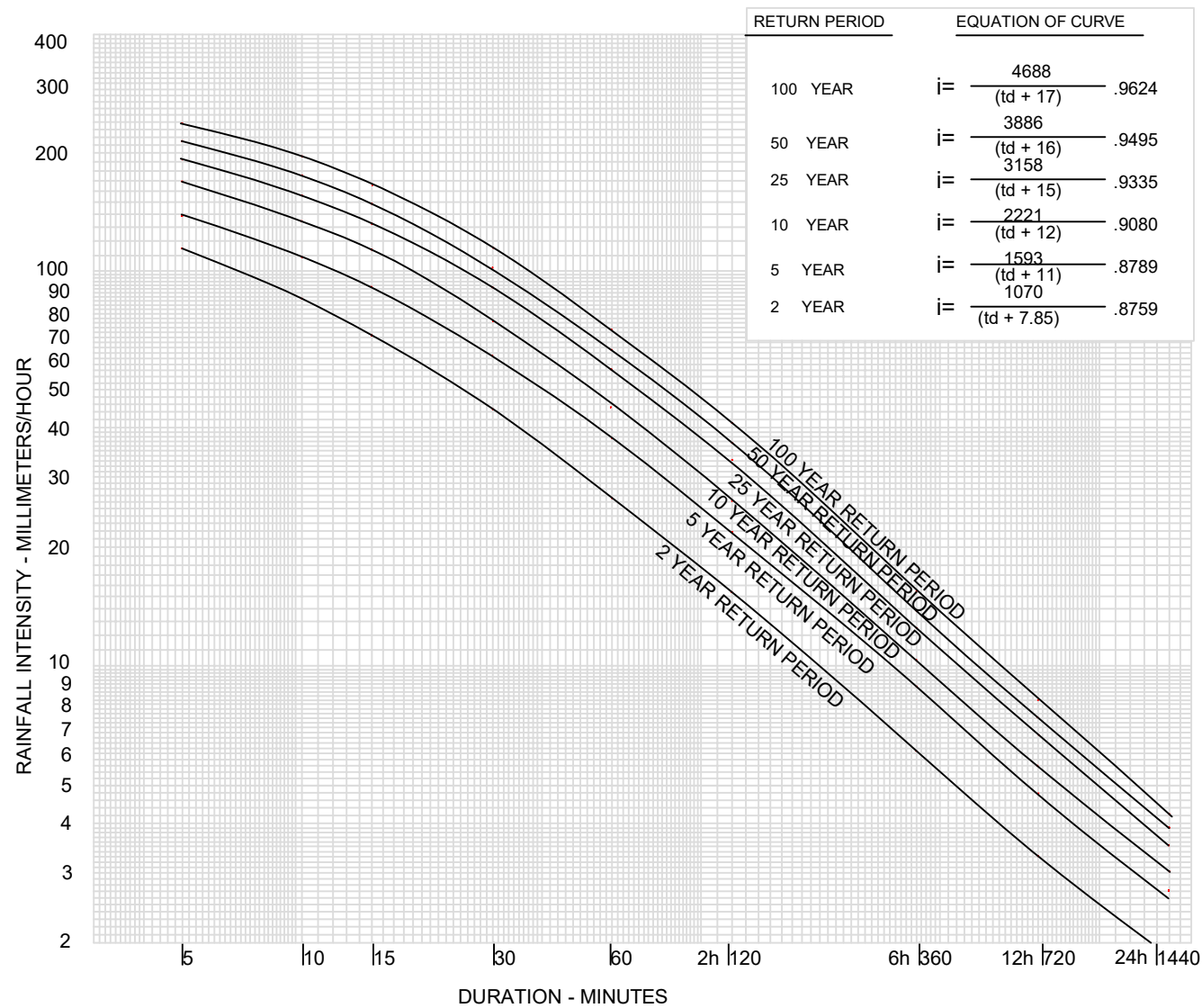
Location		Drainage Area				Runoff			Pipe Flow							
Catchment	From MH	To MH	A (ha)	C	A x C	Acc. x C	Tc (min)	I (mm/hr)	Q (L/s)	Pipe Length (m)	Pipe Diameter (m)	Pipe Slope (%)	Full Flow Capacity (L/s)	Full Flow Velocity (m/s)	Time of flow (min.)	% full
A	MH1	MH2	0.6500	0.40	0.26	0.26	15.58	164.03	118.47	108.0	0.300	0.93	93.3	1.32	1.36	127.0%
B + 404a	MH2	CBMH3	1.4900	0.31	0.46	0.72	16.94	157.68	316.19	20.0	0.375	0.30	96.0	0.87	0.38	329.3%
	CBMH3	MH4	0.0000	0.00	0.00	0.72	17.33	155.98	312.79	15.5	0.375	0.30	96.0	0.87	0.30	325.7%
	MH4	MH5	0.0000	0.00	0.00	0.72	17.62	154.70	310.21	58.0	0.375	0.30	96.0	0.87	1.11	323.0%
	MH5	OUTFALL	0.0000	0.00	0.00	0.72	18.74	150.06	300.92	7.0	0.375	0.30	96.0	0.87	0.13	313.3%

Project Notes:
 1. Refer to Phase 1 engineering drawings for Catchment A and Catchment B.
 2. Surcharged flow at CBMH3 to be conveyed by existing major system overflow channel to existing stormwater management facility in Stellar Estates Phase 1 Block 14.
 3. Assumed runoff coefficient for Catchment 404a is 0.30.

Manning's n = 0.013
 Storm Event: 100 year
 where:
 A= 4688
 B= 17
 C= 0.9624

$$I = \frac{A}{(t_c + B)^C}$$

PROJECT: Stellar Estates Phase 2, Town of Caledon
PROJECT No: Ecometrix: 22-3001
CLIENT: Stellar Homes Inc.



RETURN PERIOD	EQUATION OF CURVE
100 YEAR	$i = \frac{4688}{(td + 17)} \cdot .9624$
50 YEAR	$i = \frac{3886}{(td + 16)} \cdot .9495$
25 YEAR	$i = \frac{3158}{(td + 15)} \cdot .9335$
10 YEAR	$i = \frac{2221}{(td + 12)} \cdot .9080$
5 YEAR	$i = \frac{1593}{(td + 11)} \cdot .8789$
2 YEAR	$i = \frac{1070}{(td + 7.85)} \cdot .8759$

INLET TIMES	
SUBURBAN RESIDENTIAL (ROOF DRAINS UNCONNECTED)	15 min
(ROOF DRAINS CONNECTED)	10 min
SUBURBAN, COMMERCIAL, INDUSTRIAL MULTIPLE FAMILY	10 min
DOWNTOWN COMMERCIAL, HIGH DENSITY APARTMENTS, EXPRESSWAYS	5 min

RUNOFF COEFFICIENT	
COMMERCIAL - DOWNTOWN & SUBURBAN SHOPPING	0.90
INDUSTRIAL - DOWNTOWN - SUBURBAN INDUSTRIAL PARKS	0.90 0.75
RESIDENTIAL - APARTMENTS - ROW DWELLINGS - DUPLEX DWELLINGS - SEMIDETACHED - DOWNTOWN - SINGLE FAMILY - DOWNTOWN - SEMIDETACHED - SUBURBAN - SINGLE FAMILY - SUBURBAN	0.75 0.70 0.70 0.60 0.60 0.50 0.40
SCHOOLS, CHURCHES, HOSPITALS	0.75
PARKS, CEMETERIES, RAIL YARDS (OVER 4 Ha) (UNDER 4 Ha)	0.20 0.25
PARKING LOTS ASPHALT & GRAVEL	0.90

TOWN OF CALEDON				APR'D: C.C.	DATE: FEB 2000
RAINFALL INTENSITY CURVES	3	ADDITION OF TEXT	APR 19	DRAWN: BJM	SCALE: N.T.S.
	2	STANDARD 104 NOW 103	JAN 08		
	1	STANDARD 112.01 NOW 104	JUNE 08	STANDARD No. 103	
	NO.	REVISION	APR'D		

TABLE B.5

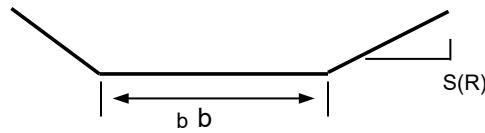
STELLAR ESTATES OVERFLOW SWALE TO BLOCK 14 SWM FACILITY

Channel Hydraulic Calculations

Grass Lined Channel

b = 1.000 m
 S(L) = 3.000
 S(R) = 3.000

 n = 0.030



Design Flow = **316.2 L/s**
 1,138.3 cu.m/h
 27,318.8 cu./day

Capacity at 0.3 m Depth = **454.4 L/s**
 1,636.0 cu.m/h
 39,264.5 cu./day

Depth (m)	Slope (%)	A (m²)	P (m)	R (m)	Q (m³/s)	V (m/s)	T (m)	Fr	Flow Type	Meet Criteria ?
0.050	0.500%	0.06	1.32	0.04	0.017	0.29	1.30	0.44	<i>sub-critical</i>	YES
0.100	0.500%	0.13	1.63	0.08	0.057	0.44	1.60	0.49	<i>sub-critical</i>	YES
0.200	0.500%	0.32	2.26	0.14	0.205	0.64	2.20	0.54	<i>sub-critical</i>	YES
0.300	0.500%	0.57	2.90	0.20	0.454	0.80	2.80	0.56	<i>sub-critical</i>	YES
0.350	0.500%	0.72	3.21	0.22	0.622	0.87	3.10	0.58	<i>sub-critical</i>	YES
0.384	0.500%	0.83	3.43	0.24	0.754	0.91	3.30	0.58	<i>sub-critical</i>	YES
0.400	0.500%	0.88	3.53	0.25	0.822	0.93	3.40	0.59	<i>sub-critical</i>	YES

Note:

- A cross-sectional area of flow in square metres
- P wetted perimeter in metres
- R hydraulic radius in metres
- Q flow in cubic metres per second
- V velocity in metres per second
- T Topwidth
- Fr Froud Number
- n Manning's "n" (roughness coefficient)
- b channel basewidth in metres
- S channel side slope

TABLE B.6
STELLAR ESTATES PHASE 2
FIREWATER SUPPLY CALCULATIONS

Address: 0 Mulloy Court, Town of Caledon, Regional Municipality of Peel
 Client: Stellar Homes Inc.
 Project #: 22-3001
 Date: January 17, 2025

Proposed Development ^{1,2}										Fire Flow															
Building ID	Usage	# of units	Bldg Ground Floor Area sq.m.	Bldg GFA sq.m.	Building Volume cu.m.	Building Setback/Separation (m)				K ⁵	V	S _{tot} ⁶	OBC A-3.2.5.7 - Water Supply			Fire Underwriters Survey (1999)							F max (OBC or FUS) L/s		
						North	East	South	West				Q L	F L/min	F L/s	C ⁷	A ⁸	F	Occupancy Reduction ⁹	F L/min	Sprinkler Reduction ¹⁰	Building Exposure ¹¹		F L/min	F L/s
Single	Residential	1	200.0	400.0	1,219.2	50	15	50	15	16	1219	2	39,014	2,700.0	45.0	1.0	400.0	4,400	0%	4,400	0%	30%	5,720	95.3	95.3

Notes

1 Building details assumed based on typical size of Stellar Estates Phase 1 dwellings.

2 Building Volume Determination

Floor	GFA (sq.m.)	Height (m)	Volume (cu.m.)
1	200	3.048	609.6
2	200	3.048	609.6
3	0	3.048	0.0
Total	400		1,219.2

5 Group C Occupancy

Assumption: Building is of combustible construction with fire separations and fire-resistance ratings provided in accordance with Subsection 3.2.2 of the OBC, including loadbearing walls, columns and arches. Noncombustible construction may be used in lieu of fire-resistance rating where permitted in Subject

6 Stot determined based on building separations indicated in the proposed development description

7 C Description

- 1.5 wood frame construction (structure essentially all combustible)
- 1.0 ordinary construction (brick or masonry walls, combustible floor and interior)
- 0.8 non-combustible construction (unprotected metal structural components, masonry or metal walls)
- 0.6 fire resistive construction (fully protected frame, floors, roof)

8 GFA of building (sq.m).

9 Occupancy Credit/Charge

Non-combustible	-25%
Limited Combustible	-15%
Combustible	0%
Free Burning	15%
Rapid Burning	25%

10 Sprinkler Credit

System conforming to NFPA 13 and other NFPA standards	-30%
Water supply standard for both the system and fire department hose lines required	-10%
Fully supervised system	-10%

11 Building Exposure Charge

Determined based on separations indicated in the proposed development description

Separation	Charge
0 to 3m	25%
3.1 to 10m	20%
10.1 to 20m	15%
20.1 to 30m	10%
30.1 to 45m	5%

Total percentage is the sum of all sides not to exceed 75%.

Fire flow not to exceed 45,000 L/min or be less than 2,000 L/min

TABLE B.7

Proposed Bioswale - Storage Calculations

Project: Stellar Estates Subdivision Phase 2
Project #: 22-3001
Date: April 7, 2026

Bioswale Soil Media Dimensions

Nominal Width of Soil Media: 0.75 m
 Soil Media Depth: 1.15 m
 Side Slope Area outside Vertical Cut: 0.00 sq.m (assumed)
 Total Cross-Sectional Area: 0.86 sq.m

Design Assumptions

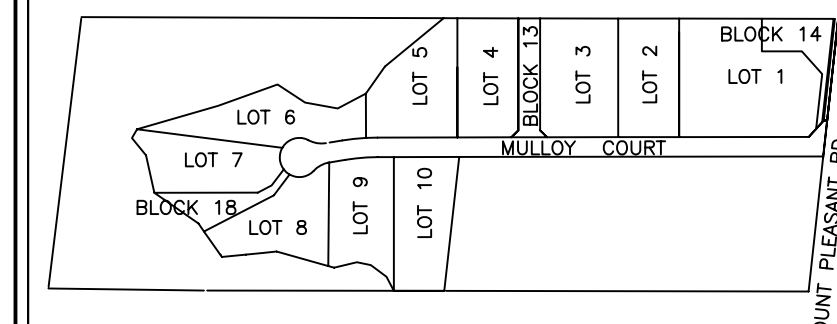
Geometry: Parabolic cross-section with 0.75 metre nominal base width
 Swale Side Slopes: 4H:1V
 Minimum Swale Depth: 0.15 m
 Maximum Swale Depth: 0.30 m
 Swale Surface Cross-Sectional Area: 0.59 sq.m (at maximum depth)
 Assumed Soil Hydrologic Group: CD
 Soil Hydraulic Conductivity: 1×10^{-6} cm/s
 Soil Porosity: 0.40
 Underdrain Required: Yes Soil Hydraulic Conductivity 1×10^{-6} cm/s

BIOSWALE STORAGE VOLUME CALCULATIONS

Location	Swale Drainage Area (ha)	Swale Media Cross-Sectional Area (sq.m.)	Soil Porosity	Swale Media Storage per metre (sq.m/m)	Swale Surface Storage per metre (cu.m)	Swale Length (m)	Swale Storage (cu.m)
Mulloy Court Blvd. North Side	<0.8 Ha	0.86	40%	0.345	0.59	30	27.90
Mulloy Court Blvd. South Side	<0.8 Ha	0.86	40%	0.345	0.59	30	27.90
Totals:						60	55.80

Notes:

- Units: ha - hectares; sq.m - square metres; m - metres; cu.m - cubic metres; cm/s - centimetres per second.
- Refer to project engineering plans for preliminary location of bioswales. Locations and configuration to be finalized at detailed design stage.
- Refer to project engineering plans for typical bioswale detail: Detail 4 on Drawing 22-3001-09.



KEY PLAN N.T.S.

GENERAL NOTES:

- MEASUREMENTS
ALL DIMENSIONS ARE IN METERS, EXCEPT PIPE DIAMETERS WHICH ARE IN MILLIMETRES, UNLESS OTHERWISE SPECIFIED.
- CONSTRUCTION FOR THIS PROJECT TO COMPLY WITH THE MOST CURRENT VERSION OF THE DEVELOPMENT STANDARDS, POLICIES AND GUIDELINES, PREPARED BY THE TOWN OF CALEDON INFRASTRUCTURE DEPARTMENT REGIONAL MUNICIPALITY OF PEEL PUBLIC WORKS STANDARDS AND SPECIFICATIONS AND THE ONTARIO PROVINCIAL STANDARDS AND SPECIFICATIONS.
 - ALL UNDERGROUND SERVICE MATERIALS AND INSTALLATIONS TO BE IN ACCORDANCE WITH THE LATEST STANDARDS AND CODES AND BE IN GENERAL CONFORMANCE WITH THE MINISTRY OF ENVIRONMENT GUIDELINES.
 - ALL PROPOSED CONSTRUCTION SHALL BE CARRIED OUT IN ACCORDANCE WITH THE REQUIREMENTS OF THE OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS.
 - LOCATION OF EXISTING SERVICES AND UTILITIES ARE NOT GUARANTEED. THE CONTRACTOR SHALL BE RESPONSIBLE FOR LOCATING AND MAINTAINING EXISTING UTILITIES. ANY CHANGES SHALL BE REPAIRED AT THE CONTRACTORS COST TO THE SATISFACTION OF THE APPROPRIATE UTILITY.
 - A MINIMUM OF FORTY-EIGHT HOURS PRIOR TO COMMENCING CONSTRUCTION WITHIN THE MUNICIPAL RIGHT OF WAY THE CONTRACTOR MUST CONTACT THE FOLLOWING:
 - THE TOWN OF CALEDON PUBLIC WORKS AND ENGINEERING DEPARTMENT - 905-584-2272
 - THE REGION OF PEEL - 905-791-7800
 - ENBRIDGE CONSUMERS GAS - 905-758-7924
 - HYDRO ONE - 519-461-1211
 - BELL CANADA - 416-296-6927
 - FIRE AND EMERGENCY SERVICES - 905-584-1477
 - SEDIMENT CONTROL DEVICES ARE TO BE INSTALLED PRIOR TO ANY CONSTRUCTION ON THE SITE AND SHALL BE MAINTAINED THROUGHOUT THE CONSTRUCTION PERIOD TO THE SATISFACTION OF THE TOWN AND THE APPLICABLE CONSERVATION AUTHORITY.
 - A MINIMUM OF 1.2m CLEARANCE IS TO BE PROVIDED FROM THE LIMITS OF ALL DRIVEWAYS TO EXISTING UTILITY STRUCTURES WITHIN THE MUNICIPAL RIGHT OF WAY. IF THIS CLEARANCE IS NOT MAINTAINED THEY SHALL RELOCATE AT THE APPLICANT'S EXPENSE.
 - ALL BOULEVARDERS TO BE RESTORED WITH 150mm MINIMUM OF TOPSOIL AND 500 TO THE SATISFACTION OF THE TOWN OF CALEDON PUBLIC WORKS AND ENGINEERING DEPARTMENT.
 - THE MINIMUM PAVEMENT DESIGN FOR THE ASPHALT DRIVEWAY APRON WITHIN THE MUNICIPAL ROAD ALLOWANCE SHALL BE AS FOLLOWS:
 - 40mm HLB ASPHALT
 - 50mm HLB ASPHALT
 - 150mm GRANULAR 'A'
 - 300mm GRANULAR 'B'
 - A ROAD OCCUPANCY PERMIT MUST BE OBTAINED PRIOR TO COMMENCING ANY WORKS WITHIN THE ROAD ALLOWANCE FROM THE TOWN OF CALEDON PUBLIC WORKS DEPARTMENT. THE CONTRACTOR WILL BE RESPONSIBLE FOR TRAFFIC CONTROL.
 - NATIVE AND GRANULAR MATERIAL, SUITABLE FOR BACKFILL, SHALL BE COMPACTED TO A MIN. 95% SPMD EXCEPT TOP 0.5m WHICH MUST BE COMPACTED TO 98% SPMD, OR AS RECOMMENDED BY A QUALIFIED SOILS CONSULTANT.

REGION OF PEEL



TOWN OF CALEDON

Calder Engineering Ltd.
12246 Allison Vaughan Road, Caledon, ON L7U 1C0
T 905-857-7600 F 905-857-5900 www.caldereng.com

DESIGNED BY _____ APPROVED BY _____

Drawing N° _____ Date _____ Sheet Title _____
Reference Drawings _____

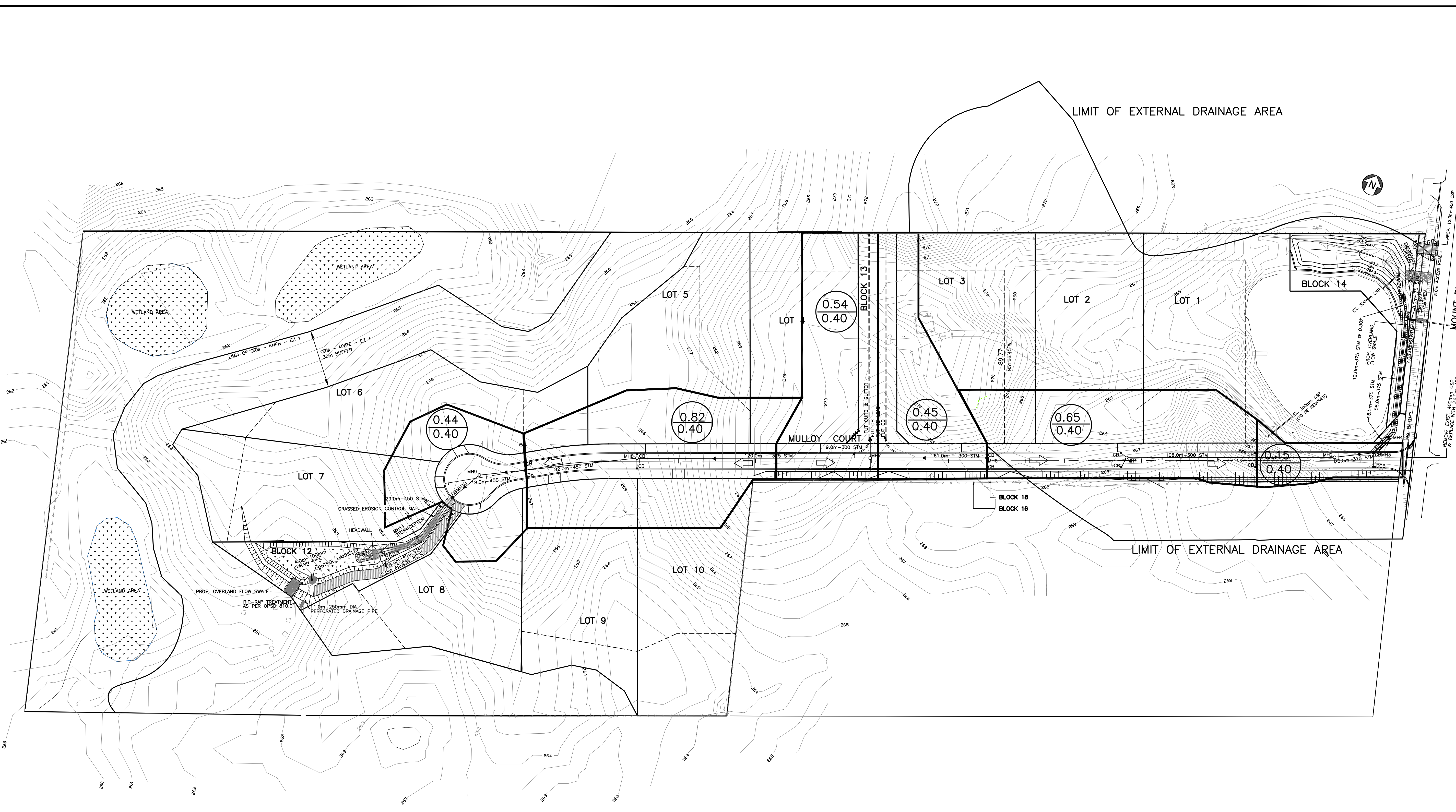
N°	Date	Revisions	Dwn.	Dsg'd	Chk'd
5	31/MAY/12	FINAL TOWN COMMENTS	D.H.	D.H.	R.J.W.
4	12/MAR/12	THIRD SUBMISSION TO TOWN AND REGION	D.H.	D.H.	R.J.W.
3	27/JUNE/11	PER TRCA COMMENTS	D.H.	D.H.	R.J.W.
2	15/APR/11	SECOND SUBMISSION	D.H.	D.H.	E.M.
1	2/DEC/10	FIRST SUBMISSION	D.H.	D.H.	R.J.W.

Client: **STELLAR HOMES INC.**
21T-07001C

PROJECT: **STELLAR ESTATES
RESIDENTIAL DEVELOPMENT
LOTS 1 TO 10**

TITLE: **STORM DRAINAGE AREA PLAN**

Scale: **1:1000** Drawing No. **10-109-A-1A**



DEVELOPMENT STELLAR HOMES
CONSULTANT CALDER ENGINEERING LTD.
MAJOR DRAINAGE AREA _____
2 YEAR

SHEET No. 1 OF 1 DATE MARCH/2011
DESIGNED BY D. HAY
CHECKED BY E. MINOR

THE TOWN OF CALEDON
PUBLIC WORKS AND ENGINEERING DEPARTMENT
STORM DRAINAGE DESIGN CHART
FOR CIRCULAR DRAINS FLOWING FULL

STREET	LOCATION		DRAINAGE AREA				RUNOFF				PIPE SELECTION				PROFILE				NOTES/DESCRIPTION							
	FROM	TO	A	C	A x C	CUMUL. A x C	To EXTERNAL	Q ₁₅ (mm/h)	Q ₃₀ (mm/h)	Q ₆₀ (mm/h)	PIPE L ₁ (m)	PIPE S ₁ (mm)	PIPE DIA. (mm)	ACTUAL CAPACITY (FULL) (L/S)	VELOCITY (m/s)	TIME OF FLOW (min)	MINOR LOSSES (m)	FALL (m)		UPSTREAM SURFACE ELEV. (m)	INV. ELEV. (m)	COVER (m)	DOWNSTREAM SURFACE ELEV. (m)	INV. ELEV. (m)	COVER (m)	
SITE	MH1	MH2	0.65	0.40	0.26	0.26	10.00	85.71	0.062	108.0	0.93	300	0.097	1.33	1.16	1.0	0.0	267.09	265.20	1.51	265.43	264.20	0.86			
	MH2	CBMH3	0.15	0.40	0.06	0.32	11.16	81.12	0.072	20.0	0.30	375	0.10	0.88	0.38	0.06	0.06	265.43	264.20	0.86	265.13	264.06	0.70			
	MH3	MH4	---	0.40	---	0.32	11.54	79.72	0.07	15.5	0.30	375	0.10	0.88	0.29	0.05	0.05	265.13	264.04	0.88	264.90	263.99	0.54			
	MH4	MH5	---	---	---	0.32	11.83	78.70	0.07	58.0	0.30	375	0.10	0.88	1.09	0.17	0.17	264.90	263.97	0.56	264.60	263.80	0.43			
	MH5	OUTFALL								7.0	0.30	375	0.10	0.88												
	MH6	MH7	0.45	0.40	0.18	0.18	10.00	85.71	0.043	61.0	0.50	300	0.071	0.98	1.03	0.31	0.31	266.61	265.80	1.61	268.09	265.49	2.30			
	MH7	MH8	0.54	0.40	0.22	0.40	11.03	81.61	0.091	120.0	0.50	375	0.129	1.13	1.76	0.60	0.60	268.09	265.41	2.30	267.22	264.81	2.04			
	MH8	MH9	0.82	0.40	0.33	0.73	12.79	75.48	0.153	82.0	0.50	450	0.210	1.28	1.06	0.60	0.60	267.22	264.73	2.04	266.53	264.32	1.76			
	MH9	CBMH10	0.44	0.40	0.18	0.91	13.85	72.24	0.182	18.0	1.0	450	0.297	1.81	0.17	0.18	0.18	266.53	264.27	1.81	265.92	264.09	1.38			
	CBMH10	MH11	---	---	---	0.91	14.02	71.75	0.182	29.0	0.50	450	0.210	1.28	0.17	0.15	0.15	265.92	263.04	2.43	265.60	262.89	2.26			
	MH11	HEADWALL	---	---	---	0.91	14.19	71.26	0.182	24.0	0.50	450	0.210	1.28												

0.24
0.40

--- DRAINAGE AREA (HECTARES)
--- RUN-OFF COEFFICIENT
--- LIMIT OF BUILDING ENVELOPE

○ PROPOSED MANHOLE
⊕ PROPOSED DOUBLE CATCHBASIN
⊕ PROPOSED DOUBLE CATCHBASIN MANHOLE
→ PROPOSED DIRECTION OF OVERLAND FLOW
--- PROPOSED STORM SEWER

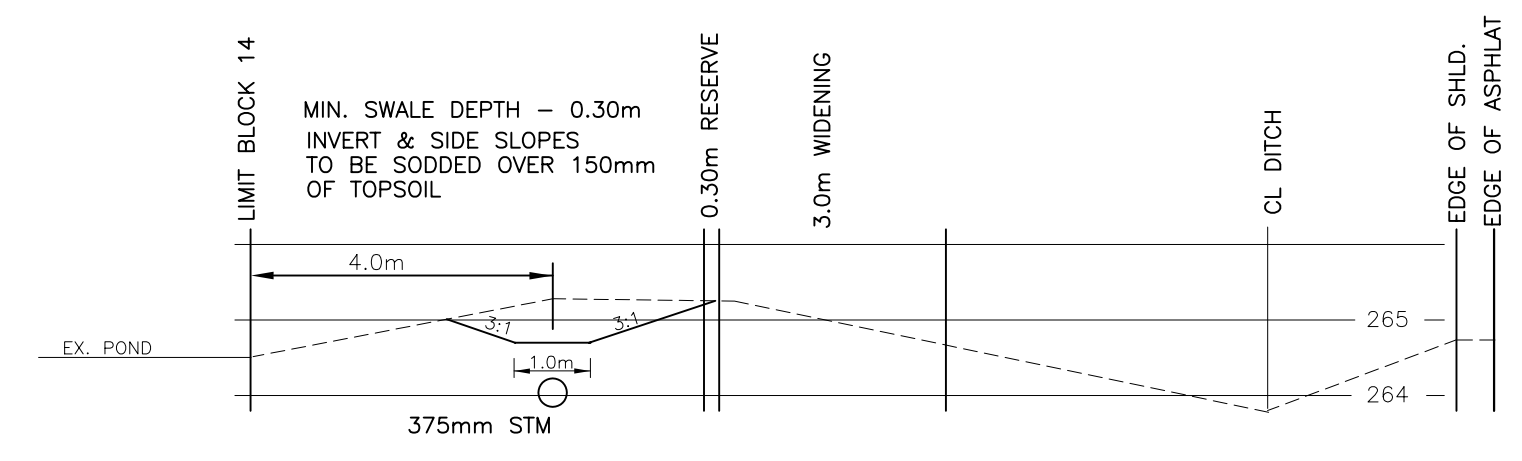
LEGEND

TOWN OF CALEDON
APPROVED AS NOTED

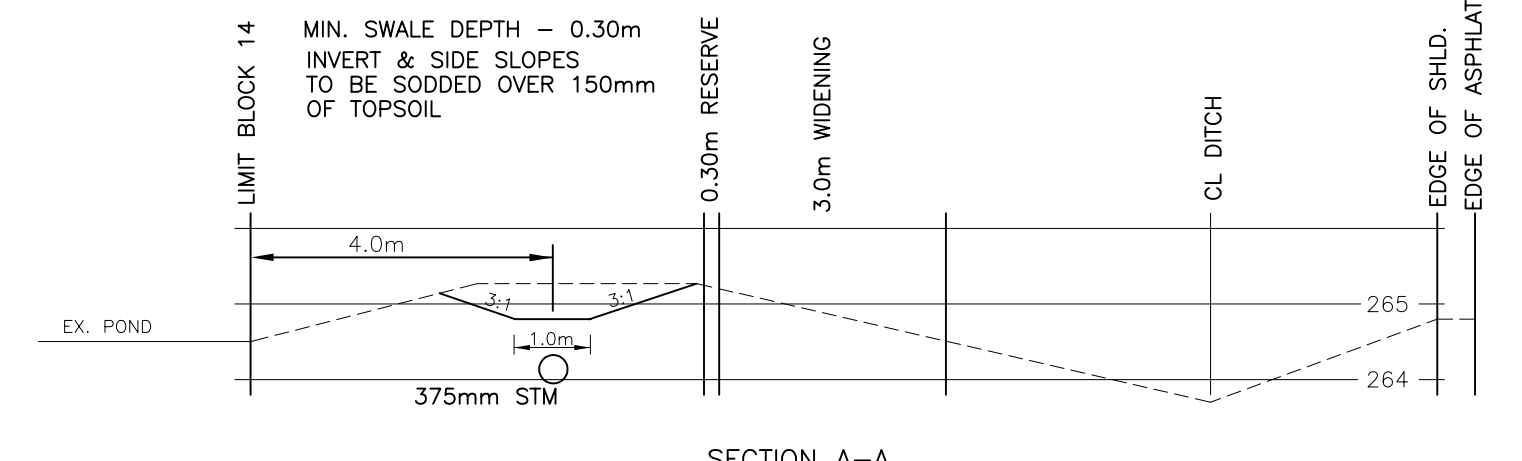
THIS APPROVAL CONSTITUTES A GENERAL REVIEW AND DOES NOT CERTIFY DIMENSIONAL ACCURACY.

THIS APPROVAL IS SUBJECT TO FURTHER CERTIFICATION OF THE "AS CONSTRUCTED" WORKS BY A REGISTERED PROFESSIONAL ENGINEER/ARCHITECT (AS APPROPRIATE) OF THE PROVINCE OF ONTARIO

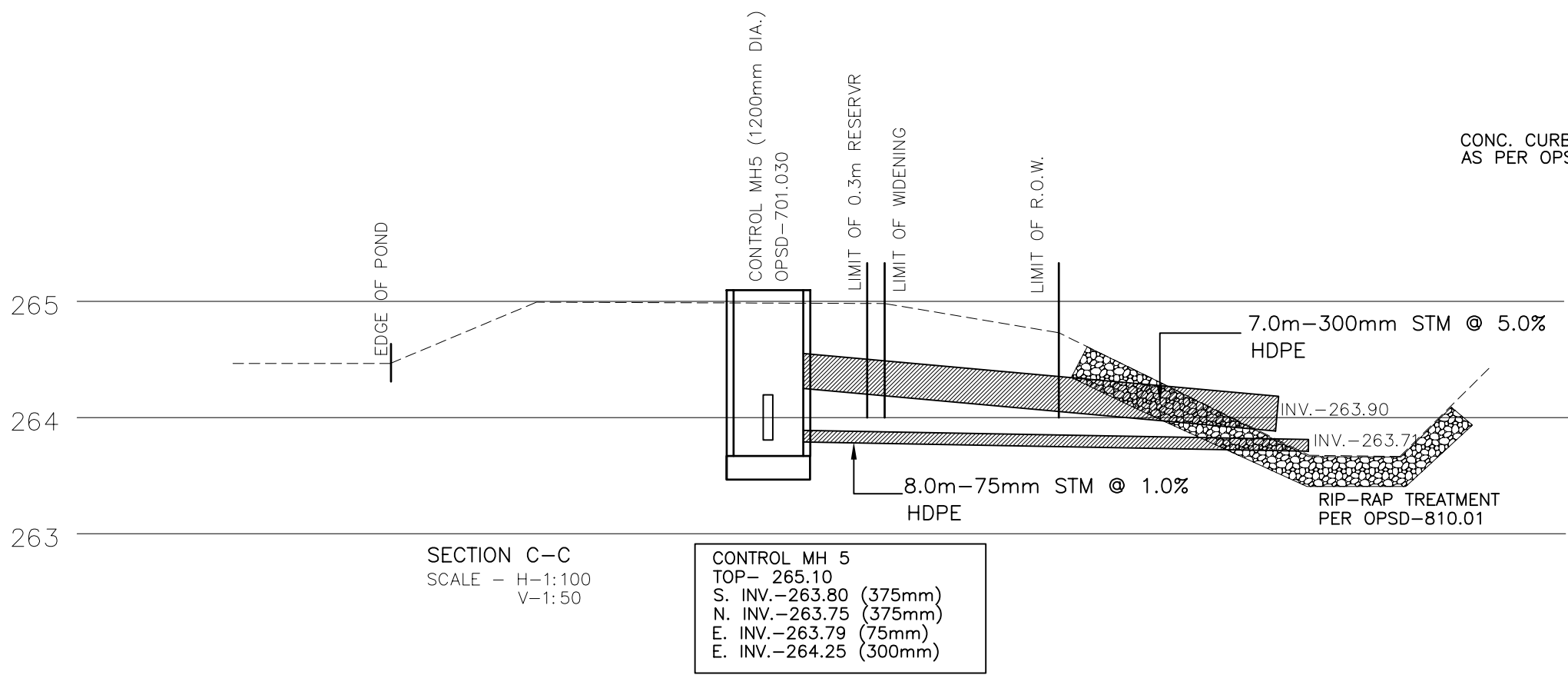
DATE: _____
APPROVED BY: _____
MARY HALL MCIP RPP
DIRECTOR



SECTION B-B
SCALE - H=1:100
V=1:50

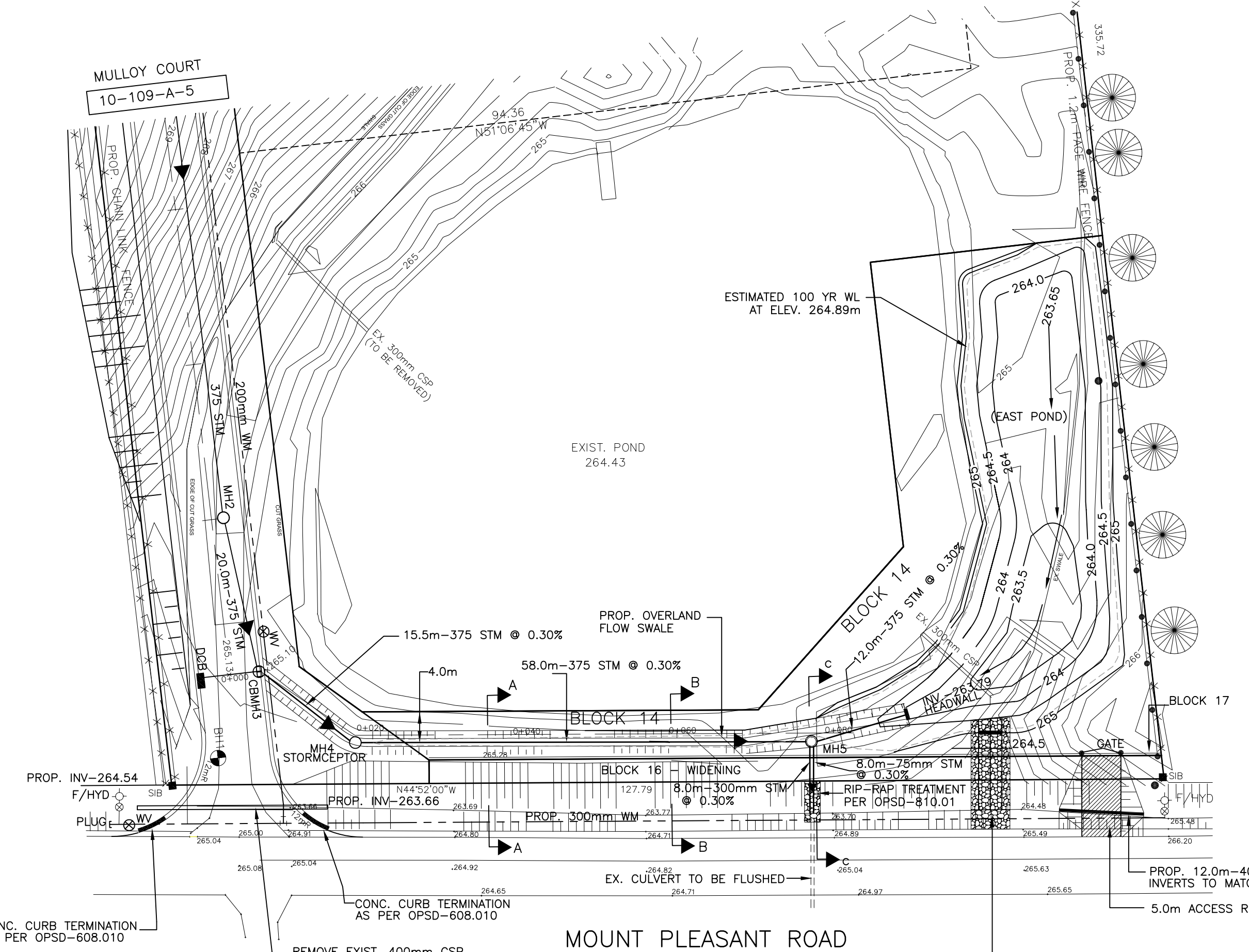


SECTION A-A
SCALE - H=1:100
V=1:50

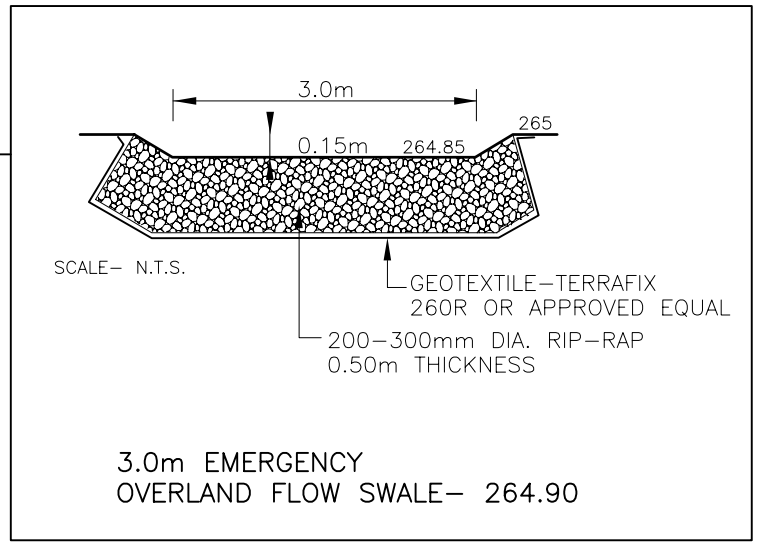


SECTION C-C
SCALE - H=1:100
V=1:50

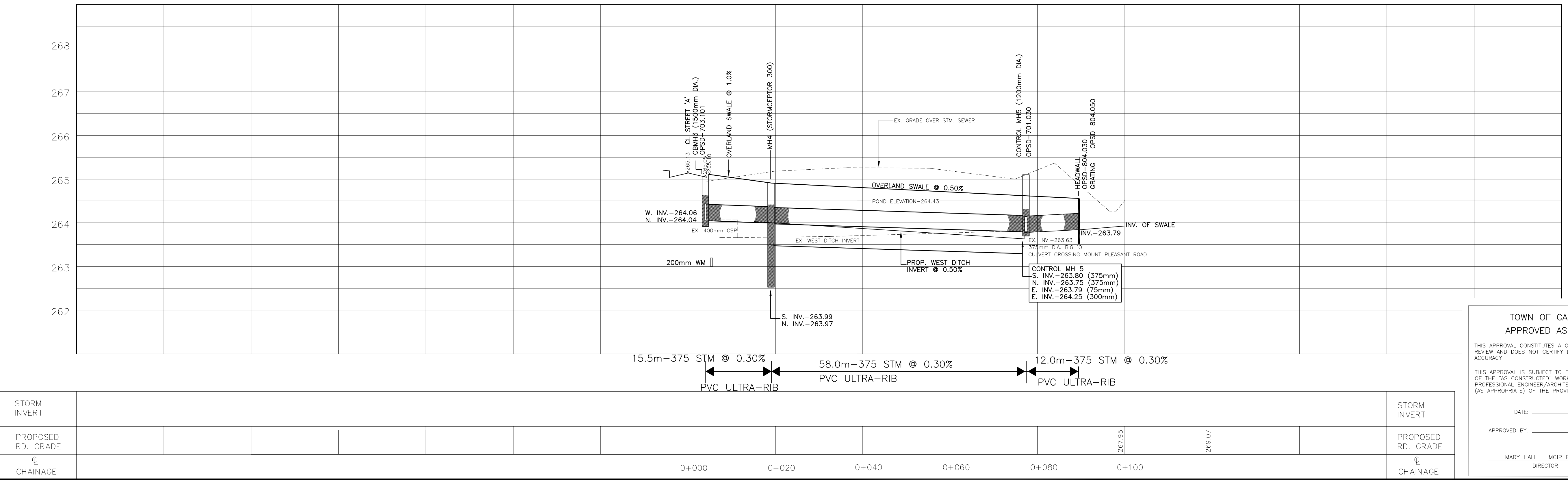
CONTROL MH 5
TOP - 265.10
S. INV. - 263.80 (375mm)
N. INV. - 263.75 (375mm)
E. INV. - 263.79 (75mm)
I. INV. - 264.25 (300mm)



MOUNT PLEASANT ROAD



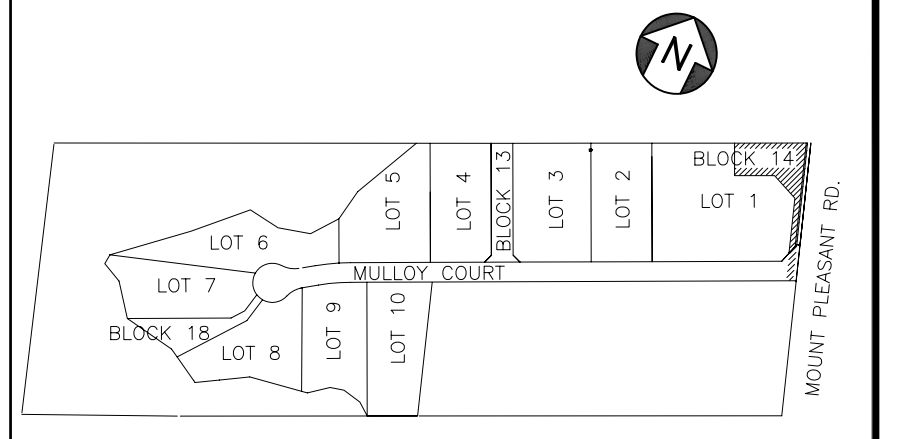
3.0m EMERGENCY OVERLAND FLOW SWALE - 264.90



STORM INVERT
PROPOSED RD. GRADE
CHAINAGE

STORM INVERT
PROPOSED RD. GRADE
CHAINAGE

TOWN OF CALEDON
APPROVED AS NOTED
THIS APPROVAL CONSTITUTES A GENERAL REVIEW AND DOES NOT CERTIFY DIMENSIONAL ACCURACY.
THIS APPROVAL IS SUBJECT TO FURTHER CERTIFICATION OF THE "AS CONSTRUCTED" WORKS BY A REGISTERED PROFESSIONAL ENGINEER/ARCHITECT (AS APPROPRIATE) OF THE PROVINCE OF ONTARIO.
DATE: _____
APPROVED BY: _____
MARY HALL M.C.P. R.P.P.
DIRECTOR



KEY PLAN N.T.S.

GENERAL NOTES:

- MEASUREMENTS
ALL DIMENSIONS ARE IN METERS, EXCEPT PIPE DIAMETERS WHICH ARE IN MILLIMETRES, UNLESS OTHERWISE SPECIFIED.
- CONSTRUCTION FOR THIS PROJECT TO COMPLY WITH THE MOST CURRENT VERSION OF THE DEVELOPMENT STANDARDS, POLICIES AND GUIDELINES PREPARED BY THE TOWN OF CALEDON INFRASTRUCTURE DEPARTMENT/REGIONAL MUNICIPALITY OF PEEL PUBLIC WORKS STANDARDS AND SPECIFICATIONS AND THE ONTARIO PROVINCIAL STANDARDS AND SPECIFICATIONS.
 - ALL UNDERGROUND SERVICE MATERIALS AND INSTALLATIONS TO BE IN ACCORDANCE WITH THE LATEST STANDARDS AND CODES AND IN GENERAL CONFORMANCE WITH THE REQUIREMENTS OF THE OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS.
 - LOCATION OF EXISTING SERVICES AND UTILITIES ARE NOT GUARANTEED. THE CONTRACTOR SHALL BE RESPONSIBLE FOR LOCATING AND MAINTAINING EXISTING UTILITIES. ANY CHANGES SHALL BE REPAIRED AT THE CONTRACTORS COST TO THE SATISFACTION OF THE APPROPRIATE UTILITY.
 - A MINIMUM OF FORTY-EIGHT HOURS PRIOR TO COMMENCING CONSTRUCTION WITHIN THE MUNICIPAL RIGHT OF WAY THE CONTRACTOR MUST CONTACT THE FOLLOWING:
- THE TOWN OF CALEDON PUBLIC WORKS AND ENGINEERING DEPARTMENT - 905-584-2272
- THE REGION OF PEEL - 905-791-7800
- ENBRIDGE CONSUMERS GAS - 905-758-7924
- HYDRO ONE - 519-941-1211
- BELL CANADA - 416-298-8227
- FIRE AND EMERGENCY SERVICES - 905-584-1477
 - SEDIMENT CONTROL DEVICES ARE TO BE INSTALLED PRIOR TO ANY CONSTRUCTION ON THE SITE AND SHALL BE MAINTAINED THROUGHOUT THE CONSTRUCTION PERIOD TO THE SATISFACTION OF THE TOWN AND THE APPLICABLE CONSERVATION AUTHORITY.
 - A MINIMUM OF 1.2m CLEARANCE IS TO BE PROVIDED FROM THE LIMITS OF ALL DRAWINGS TO EXISTING UTILITY STRUCTURES WITHIN THE MUNICIPAL RIGHT OF WAY IF THIS CLEARANCE IS NOT MAINTAINED THEY SHALL RELOCATE AT THE APPLICANT'S EXPENSE.
 - ALL BOULEVARDS TO BE RESTORED WITH 150mm MINIMUM OF TOPSOIL AND 500 TO THE SATISFACTION OF THE TOWN OF CALEDON PUBLIC WORKS AND ENGINEERING DEPARTMENT.
 - THE MINIMUM PAVEMENT DESIGN FOR THE ASPHALT DRIVEWAY APRON WITHIN THE MUNICIPAL ROAD ALLOWANCE SHALL BE AS FOLLOWS:
- 40mm H.E. ASPHALT
- 50mm H.E. ASPHALT
- 150mm GRANULAR 'A'
- 300mm GRANULAR 'B'
 - A ROAD OCCUPANCY PERMIT MUST BE OBTAINED PRIOR TO COMMENCING ANY WORKS WITHIN THE ROAD ALLOWANCE FROM THE TOWN OF CALEDON PUBLIC WORKS DEPARTMENT. THE CONTRACTOR WILL BE RESPONSIBLE FOR TRAFFIC CONTROL.
 - NATIVE AND GRANULAR MATERIAL, SUITABLE FOR BACKFILL, SHALL BE COMPACTED TO A MIN. 95% SPND EXCEPT TOP 10% WHICH MUST BE COMPACTED TO 98% SPND, OR AS RECOMMENDED BY A QUALIFIED SOILS CONSULTANT.

REGION OF PEEL
TOWN OF CALEDON
Calder Engineering Ltd.
12246 Allison Vaughan Road, Richmond Hill, ON L4B 1C9
T 905-857-7600 F 905-857-5900 www.caldereng.com

DESIGNED BY	APPROVED BY			
Drawing No	Date			
Reference Drawings	Sheet Title			
5 31/MAY/12	FINAL TOWN COMMENTS	D.H.	D.H.	R.J.W.
4 12/MARCH/12	THIRD SUBMISSION TO TOWN AND REGION	D.H.	D.H.	R.J.W.
3 27/JUNE/11	PER TRCA COMMENTS	D.H.	D.H.	R.J.W.
2 15/APR/11	SECOND SUBMISSION	D.H.	D.H.	E.M.
1 2/DEC/10	FIRST SUBMISSION	D.H.	D.H.	R.J.W.
Date	Revisions	Dwn.	Dsg'd	Chk'd
Client:	STELLAR HOMES INC. 21T-07001C			
PROJECT:	STELLAR ESTATES RESIDENTIAL DEVELOPMENT LOTS 1 TO 10			
TITLE:	STORM SEWER OUTFALL BLOCK 14			
Scale:	HOR 1:500 VERT. 1:50	Drawing No.	10-109-A-8	

FIGURE B.1 - SWMHYMO MODEL SCHEMATIC OF EXISTING AND POST-DEVELOPMENT CONDITIONS

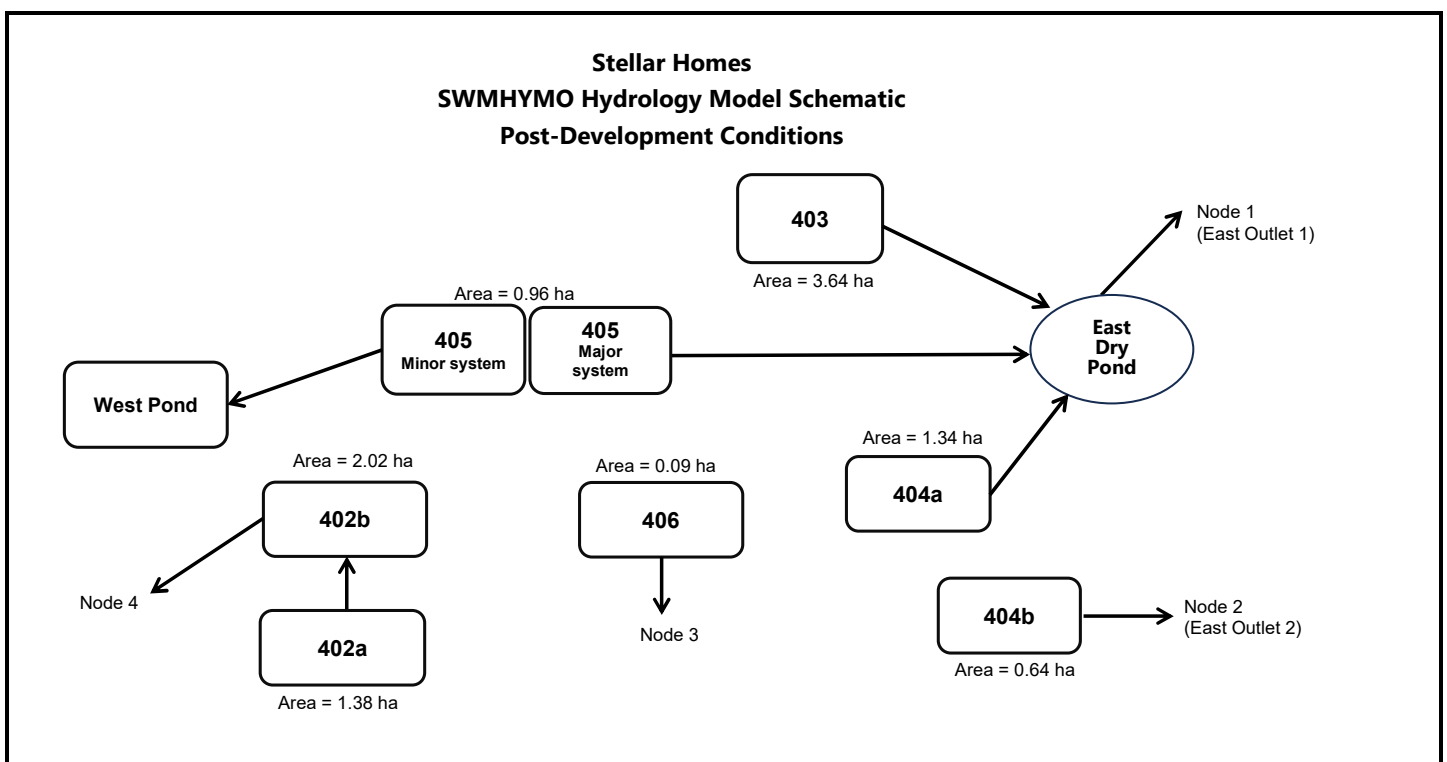
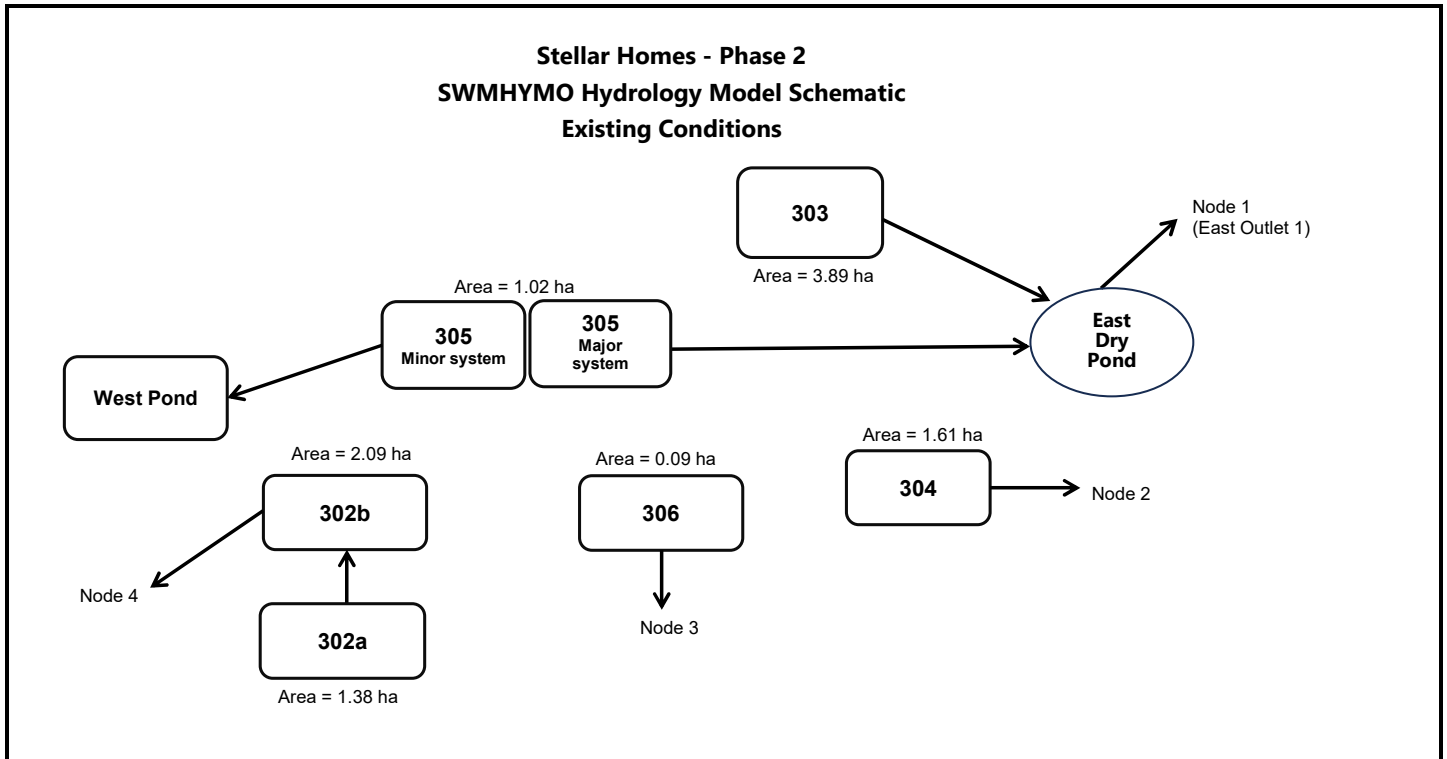
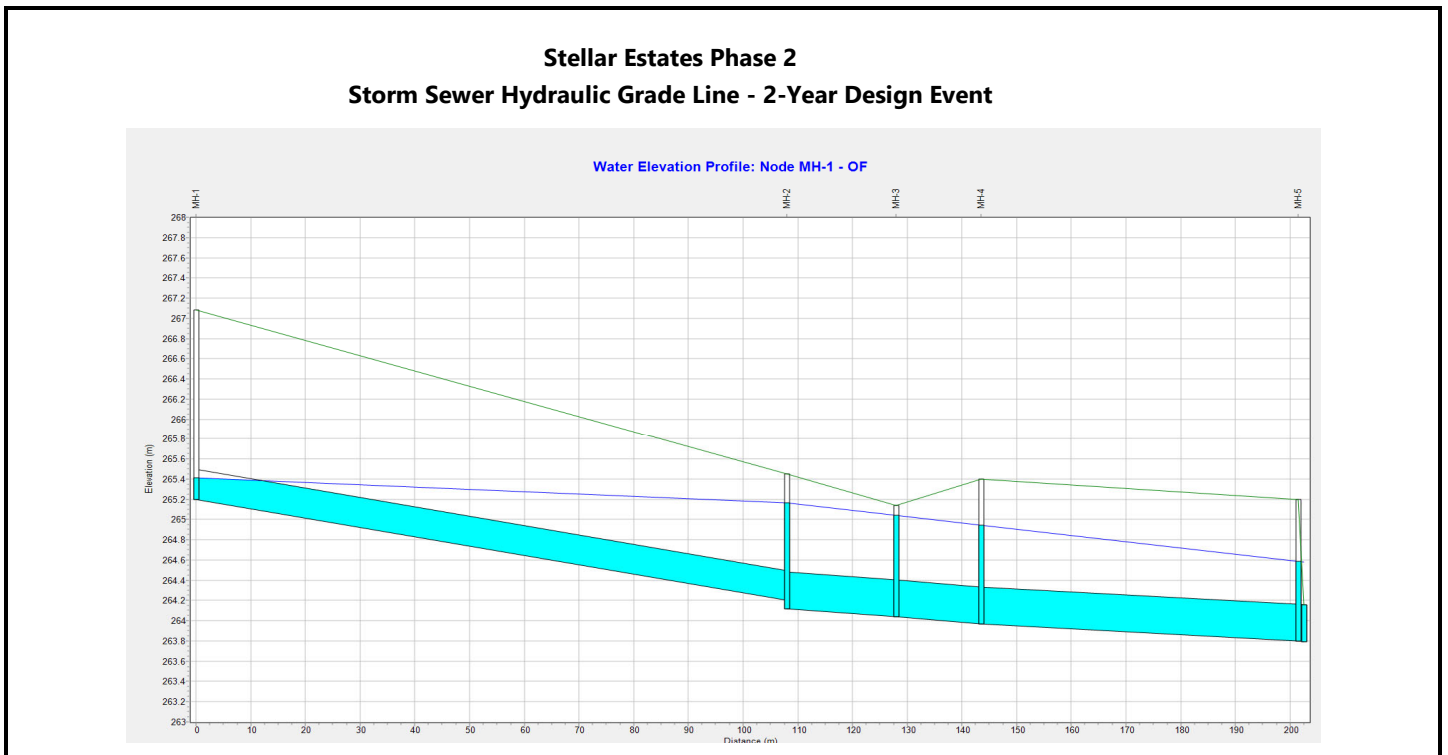
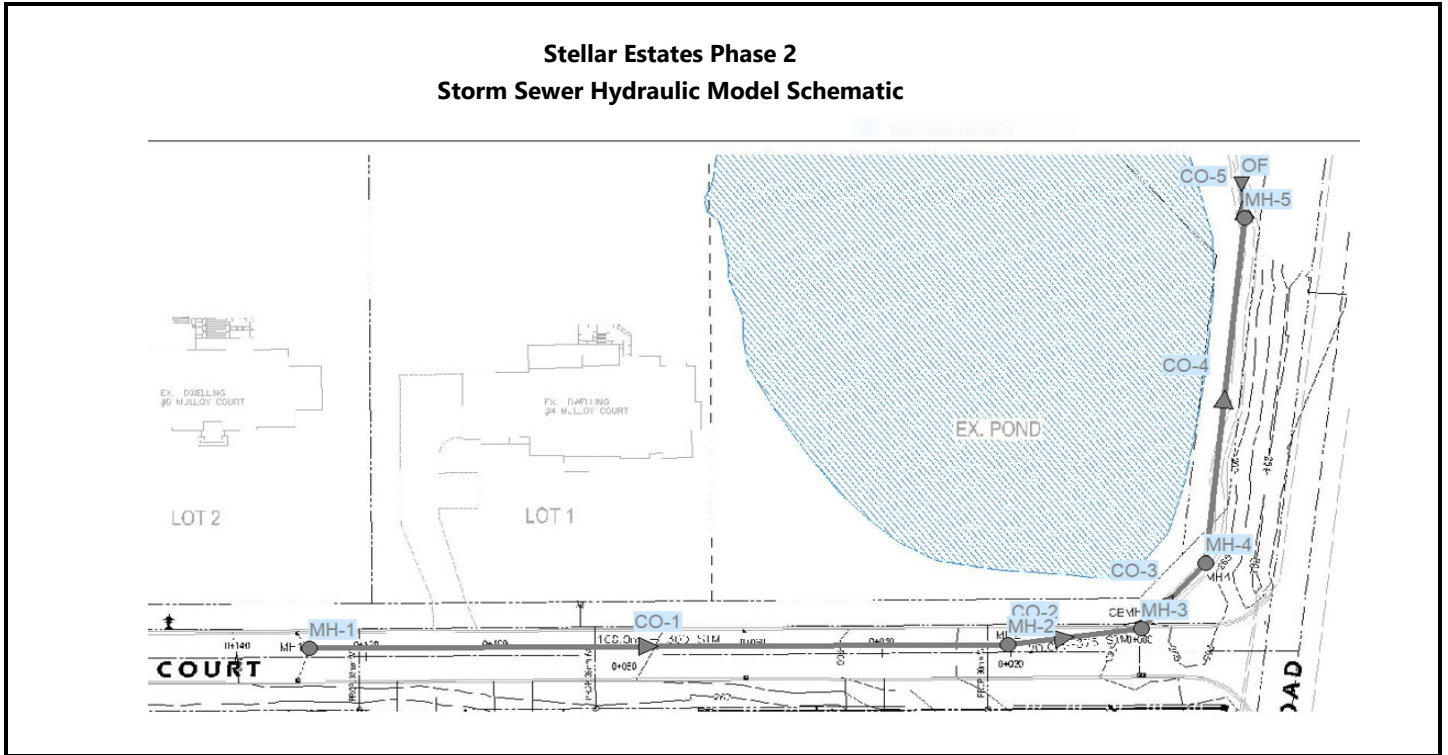


FIGURE B.2 - STORM SEWER HYDRAULIC MODEL SCHEMATIC AND RESULTS



```

00001> 2      Metric units
00002> #*****
00003> # Project Name: [Stella Homes Phase 2]      Project Number: [22-3001]
00004> # Date       : 2024-01-30a
00005> # Modeller   : [MYS]
00006> # Company    : Ecometrix Incorporated
00007> # License #   : 3375279
00008> #*****
00009> * Existing Conditions for Phase 2 Subdivision
00010> * Filename: S2-E.dat
00011> *
00012> #*****
00013> START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[0]
00014> # ["2Y6.STM"] <--storm filename, one per line for NSTORM time
00015> # ["5Y6.STM"]
00016> # ["10Y6.STM"]
00017> # ["25Y6.STM"]
00018> # ["50Y6.STM"]
00019> # ["100Y6.STM"]
00020> #-----|
00021> READ STORM      STORM_FILENAME=["STORM.001"]
00022> #-----|
00023> CALIB NASHYD    ID=[ 1 ], NHYD=["303*"], DT=[ 1 ]min, AREA=[3.89] (ha),
00024> DWF=[ 0 ](cms), CN/C=[ 82 ], IA=[ 10 ](mm),
00025> N=[ 3 ], TP=[0.32] hrs,
00026> RAINFALL=[ , , , ](mm/hr), END=-1
00027> #-----|
00028> CALIB NASHYD    ID=[ 2 ], NHYD=["305*"], DT=[ 1 ]min, AREA=[1.02] (ha),
00029> DWF=[ 0 ](cms), CN/C=[ 84 ], IA=[ 10 ](mm),
00030> N=[ 3 ], TP=[ 0.19 ]hrs,
00031> RAINFALL=[ , , , ](mm/hr), END=-1
00032> #-----|
00033> * For Catchment 305:
00034> * Minor system goes to West outlet, major system goes to East Outlet 1
00035> #-----|
00036> COMPUTE DUALHYD IDin=[ 2 ], CINLET=[0.129 ](cms), MINLET=[ 1 ],
00037> MAJID=[ 3 ], MAJNHYD=["Major" ],
00038> MINID=[ 4 ], MINNHYD=["Minor" ],
00039> TWISTO=[ 0 ](cu-m)
00040> #-----|
00041> ADD HYD         IDsum=[ 5 ], NHYD=["to EP"], IDs to add=[ 1+3]
00042> #-----|
00043> ROUTE RESERVOIR IDout=[ 6 ], NHYD=["EPond"], IDin=[ 5 ],
00044> RDT=[ 1 ](min),
00045> TABLE of ( OUTFLOW-STORAGE ) values
00046> (cms) - (ha-m)
00047> (0.0000 , 0.0000)
00048> (0.0056 , 0.0190)
00049> (0.0068 , 0.0254)
00050> (0.0078 , 0.0324)
00051> (0.0521 , 0.0400)
00052> (0.0847 , 0.0483)
00053> (0.1073 , 0.0572)
00054> (0.1258 , 0.0668)
00055> (0.1419 , 0.0770)
00056> (0.1562 , 0.0880)
00057> (0.2230 , 0.0996)
00058> (0.4348 , 0.1119)
00059> [ -1 , -1 ] (max twenty pts)
00060> IDovf=[ 7 ], NHYDovf=["EPOVF"]
00061> #-----|
00062> CALIB NASHYD    ID=[ 8 ], NHYD=["304*"], DT=[ 1 ]min, AREA=[ 1.61 ](ha),
00063> DWF=[ 0 ](cms), CN/C=[ 83 ], IA=[ 10 ](mm),
00064> N=[ 3 ], TP=[0.23] hrs,
00065> RAINFALL=[ , , , ](mm/hr), END=-1
00066> #-----|
00067> CALIB NASHYD    ID=[ 9 ], NHYD=["306*"], DT=[ 1 ]min, AREA=[ 0.09 ](ha),
00068> DWF=[ 0 ](cms), CN/C=[ 83 ], IA=[ 10 ](mm),
00069> N=[ 3 ], TP=[0.11] hrs,
00070> RAINFALL=[ , , , ](mm/hr), END=-1
00071> #-----|
00072> CALIB NASHYD    ID=[ 1 ], NHYD=["302a*"], DT=[ 1 ]min, AREA=[ 1.38 ](ha),
00073> DWF=[ 0 ](cms), CN/C=[ 74 ], IA=[ 10 ](mm),
00074> N=[ 3 ], TP=[0.23] hrs,
00075> RAINFALL=[ , , , ](mm/hr), END=-1
00076> #-----|
00077> CALIB NASHYD    ID=[ 2 ], NHYD=["302b*"], DT=[ 1 ]min, AREA=[ 2.09 ](ha),
00078> DWF=[ 0 ](cms), CN/C=[ 81 ], IA=[ 10 ](mm),
00079> N=[ 3 ], TP=[0.30] hrs,
00080> RAINFALL=[ , , , ](mm/hr), END=-1
00081> #-----|
00082> ADD HYD         IDsum=[ 3 ], NHYD=["Node 4*"], IDs to add=[ 1+2 ]
00083> #-----|
00084> START      TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[2]
00085> # ["5Y6.STM"] <--storm filename, one per line for NSTORM time
00086> #-----|
00087> START      TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[3]
00088> # ["10Y6.STM"] <--storm filename, one per line for NSTORM time
00089> #-----|
00090> START      TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[4]
00091> # ["25Y6.STM"] <--storm filename, one per line for NSTORM time
00092> #-----|
00093> START      TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[5]
00094> # ["50Y6.STM"] <--storm filename, one per line for NSTORM time
00095> #-----|
00096> START      TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[6]
00097> # ["100Y6.STM"] <--storm filename, one per line for NSTORM tim
00098> #-----|
00099> FINISH
00100>
00101>

```

```

00001>=====
00002>
00003> SSSSS W W M M H H Y Y M M O O 999 999 =====
00004> S W W W M M H H Y Y M M O O 9 9 9 9
00005> SSSSS W W M M H H H H Y Y M M O O ## 9 9 9 9 Ver 4.05
00006> S W W M M H H Y Y M M O O 9999 9999 Sept 2011
00007> SSSSS W W M M H H Y Y M M O O 9 9 9 9 =====
00008> StormWater Management Hydrologic Model 999 999 =====
00009>
00010>
00011> ***** SWMHYMO Ver/4.05 *****
00012> ***** A single event and continuous hydrologic simulation model *****
00013> ***** based on the principles of HYMO and its successors *****
00014> ***** OTTHYMO-83 and OTTHYMO-89. *****
00015> ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00016> ***** Ottawa, Ontario: (613) 836-3884 *****
00017> ***** Gatineau, Quebec: (819) 243-6858 *****
00018> ***** E-Mail: swmhyo@jfsa.com *****
00019> *****
00020> *****
00021> *****
00022> *****
00023> ***** Licensed user: Calder Engineering Ltd. *****
00024> ***** Bolton SERIAL#:3375279 *****
00025> *****
00026> *****
00027> *****
00028> ***** PROGRAM ARRAY DIMENSIONS *****
00029> ***** Maximum value for ID numbers : 10 *****
00030> ***** Max. number of rainfall points: 105408 *****
00031> ***** Max. number of flow points : 105408 *****
00032> *****
00033> *****
00034> *****
00035> *****
00036> ***** D E T A I L E D O U T P U T *****
00037> *****
00038> ***** DATE: 2024-01-30 TIME: 15:00:31 RUN COUNTER: 000507 *****
00039> *****
00040> * Input filename: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\S2-E.dat *
00041> * Output filename: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\S2-E.sum *
00042> * Summary filename: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\S2-E.sum *
00043> * User comments: *
00044> * 1: *
00045> * 2: *
00046> * 3: *
00047> *****
00048> *****
00049> *****
00050> 001:0001-----
00051> * Project Name: [Stella Homes Phase 2] Project Number: [22-3001]
00052> * Date : 2024-01-30a
00053> * Modeller : [MYS]
00054> * Company : Ecometric Incorporated
00055> * License # : 3375279
00056> *****
00057> * Existing Conditions for Phase 2 Subdivision
00058> * Filename: S2-E.dat
00059> *
00060> *
00061> *****
00062> *****
00063> | START | Project dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00064> | Rainfall dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00065> | TZERO = .00 hrs on 0
00066> | METOUT= 2 (output = METRIC)
00067> | NRUN = 001
00068> | NSTORM= 1
00069> | # 1=2Y6.STM
00070> *****
00071> 001:0002-----
00072> *****
00073> | READ STORM | Filename: 2yr/6hr
00074> | Ptotal= 36.00 mm | Comments: 2yr/6hr
00075> *****
00076> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
00077> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00078> .25 .000 | 2.00 12.240 | 3.75 5.040 | 5.50 .720
00079> .50 .720 | 2.25 12.240 | 4.00 2.880 | 5.75 .720
00080> .75 .720 | 2.50 33.120 | 4.25 2.880 | 6.00 .720
00081> 1.00 .720 | 2.75 33.120 | 4.50 1.440 | 6.25 .720
00082> 1.25 .720 | 3.00 9.360 | 4.75 1.440 |
00083> 1.50 4.320 | 3.25 9.360 | 5.00 .720 |
00084> 1.75 4.320 | 3.50 5.040 | 5.25 .720 |
00085> *****
00086> *****
00087> 001:0003-----
00088> *****
00089> | CALIB NASHYD | Area (ha)= 3.89 Curve Number (CN)=82.00
00090> | 01:303 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00091> | U.H. Tp (hrs)= .320
00092> *****
00093> Unit Hyd Qpeak (cms)= .464
00094> *****
00095> PEAK FLOW (cms)= .063 (i)
00096> TIME TO PEAK (hrs)= 3.033
00097> RUNOFF VOLUME (mm)= 8.268
00098> TOTAL RAINFALL (mm)= 36.000
00099> RUNOFF COEFFICIENT = .230
00100> *****
00101> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00102> *****
00103> *****
00104> 001:0004-----
00105> *****
00106> | CALIB NASHYD | Area (ha)= 1.02 Curve Number (CN)=84.00
00107> | 02:305 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00108> | U.H. Tp (hrs)= .190
00109> *****
00110> Unit Hyd Qpeak (cms)= .205
00111> *****
00112> PEAK FLOW (cms)= .025 (i)
00113> TIME TO PEAK (hrs)= 2.850
00114> RUNOFF VOLUME (mm)= 9.088
00115> TOTAL RAINFALL (mm)= 36.000
00116> RUNOFF COEFFICIENT = .252
00117> *****
00118> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00119> *****
00120> *****
00121> 001:0005-----
00122> * For Catchment 305:
00123> * Minor system goes to West outlet, major system goes to East Outlet 1
00124> *****
00125> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .129 (cms)
00126> | TotalHyd 02:305 | Number of inlets in system [NINLET] = 1
00127> | TotalHyd 02:305 | Total minor system capacity = .129 (cms)
00128> | Total major system storage [TMJSTO] = 0. (cu.m.)
00129> *****
00130> ID: NHYD AREA QPEAK TPEAK R.V. DWF
00131> (ha) (cms) (hrs) (mm) (cms)
00132> TOTAL HYD. 02:305 1.02 .025 2.850 9.088 .000
00133> *****
00134> MAJOR SYST 03:Major .00 .000 .000 .000 .000
00135> MINOR SYST 04:Minor 1.02 .025 2.850 9.088 .000

```

```

00136>
00137> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00138>
00139>-----
00140> 001:0006-----
00141>-----
00142> | ADD HYD (to EP ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00143> (ha) (cms) (hrs) (mm) (cms)
00144> ID1 01:303 3.89 .063 3.03 8.27 .000
00145> +ID2 03:Major .00 .000 .00 .00 .000
00146>-----
00147> SUM 05:to EP 3.89 .063 3.03 8.27 .000
00148>-----
00149> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00150>-----
00151>-----
00152> 001:0007-----
00153>-----
00154> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00155> | IN>05:(to EP ) |
00156> | OUT<06:(EPond ) | ***** OUTFLOW STORAGE TABLE *****
00157> OUTFLOW STORAGE | OUTFLOW STORAGE
00158> (cms) (ha.m.) | (cms) (ha.m.)
00159> .000 .000E+00 | .107 .5720E-01
00160> .006 .1900E-01 | .126 .6680E-01
00161> .007 .2540E-01 | .142 .7700E-01
00162> .008 .3240E-01 | .156 .8800E-01
00163> .052 .4000E-01 | .223 .9900E-01
00164> .085 .4830E-01 | .435 .1119E+00
00165>-----
00166> ROUTING RESULTS AREA QPEAK TPEAK R.V.
00167> (ha) (cms) (hrs) (mm)
00168> INFLOW >05: (to EP ) 3.89 .063 3.033 8.268
00169> OUTFLOW<06: (EPond ) 3.89 .007 5.167 8.268
00170> OVERFLOW<07: (EPOVF ) .00 .000 .000 .000
00171>-----
00172> TOTAL NUMBER OF SIMULATED OVERFLOWS = .00
00173> CUMULATIVE TIME OF OVERFLOWS (hours) = .00
00174> PERCENTAGE OF TIME OVERFLOWING (%) = .00
00175>-----
00176>-----
00177> PEAK FLOW REDUCTION [Qout/Qin] (%) = 10.701
00178> TIME SHIFT OF PEAK FLOW (min) = 128.00
00179> MAXIMUM STORAGE USED (ha.m.) = .2515E-01
00180>-----
00181>-----
00182> 001:0008-----
00183>-----
00184> | CALIB NASHYD | Area (ha)= 1.61 Curve Number (CN)=83.00
00185> | 08:304 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00186> | U.H. Tp (hrs)= .230
00187> *****
00188> Unit Hyd Qpeak (cms)= .267
00189> *****
00190> PEAK FLOW (cms)= .033 (i)
00191> TIME TO PEAK (hrs)= 2.900
00192> RUNOFF VOLUME (mm)= 8.664
00193> TOTAL RAINFALL (mm)= 36.000
00194> RUNOFF COEFFICIENT = .241
00195> *****
00196> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00197> *****
00198> *****
00199> 001:0009-----
00200>-----
00201> | CALIB NASHYD | Area (ha)= .09 Curve Number (CN)=83.00
00202> | 09:306 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00203> | U.H. Tp (hrs)= .110
00204> *****
00205> Unit Hyd Qpeak (cms)= .031
00206> *****
00207> PEAK FLOW (cms)= .003 (i)
00208> TIME TO PEAK (hrs)= 2.783
00209> RUNOFF VOLUME (mm)= 8.661
00210> TOTAL RAINFALL (mm)= 36.000
00211> RUNOFF COEFFICIENT = .241
00212> *****
00213> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00214> *****
00215>-----
00216> 001:0010-----
00217>-----
00218> | CALIB NASHYD | Area (ha)= 1.38 Curve Number (CN)=74.00
00219> | 01:302a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00220> | U.H. Tp (hrs)= .230
00221> *****
00222> Unit Hyd Qpeak (cms)= .229
00223> *****
00224> PEAK FLOW (cms)= .019 (i)
00225> TIME TO PEAK (hrs)= 2.900
00226> RUNOFF VOLUME (mm)= 5.866
00227> TOTAL RAINFALL (mm)= 36.000
00228> RUNOFF COEFFICIENT = .163
00229> *****
00230> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00231> *****
00232>-----
00233>-----
00234>-----
00235> | CALIB NASHYD | Area (ha)= 2.09 Curve Number (CN)=81.00
00236> | 02:302b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00237> | U.H. Tp (hrs)= .300
00238> *****
00239> Unit Hyd Qpeak (cms)= .266
00240> *****
00241> PEAK FLOW (cms)= .033 (i)
00242> TIME TO PEAK (hrs)= 3.000
00243> RUNOFF VOLUME (mm)= 7.899
00244> TOTAL RAINFALL (mm)= 36.000
00245> RUNOFF COEFFICIENT = .219
00246> *****
00247> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00248>-----
00249>-----
00250> 001:0012-----
00251>-----
00252> | ADD HYD (Node 4 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00253> (ha) (cms) (hrs) (mm) (cms)
00254> ID1 01:302a 1.38 .019 2.90 5.87 .000
00255> +ID2 02:302b 2.09 .033 3.00 7.90 .000
00256>-----
00257> SUM 03:Node 4 3.47 .051 2.95 7.09 .000
00258>-----
00259> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00260>-----
00261>-----
00262> 001:0013-----
00263> ** END OF RUN : 1
00264>-----
00265> *****
00266>-----
00267>-----
00268>-----
00269>-----
00270>-----

```

```

00271> -----
00272> | START | Project dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00273> | Rainfall dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00274> | TZERO = .00 hrs on
00275> | METOUT= 2 (output = METRIC)
00276> | NRUN = 002
00277> | NSTORM= 1
00278> | # 1=5Y6_STM
00279> -----
00280> 002:0002-----
00281> *-----
00282> *# Project Name: [Stella Homes Phase 2] Project Number: [22-3001]
00283> *# Date : 2024-01-30a
00284> *# Modeller : [MYS]
00285> *# Company : Ecmetrix Incorporated
00286> *# License # : 3375279
00287> *-----
00288> * Existing Conditions for Phase 2 Subdivision
00289> * Filename: S2-E.dat
00290> *
00291> *-----
00292> -----
00293> 002:0002-----
00294> -----
00295> | READ STORM | Filename: 5yr/6hr
00296> | Ptotal= 47.81 mm | Comments: 5yr/6hr
00297> -----
00298> | TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
00299> | hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00300> | .25 .000 | 2.00 16.250 | 3.75 6.690 | 5.50 .960
00301> | .50 .960 | 2.25 16.250 | 4.00 3.820 | 5.75 .960
00302> | .75 .960 | 2.50 43.980 | 4.25 3.820 | 6.00 .960
00303> | 1.00 .960 | 2.75 43.980 | 4.50 1.910 | 6.25 .960
00304> | 1.25 .960 | 3.00 12.430 | 4.75 1.910 |
00305> | 1.50 5.740 | 3.25 12.430 | 5.00 .960 |
00306> | 1.75 5.740 | 3.50 6.690 | 5.25 .960 |
00307> -----
00308> -----
00309> 002:0003-----
00310> -----
00311> | CALIB NASHYD | Area (ha)= 3.89 Curve Number (CN)=82.00
00312> | 01:303 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00313> | U.H. Tp(hrs)= .320
00314> -----
00315> | Unit Hyd Qpeak (cms)= .464
00316> -----
00317> | PEAK FLOW (cms)= .124 (i)
00318> | TIME TO PEAK (hrs)= 2.953
00319> | RUNOFF VOLUME (mm)= 15.279
00320> | TOTAL RAINFALL (mm)= 47.810
00321> | RUNOFF COEFFICIENT = .320
00322> -----
00323> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00324> -----
00325> -----
00326> 002:0004-----
00327> -----
00328> | CALIB NASHYD | Area (ha)= 1.02 Curve Number (CN)=84.00
00329> | 02:305 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00330> | U.H. Tp(hrs)= .190
00331> -----
00332> | Unit Hyd Qpeak (cms)= .205
00333> -----
00334> | PEAK FLOW (cms)= .047 (i)
00335> | TIME TO PEAK (hrs)= 2.833
00336> | RUNOFF VOLUME (mm)= 16.586
00337> | TOTAL RAINFALL (mm)= 47.810
00338> | RUNOFF COEFFICIENT = .347
00339> -----
00340> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00341> -----
00342> -----
00343> -----
00344> * For Catchment 305:
00345> * Minor system goes to West outlet, major system goes to East Outlet 1
00346> -----
00347> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .129 (cms)
00348> | TotalHyd 02:305 | Number of inlets in system [NINLET] = 1
00349> | Total minor system capacity = .129 (cms)
00350> | Total major system storage [TMJSTO] = 0. (cu.m.)
00351> -----
00352> | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00353> | (ha) (cms) (hrs) (mm) (cms)
00354> | TOTAL HYD. 02:305 1.02 .047 2.833 16.586 .000
00355> |-----|-----|-----|-----|-----|-----|
00356> | MAJOR SYST 03:Major .00 .000 .000 .000 .000 .000
00357> | MINOR SYST 04:Minor 1.02 .047 2.833 16.586 .000
00358> -----
00359> | NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00360> -----
00361> -----
00362> 002:0006-----
00363> -----
00364> | ADD HYD (to EP ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00365> | (ha) (cms) (hrs) (mm) (cms)
00366> | ID1 01:303 3.89 .124 2.98 15.28 .000
00367> | +ID2 03:Major .00 .000 .000 .000 .000
00368> |-----|-----|-----|-----|-----|-----|
00369> | SUM 05:to EP 3.89 .124 2.98 15.28 .000
00370> -----
00371> | NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00372> -----
00373> -----
00374> 002:0007-----
00375> -----
00376> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00377> | IN>05: (to EP ) |
00378> | OUT<06: (EPond ) |
00379> |-----|-----|-----|-----|-----|-----|
00380> | OUTFLOW STORAGE | OUTFLOW STORAGE
00381> | (cms) (ha.m.) | (cms) (ha.m.)
00382> | .000 .0000E+00 | .107 .5720E-01
00383> | .006 .1900E-01 | .126 .6680E-01
00384> | .007 .2540E-01 | .142 .7700E-01
00385> | .008 .3240E-01 | .156 .8800E-01
00386> | .052 .4000E-01 | .223 .9960E-01
00387> | .085 .4830E-01 | .435 .1119E+00
00388> -----
00389> | ROUTING RESULTS AREA QPEAK TPEAK R.V.
00390> | (ha) (cms) (hrs) (mm)
00391> | INFLOW >05: (to EP ) 3.89 .124 2.983 15.279
00392> | OUTFLOW<06: (EPond ) 3.89 .041 4.083 15.279
00393> | OVERFLOW<07: (EPOVF ) .00 .000 .000 .000
00394> -----
00395> | TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
00396> | CUMULATIVE TIME OF OVERFLOWS (hours) = .00
00397> | PERCENTAGE OF TIME OVERFLOWING (%) = .00
00398> -----
00399> | PEAK FLOW REDUCTION [Qout/Qin] (%) = 33.099
00400> | TIME SHIFT OF PEAK FLOW (min) = 66.00
00401> | MAXIMUM STORAGE USED (ha.m.) = .3810E-01
00402> -----
00403> -----
00404> 002:0008-----
00405> -----

```

```

00406> | CALIB NASHYD | Area (ha)= 1.61 Curve Number (CN)=83.00
00407> | 08:304 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00408> | U.H. Tp(hrs)= .230
00409> -----
00410> | Unit Hyd Qpeak (cms)= .267
00411> -----
00412> | PEAK FLOW (cms)= .065 (i)
00413> | TIME TO PEAK (hrs)= 2.867
00414> | RUNOFF VOLUME (mm)= 15.914
00415> | TOTAL RAINFALL (mm)= 47.810
00416> | RUNOFF COEFFICIENT = .333
00417> -----
00418> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00419> -----
00420> -----
00421> 002:0009-----
00422> -----
00423> | CALIB NASHYD | Area (ha)= .09 Curve Number (CN)=83.00
00424> | 09:306 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00425> | U.H. Tp(hrs)= .110
00426> -----
00427> | Unit Hyd Qpeak (cms)= .031
00428> -----
00429> | PEAK FLOW (cms)= .005 (i)
00430> | TIME TO PEAK (hrs)= 2.767
00431> | RUNOFF VOLUME (mm)= 15.911
00432> | TOTAL RAINFALL (mm)= 47.810
00433> | RUNOFF COEFFICIENT = .333
00434> -----
00435> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00436> -----
00437> -----
00438> -----
00439> -----
00440> | CALIB NASHYD | Area (ha)= 1.38 Curve Number (CN)=74.00
00441> | 01:302a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00442> | U.H. Tp(hrs)= .230
00443> -----
00444> | Unit Hyd Qpeak (cms)= .229
00445> -----
00446> | PEAK FLOW (cms)= .038 (i)
00447> | TIME TO PEAK (hrs)= 2.883
00448> | RUNOFF VOLUME (mm)= 11.252
00449> | TOTAL RAINFALL (mm)= 47.810
00450> | RUNOFF COEFFICIENT = .235
00451> -----
00452> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00453> -----
00454> -----
00455> 002:0011-----
00456> -----
00457> | CALIB NASHYD | Area (ha)= 2.09 Curve Number (CN)=81.00
00458> | 02:302b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00459> | U.H. Tp(hrs)= .300
00460> -----
00461> | Unit Hyd Qpeak (cms)= .266
00462> -----
00463> | PEAK FLOW (cms)= .066 (i)
00464> | TIME TO PEAK (hrs)= 2.967
00465> | RUNOFF VOLUME (mm)= 14.679
00466> | TOTAL RAINFALL (mm)= 47.810
00467> | RUNOFF COEFFICIENT = .307
00468> -----
00469> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00470> -----
00471> -----
00472> 002:0012-----
00473> -----
00474> | ADD HYD (Node 4 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00475> | (ha) (cms) (hrs) (mm) (cms)
00476> | ID1 01:302a 1.38 .038 2.88 11.25 .000
00477> | +ID2 02:302b 2.09 .066 2.97 14.68 .000
00478> |-----|-----|-----|-----|-----|-----|
00479> | SUM 03:Node 4 3.47 .103 2.93 13.32 .000
00480> -----
00481> | NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00482> -----
00483> -----
00484> 002:0013-----
00485> -----
00486> 002:0002-----
00487> | ** END OF RUN : 2
00488> -----
00489> *-----
00490> -----
00491> -----
00492> -----
00493> -----
00494> -----
00495> -----
00496> | START | Project dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00497> | Rainfall dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00498> | TZERO = .00 hrs on
00499> | METOUT= 2 (output = METRIC)
00500> | NRUN = 003
00501> | NSTORM= 1
00502> | # 1=10Y6_STM
00503> -----
00504> 003:0002-----
00505> *-----
00506> *# Project Name: [Stella Homes Phase 2] Project Number: [22-3001]
00507> *# Date : 2024-01-30a
00508> *# Modeller : [MYS]
00509> *# Company : Ecmetrix Incorporated
00510> *# License # : 3375279
00511> *-----
00512> * Existing Conditions for Phase 2 Subdivision
00513> * Filename: S2-E.dat
00514> *
00515> *-----
00516> -----
00517> 003:0002-----
00518> -----
00519> | READ STORM | Filename: 10yr/6hr
00520> | Ptotal= 55.69 mm | Comments: 10yr/6hr
00521> -----
00522> | TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
00523> | hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00524> | .25 .000 | 2.00 18.940 | 3.75 7.800 | 5.50 1.110
00525> | .50 1.110 | 2.25 18.940 | 4.00 4.460 | 5.75 1.110
00526> | .75 1.110 | 2.50 51.240 | 4.25 4.460 | 6.00 1.110
00527> | 1.00 1.110 | 2.75 51.240 | 4.50 2.230 | 6.25 1.110
00528> | 1.25 1.110 | 3.00 14.480 | 4.75 2.230 |
00529> | 1.50 6.680 | 3.25 14.480 | 5.00 1.110 |
00530> | 1.75 6.680 | 3.50 7.800 | 5.25 1.110 |
00531> -----
00532> -----
00533> 003:0003-----
00534> -----
00535> | CALIB NASHYD | Area (ha)= 3.89 Curve Number (CN)=82.00
00536> | 01:303 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00537> | U.H. Tp(hrs)= .320
00538> -----
00539> | Unit Hyd Qpeak (cms)= .464
00540> -----

```

```

00541> PEAK FLOW (cms)= .171 (i)
00542> TIME TO PEAK (hrs)= 2.967
00543> RUNOFF VOLUME (mm)= 20.578
00544> TOTAL RAINFALL (mm)= 55.690
00545> RUNOFF COEFFICIENT = .370
00546>
00547> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00548>
00549>
00550> 003:0004-----
00551>
00552> | CALIB NASHYD | Area (ha)= 1.02 Curve Number (CN)=84.00
00553> | 02:305 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00554> | U.H. Tp(hrs)= .190
00555>
00556> Unit Hyd Qpeak (cms)= .205
00557>
00558> PEAK FLOW (cms)= .064 (i)
00559> TIME TO PEAK (hrs)= 2.833
00560> RUNOFF VOLUME (mm)= 22.191
00561> TOTAL RAINFALL (mm)= 55.690
00562> RUNOFF COEFFICIENT = .398
00563>
00564> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00565>
00566>
00567> 003:0005-----
00568> * For Catchment 305:
00569> * Minor system goes to West outlet, major system goes to East Outlet 1
00570>
00571> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .129 (cms)
00572> | TotalHyd 02:305 | Number of inlets in system [NINLET] = 1
00573> | Total minor system capacity = .129 (cms)
00574> | Total major system storage [TMJSTO] = 0. (cu.m.)
00575>
00576> ID: NHYD AREA QPEAK TPEAK R.V. DWF
00577> (ha) (cms) (hrs) (mm) (cms)
00578> TOTAL HYD. 02:305 1.02 .064 2.833 22.191 .000
00579>
00580> MAJOR SYST 03:Major .00 .000 .000 .000 .000
00581> MINOR SYST 04:Minor 1.02 .064 2.833 22.191 .000
00582>
00583> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00584>
00585>
00586> 003:0006-----
00587>
00588> | ADD HYD (to EP ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00589> (ha) (cms) (hrs) (mm) (cms)
00590> | ID1 01:303 3.89 .171 2.97 20.58 .000
00591> | +ID2 03:Major .00 .000 .000 .000 .000
00592>
00593> SUM 05:to EP 3.89 .171 2.97 20.58 .000
00594>
00595> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00596>
00597>
00598> 003:0007-----
00599>
00600> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00601> | IN>05: (to EP ) |
00602> | OUT<06: (EPOnd ) |
00603>
00604> ===== OUTFLOW STORAGE TABLE =====
00605> OUTFLOW STORAGE | OUTFLOW STORAGE
00606> (cms) (ha.m.) | (cms) (ha.m.)
00607> .000 .0000E+00 | .107 .5720E-01
00608> .006 .1900E-01 | .126 .6680E-01
00609> .007 .2540E-01 | .142 .7700E-01
00610> .008 .3240E-01 | .156 .8800E-01
00611> .052 .4000E-01 | .223 .9960E-01
00612> .085 .4830E-01 | .435 .1119E+00
00613>
00614> ROUTING RESULTS AREA QPEAK TPEAK R.V.
00615> (ha) (cms) (hrs) (mm)
00616> INFLOW >05: (to EP ) 3.89 .171 2.967 20.578
00617> OUTFLOW<06: (EPOnd ) 3.89 .069 3.850 20.578
00618> OVERFLOW<07: (EPOVF ) .00 .000 .000 .000
00619>
00620> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
00621> CUMULATIVE TIME OF OVERFLOWS (hours) = .00
00622> PERCENTAGE OF TIME OVERFLOWING (%) = .00
00623>
00624> PEAK FLOW REDUCTION [Qout/Qin] (%) = 40.648
00625> TIME SHIFT OF PEAK FLOW (min) = 53.000
00626> MAXIMUM STORAGE USED (ha.m.) = .4441E-01
00627>
00628> 003:0008-----
00629>
00630> | CALIB NASHYD | Area (ha)= 1.61 Curve Number (CN)=83.00
00631> | 08:304 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00632> | U.H. Tp(hrs)= .230
00633>
00634> Unit Hyd Qpeak (cms)= .267
00635>
00636> PEAK FLOW (cms)= .088 (i)
00637> TIME TO PEAK (hrs)= 2.867
00638> RUNOFF VOLUME (mm)= 21.364
00639> TOTAL RAINFALL (mm)= 55.690
00640> RUNOFF COEFFICIENT = .384
00641>
00642> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00643>
00644>
00645> 003:0009-----
00646>
00647> | CALIB NASHYD | Area (ha)= .09 Curve Number (CN)=83.00
00648> | 09:306 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00649> | U.H. Tp(hrs)= .110
00650>
00651> Unit Hyd Qpeak (cms)= .031
00652>
00653> PEAK FLOW (cms)= .006 (i)
00654> TIME TO PEAK (hrs)= 2.767
00655> RUNOFF VOLUME (mm)= 21.362
00656> TOTAL RAINFALL (mm)= 55.690
00657> RUNOFF COEFFICIENT = .384
00658>
00659> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00660>
00661>
00662> 003:0010-----
00663>
00664> | CALIB NASHYD | Area (ha)= 1.38 Curve Number (CN)=74.00
00665> | 01:302a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00666> | U.H. Tp(hrs)= .230
00667>
00668> Unit Hyd Qpeak (cms)= .229
00669>
00670> PEAK FLOW (cms)= .053 (i)
00671> TIME TO PEAK (hrs)= 2.867
00672> RUNOFF VOLUME (mm)= 15.471
00673> TOTAL RAINFALL (mm)= 55.690
00674> RUNOFF COEFFICIENT = .278
00675>

```

```

00676> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00677>
00678>
00679> 003:0011-----
00680>
00681> | CALIB NASHYD | Area (ha)= 2.09 Curve Number (CN)=81.00
00682> | 02:302b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00683> | U.H. Tp(hrs)= .300
00684>
00685> Unit Hyd Qpeak (cms)= .266
00686>
00687> PEAK FLOW (cms)= .091 (i)
00688> TIME TO PEAK (hrs)= 2.950
00689> RUNOFF VOLUME (mm)= 19.831
00690> TOTAL RAINFALL (mm)= 55.690
00691> RUNOFF COEFFICIENT = .356
00692>
00693> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00694>
00695>
00696> 003:0012-----
00697>
00698> | ADD HYD (Node 4 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00699> (ha) (cms) (hrs) (mm) (cms)
00700> | ID1 01:302a 1.38 .053 2.87 15.47 .000
00701> | +ID2 02:302b 2.09 .091 2.95 19.83 .000
00702>
00703> SUM 03:Node 4 3.47 .143 2.92 18.10 .000
00704>
00705> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00706>
00707>
00708> 003:0013-----
00709>
00710> 003:0002-----
00711>
00712> 003:0002-----
00713> ** END OF RUN : 3
00714>
00715> *****
00716>
00717>
00718>
00719>
00720>
00721>
00722> | START | Project dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00723> | Rainfall dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00724> TZERO = .00 hrs on 0
00725> METOUT= 2 (output = METRIC)
00726> NRUN = 004
00727> NSTORM= 1
00728> # 1=25Y6.STM
00729>
00730> 004:0002-----
00731> *****
00732> ** Project Name: [Stella Homes Phase 2] Project Number: [22-3001]
00733> # Date : 2024-01-30a
00734> ** Modeller : [MVS]
00735> ** Company : Ecometrix Incorporated
00736> ** License # : 3375279
00737> *****
00738> * Existing Conditions for Phase 2 Subdivision
00739> * Filename: S2-E.dat
00740> *
00741> *****
00742>
00743>
00744>
00745> | READ STORM | Filename: 25yr/6hr
00746> | Ptotal= 65.59 mm | Comments: 25yr/6hr
00747>
00748> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
00749> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00750> .25 .000 | 2.00 22.300 | 3.75 9.180 | 5.50 1.310
00751> .50 1.310 | 2.25 22.300 | 4.50 5.250 | 5.75 1.310
00752> .75 1.310 | 2.50 60.350 | 4.25 5.250 | 6.00 1.310
00753> 1.00 1.310 | 2.75 60.350 | 4.50 2.620 | 6.25 1.310
00754> 1.25 1.310 | 3.00 17.060 | 4.75 2.620 |
00755> 1.50 7.870 | 3.25 17.060 | 5.00 1.310 |
00756> 1.75 7.870 | 3.50 9.180 | 5.25 1.310 |
00757>
00758>
00759> 004:0003-----
00760>
00761> | CALIB NASHYD | Area (ha)= 3.89 Curve Number (CN)=82.00
00762> | 01:303 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00763> | U.H. Tp(hrs)= .320
00764>
00765> Unit Hyd Qpeak (cms)= .464
00766>
00767> PEAK FLOW (cms)= .235 (i)
00768> TIME TO PEAK (hrs)= 2.950
00769> RUNOFF VOLUME (mm)= 27.753
00770> TOTAL RAINFALL (mm)= 65.590
00771> RUNOFF COEFFICIENT = .423
00772>
00773> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00774>
00775>
00776> 004:0004-----
00777>
00778> | CALIB NASHYD | Area (ha)= 1.02 Curve Number (CN)=84.00
00779> | 02:305 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00780> | U.H. Tp(hrs)= .190
00781>
00782> Unit Hyd Qpeak (cms)= .205
00783>
00784> PEAK FLOW (cms)= .086 (i)
00785> TIME TO PEAK (hrs)= 2.817
00786> RUNOFF VOLUME (mm)= 29.722
00787> TOTAL RAINFALL (mm)= 65.590
00788> RUNOFF COEFFICIENT = .453
00789>
00790> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00791>
00792>
00793> 004:0005-----
00794> * For Catchment 305:
00795> * Minor system goes to West outlet, major system goes to East Outlet 1
00796>
00797> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .129 (cms)
00798> | TotalHyd 02:305 | Number of inlets in system [NINLET] = 1
00799> | Total minor system capacity = .129 (cms)
00800> | Total major system storage [TMJSTO] = 0. (cu.m.)
00801>
00802> ID: NHYD AREA QPEAK TPEAK R.V. DWF
00803> (ha) (cms) (hrs) (mm) (cms)
00804> TOTAL HYD. 02:305 1.02 .086 2.817 29.722 .000
00805>
00806> MAJOR SYST 03:Major .00 .000 .000 .000 .000
00807> MINOR SYST 04:Minor 1.02 .086 2.817 29.722 .000
00808>
00809> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00810>

```

```

00811>-----
00812> 004:0006-----
00813>-----
00814> | ADD HYD (to EP ) | ID: NHYD      AREA   QPEAK  TPEAK  R.V.  DWF
00815>-----|-----|-----|-----|-----|-----
00816>          ID1 01:303      3.89   .235  2.95  27.75  .000
00817>          +ID2 03:Major    .00   .000  .00   .00   .000
00818>-----|-----|-----|-----|-----|-----
00819>          SUM 05:to EP    3.89   .235  2.95  27.75  .000
00820>-----
00821> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00822>-----
00823>-----
00824> 004:0007-----
00825>-----
00826> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00827> | IN>05:(to EP ) |
00828> | OUT<06:(EPond ) |
00829>-----|-----|-----|-----|-----|-----
00830>          OUTFLOW STORAGE | OUTFLOW STORAGE
00831>          (cms) (ha.m.) | (cms) (ha.m.)
00832>          .000 .0000E+00 | .107 .5720E-01
00833>          .006 .1900E-01 | .126 .6680E-01
00834>          .007 .2540E-01 | .142 .7700E-01
00835>          .008 .3240E-01 | .156 .8800E-01
00836>          .052 .4000E-01 | .223 .9960E-01
00837>          .085 .4830E-01 | .435 .1119E+00
00838>-----
00839> ROUTING RESULTS      AREA QPEAK TPEAK R.V.
00840>-----|-----|-----|-----|-----
00841> INFLOW >05:(to EP ) 3.89 .235 2.950 27.753
00842> OUTFLOW<06:(EPond ) 3.89 .101 3.750 27.753
00843> OVERFLOW<07:(EPOVF) .00 .000 .000 .000
00844>-----
00845> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
00846> CUMULATIVE TIME OF OVERFLOWS (hours) = .00
00847> PERCENTAGE OF TIME OVERFLOWING (%) = .00
00848>-----
00849> PEAK FLOW REDUCTION [Qout/Qin](%) = 43.020
00850> TIME SHIFT OF PEAK FLOW (min) = 48.00
00851> MAXIMUM STORAGE USED (ha.m.) = .5468E-01
00852>-----
00853>-----
00854> 004:0008-----
00855>-----
00856> | CALIB NASHYD | Area (ha) = 1.61 Curve Number (CN)=83.00
00857> | 08:304 DT= 1.00 | Ia (mm) = 10.000 # of Linear Res. (N) = 3.00
00858>-----|-----|-----|-----|-----
00859>          U.H. Tp (hrs) = .230
00860>-----
00861> Unit Hyd Qpeak (cms) = .267
00862>-----
00863> PEAK FLOW (cms) = .120 (i)
00864> TIME TO PEAK (hrs) = 2.850
00865> RUNOFF VOLUME (mm) = 28.716
00866> TOTAL RAINFALL (mm) = 65.590
00867> RUNOFF COEFFICIENT = .438
00868>-----
00869> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00870>-----
00871> 004:0009-----
00872>-----
00873> | CALIB NASHYD | Area (ha) = 1.09 Curve Number (CN)=83.00
00874> | 09:306 DT= 1.00 | Ia (mm) = 10.000 # of Linear Res. (N) = 3.00
00875>-----|-----|-----|-----|-----
00876>          U.H. Tp (hrs) = .110
00877>-----
00878> Unit Hyd Qpeak (cms) = .031
00879>-----
00880> PEAK FLOW (cms) = .009 (i)
00881> TIME TO PEAK (hrs) = 2.767
00882> RUNOFF VOLUME (mm) = 28.714
00883> TOTAL RAINFALL (mm) = 65.590
00884> RUNOFF COEFFICIENT = .438
00885>-----
00886> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00887>-----
00888>-----
00889> 004:0010-----
00890>-----
00891> | CALIB NASHYD | Area (ha) = 1.38 Curve Number (CN)=74.00
00892> | 01:302a DT= 1.00 | Ia (mm) = 10.000 # of Linear Res. (N) = 3.00
00893>-----|-----|-----|-----|-----
00894>          U.H. Tp (hrs) = .230
00895>-----
00896> Unit Hyd Qpeak (cms) = .229
00897>-----
00898> PEAK FLOW (cms) = .074 (i)
00899> TIME TO PEAK (hrs) = 2.867
00900> RUNOFF VOLUME (mm) = 21.336
00901> TOTAL RAINFALL (mm) = 65.590
00902> RUNOFF COEFFICIENT = .325
00903>-----
00904> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00905>-----
00906> 004:0011-----
00907>-----
00908> | CALIB NASHYD | Area (ha) = 2.09 Curve Number (CN)=81.00
00909> | 02:302b DT= 1.00 | Ia (mm) = 10.000 # of Linear Res. (N) = 3.00
00910>-----|-----|-----|-----|-----
00911>          U.H. Tp (hrs) = .300
00912>-----
00913> Unit Hyd Qpeak (cms) = .266
00914>-----
00915> PEAK FLOW (cms) = .126 (i)
00916> TIME TO PEAK (hrs) = 2.933
00917> RUNOFF VOLUME (mm) = 26.832
00918> TOTAL RAINFALL (mm) = 65.590
00919> RUNOFF COEFFICIENT = .409
00920>-----
00921> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00922>-----
00923>-----
00924> 004:0012-----
00925>-----
00926> | ADD HYD (Node 4 ) | ID: NHYD      AREA   QPEAK  TPEAK  R.V.  DWF
00927>-----|-----|-----|-----|-----|-----
00928>          ID1 01:302a    1.38   .074  2.87  21.34  .000
00929>          +ID2 02:302b    2.09   .126  2.93  26.83  .000
00930>-----|-----|-----|-----|-----|-----
00931>          SUM 03:Node 4    3.47   .198  2.90  24.65  .000
00932>-----
00933> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00934>-----
00935>-----
00936> 004:0002-----
00937>-----
00938> 004:0002-----
00939>-----
00940> 004:0002-----
00941> ** END OF RUN : 4
00942>-----
00943>-----
00944>-----
00945>-----

```

```

00946>-----
00947>-----
00948>-----
00949>-----
00950> | START | Project dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00951>-----|-----|-----|-----|-----|-----
00952> TZERO = .00 hrs on 0
00953> METOUT= 2 (output = METRIC)
00954> NRUN = 005
00955> NSTORM= 1
00956> # 1=50Y6.STM
00957>-----
00958>-----
00959> *****
00960> *# Project Name: [Stella Homes Phase 2] Project Number: [22-3001]
00961> *# Date : 2024-01-30a
00962> *# Modeller : [MYS]
00963> *# Company : Ecotriax Incorporated
00964> *# License # : 3375279
00965> *****
00966> * Existing Conditions for Phase 2 Subdivision
00967> * Filename: S2-E.dat
00968> *
00969> *****
00970>-----
00971> 005:0002-----
00972>-----
00973> | READ STORM | | Filename: 50yr/ghr
00974> | Ptotal= 73.00 mm | Comments: 50yr/ghr
00975>-----
00976>-----
00977> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
00978>-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----
00979> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00980> .25 .000 | 2.00 24.820 | 3.75 10.220 | 5.50 1.460
00981> .50 1.460 | 2.25 24.820 | 4.00 5.840 | 5.75 1.460
00982> .75 1.460 | 2.50 67.160 | 4.25 5.840 | 6.00 1.460
00983> 1.00 1.460 | 2.75 67.160 | 4.50 2.920 | 6.25 1.460
00984> 1.25 1.460 | 3.00 18.980 | 4.75 2.920 |
00985> 1.50 8.760 | 3.25 18.980 | 5.00 1.460 |
00986> 1.75 8.760 | 3.50 10.220 | 5.25 1.460 |
00987>-----
00988>-----
00989> 005:0003-----
00990>-----
00991> | CALIB NASHYD | Area (ha) = 3.89 Curve Number (CN)=82.00
00992> | 01:303 DT= 1.00 | Ia (mm) = 10.000 # of Linear Res. (N) = 3.00
00993>-----|-----|-----|-----|-----|-----
00994>          U.H. Tp (hrs) = .320
00995>-----
00996> Unit Hyd Qpeak (cms) = .464
00997>-----
00998> PEAK FLOW (cms) = .285 (i)
00999> TIME TO PEAK (hrs) = 2.950
01000> RUNOFF VOLUME (mm) = 33.421
01001> TOTAL RAINFALL (mm) = 73.000
01002> RUNOFF COEFFICIENT = .458
01003>-----
01004> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01005>-----
01006> 005:0004-----
01007>-----
01008> | CALIB NASHYD | Area (ha) = 1.02 Curve Number (CN)=84.00
01009> | 02:305 DT= 1.00 | Ia (mm) = 10.000 # of Linear Res. (N) = 3.00
01010>-----|-----|-----|-----|-----|-----
01011>          U.H. Tp (hrs) = .190
01012>-----
01013> Unit Hyd Qpeak (cms) = .205
01014>-----
01015> PEAK FLOW (cms) = .103 (i)
01016> TIME TO PEAK (hrs) = 2.617
01017> RUNOFF VOLUME (mm) = 35.634
01018> TOTAL RAINFALL (mm) = 73.000
01019> RUNOFF COEFFICIENT = .488
01020>-----
01021> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01022>-----
01023> 005:0005-----
01024>-----
01025> * For Catchment 305:
01026> Minor system goes to West outlet, major system goes to East Outlet 1
01027>-----
01028> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .129 (cms)
01029> | TotalHyd 02:305 | Number of inlets in system [NINLET] = 1
01030>-----|-----|-----|-----|-----|-----
01031>          Total minor system capacity = .129 (cms)
01032>          Total major system storage [TMJSTO] = 0. (cu.cm.)
01033>-----
01034> ID: NHYD      AREA   QPEAK  TPEAK  R.V.  DWF
01035>-----|-----|-----|-----|-----|-----
01036> MAJOR SYST 03:Major    .00 .000 .000 .000 .000
01037> MINOR SYST 04:Minor    1.02 .103 2.817 35.634 .000
01038>-----
01039> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01040>-----
01041> 005:0006-----
01042>-----
01043> | ADD HYD (to EP ) | ID: NHYD      AREA   QPEAK  TPEAK  R.V.  DWF
01044>-----|-----|-----|-----|-----|-----
01045>          ID1 01:303      3.89   .285  2.95  33.42  .000
01046>          +ID2 03:Major    .00   .000  .00   .00   .000
01047>-----|-----|-----|-----|-----|-----
01048>          SUM 05:to EP    3.89   .285  2.95  33.42  .000
01049>-----
01050> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01051>-----
01052> 005:0007-----
01053>-----
01054> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
01055> | IN>05:(to EP ) |
01056> | OUT<06:(EPond ) |
01057>-----|-----|-----|-----|-----|-----
01058>          OUTFLOW STORAGE | OUTFLOW STORAGE
01059>          (cms) (ha.m.) | (cms) (ha.m.)
01060>          .000 .0000E+00 | .107 .5720E-01
01061>          .006 .1900E-01 | .126 .6680E-01
01062>          .007 .2540E-01 | .142 .7700E-01
01063>          .008 .3240E-01 | .156 .8800E-01
01064>          .052 .4000E-01 | .223 .9960E-01
01065>          .085 .4830E-01 | .435 .1119E+00
01066>-----
01067> ROUTING RESULTS      AREA QPEAK TPEAK R.V.
01068>-----|-----|-----|-----|-----
01069> INFLOW >05:(to EP ) 3.89 .285 2.950 33.421
01070> OUTFLOW<06:(EPond ) 3.89 .121 3.733 33.421
01071> OVERFLOW<07:(EPOVF) .00 .000 .000 .000
01072>-----
01073> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
01074> CUMULATIVE TIME OF OVERFLOWS (hours) = .00
01075> PERCENTAGE OF TIME OVERFLOWING (%) = .00
01076>-----
01077> PEAK FLOW REDUCTION [Qout/Qin](%) = 42.346
01078> TIME SHIFT OF PEAK FLOW (min) = 47.00
01079> MAXIMUM STORAGE USED (ha.m.) = .6415E-01
01080>-----

```

```

01081>-----
01082> 005:0008-----
01083>-----
01084> | CALIB NASHYD | Area (ha)= 1.61 Curve Number (CN)=83.00
01085> | 08:304 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01086>-----
01087> U.H. Tp(hrs)= .230
01088>-----
01089> Unit Hyd Qpeak (cms)= .267
01090>-----
01091> PEAK FLOW (cms)= .145 (i)
01092> TIME TO PEAK (hrs)= 2.850
01093> RUNOFF VOLUME (mm)= 34.506
01094> TOTAL RAINFALL (mm)= 73.000
01095> RUNOFF COEFFICIENT = .473
01096>-----
01097> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01098>-----
01099> 005:0009-----
01100>-----
01101> | CALIB NASHYD | Area (ha)= .09 Curve Number (CN)=83.00
01102> | 09:306 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01103>-----
01104> U.H. Tp(hrs)= .110
01105>-----
01106> Unit Hyd Qpeak (cms)= .031
01107>-----
01108> PEAK FLOW (cms)= .010 (i)
01109> TIME TO PEAK (hrs)= 2.767
01110> RUNOFF VOLUME (mm)= 34.503
01111> TOTAL RAINFALL (mm)= 73.000
01112> RUNOFF COEFFICIENT = .473
01113>-----
01114> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01115>-----
01116> 005:0010-----
01117>-----
01118> | CALIB NASHYD | Area (ha)= 1.38 Curve Number (CN)=74.00
01119> | 01:302a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01120>-----
01121> U.H. Tp(hrs)= .230
01122>-----
01123> Unit Hyd Qpeak (cms)= .229
01124>-----
01125> PEAK FLOW (cms)= .091 (i)
01126> TIME TO PEAK (hrs)= 2.867
01127> RUNOFF VOLUME (mm)= 26.070
01128> TOTAL RAINFALL (mm)= 73.000
01129> RUNOFF COEFFICIENT = .357
01130>-----
01131> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01132>-----
01133> 005:0011-----
01134>-----
01135> | CALIB NASHYD | Area (ha)= 2.09 Curve Number (CN)=81.00
01136> | 02:302b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01137>-----
01138> U.H. Tp(hrs)= .300
01139>-----
01140> Unit Hyd Qpeak (cms)= .266
01141>-----
01142> PEAK FLOW (cms)= .153 (i)
01143> TIME TO PEAK (hrs)= 2.933
01144> RUNOFF VOLUME (mm)= 32.379
01145> TOTAL RAINFALL (mm)= 73.000
01146> RUNOFF COEFFICIENT = .444
01147>-----
01148> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01149>-----
01150> 005:0012-----
01151>-----
01152> | ADD HYD (Node 4 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01153> (ha) (cms) (hrs) (mm) (cms)
01154> ID1 01:302a 1.38 .091 2.87 26.07 .000
01155> +ID2 02:302b 2.09 .153 2.93 32.38 .000
01156>-----
01157> SUM 03:Node 4 3.47 .243 2.90 29.87 .000
01158>-----
01159> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01160>-----
01161>-----
01162> 005:0013-----
01163>-----
01164> 005:0002-----
01165>-----
01166> 005:0002-----
01167>-----
01168> 005:0002-----
01169>-----
01170> 005:0002-----
01171> ** END OF RUN : 5
01172>-----
01173>-----
01174>-----
01175>-----
01176>-----
01177>-----
01178>-----
01179>-----
01180> | START | Project dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
01181> Rainfall dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
01182> TZERO = .00 hrs on 0
01183> METOUT= 2 (output = METRIC)
01184> NRUN = 006
01185> NSTORM= 1
01186> # 1=100Y6.STM
01187>-----
01188> 006:0002-----
01189> #*****
01190> *# Project Name: [Stella Homes Phase 2] Project Number: [22-3001]
01191> *# Date : 2024-01-30a
01192> *# Modeller : [MYS]
01193> *# Company : Ecometric Incorporated
01194> *# License # : 3375279
01195> #*****
01196> * Existing Conditions for Phase 2 Subdivision
01197> * Filename: S2-E.dat
01198> *
01199> #*****
01200>-----
01201> 006:0002-----
01202>-----
01203> | READ STORM | Filename: 100yr/6hr
01204> | Ptotal= 80.31 mm | Comments: 100yr/6hr
01205>-----
01206> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
01207> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
01208> .25 .000 | 2.00 27.300 | 3.75 11.240 | 5.50 1.610
01209> .50 1.610 | 2.25 27.300 | 4.00 6.420 | 5.75 1.610
01210> .75 1.610 | 2.50 73.880 | 4.25 6.420 | 6.00 1.610
01211> 1.00 1.610 | 2.75 73.880 | 4.50 3.210 | 6.25 1.610
01212> 1.25 1.610 | 3.00 20.880 | 4.75 3.210 |
01213> 1.50 9.640 | 3.25 20.880 | 5.00 1.610 |
01214> 1.75 9.640 | 3.50 11.240 | 5.25 1.610 |
01215>-----

```

```

01216>-----
01217> 006:0003-----
01218>-----
01219> | CALIB NASHYD | Area (ha)= 3.89 Curve Number (CN)=82.00
01220> | 01:303 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01221>-----
01222> U.H. Tp(hrs)= .320
01223>-----
01224> Unit Hyd Qpeak (cms)= .464
01225>-----
01226> PEAK FLOW (cms)= .337 (i)
01227> TIME TO PEAK (hrs)= 2.933
01228> RUNOFF VOLUME (mm)= 39.213
01229> TOTAL RAINFALL (mm)= 80.310
01230> RUNOFF COEFFICIENT = .488
01231>-----
01232> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01233>-----
01234> 006:0004-----
01235>-----
01236> | CALIB NASHYD | Area (ha)= 1.02 Curve Number (CN)=84.00
01237> | 02:305 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01238>-----
01239> U.H. Tp(hrs)= .190
01240>-----
01241> Unit Hyd Qpeak (cms)= .205
01242>-----
01243> PEAK FLOW (cms)= .121 (i)
01244> TIME TO PEAK (hrs)= 2.617
01245> RUNOFF VOLUME (mm)= 41.650
01246> TOTAL RAINFALL (mm)= 80.310
01247> RUNOFF COEFFICIENT = .519
01248>-----
01249> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01250>-----
01251> 006:0005-----
01252> * For Catchment 305:
01253> Minor system goes to West outlet, major system goes to East Outlet 1
01254>-----
01255> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .129 (cms)
01256> | TotalHyd 02:305 | Number of inlets in system [MINLET] = 1
01257>-----
01258> Total minor system capacity = .129 (cms.)
01259> Total major system storage [TMJSTO] = 0. (cu.cm.)
01260>-----
01261> ID: NHYD AREA QPEAK TPEAK R.V. DWF
01262> (ha) (cms) (hrs) (mm) (cms)
01263> MAJOR HYD. 02:305 1.02 .121 2.817 41.650 .000
01264> MAJOR SYST 03:Major .00 .000 .000 .000 .000
01265> MINOR SYST 04:Minor 1.02 .121 2.817 41.650 .000
01266>-----
01267> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01268>-----
01269>-----
01270> 006:0006-----
01271>-----
01272> | ADD HYD (to EP ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01273> (ha) (cms) (hrs) (mm) (cms)
01274> ID1 01:303 3.89 3.89 .337 2.93 39.21 .000
01275> +ID2 03:Major .00 .000 .00 .00 .00 .000
01276>-----
01277> SUM 05:to EP 3.89 .337 2.93 39.21 .000
01278>-----
01279> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01280>-----
01281>-----
01282> 006:0007-----
01283>-----
01284> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
01285> | IN>05:(to EP ) |
01286> | OUT<06:(EPond ) |
01287>-----
01288> ===== OUTFLOW STORAGE TABLE =====
01289> OUTFLOW STORAGE | OUTFLOW STORAGE
01290> (cms) (ha.m.) | (cms) (ha.m.)
01291> .000 .000E+00 | .107 .5720E-01
01292> .006 .1900E-01 | .126 .6680E-01
01293> .007 .2540E-01 | .142 .7700E-01
01294> .008 .3240E-01 | .156 .8800E-01
01295> .052 .4000E-01 | .223 .9960E-01
01296> .085 .4830E-01 | .435 .1119E+00
01297>-----
01298> ROUTING RESULTS AREA QPEAK TPEAK R.V.
01299> (ha) (cms) (hrs) (mm)
01300> INFLOW>05: (to EP ) 3.89 .337 2.933 39.213
01301> OUTFLOW<06: (EPond ) 3.89 .138 3.733 39.213
01302> OVERFLOW<07: (EPOVF ) .00 .000 .000 .000
01303>-----
01304> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
01305> CUMULATIVE TIME OF OVERFLOWS (hours)= .00
01306> PERCENTAGE OF TIME OVERFLOWING (%) = .00
01307>-----
01308> PEAK FLOW REDUCTION [Qout/Qin] (%) = 41.111
01309> TIME SHIFT OF PEAK FLOW (min) = 48.00
01310> MAXIMUM STORAGE USED (ha.m.) = .7476E+01
01311>-----
01312> 006:0008-----
01313>-----
01314> | CALIB NASHYD | Area (ha)= 1.61 Curve Number (CN)=83.00
01315> | 08:304 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01316>-----
01317> U.H. Tp(hrs)= .230
01318>-----
01319> Unit Hyd Qpeak (cms)= .267
01320>-----
01321> PEAK FLOW (cms)= .171 (i)
01322> TIME TO PEAK (hrs)= 2.850
01323> RUNOFF VOLUME (mm)= 40.410
01324> TOTAL RAINFALL (mm)= 80.310
01325> RUNOFF COEFFICIENT = .503
01326>-----
01327> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01328>-----
01329> 006:0009-----
01330>-----
01331> | CALIB NASHYD | Area (ha)= .09 Curve Number (CN)=83.00
01332> | 09:306 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01333>-----
01334> U.H. Tp(hrs)= .110
01335>-----
01336> Unit Hyd Qpeak (cms)= .031
01337>-----
01338> PEAK FLOW (cms)= .012 (i)
01339> TIME TO PEAK (hrs)= 2.767
01340> RUNOFF VOLUME (mm)= 40.407
01341> TOTAL RAINFALL (mm)= 80.310
01342> RUNOFF COEFFICIENT = .503
01343>-----
01344> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01345>-----
01346> 006:0010-----
01347>-----
01348> | CALIB NASHYD | Area (ha)= 1.38 Curve Number (CN)=74.00
01349> | 01:302a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01350>-----
01351> U.H. Tp(hrs)= .230

```

```
01351>
01352> Unit Hyd Qpeak (cms)= .229
01353>
01354> PEAK FLOW (cms)= .109 (i)
01355> TIME TO PEAK (hrs)= 2.850
01356> RUNOFF VOLUME (mm)= 30.983
01357> TOTAL RAINFALL (mm)= 80.310
01358> RUNOFF COEFFICIENT = .386
01359>
01360> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01361>
01362> -----
01363> 006:0011-----
01364> -----
01365> | CALIB NASHYD | Area (ha)= 2.09 Curve Number (CN)=81.00
01366> | 02:302b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res.(N)= 3.00
01367> -----
01368> U.H. Tp(hrs)= .300
01369>
01369> Unit Hyd Qpeak (cms)= .266
01370>
01371> PEAK FLOW (cms)= .181 (i)
01372> TIME TO PEAK (hrs)= 2.917
01373> RUNOFF VOLUME (mm)= 38.059
01374> TOTAL RAINFALL (mm)= 80.310
01375> RUNOFF COEFFICIENT = .474
01376>
01377> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01378>
01379> -----
01380> 006:0012-----
01381> -----
01382> | ADD HYD (Node 4 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01383> (ha) (cms) (hrs) (mm) (cms)
01384> ID1 01:302a 1.38 .109 2.85 30.98 .000
01385> +ID2 02:302b 2.09 .181 2.92 38.06 .000
01386> =====
01387> SUM 03:Node 4 3.47 .288 2.88 35.24 .000
01388>
01389> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01390>
01391> -----
01392> 006:0013-----
01393> -----
01394> 006:0002-----
01395> -----
01396> 006:0002-----
01397> -----
01398> 006:0002-----
01399> -----
01400> 006:0002-----
01401> -----
01402> 006:0002-----
01403> FINISH
01404> -----
01405> *****
01406> WARNINGS / ERRORS / NOTES
01407> -----
01408> Simulation ended on 2024-01-30 at 15:00:32
01409> -----
01410>
01411>
```

```

00001> 2      Metric units
00002> #*****
00003> # Project Name: [Stella Homes Phase 2]      Project Number: [22-3001]
00004> # Date       : 2024-01-30a
00005> # Modeller   : [MYS]
00006> # Company    : Ecometrix Incorporated
00007> # License #   : 3375279
00008> #*****
00009> * Proposed Conditions for Phase 2 Subdivision
00010> * Filename: S2-P.dat
00011> *
00012> #*****
00013> START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[0]
00014> # ["2Y6.STM"] <--storm filename, one per line for NSTORM time
00015> # ["5Y6.STM"]
00016> # ["10Y6.STM"]
00017> # ["25Y6.STM"]
00018> # ["50Y6.STM"]
00019> # ["100Y6.STM"]
00020> #-----|
00021> READ STORM      STORM_FILENAME=["STORM.001"]
00022> #-----|
00023> CALIB NASHYD    ID=[ 1 ], NHYD=["403"], DT=[ 1 ]min, AREA=[3.64] (ha),
00024> DWF=[0] (cms), CN/C=[ 82 ], IA=[ 10 ](mm),
00025> N=[ 3 ], TP=[0.32] hrs,
00026> RAINFALL=[ , , , ](mm/hr), END=-1
00027> #-----|
00028> CALIB NASHYD    ID=[ 2 ], NHYD=["405"], DT=[ 1 ]min, AREA=[0.96] (ha),
00029> DWF=[ 0 ](cms), CN/C=[ 84 ], IA=[ 10 ](mm),
00030> N=[ 3 ], TP=[ 0.19 ]hrs,
00031> RAINFALL=[ , , , ](mm/hr), END=-1
00032> #-----|
00033> * For Catchment 405:
00034> * Minor system goes to West outlet, major system goes to East Outlet 1
00035> #-----|
00036> COMPUTE DUALHYD IDin=[2 ], CINLET=[0.129 ](cms), MINLET=[1 ],
00037> MAJID=[3 ], MAJNHYD=["Major"],
00038> MINID=[4 ], MINNHYD=["Minor"],
00039> TWISTO=[ 0 ](cu-m)
00040> #-----|
00041> CALIB NASHYD    ID=[ 5 ], NHYD=["404a"], DT=[ 1 ]min, AREA=[1.34] (ha),
00042> DWF=[ 0 ](cms), CN/C=[ 83 ], IA=[ 10 ](mm),
00043> N=[ 3 ], TP=[ 0.17 ]hrs,
00044> RAINFALL=[ , , , ](mm/hr), END=-1
00045> #-----|
00046> ADD HYD          IDsum=[ 6 ], NHYD=["to EP"], IDs to add=[ 1+3+5]
00047> #-----|
00048> ROUTE RESERVOIR IDoute=[ 7 ], NHYD=["EPond"], IDin=[ 6 ],
00049> RDT=[ 1 ](min),
00050> TABLE of ( OUTFLOW-STORAGE ) values
00051> (cms) - (ha-m)
00052> (0.0000 , 0.0000)
00053> (0.0056 , 0.0190)
00054> (0.0068 , 0.0254)
00055> (0.0078 , 0.0324)
00056> (0.0521 , 0.0400)
00057> (0.0847 , 0.0483)
00058> (0.1073 , 0.0572)
00059> (0.1258 , 0.0668)
00060> (0.1419 , 0.0770)
00061> (0.1562 , 0.0880)
00062> (0.2230 , 0.0996)
00063> (0.4348 , 0.1119)
00064> *-----|
00065> IDovf=[ 8 ], NHYDovf=["EPOVF"]
00066> #-----|
00067> CALIB NASHYD    ID=[ 9 ], NHYD=["404b"], DT=[ 1 ]min, AREA=[ 0.64] (ha),
00068> DWF=[ 0 ](cms), CN/C=[ 80 ], IA=[ 10 ](mm),
00069> N=[ 3 ], TP=[ 0.20 ]hrs,
00070> RAINFALL=[ , , , ](mm/hr), END=-1
00071> #-----|
00072> CALIB NASHYD    ID=[ 1 ], NHYD=["406"], DT=[ 1 ]min, AREA=[ 0.09 ](ha),
00073> DWF=[ 0 ](cms), CN/C=[ 76 ], IA=[ 10 ](mm),
00074> N=[ 3 ], TP=[ 0.11 ]hrs,
00075> RAINFALL=[ , , , ](mm/hr), END=-1
00076> #-----|
00077> CALIB NASHYD    ID=[ 2 ], NHYD=["402a"], DT=[ 1 ]min, AREA=[ 1.38 ](ha),
00078> DWF=[ 0 ](cms), CN/C=[ 74 ], IA=[ 10 ](mm),
00079> N=[ 3 ], TP=[ 0.23 ]hrs,
00080> RAINFALL=[ , , , ](mm/hr), END=-1
00081> #-----|
00082> CALIB NASHYD    ID=[ 3 ], NHYD=["402b"], DT=[ 1 ]min, AREA=[ 2.02 ](ha),
00083> DWF=[ 0 ](cms), CN/C=[ 78 ], IA=[ 10 ](mm),
00084> N=[ 3 ], TP=[ 0.30 ]hrs,
00085> RAINFALL=[ , , , ](mm/hr), END=-1
00086> #-----|
00087> ADD HYD          IDsum=[ 4 ], NHYD=["Node 4"], IDs to add=[ 2+3 ]
00088> #-----|
00089> START      TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[2]
00090> # ["5Y6.STM"] <--storm filename, one per line for NSTORM time
00091> #-----|
00092> START      TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[3]
00093> # ["10Y6.STM"] <--storm filename, one per line for NSTORM time
00094> #-----|
00095> START      TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[4]
00096> # ["25Y6.STM"] <--storm filename, one per line for NSTORM time
00097> #-----|
00098> START      TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[5]
00099> # ["50Y6.STM"] <--storm filename, one per line for NSTORM time
00100> #-----|
00101> START      TZERO=[0.0]hrs or date, METOUT=[2], NSTORM=[1], NRUN=[6]
00102> # ["100Y6.STM"] <--storm filename, one per line for NSTORM tim
00103> #-----|
00104> FINISH
00105>
00106>

```

```

00001> =====
00002>
00003> SSSSS W W M M H H Y Y M M OOO 999 999 =====
00004> S W W W M M M H H Y Y M M M O O 9 9 9 9
00005> SSSSS W W M M M H H H Y Y M M M O O ## 9 9 9 9 Ver 4.05
00006> S W W M M M H H Y Y M M O O 9999 9999 Sept 2011
00007> SSSSS W W M M H H Y Y M M OOO 9 9 9 =====
00008> StormWater Management Hydrologic Model 999 999 =====
00009>
00010>
00011> *****
00012> ***** SWMHYMO Ver/4.05 *****
00013> ***** A single event and continuous hydrologic simulation model *****
00014> ***** based on the principles of HYMO and its successors *****
00015> ***** OTTHYMO-83 and OTTHYMO-89. *****
00016> *****
00017> ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00018> ***** Ottawa, Ontario: (613) 836-3884 *****
00019> ***** Gatineau, Quebec: (819) 243-6858 *****
00020> ***** E-Mail: swmhyomj@fsa.com *****
00021> *****
00022>
00023> *****
00024> ***** Licensed user: Calder Engineering Ltd. *****
00025> ***** Bolton SERIAL#:3375279 *****
00026> *****
00027> *****
00028> ***** PROGRAM ARRAY DIMENSIONS *****
00029> *****
00030> ***** Maximum value for ID numbers : 10 *****
00031> ***** Max. number of rainfall points: 105408 *****
00032> ***** Max. number of flow points : 105408 *****
00033> *****
00034> *****
00035> *****
00036> ***** D E T A I L E D O U T P U T *****
00037> *****
00038> ***** DATE: 2024-01-30 TIME: 15:02:53 RUN COUNTER: 000508 *****
00039> *****
00040> * Input filename: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\S2-P.dat *
00041> * Output filename: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\S2-P.sum *
00042> * Summary filename: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\S2-P.sum *
00043> * User comments: *
00044> * 1: *
00045> * 2: *
00046> * 3: *
00047> *****
00048> *****
00049> *****
00050> 001:0001-----
00051> * Project Name: [Stella Homes Phase 2] Project Number: [22-3001]
00052> * Date : 2024-01-30a
00053> * Modeler : [MYS]
00054> * Company : Ecometrix Incorporated
00055> * License # : 3375279
00056> *****
00057> *****
00058> * Proposed Conditions for Phase 2 Subdivision
00059> * Filename: S2-P.dat
00060> *
00061> *****
00062> *****
00063> | START | Project dir : C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00064> | Rainfall dir: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00065> | TZERO = .00 hrs on 0
00066> | METOUT= 2 (output = METRIC)
00067> | NRUN = 001
00068> | NSTORM= 1
00069> | # 1=2Y6.STM
00070> *****
00071> 001:0002-----
00072> *****
00073> | READ STORM | Filename: 2yr/6hr
00074> | Ptotal= 36.00 mm | Comments: 2yr/6hr
00075> *****
00076>
00077> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
00078> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00079> .25 .000 | 2.00 12.240 | 3.75 5.040 | 5.50 .720
00080> .50 .720 | 2.25 12.240 | 4.00 2.880 | 5.75 .720
00081> .75 .720 | 2.50 33.120 | 4.25 2.880 | 6.00 .720
00082> 1.00 .720 | 2.75 33.120 | 4.50 1.440 | 6.25 .720
00083> 1.25 .720 | 3.00 9.360 | 4.75 1.440 |
00084> 1.50 4.320 | 3.25 9.360 | 5.00 .720 |
00085> 1.75 4.320 | 3.50 5.040 | 5.25 .720 |
00086> *****
00087> 001:0003-----
00088> *****
00089> | CALIB NASHYD | Area (ha)= 3.64 Curve Number (CN)=82.00
00090> | 01:403 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00091> | U.H. Tp (hrs)= .320
00092> *****
00093> Unit Hyd Qpeak (cms)= .434
00094> *****
00095> PEAK FLOW (cms)= .059 (i)
00096> TIME TO PEAK (hrs)= 3.033
00097> RUNOFF VOLUME (mm)= 8.268
00098> TOTAL RAINFALL (mm)= 36.000
00099> RUNOFF COEFFICIENT = .230
00100> *****
00101> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00102> *****
00103> *****
00104> 001:0004-----
00105> *****
00106> | CALIB NASHYD | Area (ha)= .96 Curve Number (CN)=84.00
00107> | 02:405 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00108> | U.H. Tp (hrs)= .190
00109> *****
00110> Unit Hyd Qpeak (cms)= .193
00111> *****
00112> PEAK FLOW (cms)= .023 (i)
00113> TIME TO PEAK (hrs)= 2.850
00114> RUNOFF VOLUME (mm)= 9.088
00115> TOTAL RAINFALL (mm)= 36.000
00116> RUNOFF COEFFICIENT = .252
00117> *****
00118> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00119> *****
00120> *****
00121> 001:0005-----
00122> * For Catchment 405:
00123> * Minor system goes to West outlet, major system goes to East Outlet 1
00124> *****
00125> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .129 (cms)
00126> | TotalHyd 02:405 | Number of inlets in system [NINLET] = 1
00127> | Total minor system capacity = .129 (cms)
00128> | Total major system storage [TMJSTO] = 0. (cu.m.)
00129> *****
00130> ID: NHYD AREA QPEAK TPEAK R.V. DWF
00131> (ha) (cms) (hrs) (mm) (mm) (cms)
00132> TOTAL HYD. 02:405 .96 .023 2.850 9.088 .000
00133> *****
00134> MAJOR SYST 03:Major .00 .000 .000 .000 .000
00135> MINOR SYST 04:Minor .96 .023 2.850 9.088 .000

```

```

00136>
00137> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00138>
00139> -----
00140> 001:0006-----
00141> *****
00142> | CALIB NASHYD | Area (ha)= 1.34 Curve Number (CN)=83.00
00143> | 05:404a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00144> | U.H. Tp (hrs)= .170
00145> *****
00146> Unit Hyd Qpeak (cms)= .301
00147> *****
00148> PEAK FLOW (cms)= .032 (i)
00149> TIME TO PEAK (hrs)= 2.833
00150> RUNOFF VOLUME (mm)= 8.664
00151> TOTAL RAINFALL (mm)= 36.000
00152> RUNOFF COEFFICIENT = .241
00153> *****
00154> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00155> *****
00156> *****
00157> 001:0007-----
00158> *****
00159> | ADD HYD (to EP ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00160> (ha) (cms) (hrs) (mm) (mm) (cms)
00161> ID1 01:403 3.64 .059 3.03 8.27 .000
00162> +ID2 03:Major .00 .000 .000 .00 .000
00163> +ID3 05:404a 1.34 .032 2.83 8.66 .000
00164> *****
00165> SUM 06:to EP 4.98 .085 2.93 8.37 .000
00166> *****
00167> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00168> *****
00169> *****
00170> 001:0008-----
00171> *****
00172> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00173> | IN<: (to EP) |
00174> | OUT<: (EPond) | ***** OUTFLOW STORAGE TABLE *****
00175> OUTFLOW STORAGE | OUTFLOW STORAGE
00176> (cms) (ha.m.) | (cms) (ha.m.)
00177> .000 .0000E+00 | .107 .5720E-01
00178> .006 .1900E-01 | .126 .6680E-01
00179> .007 .2540E-01 | .142 .7700E-01
00180> .008 .3240E-01 | .156 .8800E-01
00181> .052 .4000E-01 | .223 .9960E-01
00182> .085 .4830E-01 | .435 .1119E+00
00183> *****
00184> ROUTING RESULTS AREA QPEAK TPEAK R.V.
00185> (ha) (cms) (hrs) (mm)
00186> INFLOW >06: (to EP) 4.98 .085 2.933 8.375
00187> OUTFLOW<07: (EPond) 4.98 .010 4.983 8.375
00188> OVERFLOW<08: (EPOVF) .00 .000 .000 .000
00189> *****
00190> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
00191> CUMULATIVE TIME OF OVERFLOWS (hours) = .00
00192> PERCENTAGE OF TIME OVERFLOWING (%) = .00
00193> *****
00194> PEAK FLOW REDUCTION [Qout/Qin] (%) = 11.953
00195> TIME SHIFT OF PEAK FLOW (min) = 123.00
00196> MAXIMUM STORAGE USED (ha.m.) = 3.281E-01
00197> *****
00198> *****
00199> *****
00200> 001:0009-----
00201> *****
00202> | CALIB NASHYD | Area (ha)= .64 Curve Number (CN)=80.00
00203> | 09:404b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00204> | U.H. Tp (hrs)= .200
00205> *****
00206> Unit Hyd Qpeak (cms)= .122
00207> *****
00208> PEAK FLOW (cms)= .012 (i)
00209> TIME TO PEAK (hrs)= 2.867
00210> RUNOFF VOLUME (mm)= 7.552
00211> TOTAL RAINFALL (mm)= 36.000
00212> RUNOFF COEFFICIENT = .210
00213> *****
00214> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00215> *****
00216> *****
00217> 001:0010-----
00218> *****
00219> | CALIB NASHYD | Area (ha)= .09 Curve Number (CN)=76.00
00220> | 01:406 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00221> | U.H. Tp (hrs)= .110
00222> *****
00223> Unit Hyd Qpeak (cms)= .031
00224> *****
00225> PEAK FLOW (cms)= .002 (i)
00226> TIME TO PEAK (hrs)= 2.783
00227> RUNOFF VOLUME (mm)= 6.362
00228> TOTAL RAINFALL (mm)= 36.000
00229> RUNOFF COEFFICIENT = .177
00230> *****
00231> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00232> *****
00233> *****
00234> 001:0011-----
00235> *****
00236> | CALIB NASHYD | Area (ha)= 1.38 Curve Number (CN)=74.00
00237> | 02:402a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00238> | U.H. Tp (hrs)= .230
00239> *****
00240> Unit Hyd Qpeak (cms)= .229
00241> *****
00242> PEAK FLOW (cms)= .019 (i)
00243> TIME TO PEAK (hrs)= 2.900
00244> RUNOFF VOLUME (mm)= 5.866
00245> TOTAL RAINFALL (mm)= 36.000
00246> RUNOFF COEFFICIENT = .163
00247> *****
00248> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00249> *****
00250> *****
00251> 001:0012-----
00252> *****
00253> | CALIB NASHYD | Area (ha)= 2.02 Curve Number (CN)=78.00
00254> | 03:402b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00255> | U.H. Tp (hrs)= .300
00256> *****
00257> Unit Hyd Qpeak (cms)= .257
00258> *****
00259> PEAK FLOW (cms)= .028 (i)
00260> TIME TO PEAK (hrs)= 3.000
00261> RUNOFF VOLUME (mm)= 6.923
00262> TOTAL RAINFALL (mm)= 36.000
00263> RUNOFF COEFFICIENT = .192
00264> *****
00265> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00266> *****
00267> *****
00268> *****
00269> *****
00270> | ADD HYD (Node 4 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF

```

```

00271>-----
00272> ID1 02:402a      (ha) (cms) (hrs) (mm) (cms)
+ID2 03:402b      1.38 .019 2.90 5.87 .000
00273>-----
00274>-----
00275> SUM 04:Node 4      3.40 .046 2.95 6.49 .000
00276>-----
00277> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00278>-----
00279>-----
00280> 001:0014-----
00281> ** END OF RUN : 1
00282>-----
00283>-----
00284>-----
00285>-----
00286>-----
00287>-----
00288>-----
00289>-----
00290> | START | Project dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00291> | Rainfall dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00292> | TZERO = .00 hrs on 0
00293> | METOUT= 2 (output = METRIC)
00294> | NRUN = 002
00295> | NSTORM= 1
00296> | # 1=5Y6.STM
00297>-----
00298>-----
00299> * Project Name: [Stella Homes Phase 2] Project Number: [22-3001]
00300> * # Date : 2024-01-30a
00301> * # Modeller : [MYS]
00302> * # Company : Ecometric Incorporated
00303> * # License # : 3375279
00304> *-----
00305> * Proposed Conditions for Phase 2 Subdivision
00306> * Filename: S2-P.dat
00307> *-----
00308> *-----
00309> *-----
00310>-----
00311> 002:0002-----
00312>-----
00313> | READ STORM | Filename: Syc/ghr
00314> | Ptotal= 47.81 mm | Comments: Syc/ghr
00315>-----
00316>-----
00317> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
00318> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00319> .25 .000 | 2.00 16.250 | 3.75 6.690 | 5.50 .960
00320> .50 .960 | 2.25 16.250 | 4.00 3.820 | 5.75 .960
00321> .75 .960 | 2.50 43.980 | 4.25 3.820 | 6.00 .960
00322> 1.00 .960 | 2.75 43.980 | 4.50 1.910 | 6.25 .960
00323> 1.25 .960 | 3.00 12.430 | 4.75 1.910 |
00324> 1.50 5.740 | 3.25 12.430 | 5.00 .960 |
00325> 1.75 5.740 | 3.50 6.690 | 5.25 .960 |
00326>-----
00327> 002:0003-----
00328>-----
00329> | CALIB NASHYD | Area (ha)= 3.64 Curve Number (CN)=82.00
00330> | 01:403 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00331> | U.H. Tp (hrs)= .320
00332>-----
00333> Unit Hyd Qpeak (cms)= .434
00334>-----
00335> PEAK FLOW (cms)= .116 (i)
00336> TIME TO PEAK (hrs)= 2.983
00337> RUNOFF VOLUME (mm)= 15.279
00338> TOTAL RAINFALL (mm)= 47.810
00339> RUNOFF COEFFICIENT = .320
00340>-----
00341> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00342>-----
00343>-----
00344> 002:0004-----
00345>-----
00346> | CALIB NASHYD | Area (ha)= .96 Curve Number (CN)=84.00
00347> | 02:405 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00348> | U.H. Tp (hrs)= .190
00349>-----
00350> Unit Hyd Qpeak (cms)= .193
00351>-----
00352> PEAK FLOW (cms)= .044 (i)
00353> TIME TO PEAK (hrs)= 2.833
00354> RUNOFF VOLUME (mm)= 16.586
00355> TOTAL RAINFALL (mm)= 47.810
00356> RUNOFF COEFFICIENT = .347
00357>-----
00358> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00359>-----
00360>-----
00361> 002:0005-----
00362> * For Catchment 405:
00363> * Minor system goes to West outlet, major system goes to East Outlet 1
00364>-----
00365> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .129 (cms)
00366> | TotalHyd 02:405 | Number of inlets in system [NINLET] = 1
00367> | Total minor system capacity = .129 (cms)
00368> | Total major system storage [TMJSTO] = 0 (cu.m.)
00369>-----
00370> ID: NHYD AREA QPEAK TPEAK R.V. DWF
00371> (ha) (cms) (hrs) (mm) (cms)
00372>-----
00373> MAJOR SYST 03:Major .00 .000 .000 .000 .000
00374> MINOR SYST 04:Minor .96 .044 2.833 16.586 .000
00375>-----
00376>-----
00377> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00378>-----
00379>-----
00380> 002:0006-----
00381>-----
00382> | CALIB NASHYD | Area (ha)= 1.34 Curve Number (CN)=83.00
00383> | 05:404a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00384> | U.H. Tp (hrs)= .170
00385>-----
00386> Unit Hyd Qpeak (cms)= .301
00387>-----
00388> PEAK FLOW (cms)= .062 (i)
00389> TIME TO PEAK (hrs)= 2.817
00390> RUNOFF VOLUME (mm)= 15.914
00391> TOTAL RAINFALL (mm)= 47.810
00392> RUNOFF COEFFICIENT = .333
00393>-----
00394> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00395>-----
00396>-----
00397> 002:0007-----
00398>-----
00399> | ADD HYD (to EP ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00400> (ha) (cms) (hrs) (mm) (cms)
00401>-----
00402> ID1 01:403 3.64 .116 2.98 15.28 .000
00403> +ID2 03:Major .00 .000 .00 .00 .000
00404> +ID3 05:404a 1.34 .062 2.82 15.91 .000
00405>-----
00406> SUM 06:to EP 4.98 .168 2.90 15.45 .000

```

```

00406>-----
00407> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00408>-----
00409>-----
00410> 002:0008-----
00411>-----
00412> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00413> | IN>06: (to EP ) |
00414> | OUT<07: (EPond ) | ===== OUTFLOW STORAGE TABLE =====
00415>-----
00416> OUTFLOW STORAGE | OUTFLOW STORAGE
00417> (cms) (ha.m.) | (cms) (ha.m.)
00418> .000 .0000E+00 | .107 .5720E-01
00419> .006 .1900E-01 | .126 .6680E-01
00420> .007 .2540E-01 | .142 .7700E-01
00421> .008 .3240E-01 | .156 .8800E-01
00422> .052 .4000E-01 | .223 .9960E-01
00423> .085 .4830E-01 | .435 .1119E+00
00424>-----
00425> ROUTING RESULTS AREA QPEAK TPEAK R.V.
00426> (ha) (cms) (hrs) (mm)
00427> INFLOW >06: (to EP ) 4.98 .168 2.900 15.450
00428> OUTFLOW<07: (EPond ) 4.98 .065 3.867 15.449
00429> OVERFLOW<08: (EPOVF ) .00 .000 .000 .000
00430>-----
00431> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
00432> CUMULATIVE TIME OF OVERFLOWS (hours)= .00
00433> PERCENTAGE OF TIME OVERFLOWING (%) = .00
00434>-----
00435> PEAK FLOW REDUCTION [Qout/Qin] (%) = 38.483
00436> TIME SHIFT OF PEAK FLOW (min)= 58.00
00437> MAXIMUM STORAGE USED (ha.m.)= .4322E-01
00438>-----
00439>-----
00440> 002:0009-----
00441>-----
00442> | CALIB NASHYD | Area (ha)= .64 Curve Number (CN)=80.00
00443> | 09:404b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00444> | U.H. Tp (hrs)= .200
00445>-----
00446> Unit Hyd Qpeak (cms)= .122
00447>-----
00448> PEAK FLOW (cms)= .024 (i)
00449> TIME TO PEAK (hrs)= 2.850
00450> RUNOFF VOLUME (mm)= 14.111
00451> TOTAL RAINFALL (mm)= 47.810
00452> RUNOFF COEFFICIENT = .295
00453>-----
00454> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00455>-----
00456>-----
00457> 002:0010-----
00458>-----
00459> | CALIB NASHYD | Area (ha)= .09 Curve Number (CN)=76.00
00460> | 01:406 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00461> | U.H. Tp (hrs)= .110
00462>-----
00463> Unit Hyd Qpeak (cms)= .031
00464>-----
00465> PEAK FLOW (cms)= .004 (i)
00466> TIME TO PEAK (hrs)= 2.783
00467> RUNOFF VOLUME (mm)= 12.111
00468> TOTAL RAINFALL (mm)= 47.810
00469> RUNOFF COEFFICIENT = .253
00470>-----
00471> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00472>-----
00473>-----
00474> 002:0011-----
00475>-----
00476> | CALIB NASHYD | Area (ha)= 1.38 Curve Number (CN)=74.00
00477> | 02:402a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00478> | U.H. Tp (hrs)= .230
00479>-----
00480> Unit Hyd Qpeak (cms)= .229
00481>-----
00482> PEAK FLOW (cms)= .038 (i)
00483> TIME TO PEAK (hrs)= 2.883
00484> RUNOFF VOLUME (mm)= 11.252
00485> TOTAL RAINFALL (mm)= 47.810
00486> RUNOFF COEFFICIENT = .235
00487>-----
00488> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00489>-----
00490>-----
00491> 002:0012-----
00492>-----
00493> | CALIB NASHYD | Area (ha)= 2.02 Curve Number (CN)=78.00
00494> | 03:402b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00495> | U.H. Tp (hrs)= .300
00496>-----
00497> Unit Hyd Qpeak (cms)= .257
00498>-----
00499> PEAK FLOW (cms)= .056 (i)
00500> TIME TO PEAK (hrs)= 2.967
00501> RUNOFF VOLUME (mm)= 13.061
00502> TOTAL RAINFALL (mm)= 47.810
00503> RUNOFF COEFFICIENT = .273
00504>-----
00505> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00506>-----
00507>-----
00508> 002:0013-----
00509>-----
00510> | ADD HYD (Node 4 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00511> (ha) (cms) (hrs) (mm) (cms)
00512>-----
00513> ID1 02:402a 1.38 .038 2.88 11.25 .000
00514> +ID2 03:402b 2.02 .056 2.97 13.06 .000
00515>-----
00516> SUM 04:Node 4 3.40 .093 2.92 12.33 .000
00517>-----
00518> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00519>-----
00520> 002:0014-----
00521>-----
00522> 002:0002-----
00523> ** END OF RUN : 2
00524>-----
00525> *-----
00526> *-----
00527> *-----
00528> *-----
00529> *-----
00530> *-----
00531> *-----
00532> | START | Project dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00533> | Rainfall dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00534> | TZERO = .00 hrs on 0
00535> | METOUT= 2 (output = METRIC)
00536> | NRUN = 003
00537> | NSTORM= 1
00538> | # 1=10Y6.STM
00539>-----
00540> 003:0002-----

```

```

00541> *#*****
00542> *# Project Name: [Stella Homes Phase 2] Project Number: [22-3001]
00543> *# Date : 2024-01-30a
00544> *# Modeller : [MYS]
00545> *# Company : Ecometrix Incorporated
00546> *# License # : 3375279
00547> *#*****
00548> * Proposed Conditions for Phase 2 Subdivision
00549> * Filename: S2-P.dat
00550> *
00551> *#*****
00552> -----
00553> 003:0002-----
00554> -----
00555> | READ STORM | Filename: 10yr/6hr
00556> | Ptotal= 55.69 mm | Comments: 10yr/6hr
00557> -----
00558> | TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
00559> | hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00560> |.25 .000 | 2.00 18.940 | 3.75 7.800 | 5.50 1.110
00561> |.50 1.110 | 2.25 18.940 | 4.00 4.460 | 5.75 1.110
00562> |.75 1.110 | 2.50 51.240 | 4.25 4.460 | 6.00 1.110
00563> |1.00 1.110 | 2.75 51.240 | 4.50 2.230 | 6.25 1.110
00564> |1.25 1.110 | 3.00 14.480 | 4.75 2.230 |
00565> |1.50 6.680 | 3.25 14.480 | 5.00 1.110 |
00566> |1.75 6.680 | 3.50 7.800 | 5.25 1.110 |
00567> -----
00568> -----
00569> 003:0003-----
00570> -----
00571> | CALIB NASHYD | Area (ha)= 3.64 Curve Number (CN)=82.00
00572> | 01:403 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00573> | U.H. Tp(hrs)= .320
00574> -----
00575> | Unit Hyd Qpeak (cms)= .434
00576> -----
00577> | PEAK FLOW (cms)= .160 (i)
00578> | TIME TO PEAK (hrs)= 2.967
00579> | RUNOFF VOLUME (mm)= 20.578
00580> | TOTAL RAINFALL (mm)= 55.690
00581> | RUNOFF COEFFICIENT = .370
00582> -----
00583> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00584> -----
00585> -----
00586> 003:0004-----
00587> -----
00588> | CALIB NASHYD | Area (ha)= .96 Curve Number (CN)=84.00
00589> | 02:405 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00590> | U.H. Tp(hrs)= .190
00591> -----
00592> | Unit Hyd Qpeak (cms)= .193
00593> -----
00594> | PEAK FLOW (cms)= .060 (i)
00595> | TIME TO PEAK (hrs)= 2.833
00596> | RUNOFF VOLUME (mm)= 22.191
00597> | TOTAL RAINFALL (mm)= 55.690
00598> | RUNOFF COEFFICIENT = .398
00599> -----
00600> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00601> -----
00602> -----
00603> 003:0005-----
00604> * For Catchment 405:
00605> * Minor system goes to West outlet, major system goes to East Outlet 1
00606> -----
00607> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .129 (cms)
00608> | TotalHyd 02:405 | Number of inlets in system [NINLET] = 1
00609> | Total minor system capacity = .129 (cms)
00610> | Total major system storage [TMJSTO] = 0. (cu.m.)
00611> -----
00612> | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
00613> | (ha) | (cms) | (hrs) | (mm) | (cms) |
00614> | TOTAL HYD. 02:405 | .96 | .060 | 2.833 | 22.191 | .000
00615> |-----|-----|-----|-----|-----|-----|
00616> | MAJOR SYST 03:Major | .00 | .000 | .000 | .000 | .000
00617> | MINOR SYST 04:Minor | .96 | .060 | 2.833 | 22.191 | .000
00618> -----
00619> | NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00620> -----
00621> -----
00622> 003:0006-----
00623> -----
00624> | CALIB NASHYD | Area (ha)= 1.34 Curve Number (CN)=83.00
00625> | 05:404a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00626> | U.H. Tp(hrs)= .170
00627> -----
00628> | Unit Hyd Qpeak (cms)= .301
00629> -----
00630> | PEAK FLOW (cms)= .084 (i)
00631> | TIME TO PEAK (hrs)= 2.817
00632> | RUNOFF VOLUME (mm)= 21.364
00633> | TOTAL RAINFALL (mm)= 55.690
00634> | RUNOFF COEFFICIENT = .384
00635> -----
00636> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00637> -----
00638> -----
00639> 003:0007-----
00640> -----
00641> | ADD HYD (to EP ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
00642> | (ha) | (cms) | (hrs) | (mm) | (cms) |
00643> | ID1 01:403 | 3.64 | .160 | 2.97 | 20.58 | .000
00644> | +ID2 03:Major | .00 | .000 | .00 | .00 | .000
00645> | +ID3 05:404a | 1.34 | .084 | 2.82 | 21.36 | .000
00646> |-----|-----|-----|-----|-----|-----|
00647> | SUM 06:to EP | 4.98 | .232 | 2.88 | 20.79 | .000
00648> -----
00649> | NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00650> -----
00651> -----
00652> 003:0008-----
00653> -----
00654> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00655> | IN>06: (to EP ) |
00656> | OUT<07: (EPond ) |
00657> -----
00658> | ===== OUTFLOW STORAGE TABLE =====
00659> | OUTFLOW STORAGE | OUTFLOW STORAGE
00660> | (cms) (ha.m.) | (cms) (ha.m.)
00661> | .000 .000E+00 | .107 .5720E+01
00662> | .006 .1900E+01 | .126 .6680E+01
00663> | .007 .2540E+01 | .142 .7700E+01
00664> | .008 .3240E+01 | .156 .8800E+01
00665> | .052 .4000E+01 | .223 .9960E+01
00666> | .085 .4830E+01 | .435 .119E+02
00667> -----
00668> | ROUTING RESULTS | AREA | QPEAK | TPEAK | R.V.
00669> | (ha) | (cms) | (hrs) | (mm) |
00670> | INFLOW<06: (to EP ) | 4.98 | .232 | 2.883 | 20.790
00671> | OUTFLOW<07: (EPond ) | 4.98 | .096 | 3.717 | 20.789
00672> | OVERFLOW<08: (EPOVF ) | .00 | .000 | .000 | .000
00673> -----
00674> | TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
00675> | CUMULATIVE TIME OF OVERFLOWS (hours) = .00
00676> | PERCENTAGE OF TIME OVERFLOWING (%) = .00
00677> -----

```

```

00678> PEAK FLOW REDUCTION [Qout/Qin] (%) = 41.230
00679> TIME SHIFT OF PEAK FLOW (min) = 50.00
00680> MAXIMUM STORAGE USED (ha.m.) = 5256E-01
00681> -----
00682> 003:0009-----
00683> -----
00684> | CALIB NASHYD | Area (ha)= .64 Curve Number (CN)=80.00
00685> | 09:404b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00686> | U.H. Tp(hrs)= .200
00687> -----
00688> | Unit Hyd Qpeak (cms)= .122
00689> -----
00690> | PEAK FLOW (cms)= .033 (i)
00691> | TIME TO PEAK (hrs)= 2.833
00692> | RUNOFF VOLUME (mm)= 19.118
00693> | TOTAL RAINFALL (mm)= 55.690
00694> | RUNOFF COEFFICIENT = .343
00695> -----
00696> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00697> -----
00698> -----
00699> 003:0010-----
00700> -----
00701> | CALIB NASHYD | Area (ha)= .09 Curve Number (CN)=76.00
00702> | 01:406 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00703> | U.H. Tp(hrs)= .110
00704> -----
00705> | Unit Hyd Qpeak (cms)= .031
00706> -----
00707> | PEAK FLOW (cms)= .005 (i)
00708> | TIME TO PEAK (hrs)= 2.767
00709> | RUNOFF VOLUME (mm)= 16.579
00710> | TOTAL RAINFALL (mm)= 55.690
00711> | RUNOFF COEFFICIENT = .298
00712> -----
00713> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00714> -----
00715> -----
00716> 003:0011-----
00717> -----
00718> | CALIB NASHYD | Area (ha)= 1.38 Curve Number (CN)=74.00
00719> | 02:402a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00720> | U.H. Tp(hrs)= .230
00721> -----
00722> | Unit Hyd Qpeak (cms)= .229
00723> -----
00724> | PEAK FLOW (cms)= .053 (i)
00725> | TIME TO PEAK (hrs)= 2.867
00726> | RUNOFF VOLUME (mm)= 15.471
00727> | TOTAL RAINFALL (mm)= 55.690
00728> | RUNOFF COEFFICIENT = .278
00729> -----
00730> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00731> -----
00732> -----
00733> 003:0012-----
00734> -----
00735> | CALIB NASHYD | Area (ha)= 2.02 Curve Number (CN)=78.00
00736> | 03:402b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00737> | U.H. Tp(hrs)= .300
00738> -----
00739> | Unit Hyd Qpeak (cms)= .257
00740> -----
00741> | PEAK FLOW (cms)= .078 (i)
00742> | TIME TO PEAK (hrs)= 2.950
00743> | RUNOFF VOLUME (mm)= 17.792
00744> | TOTAL RAINFALL (mm)= 55.690
00745> | RUNOFF COEFFICIENT = .319
00746> -----
00747> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00748> -----
00749> -----
00750> 003:0013-----
00751> -----
00752> | ADD HYD (Node 4 ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
00753> | (ha) | (cms) | (hrs) | (mm) | (cms) |
00754> | ID1 02:402a | 1.38 | .053 | 2.87 | 15.47 | .000
00755> | +ID2 03:402b | 2.02 | .078 | 2.95 | 17.79 | .000
00756> |-----|-----|-----|-----|-----|-----|
00757> | SUM 04:Node 4 | 3.40 | .130 | 2.92 | 16.85 | .000
00758> -----
00759> | NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00760> -----
00761> -----
00762> 003:0014-----
00763> -----
00764> 003:0002-----
00765> -----
00766> 003:0002-----
00767> ** END OF RUN : 3
00768> -----
00769> *#*****
00770> -----
00771> -----
00772> -----
00773> -----
00774> -----
00775> -----
00776> | START | Project dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00777> | Rainfall dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
00778> | TZERO .00 hrs on
00779> | METOUT= 2 (output = METRIC)
00780> | NRUN = 004
00781> | NSTORM= 1
00782> | # I=25Y6.STM
00783> -----
00784> 004:0002-----
00785> *#*****
00786> *# Project Name: [Stella Homes Phase 2] Project Number: [22-3001]
00787> *# Date : 2024-01-30a
00788> *# Modeller : [MYS]
00789> *# Company : Ecometrix Incorporated
00790> *# License # : 3375279
00791> *#*****
00792> * Proposed Conditions for Phase 2 Subdivision
00793> * Filename: S2-P.dat
00794> *#*****
00795> *#*****
00796> *#*****
00797> 004:0002-----
00798> -----
00799> | READ STORM | Filename: 25yr/6hr
00800> | Ptotal= 65.59 mm | Comments: 25yr/6hr
00801> -----
00802> | TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
00803> | hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00804> |.25 .000 | 2.00 22.300 | 3.75 9.180 | 5.50 1.310
00805> |.50 1.310 | 2.25 22.300 | 4.00 5.250 | 5.75 1.310
00806> |.75 1.310 | 2.50 60.350 | 4.25 5.250 | 6.00 1.310
00807> |1.00 1.310 | 2.75 60.350 | 4.50 2.620 | 6.25 1.310
00808> |1.25 1.310 | 3.00 17.060 | 4.75 2.620 |
00809> |1.50 7.870 | 3.25 17.060 | 5.00 1.310 |
00810> |1.75 7.870 | 3.50 9.180 | 5.25 1.310 |

```

```

00811>
00812>-----
00813> 004:0003-----
00814>-----
00815> | CALIB NASHYD | Area (ha)= 3.64 Curve Number (CN)=82.00
00816> | 01:403 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00817>-----
00818> U.H. Tp(hrs)= .320
00819> Unit Hyd Qpeak (cms)= .434
00820>-----
00821> PEAK FLOW (cms)= .219 (i)
00822> TIME TO PEAK (hrs)= 2.950
00823> RUNOFF VOLUME (mm)= 27.753
00824> TOTAL RAINFALL (mm)= 65.590
00825> RUNOFF COEFFICIENT = .423
00826>-----
00827> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00828>-----
00830> 004:0004-----
00831>-----
00832> | CALIB NASHYD | Area (ha)= .96 Curve Number (CN)=84.00
00833> | 02:405 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00834>-----
00835> U.H. Tp(hrs)= .190
00836> Unit Hyd Qpeak (cms)= .193
00837>-----
00838> PEAK FLOW (cms)= .081 (i)
00839> TIME TO PEAK (hrs)= 2.817
00840> RUNOFF VOLUME (mm)= 29.722
00841> TOTAL RAINFALL (mm)= 65.590
00842> RUNOFF COEFFICIENT = .453
00843>-----
00844> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00845>-----
00846>-----
00847> 004:0005-----
00848> * For Catchment 405:
00849> * Minor system goes to West outlet, major system goes to East Outlet 1
00850>-----
00851> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .129 (cms)
00852> | TotalHyd 02:405 | Number of inlets in system [NINLET] = 1
00853> | | Total minor system capacity = .129 (cms)
00854> | | Total major system storage [TMJSTO] = 0. (cu.m.)
00855>-----
00856> ID: NHYD AREA QPEAK TPEAK R.V. DWF
00857> (ha) (cms) (hrs) (mm) (cms)
00858>-----
00859> TOTAL HYD. 02:405 .96 .081 2.817 29.722 .000
00860> MAJOR SYST 03:Major .00 .000 .000 .000 .000
00861> MINOR SYST 04:Minor .96 .081 2.817 29.722 .000
00862>-----
00863> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00864>-----
00866> 004:0006-----
00867>-----
00868> | CALIB NASHYD | Area (ha)= 1.34 Curve Number (CN)=83.00
00869> | 05:404a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00870>-----
00871> U.H. Tp(hrs)= .170
00872> Unit Hyd Qpeak (cms)= .301
00873>-----
00874> PEAK FLOW (cms)= .113 (i)
00875> TIME TO PEAK (hrs)= 2.800
00876> RUNOFF VOLUME (mm)= 28.716
00877> TOTAL RAINFALL (mm)= 65.590
00878> RUNOFF COEFFICIENT = .438
00879>-----
00880> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00881>-----
00882>-----
00884> 004:0007-----
00885> | ADD HYD (to EP ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00886> (ha) (cms) (hrs) (mm) (cms)
00887>-----
00888> ID1 01:403 3.64 .219 2.95 27.75 .000
00889> +ID2 03:Major .00 .000 .00 .00 .000
00890> +ID3 05:404a 1.34 .113 2.80 28.72 .000
00891>-----
00892> SUM 06:to EP 4.98 .318 2.88 28.01 .000
00893>-----
00894> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00895>-----
00896> 004:0008-----
00897>-----
00898> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00899> | IN>06:(to EP ) |
00900> | OUT<07:(EPond ) | ===== OUTFLOW STORAGE TABLE =====
00901> OUTFLOW STORAGE | OUTFLOW STORAGE
00902> (cms) (ha.m.) | (cms) (ha.m.)
00903>-----
00904> .000 .000E+00 | .107 .5720E-01
00905> .006 .190E-01 | .126 .6680E-01
00906> .007 .2540E-01 | .142 .7700E-01
00907> .008 .3240E-01 | .156 .8800E-01
00908> .052 .4000E-01 | .223 .9960E-01
00909> .085 .4830E-01 | .435 .1119E+00
00910>-----
00911> ROUTING RESULTS AREA QPEAK TPEAK R.V.
00912> (ha) (cms) (hrs) (mm)
00913>-----
00914> INFLOW >06: (to EP ) 4.98 .318 2.883 28.012
00915> OUTFLOW<07: (EPond ) 4.98 .128 3.683 28.012
00916> OVERFLOW<08: (EPOVF ) .00 .000 .000 .000
00917>-----
00918> NUMBER OF SIMULATED OVERFLOWS = 0
00919> CUMULATIVE TIME OF OVERFLOWS (hours)= .00
00920> PERCENTAGE OF TIME OVERFLOWING (%)= .00
00921>-----
00922> PEAK FLOW REDUCTION [Qout/Qin] (%)= 40.203
00923> TIME SHIFT OF PEAK FLOW (min)= 48.00
00924> MAXIMUM STORAGE USED (ha.m.)=.6803E-01
00925>-----
00926> 004:0009-----
00927>-----
00928> | CALIB NASHYD | Area (ha)= .64 Curve Number (CN)=80.00
00929> | 09:404b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00930>-----
00931> U.H. Tp(hrs)= .200
00932> Unit Hyd Qpeak (cms)= .122
00933>-----
00934> PEAK FLOW (cms)= .045 (i)
00935> TIME TO PEAK (hrs)= 2.833
00936> RUNOFF VOLUME (mm)= 25.948
00937> TOTAL RAINFALL (mm)= 65.590
00938> RUNOFF COEFFICIENT = .396
00939>-----
00940> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00941>-----
00942>-----
00944> 004:0010-----
00945> | CALIB NASHYD | Area (ha)= .09 Curve Number (CN)=76.00

```

```

00946> | 01:406 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00947>-----
00948> U.H. Tp(hrs)= .110
00949> Unit Hyd Qpeak (cms)= .031
00950>-----
00951> PEAK FLOW (cms)= .007 (i)
00952> TIME TO PEAK (hrs)= 2.767
00953> RUNOFF VOLUME (mm)= 22.753
00954> TOTAL RAINFALL (mm)= 65.590
00955> RUNOFF COEFFICIENT = .347
00956>-----
00957> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00958>-----
00959>-----
00960> 004:0011-----
00961>-----
00962> | CALIB NASHYD | Area (ha)= 1.38 Curve Number (CN)=74.00
00963> | 02:402a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00964>-----
00965> U.H. Tp(hrs)= .230
00966> Unit Hyd Qpeak (cms)= .229
00967>-----
00968> PEAK FLOW (cms)= .074 (i)
00969> TIME TO PEAK (hrs)= 2.867
00970> RUNOFF VOLUME (mm)= 21.336
00971> TOTAL RAINFALL (mm)= 65.590
00972> RUNOFF COEFFICIENT = .325
00973>-----
00974> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00975>-----
00976>-----
00977> 004:0012-----
00978>-----
00979> | CALIB NASHYD | Area (ha)= 2.02 Curve Number (CN)=78.00
00980> | 03:402b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
00981>-----
00982> U.H. Tp(hrs)= .300
00983> Unit Hyd Qpeak (cms)= .257
00984>-----
00985> PEAK FLOW (cms)= .109 (i)
00986> TIME TO PEAK (hrs)= 2.933
00987> RUNOFF VOLUME (mm)= 24.288
00988> TOTAL RAINFALL (mm)= 65.590
00989> RUNOFF COEFFICIENT = .370
00990>-----
00991> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00992>-----
00993>-----
00994> 004:0013-----
00995>-----
00996> | ADD HYD (Node 4 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00997> (ha) (cms) (hrs) (mm) (cms)
00998>-----
00999> ID1 02:402a 1.38 .074 2.87 21.34 .000
01000> +ID2 03:402b 2.02 .109 2.93 24.29 .000
01001>-----
01002> SUM 04:Node 4 3.40 .181 2.90 23.09 .000
01003>-----
01004> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01005>-----
01006> 004:0014-----
01007>-----
01008>-----
01009>-----
01010> 004:0002-----
01011>-----
01012> 004:0002-----
01013> ** END OF RUN : 4
01014>-----
01015> *****
01016>-----
01017>-----
01018>-----
01019>-----
01020>-----
01021>-----
01022> | START | Project dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
01023> | | Rainfall dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
01024> TZERO = .00 hrs on 0
01025> METOUT= 2 (output = METRIC)
01026> NRUN = 005
01027> NSTORM= 1
01028> # 1=50Y6.STM
01029>-----
01030> 005:0002-----
01031> *****
01032> ** Project Name: [Stella Homes Phase 2] Project Number: [22-3001]
01033> ** Date : 2024-01-30a
01034> ** Modeller : [MYS]
01035> ** Company : Ecometrix Incorporated
01036> ** License # : 3375279
01037> *****
01038> * Proposed Conditions for Phase 2 Subdivision
01039> * Filename: S2-P.dat
01040> *
01041> *****
01042>-----
01043> 005:0002-----
01044>-----
01045> | READ STORM | Filename: 50yr/6hr
01046> | Ptotal= 73.00 mm | Comments: 50yr/6hr
01047>-----
01048> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
01049> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
01050>-----
01051> .25 .000 | 2.00 24.820 | 3.75 10.220 | 5.50 1.460
01052> .50 1.460 | 2.25 24.820 | 4.00 5.840 | 5.75 1.460
01053> .75 1.460 | 2.50 67.160 | 4.25 5.840 | 6.00 1.460
01054> 1.00 1.460 | 2.75 67.160 | 4.50 2.920 | 6.25 1.460
01055> 1.25 1.460 | 3.00 18.980 | 4.75 2.920 |
01056> 1.50 8.760 | 3.25 18.980 | 5.00 1.460 |
01057> 1.75 8.760 | 3.50 10.220 | 5.25 1.460 |
01058>-----
01059> 005:0003-----
01060>-----
01061> | CALIB NASHYD | Area (ha)= 3.64 Curve Number (CN)=82.00
01062> | 01:403 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01063>-----
01064> U.H. Tp(hrs)= .320
01065> Unit Hyd Qpeak (cms)= .434
01066>-----
01067> PEAK FLOW (cms)= .267 (i)
01068> TIME TO PEAK (hrs)= 2.950
01069> RUNOFF VOLUME (mm)= 33.421
01070> TOTAL RAINFALL (mm)= 73.000
01071> RUNOFF COEFFICIENT = .458
01072>-----
01073> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01074>-----
01075>-----
01076> 005:0004-----
01077>-----
01078> | CALIB NASHYD | Area (ha)= .96 Curve Number (CN)=84.00
01079> | 02:405 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01080>-----
01081> U.H. Tp(hrs)= .190

```

```

01081> Unit Hyd Qpeak (cms)= .193
01082>
01083> PEAK FLOW (cms)= .097 (i)
01084> TIME TO PEAK (hrs)= 2.817
01085> RUNOFF VOLUME (mm)= 35.634
01086> TOTAL RAINFALL (mm)= 73.000
01087> RUNOFF COEFFICIENT = .488
01088>
01089> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01090>
01091>
01092> -----
01093> 005:0005-----
01094> * For Catchment 405:
01095> * Minor system goes to West outlet, major system goes to East Outlet 1
01096> -----
01097> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .129 (cms)
01098> | TotalHyd 02:405 | Number of inlets in system [NINLET] = 1
01099> |-----| Total minor system capacity = .129 (cms)
01100> |-----| Total major system storage [TMJSTO] = 0. (cu.m.)
01101>
01102> ID: NHYD AREA QPEAK TPEAK R.V. DWF
01103> (ha) (cms) (hrs) (mm) (cms)
01104> TOTAL HYD. 02:405 .96 .097 2.817 35.634 .000
01105> =====
01106> MAJOR SYST 03:Major .00 .000 .000 .000 .000
01107> MINOR SYST 04:Minor .96 .097 2.817 35.634 .000
01108>
01109> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01110>
01111> -----
01112> 005:0006-----
01113> -----
01114> | CALIB NASHYD | Area (ha)= 1.34 Curve Number (CN)=83.00
01115> | 05:404a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res.(N)= 3.00
01116> | U.H. Tp(hrs)= .170
01117>
01118> Unit Hyd Qpeak (cms)= .301
01119>
01120> PEAK FLOW (cms)= .136 (i)
01121> TIME TO PEAK (hrs)= 2.800
01122> RUNOFF VOLUME (mm)= 34.506
01123> TOTAL RAINFALL (mm)= 73.000
01124> RUNOFF COEFFICIENT = .473
01125>
01126> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01127>
01128> -----
01129> 005:0007-----
01130> -----
01131> | ADD HYD (to EP ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01132> (ha) (cms) (hrs) (mm) (cms)
01133> ID1 01:403 3.64 .267 2.95 33.42 .000
01134> +ID2 03:Major .00 .000 .00 .00 .000
01135> +ID3 05:404a 1.34 .136 2.80 34.51 .000
01136> =====
01137> | SUM 06:to EP 4.98 .386 2.87 33.71 .000
01138>
01139> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01140>
01141> -----
01142> 005:0008-----
01143> -----
01144> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
01145> | IN>06: (to EP ) |
01146> | OUT<07: (EPond ) | ===== OUTFLOW STORAGE TABLE =====
01147> OUTFLOW STORAGE | OUTFLOW STORAGE
01148> (cms) (ha.m.) | (cms) (ha.m.)
01149> .000 .000E+00 | .107 .5720E+01
01150> .006 .1900E-01 | .126 .6680E-01
01151> .007 .2540E-01 | .142 .7700E-01
01152> .008 .3240E-01 | .156 .8800E-01
01153> .052 .4000E-01 | .223 .9960E-01
01154> .085 .4830E-01 | .435 .119E+00
01155>
01156> ROUTING RESULTS AREA QPEAK TPEAK R.V.
01157> (ha) (cms) (hrs) (mm)
01158> CUMULATIVE TIME OF OVERFLOWS (hours)= .00
01159> OUTFLOW<07: (EPond ) 4.98 .148 3.700 33.713
01160> OVERFLOW<08: (EPOVF ) .00 .000 .000 .000
01161>
01162> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
01163> CUMULATIVE TIME OF OVERFLOWS (hours)= .00
01164> PERCENTAGE OF TIME OVERFLOWING (%)= .00
01165>
01166> PEAK FLOW REDUCTION [Qout/Qin] (%)= 38.431
01167> TIME SHIFT OF PEAK FLOW (min)= 50.000
01168> MAXIMUM STORAGE USED (ha.m.)=.8188E-01
01169>
01170> -----
01171> 005:0009-----
01172> -----
01173> -----
01174> | CALIB NASHYD | Area (ha)= .64 Curve Number (CN)=80.00
01175> | 09:404b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res.(N)= 3.00
01176> | U.H. Tp(hrs)= .200
01177>
01178> Unit Hyd Qpeak (cms)= .122
01179>
01180> PEAK FLOW (cms)= .055 (i)
01181> TIME TO PEAK (hrs)= 2.833
01182> RUNOFF VOLUME (mm)= 31.375
01183> TOTAL RAINFALL (mm)= 73.000
01184> RUNOFF COEFFICIENT = .430
01185>
01186> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01187>
01188> -----
01189> 005:0010-----
01190> -----
01191> | CALIB NASHYD | Area (ha)= .09 Curve Number (CN)=76.00
01192> | 01:406 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res.(N)= 3.00
01193> | U.H. Tp(hrs)= .110
01194>
01195> Unit Hyd Qpeak (cms)= .031
01196>
01197> PEAK FLOW (cms)= .008 (i)
01198> TIME TO PEAK (hrs)= 2.767
01199> RUNOFF VOLUME (mm)= 27.732
01200> TOTAL RAINFALL (mm)= 73.000
01201> RUNOFF COEFFICIENT = .380
01202>
01203> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01204>
01205> -----
01206> 005:0011-----
01207> -----
01208> | CALIB NASHYD | Area (ha)= 1.38 Curve Number (CN)=74.00
01209> | 02:402a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res.(N)= 3.00
01210> | U.H. Tp(hrs)= .230
01211>
01212> Unit Hyd Qpeak (cms)= .229
01213>
01214> PEAK FLOW (cms)= .091 (i)
01215> TIME TO PEAK (hrs)= 2.867

```

```

01216> RUNOFF VOLUME (mm)= 26.070
01217> TOTAL RAINFALL (mm)= 73.000
01218> RUNOFF COEFFICIENT = .357
01219>
01220> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01221>
01222> -----
01223> 005:0012-----
01224> -----
01225> | CALIB NASHYD | Area (ha)= 2.02 Curve Number (CN)=78.00
01226> | 03:402b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res.(N)= 3.00
01227> | U.H. Tp(hrs)= .300
01228>
01229> Unit Hyd Qpeak (cms)= .257
01230>
01231> PEAK FLOW (cms)= .133 (i)
01232> TIME TO PEAK (hrs)= 2.933
01233> RUNOFF VOLUME (mm)= 29.478
01234> TOTAL RAINFALL (mm)= 73.000
01235> RUNOFF COEFFICIENT = .404
01236>
01237> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01238>
01239> -----
01240> 005:0013-----
01241> -----
01242> | ADD HYD (Node 4 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01243> (ha) (cms) (hrs) (mm) (cms)
01244> ID1 02:402a 1.38 .091 2.87 26.07 .000
01245> +ID2 03:402b 2.02 .133 2.93 29.48 .000
01246> =====
01247> | SUM 04:Node 4 3.40 .223 2.90 28.09 .000
01248>
01249> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01250>
01251> -----
01252> 005:0014-----
01253> -----
01254> 005:0002-----
01255> -----
01256> 005:0002-----
01257> -----
01258> 005:0002-----
01259> -----
01260> 005:0002-----
01261> ** END OF RUN : 5
01262>
01263> -----
01264> -----
01265> -----
01266> -----
01267> -----
01268> -----
01269> -----
01270> | START | Project dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
01271> | Rainfall dir.: C:\PROGRA-2\SWMHYMO\PROJECTS\S-PH2\
01272> | TZERO = .00 hrs on 0
01273> | METOUT = 2 (output = METRIC)
01274> | NRUM = 006
01275> | NSTORM = 1
01276> | # 1=100Y6.STM
01277>
01278> -----
01279> *****
01280> ** Project Name: [Stella Homes Phase 2] Project Number: [22-3001]
01281> ** Date : 2024-01-30a
01282> ** Modeller : [MYS]
01283> ** Company : Ecotrix Incorporated
01284> ** License # : 3375279
01285> *****
01286> * Proposed Conditions for Phase 2 Subdivision
01287> * Filename: S2-P.dat
01288> *
01289> *****
01290> -----
01291> 006:0002-----
01292> -----
01293> | READ STORM | Filename: 100yr/6hr
01294> | Ptotal= 80.31 mm | Comments: 100yr/6hr
01295> -----
01296> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
01297> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
01298> .25 .000 | 2.00 27.300 | 3.75 11.240 | 5.50 1.610
01299> .50 1.610 | 2.25 27.300 | 4.00 6.420 | 5.75 1.610
01300> .75 1.610 | 2.50 73.880 | 4.25 6.420 | 6.00 1.610
01301> 1.00 1.610 | 2.75 73.880 | 4.50 3.210 | 6.25 1.610
01302> 1.25 1.610 | 3.00 20.880 | 4.75 3.210 |
01303> 1.50 9.640 | 3.25 20.880 | 5.00 1.610 |
01304> 1.75 9.640 | 3.50 11.240 | 5.25 1.610 |
01305>
01306> -----
01307> 006:0003-----
01308> -----
01309> | CALIB NASHYD | Area (ha)= 3.64 Curve Number (CN)=82.00
01310> | 01:403 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res.(N)= 3.00
01311> | U.H. Tp(hrs)= .320
01312>
01313> Unit Hyd Qpeak (cms)= .434
01314>
01315> PEAK FLOW (cms)= .315 (i)
01316> TIME TO PEAK (hrs)= 2.933
01317> RUNOFF VOLUME (mm)= 39.213
01318> TOTAL RAINFALL (mm)= 80.310
01319> RUNOFF COEFFICIENT = .488
01320>
01321> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01322>
01323> -----
01324> 006:0004-----
01325> -----
01326> | CALIB NASHYD | Area (ha)= .96 Curve Number (CN)=84.00
01327> | 02:405 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res.(N)= 3.00
01328> | U.H. Tp(hrs)= .190
01329>
01330> Unit Hyd Qpeak (cms)= .193
01331>
01332> PEAK FLOW (cms)= .114 (i)
01333> TIME TO PEAK (hrs)= 2.817
01334> RUNOFF VOLUME (mm)= 41.650
01335> TOTAL RAINFALL (mm)= 80.310
01336> RUNOFF COEFFICIENT = .519
01337>
01338> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01339>
01340> -----
01341> 006:0005-----
01342> * For Catchment 405:
01343> * Minor system goes to West outlet, major system goes to East Outlet 1
01344> -----
01345> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .129 (cms)
01346> | TotalHyd 02:405 | Number of inlets in system [NINLET] = 1
01347> |-----| Total minor system capacity = .129 (cms)
01348> |-----| Total major system storage [TMJSTO] = 0. (cu.m.)
01349>
01350> ID: NHYD AREA QPEAK TPEAK R.V. DWF

```

```

01351>
01352> TOTAL HYD. 02:405 (ha) (cms) (hrs) (mm) (cms)
01353> -----
01354> MAJOR SYST 03:Major .00 .000 .000 .000 .000 .000
01355> MINOR SYST 04:Minor .96 .114 2.817 41.650 .000
01356>
01357> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01358> -----
01359> 006:0006-----
01360>
01361>
01362> | CALIB NASHYD | Area (ha)= 1.34 Curve Number (CN)=83.00
01363> | 05:404a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01364> -----
01365> U.H. Tp(hrs)= .170
01366>
01367> Unit Hyd Qpeak (cms)= .301
01368>
01369> PEAK FLOW (cms)= .160 (i)
01370> TIME TO PEAK (hrs)= 2.800
01371> RUNOFF VOLUME (mm)= 40.410
01372> TOTAL RAINFALL (mm)= 80.310
01373> RUNOFF COEFFICIENT = .503
01374>
01375> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01376> -----
01377> 006:0007-----
01378>
01379> | ADD HYD (to EP ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01380> -----
01381> ID1 01:403 (ha) (cms) (hrs) (mm) (cms)
01382> +ID2 03:Major 3.64 .315 2.93 39.21 .000
01383> +ID3 05:404a .00 .000 .00 .00 .000
01384> -----
01385> SUM 06:to EP 4.98 .455 2.87 39.54 .000
01386>
01387> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01388> -----
01389> 006:0008-----
01390>
01391>
01392> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
01393> | IN>06: (EP ) |
01394> | OUT<07: (EPond ) | ===== OUTFLOW STORAGE TABLE =====
01395> -----
01396> OUTFLOW STORAGE | OUTFLOW STORAGE
01397> (cms) (ha.m.) | (cms) (ha.m.)
01398> .000 .0000E+00 | .107 .5720E-01
01399> .006 .1900E-01 | .126 .6680E-01
01400> .007 .2540E-01 | .142 .7700E-01
01401> .008 .3240E-01 | .156 .8800E-01
01402> .052 .4000E-01 | .223 .9960E-01
01403> .085 .4830E-01 | .435 .1119E+00
01404>
01405> ROUTING RESULTS AREA QPEAK TPEAK R.V.
01406> ----- (ha) (cms) (hrs) (mm)
01407> INFLOW >06: (to EP ) 4.98 .455 2.867 39.535
01408> OUTFLOW<07: (EPond ) 4.98 .193 3.600 39.534
01409> OVERFLOW<08: (EPOVF ) .00 .000 .000 .000
01410>
01411> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
01412> CUMULATIVE TIME OF OVERFLOWS (hours)= .00
01413> PERCENTAGE OF TIME OVERFLOWING (%) = .00
01414>
01415> PEAK FLOW REDUCTION [Qout/Qin] (%) = 42.477
01416> TIME SHIFT OF PEAK FLOW (min)= 44.00
01417> MAXIMUM STORAGE USED (ha.m.)=.9446E-01
01418> -----
01419> 006:0009-----
01420>
01421>
01422> | CALIB NASHYD | Area (ha)= .64 Curve Number (CN)=80.00
01423> | 09:404b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01424> -----
01425> U.H. Tp(hrs)= .200
01426>
01427> Unit Hyd Qpeak (cms)= .122
01428>
01429> PEAK FLOW (cms)= .065 (i)
01430> TIME TO PEAK (hrs)= 2.833
01431> RUNOFF VOLUME (mm)= 36.944
01432> TOTAL RAINFALL (mm)= 80.310
01433> RUNOFF COEFFICIENT = .460
01434>
01435> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01436> -----
01437> 006:0010-----
01438>
01439> | CALIB NASHYD | Area (ha)= .09 Curve Number (CN)=76.00
01440> | 01:406 DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01441> -----
01442> U.H. Tp(hrs)= .110
01443>
01444> Unit Hyd Qpeak (cms)= .031
01445>
01446> PEAK FLOW (cms)= .010 (i)
01447> TIME TO PEAK (hrs)= 2.767
01448> RUNOFF VOLUME (mm)= 32.840
01449> TOTAL RAINFALL (mm)= 80.310
01450> RUNOFF COEFFICIENT = .409
01451>
01452> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01453> -----
01454> 006:0011-----
01455>
01456> | CALIB NASHYD | Area (ha)= 1.38 Curve Number (CN)=74.00
01457> | 02:402a DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01458> -----
01459> U.H. Tp(hrs)= .230
01460>
01461> Unit Hyd Qpeak (cms)= .229
01462>
01463> PEAK FLOW (cms)= .109 (i)
01464> TIME TO PEAK (hrs)= 2.850
01465> RUNOFF VOLUME (mm)= 30.983
01466> TOTAL RAINFALL (mm)= 80.310
01467> RUNOFF COEFFICIENT = .386
01468>
01469> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01470> -----
01471> 006:0012-----
01472>
01473> | CALIB NASHYD | Area (ha)= 2.02 Curve Number (CN)=78.00
01474> | 03:402b DT= 1.00 | Ia (mm)= 10.000 # of Linear Res. (N)= 3.00
01475> -----
01476> U.H. Tp(hrs)= .300
01477>
01478> Unit Hyd Qpeak (cms)= .257
01479>
01480> PEAK FLOW (cms)= .158 (i)
01481> TIME TO PEAK (hrs)= 2.933
01482> RUNOFF VOLUME (mm)= 34.825
01483> TOTAL RAINFALL (mm)= 80.310
01484> RUNOFF COEFFICIENT = .434
01485>
01486> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

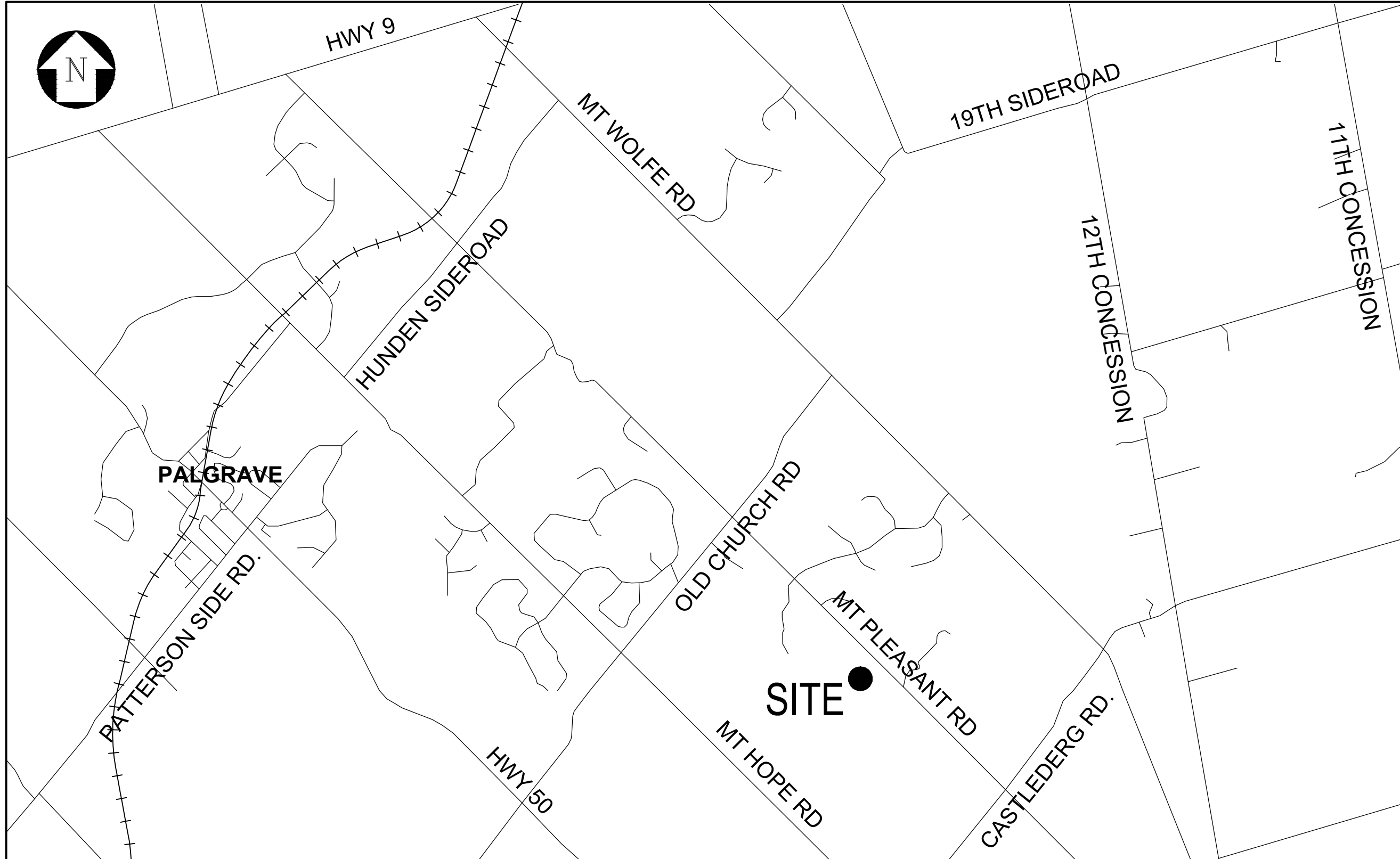
01486>
01487> -----
01488> 006:0013-----
01489>
01490> | ADD HYD (Node 4 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01491> ----- (ha) (cms) (hrs) (mm) (cms)
01492> ID1 02:402a 1.38 .109 2.85 30.98 .000
01493> +ID2 03:402b 2.02 .158 2.93 34.83 .000
01494> -----
01495> SUM 04:Node 4 3.40 .265 2.90 33.27 .000
01496>
01497> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01498> -----
01499> 006:0014-----
01500>
01501>
01502> 006:0002-----
01503>
01504> 006:0002-----
01505>
01506> 006:0002-----
01507>
01508> 006:0002-----
01509>
01510> 006:0002-----
01511> FINISH
01512>
01513> *****
01514> WARNINGS / ERRORS / NOTES
01515> -----
01516> Simulation ended on 2024-01-30 at 15:02:55
01517> -----
01518>
01519>

```

Appendix C Engineering Drawings

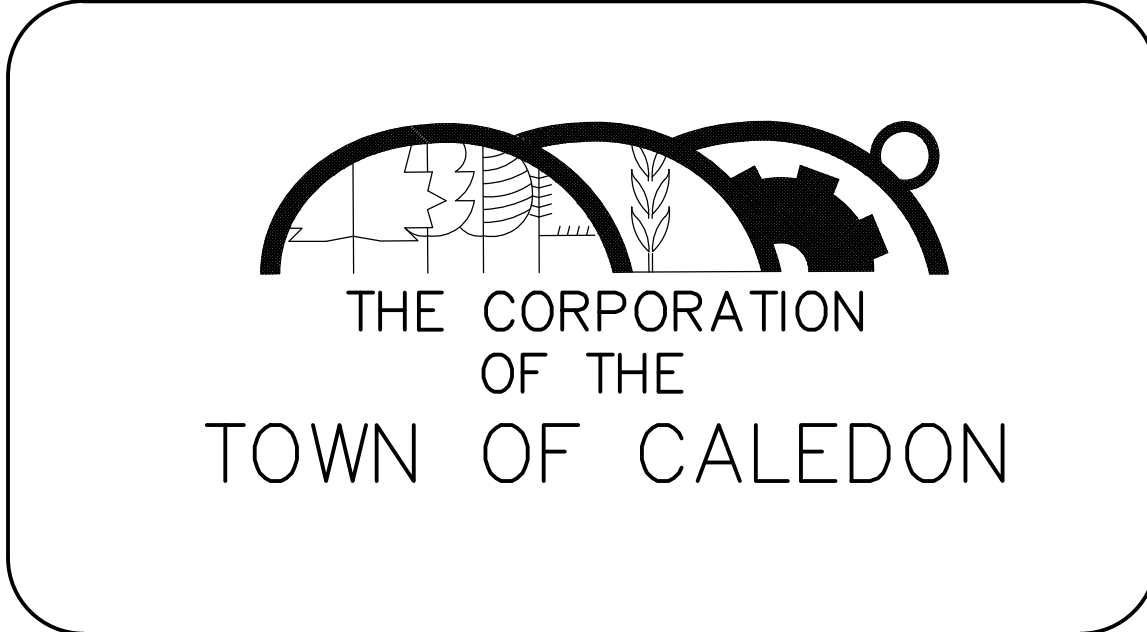
STELLAR ESTATES SUBDIVISION PHASE 2 DRAFT PLAN OF SUBDIVISION APPLICATION

0 MOUNT PLEASANT ROAD PART OF LOT 18, CONCESSION 8 (ALBION) TOWN OF CALEDON REGION OF PEEL



LIST OF DRAWINGS

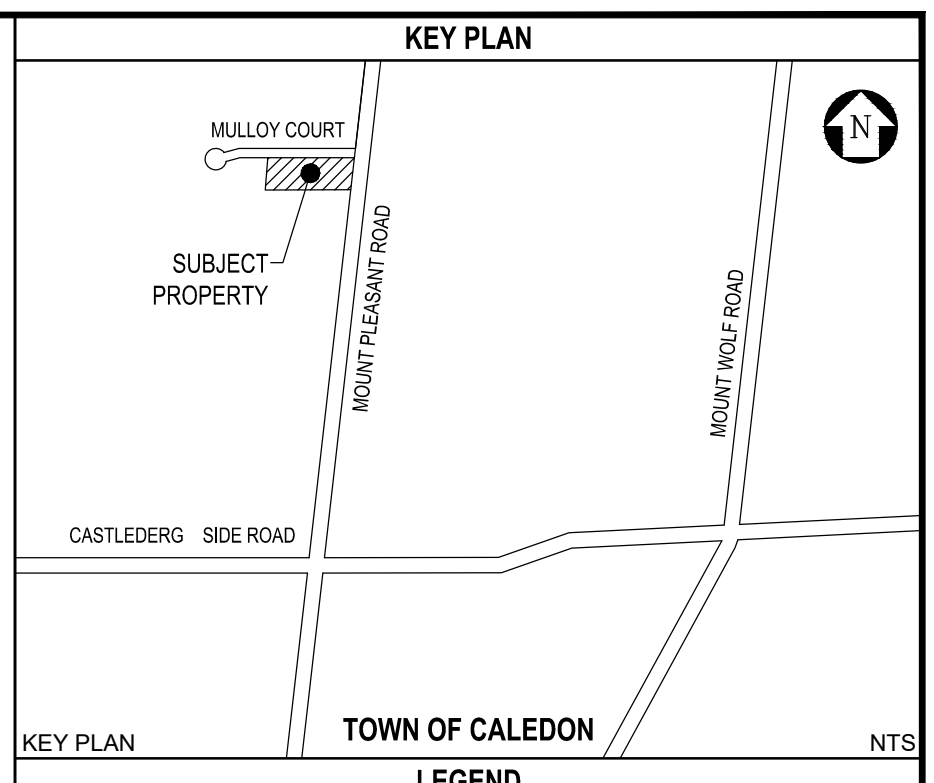
DRAWING TITLE	DRAWING	SHEET
SITE PLAN	22-3001-01	1
GENERAL ABOVE GROUND SERVICES PLAN	22-3001-02	2
GENERAL BELOW GROUND SERVICES PLAN	22-3001-03	3
WATER DISTRIBUTION PLAN	22-3001-04	4
STORM DRAINAGE PLAN	22-3001-05	5
MULLOY COURT PLAN AND PROFILE	22-3001-06	6
GRADING PLAN	22-3001-07	7
EROSION AND SEDIMENT CONTROL PLAN	22-3001-08	8
CONSTRUCTION DETAILS	22-3001-09	9
GENERAL NOTES AND SPECIFICATIONS	22-3001-10	10



LIST OF TOWN INFRASTRUCTURE

LENGTH OF ROAD	0m
LENGTH OF STORM SEWER	0m
NUMBER OF MANHOLES	0
NUMBER OF CATCH BASINS	0
NUMBER OF STREET LIGHTS	0
NUMBER OF OGS UNITS	1
NUM. OF STORMWATER MANAGEMENT FACILITIES	2





- LEGEND**
- PROPERTY LINES (PROPOSED)
 - PROPERTY LINES (EXISTING)
 - KEY NATURAL HERITAGE FEATURE
 - LIMIT OF PROP. STRUCTURE ENVELOPE
 - PROP. GRASSED SWALE
 - PROP. ENHANCED GRASS SWALE, MIN. 30.0m / LOT
 - MVPZ REHABILITATION PLANTINGS
 - LOT AREA OUTSIDE STRUCTURE ENVELOPE
 - STREETLIGHT POLE
 - ▲ HYDRO ONE TRANSFORMER
 - BHP
 - BHP
 - BHP
 - ① EX. STOP SIGN
 - ② EX. STREET SIGN
 - ③ EX. NO EXIT SIGN
 - MIN. 56 sq.m BACKYARD AMENITY AREA (CONCEPT PLAN)
- REFER TO GENERAL NOTES AND SPECIFICATIONS ON DWG 22-3001-10

LEGAL DESCRIPTION
 PART OF LOT 18, CONCESSION 8 AND BLOCK 15,
 PLAN 43M-1994 (GEOGRAPHIC TOWNSHIP OF ALBION)
 TOWN OF CALEDON
 REGIONAL MUNICIPALITY OF PEEL



DESIGNED BY		APPROVED BY	

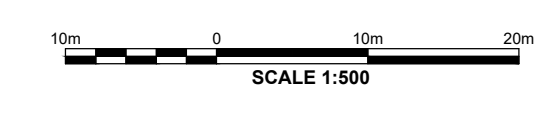
N ^o	Date	Revisions	Dwt.	Dsg'd.	Chk'd.
③	07/APR/2026	FOURTH SUBMISSION	AAF	AAF	RJW
②	21/NOV/2025	THIRD SUBMISSION	AAF	AAF	RJW
①	17/JAN/2025	SECOND SUBMISSION	AAF	AAF	RJW
①	26/JAN/2024	DPA APPLICATION	AAF	AAF	RJW

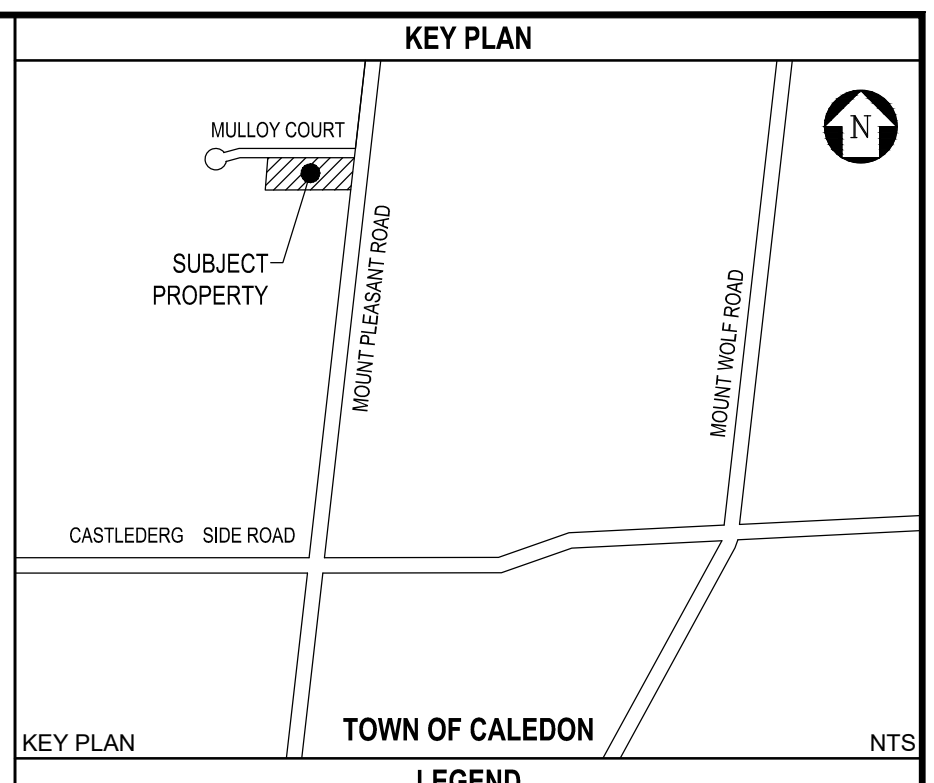
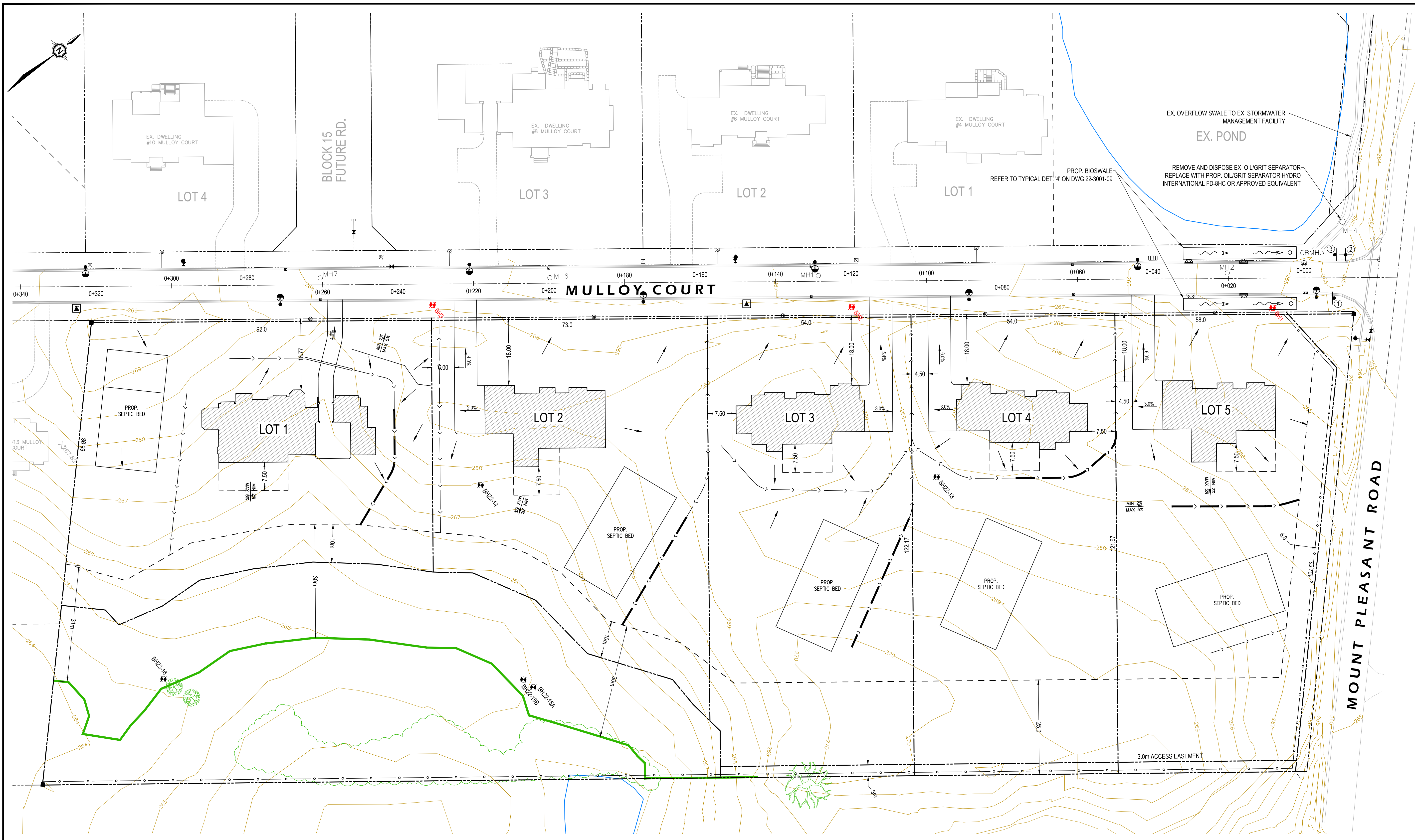
Client: **STELLAR HOMES INC.**

Project Name: **STELLAR ESTATES PHASE 2
 MULLOY COURT, TOWN OF CALEDON**

Title Name: **SITE PLAN**

Drawing N^o: **22-3001-01** Sheet N^o: **1 OF 10** Rev. N^o: **3**
 Scale: **1:500**





- LEGEND**
- PROPERTY LINES (PROPOSED)
 - PROPERTY LINES (EXISTING)
 - KEY NATURAL HERITAGE FEATURE
 - LIMIT OF PROP. STRUCTURE ENVELOPE
 - PROP. GRASSED SWALE
 - PROP. ENHANCED GRASS SWALE, MIN. 30.0m / LOT
 - PROP. POST AND WIRE FENCE
 - STREETLIGHT POLE
 - ▲ HYDRO ONE TRANSFORMER
 - ◆ BHP# 2007 BOREHOLES
 - ◆ BH22-# 2022 BOREHOLES
 - ① EX. STOP SIGN
 - ② EX. STREET SIGN
 - ③ EX. NO EXIT SIGN

REFER TO GENERAL NOTES AND SPECIFICATIONS ON DWG 22-3001-10

LOCATION OF RESIDENTIAL UNITS AND SEPTIC FIELDS ARE CONCEPTUAL ONLY. FINAL LOCATIONS TO BE DETERMINED AT THE SITE PLAN APPROVAL / BUILDING PERMIT APPLICATION STAGE

LEGAL DESCRIPTION
 PART OF LOT 18, CONCESSION 8 AND BLOCK 15,
 PLAN 43M-1994 (GEOGRAPHIC TOWNSHIP OF ALBION)
 TOWN OF CALEDON
 REGIONAL MUNICIPALITY OF PEEL



DESIGNED BY		APPROVED BY	

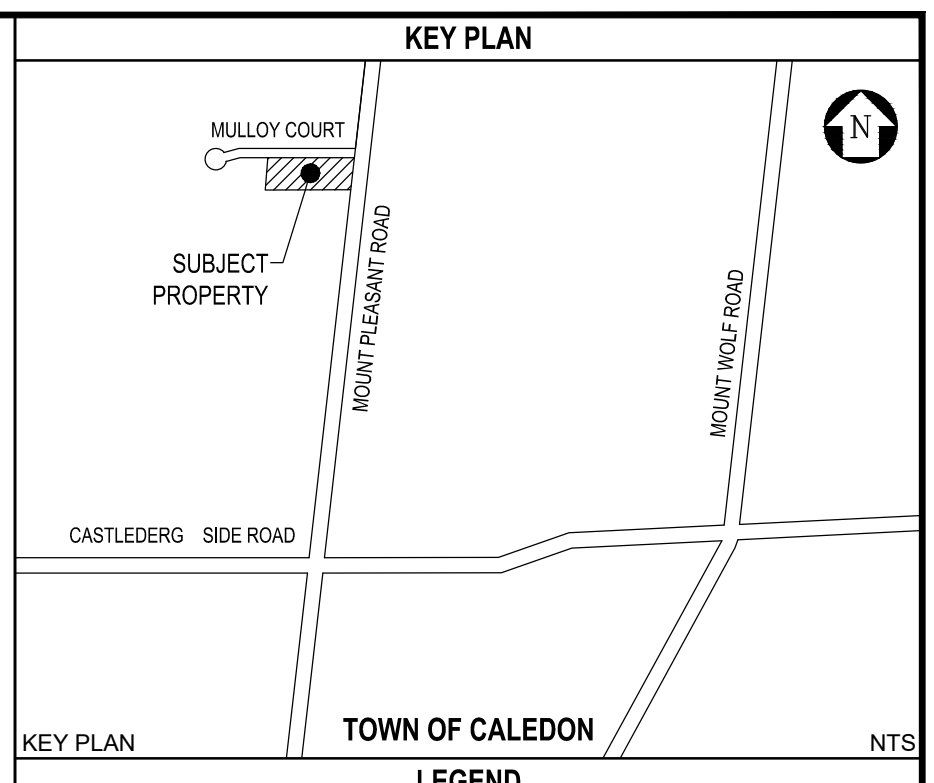
N ^o	Date	Revisions	Dwn.	Dsg'd.	Chk'd.
③	07/APR/2026	FOURTH SUBMISSION	AAF	AAF	RJW
②	21/NOV/2025	THIRD SUBMISSION	AAF	AAF	RJW
①	17/JAN/2025	SECOND SUBMISSION	AAF	AAF	RJW
①	26/JAN/2024	DPA APPLICATION	AAF	AAF	RJW

Client: **STELLAR HOMES INC.**

Project Name: **STELLAR ESTATES PHASE 2
MULLOY COURT, TOWN OF CALEDON**

Title Name: **GENERAL ABOVE
GROUND SERVICES PLAN**

Drawing N^o: **22-3001-02** Sheet N^o: **2 OF 10** Rev. N^o: **3**
 Scale: **1:500**



- LEGEND
- PROPERTY LINES (PROPOSED)
 - - - PROPERTY LINES (EXISTING)
 - KEY NATURAL HERITAGE FEATURE
 - - - LIMIT OF PROP. STRUCTURE ENVELOPE
 - - - PROP. GRASSED SWALE
 - - - PROP. ENHANCED GRASS SWALE, MIN. 30.0m / LOT
 - PROP. POST AND WIRE FENCE

REFER TO GENERAL NOTES AND SPECIFICATIONS ON
 DWG 22-3001-10
 LOCATION OF RESIDENTIAL UNITS AND SEPTIC FIELDS
 ARE CONCEPTUAL ONLY.
 FINAL LOCATIONS TO BE DETERMINED AT THE SITE
 PLAN APPROVAL / BUILDING PERMIT APPLICATION STAGE



DESIGNED BY		APPROVED BY	

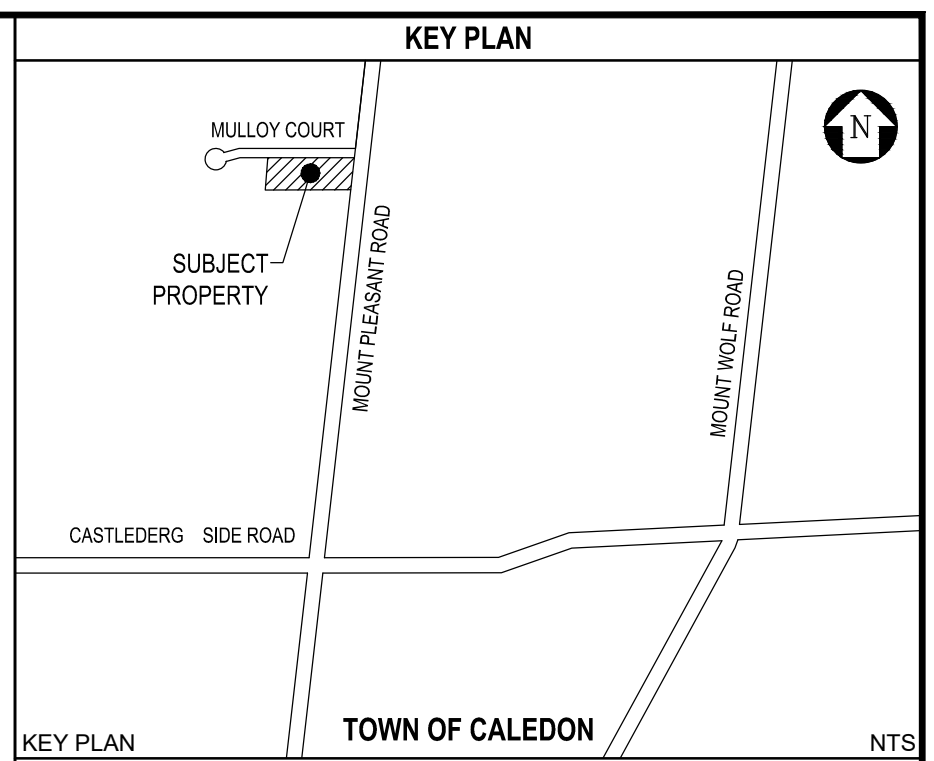
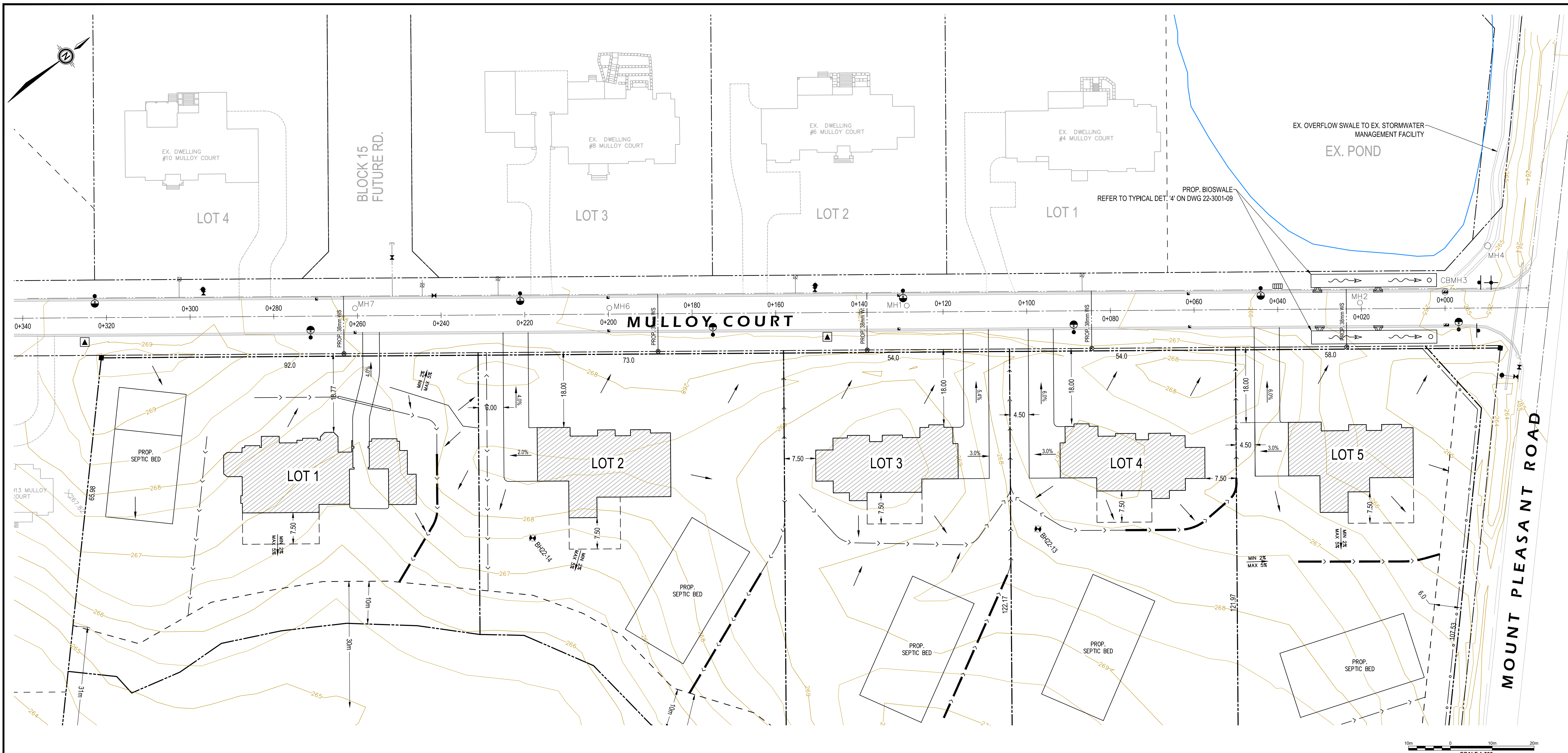
N ^o	Date	Revisions	Dwn.	Dsg'd.	Chk'd.
③	07/APR/2026	FOURTH SUBMISSION	AAF	AAF	RJW
②	21/NOV/2025	THIRD SUBMISSION	AAF	AAF	RJW
①	17/JAN/2025	SECOND SUBMISSION	AAF	AAF	RJW
①	26/JAN/2024	DPA APPLICATION	AAF	AAF	RJW

Client: **STELLAR HOMES INC.**

Project Name: **STELLAR ESTATES PHASE 2
MULLOY COURT, TOWN OF CALEDON**

Title Name: **GENERAL BELOW
GROUND SERVICES PLAN**

Drawing N^o: **22-3001-03** Sheet N^o: **3 OF 10** Rev. N^o: **3**
 Scale: **1:500**



LEGEND

- PROPERTY LINES (PROPOSED)
- PROPERTY LINES (EXISTING)
- KEY NATURAL HERITAGE FEATURE
- LIMIT OF STRUCTURE ENVELOPE (PROPOSED)
- PROP. GRASSED SWALE
- PROP. ENHANCED GRASS SWALE, MIN. 30.0m / LOT
- EX. WATERMAIN
- PROP. WATERMAIN CONNECTIONS
- EX. / PROP. WATER BOX
- ⊕ EX. GATE VALVE
- ⊙ EX. HYDRANT

SUBDIVISION STATISTICS (REGION)

SANITARY SEWER LENGTH	0m
NUMBER OF SANITARY MANHOLES	0
150mm - WATERMAIN LENGTH	0m
50mm - WATERMAIN LENGTH	0m
NUMBER OF HYDRANTS	0
NUMBER OF 38mm WATER SERVICES	5

RESIDENTIAL DEVELOPMENT CHARGES	No. OF UNITS	LOT#	METERS
No. OF SINGLE LOTS	5	-	-
No. OF SEMS (UNITS)	0	-	-
No. OF TOWNHOUSES	0	-	-
No. OF BLOCKS (FUTURE)	-	-	-
TOTAL No. OF WATER METERS	5	-	-

REFER TO GENERAL NOTES AND SPECIFICATIONS ON DWG 22-3001-10

LOCATION OF RESIDENTIAL UNITS AND SEPTIC FIELDS ARE CONCEPTUAL ONLY. FINAL LOCATIONS TO BE DETERMINED AT THE SITE PLAN APPROVAL / BUILDING PERMIT APPLICATION STAGE.



DESIGNED BY		APPROVED BY	

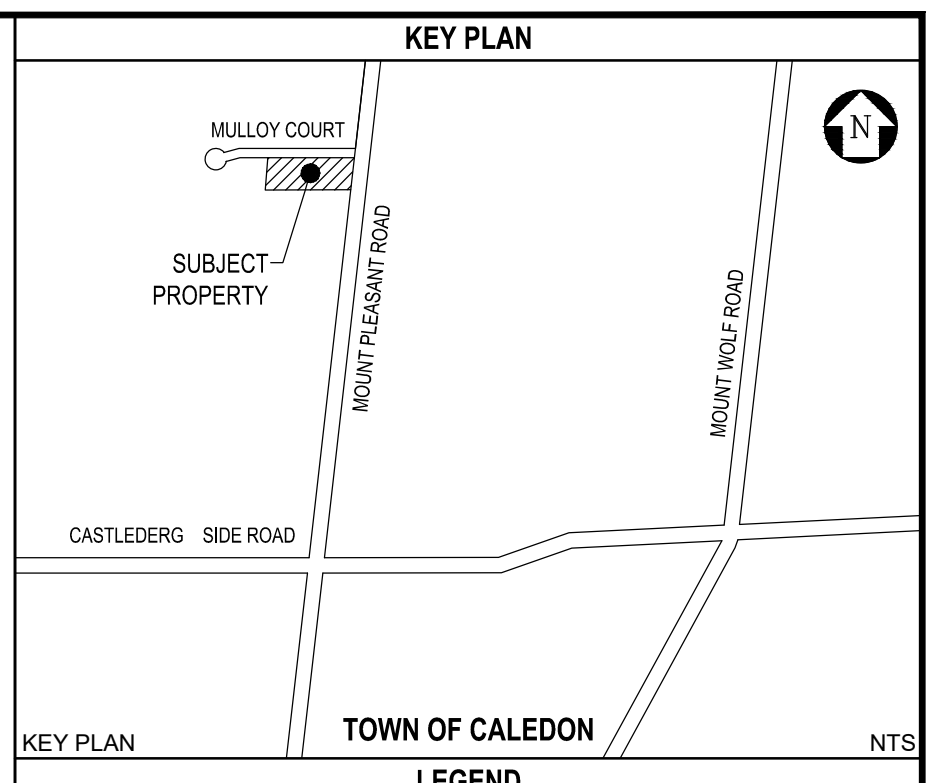
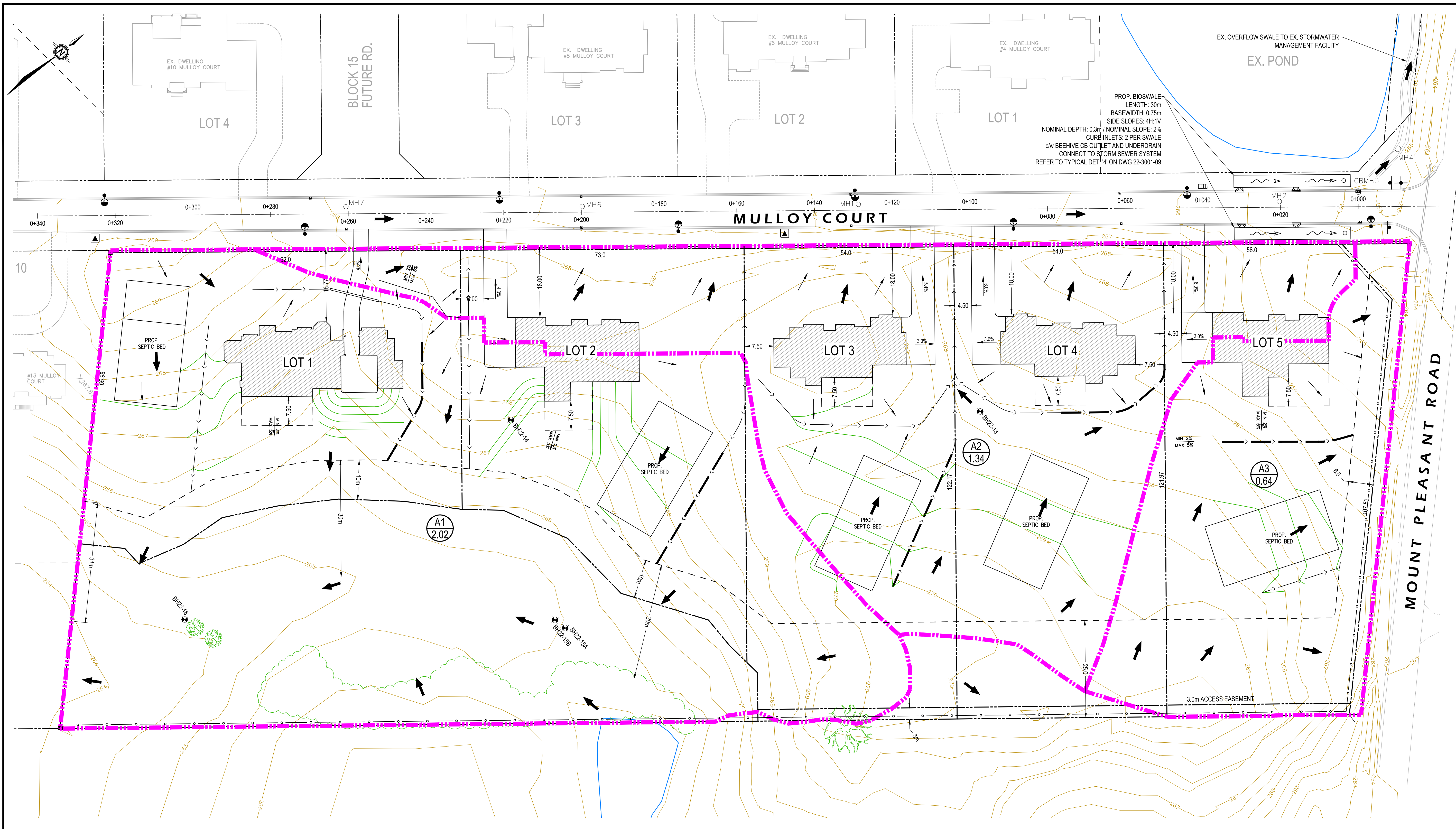
N ^o	Date	Revisions	Dwn.	Dsg'd.	Chk'd.
③	07/APR/2026	FOURTH SUBMISSION	AAF	AAF	RJW
②	21/NOV/2025	THIRD SUBMISSION	AAF	AAF	RJW
①	17/JAN/2025	SECOND SUBMISSION	AAF	AAF	RJW
①	26/JAN/2024	DPA APPLICATION	AAF	AAF	RJW

Client: **STELLAR HOMES INC.**

Project Name: **STELLAR ESTATES PHASE 2
MULLOY COURT, TOWN OF CALEDON**

Title Name: **WATER DISTRIBUTION PLAN**

Drawing N^o: **22-3001-04** Sheet N^o: **4 OF 10** Rev. N^o: **3**
 Scale: **1:500**



- LEGEND**
- PROPERTY LINES (PROPOSED)
 - PROPERTY LINES (EXISTING)
 - KEY NATURAL HERITAGE FEATURE
 - LIMIT OF STRUCTURE ENVELOPE (PROPOSED)
 - PROP. GRASSED SWALE
 - PROP. ENHANCED GRASS SWALE, MIN. 30.0m / LOT
 - PROP. STORM DRAINAGE BOUNDARY
 - PROP. DRAINAGE DIRECTION
 - A1 1.93 PROP. CATCHMENT ID
 - A2 1.34 PROP. DRAINAGE AREA (HECTARES)
 - A3 0.64
 - B# 2007 BOREHOLES
 - BH22-# 2022 BOREHOLES

REFER TO GENERAL NOTES AND SPECIFICATIONS ON DWG 22-3001-10

LOCATION OF RESIDENTIAL UNITS AND SEPTIC FIELDS ARE CONCEPTUAL ONLY. FINAL LOCATIONS TO BE DETERMINED AT THE SITE PLAN APPROVAL / BUILDING PERMIT APPLICATION STAGE.



DESIGNED BY: **R. J. WHYTE**
 49877509
 Apr. 7, 2026
 PROVINCE OF ONTARIO

APPROVED BY:

TABLE B.3
2-YEAR STORM SEWER DESIGN SHEET

Location	Drainage Area				Runoff			Pipe Flow								
	From MH	To MH	A (ha)	C	A x C	Acc. x C	Tc (min)	I (mm/hr)	Q (L/s)	Pipe Length (m)	Pipe Diameter (m)	Pipe Slope (%)	Full Flow Capacity (L/s)	Full Flow Velocity (m/s)	Time of Flow (min.)	% full
Catchment																
A	MH1	MH2	0.6500	0.40	0.26	0.26	15.58	67.55	48.78	108.0	0.300	0.93	93.3	1.32	1.36	52.3%
B + 404a	MH2	CBMH3	1.4900	0.31	0.46	0.72	16.94	64.28	128.90	20.0	0.375	0.30	96.0	0.87	0.38	134.2%
	CBMH3	MH4	0.0000	0.00	0.00	0.72	17.33	63.42	127.18	15.5	0.375	0.30	96.0	0.87	0.30	132.4%
	MH4	MH5	0.0000	0.00	0.00	0.72	17.62	62.77	125.88	58.0	0.375	0.30	96.0	0.87	1.11	131.1%
	MH5	OUTFALL	0.0000	0.00	0.00	0.72	18.74	60.47	121.25	7.0	0.375	0.30	96.0	0.87	0.13	126.3%

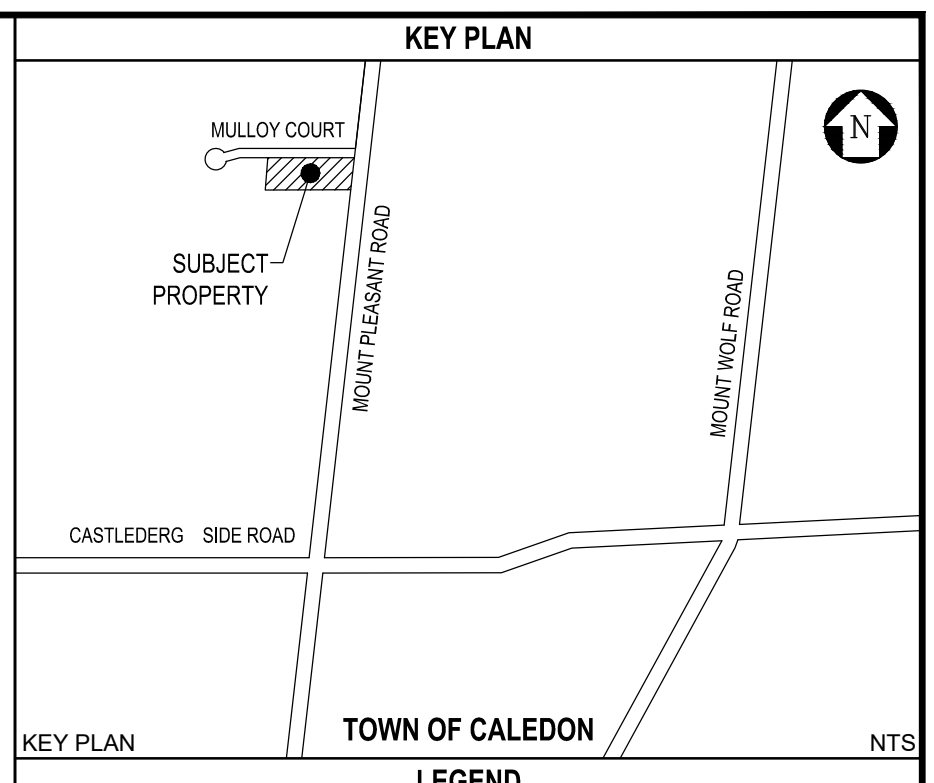
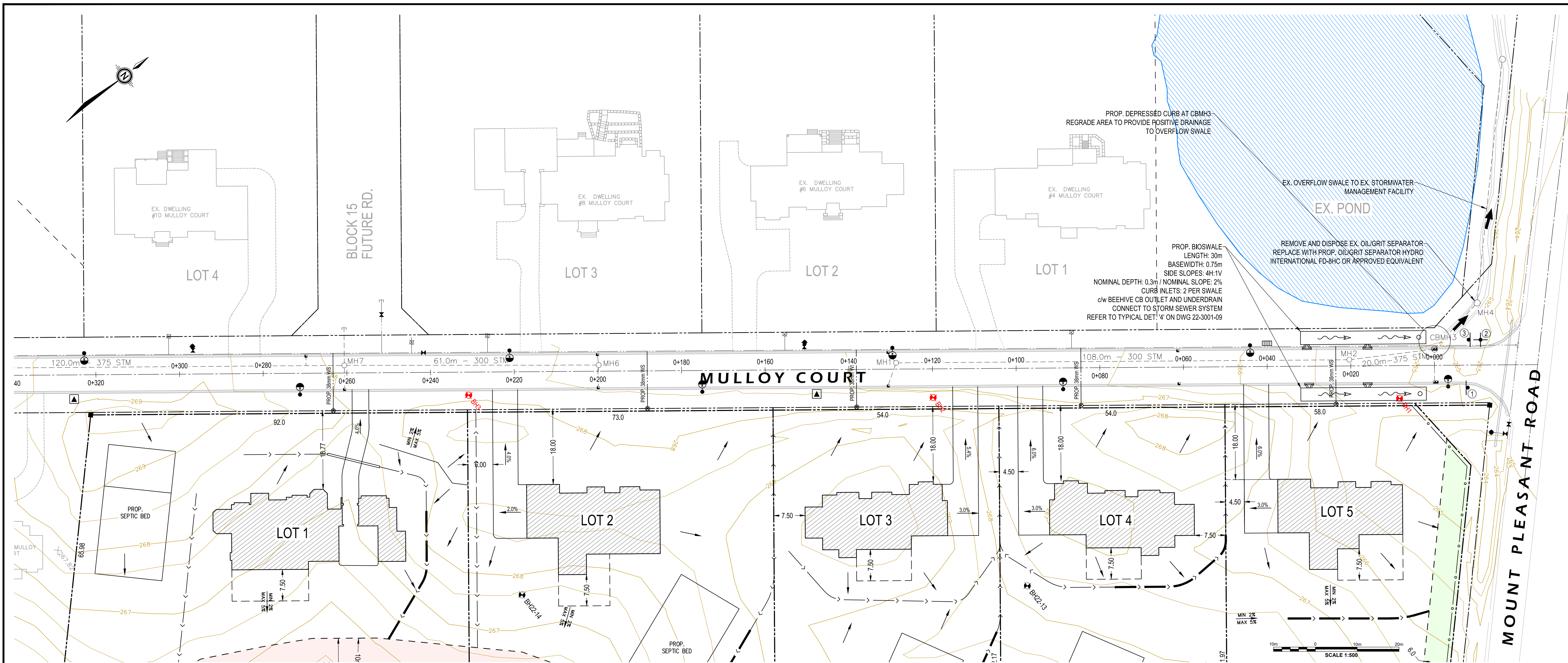
N°	Date	Revisions	Dwt.	Dsg'd.	Chk'd.
③	07/APR/2026	FOURTH SUBMISSION	AAF	AAF	RJW
②	21/NOV/2025	THIRD SUBMISSION	AAF	AAF	RJW
①	17/JAN/2025	SECOND SUBMISSION	AAF	AAF	RJW
①	26/JAN/2024	DPA APPLICATION	AAF	AAF	RJW

Client: **STELLAR HOMES INC.**

Project Name: **STELLAR ESTATES PHASE 2
MULLOY COURT, TOWN OF CALEDON**

Title Name: **STORM DRAINAGE PLAN**

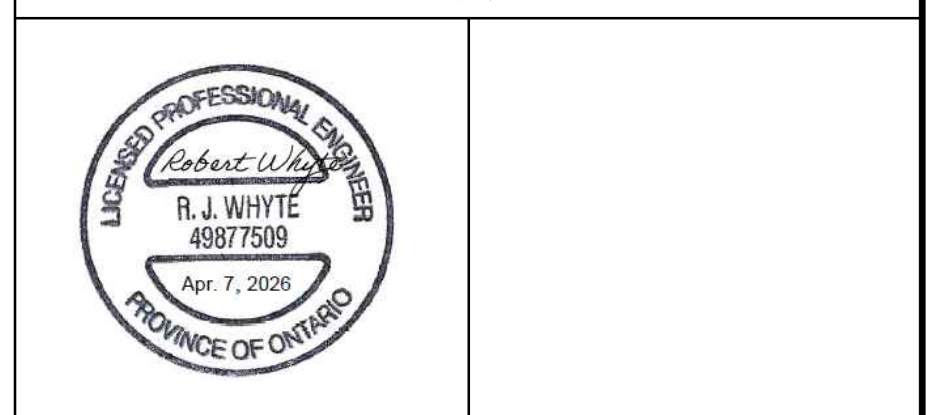
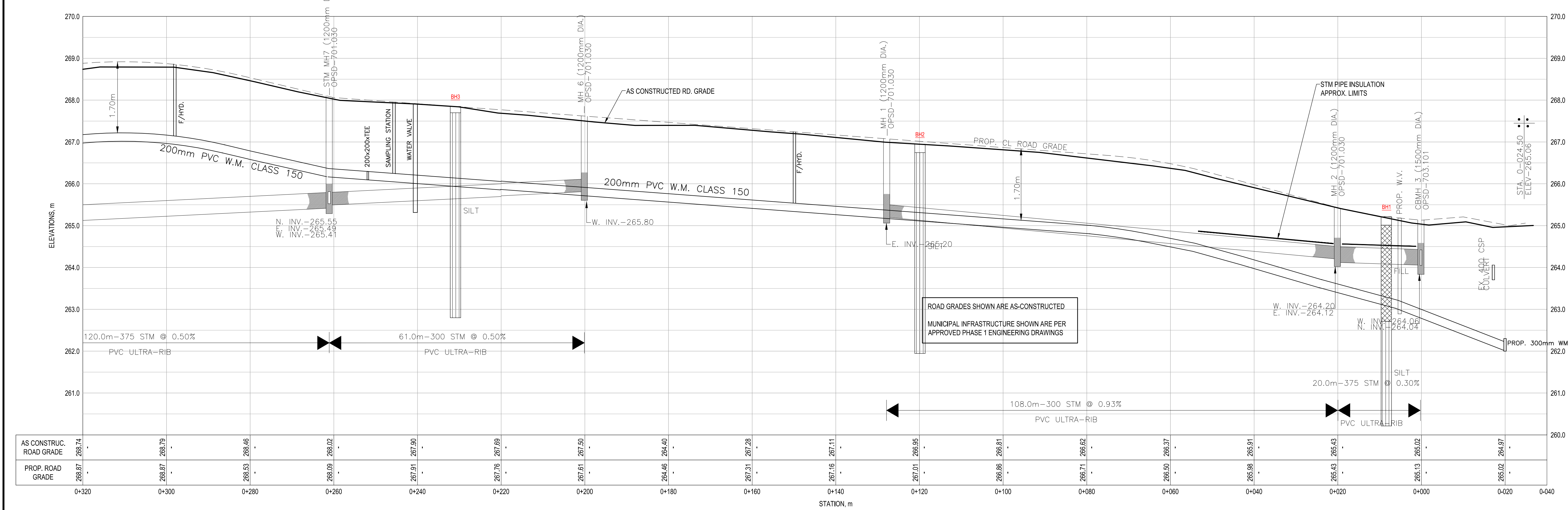
Drawing N°: **22-3001-05** Sheet N°: **5 OF 10** Rev. N°: **3**
 Scale: **1:500**



- LEGEND**
- PROPERTY LINES (PROPOSED)
 - PROPERTY LINES (EXISTING)
 - KEY NATURAL HERITAGE FEATURE
 - LIMIT OF STRUCTURE ENVELOPE (PROPOSED)
 - PROP. GRASSED SWALE
 - PROP. ENHANCED GRASS SWALE, MIN. 30.0m / LOT
 - EX. WATERMAIN
 - PROP. WATERMAIN CONNECTIONS
 - EX. / PROP. WATER BOX
 - EX. GATE VALVE
 - EX. HYDRANT
 - BH#
 - BH22-#
 - EX. STOP SIGN
 - EX. STREET SIGN
 - EX. NO EXIT SIGN

REFER TO GENERAL NOTES AND SPECIFICATIONS ON DWG 22-3001-10

LOCATION OF RESIDENTIAL UNITS AND SEPTIC FIELDS ARE CONCEPTUAL ONLY. FINAL LOCATIONS TO BE DETERMINED AT THE SITE PLAN APPROVAL / BUILDING PERMIT APPLICATION STAGE.



DESIGNED BY		APPROVED BY	

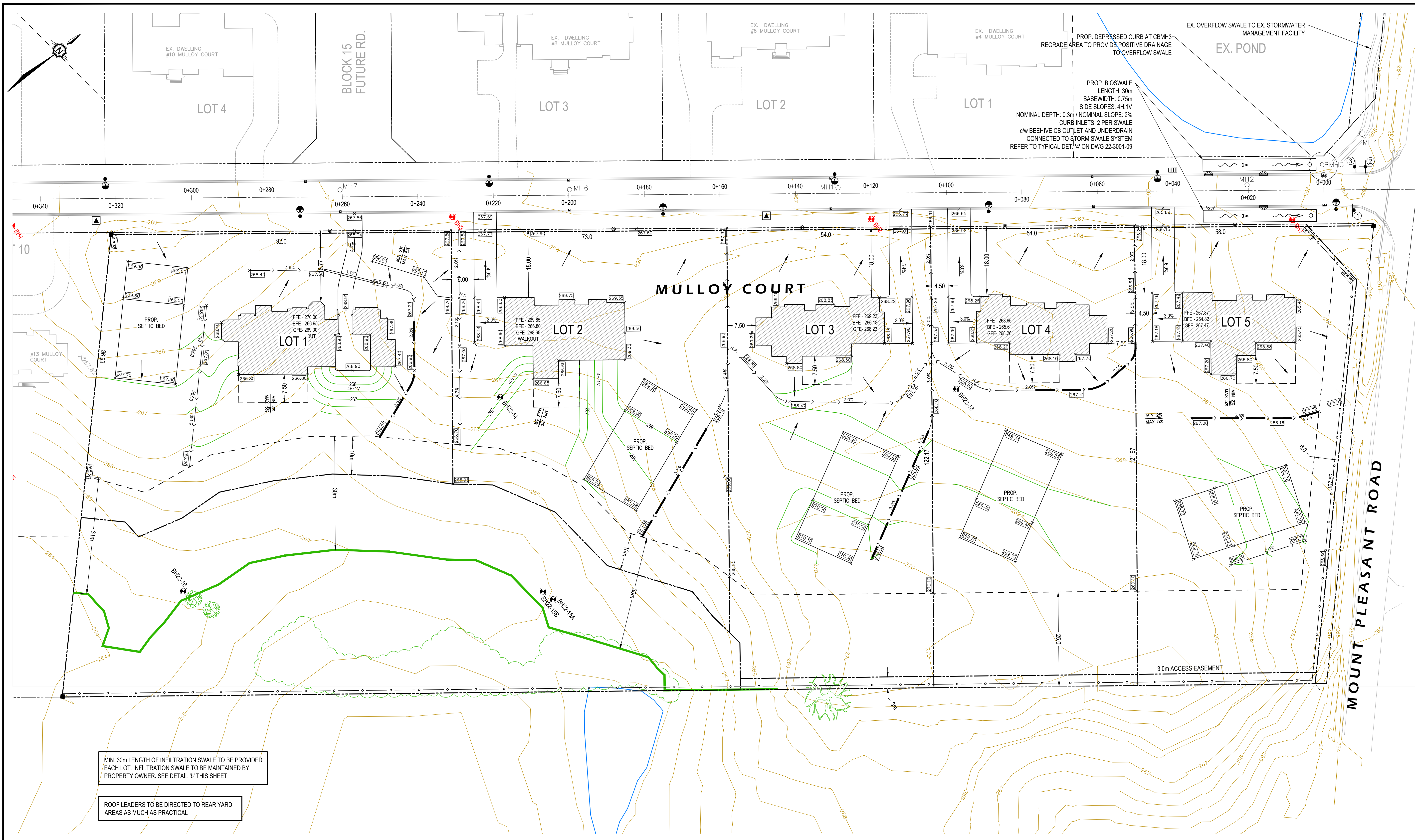
N°	Date	Revisions	Dwn.	Dsg'd.	Ch'kd.
③	07/APR/2026	FOURTH SUBMISSION	AAF	AAF	RJW
②	21/NOV/2025	THIRD SUBMISSION	AAF	AAF	RJW
①	17/JAN/2025	SECOND SUBMISSION	AAF	AAF	RJW
①	26/JAN/2024	DPA APPLICATION	AAF	AAF	RJW

Client: **STELLAR HOMES INC.**

Project Name: **STELLAR ESTATES PHASE 2 MULLOY COURT, TOWN OF CALEDON**

Title Name: **MULLOY COURT PLAN AND PROFILE**

Drawing N°: **22-3001-06** Sheet N°: **6 OF 10** Rev. N°: **3**
 Scale: **H 1:500 / V 1:50**



KEY PLAN

TOWN OF CALEDON

LEGEND

- PROPERTY LINES (PROPOSED)
- PROPERTY LINES (EXISTING)
- EX. M.R. CONTOURS (EACH 1.0m)
- EX. M.R. CONTOURS (EACH 0.5m)
- PROP. GRADE CONTOURS
- KEY NATURAL HERITAGE FEATURE
- LIMIT OF STRUCTURE ENVELOPE (PROPOSED)
- PROP. GRASSED SWALE, DET. 1' SHEET 9
- PROP. ENHANCED GRASS SWALE, MIN. 30.0m / LOT DET '2' SHEET 9
- PROP. GRADE ELEVATIONS
- PROP. POST AND WIRE FENCE
- PROP. WATER BOX
- BH# 2007 BOREHOLES
- BH22-# 2022 BOREHOLES
- EX. STOP SIGN
- EX. STREET SIGN
- EX. NO EXIT SIGN

CONCEPTUAL DWELLINGS

LOT	HOUSE TYPE	WALKOUT	GFA (m ²)	GFA (ft ²)	REFERENCE
1	BUNGALOW	YES	568.5	6,119.3	8 MULLOY COURT
2	BUNGALOW	YES	501.6	5,399.2	10 MULLOY COURT
3	BUNGALOW	NO	432.5	4,655.4	6 MULLOY COURT
4	BUNGALOW	NO	432.5	4,655.4	6 MULLOY COURT
5	BUNGALOW	NO	435.6	4,688.8	10 MULLOY COURT

REFER TO GENERAL NOTES AND SPECIFICATIONS ON DWG 22-3001-10

LOCATION OF RESIDENTIAL UNITS AND SEPTIC FIELDS ARE CONCEPTUAL ONLY. FINAL LOCATIONS TO BE DETERMINED AT THE SITE PLAN APPROVAL / BUILDING PERMIT APPLICATION STAGE.



DESIGNED BY

APPROVED BY

Robert Whyte
 R. J. WHYTE
 49877509
 Apr. 7, 2026
 PROVINCE OF ONTARIO

N ^o	Date	Revisions	Dwn.	Dsg'd.	Chk'd.
③	07/APR/2026	FOURTH SUBMISSION	AAF	AAF	RJW
②	21/NOV/2025	THIRD SUBMISSION	AAF	AAF	RJW
①	17/JAN/2025	SECOND SUBMISSION	AAF	AAF	RJW
①	26/JAN/2024	DPA APPLICATION	AAF	AAF	RJW

STELLAR HOMES INC.

Project Name: **STELLAR ESTATES PHASE 2
MULLOY COURT, TOWN OF CALEDON**

Title Name: **GRADING PLAN**

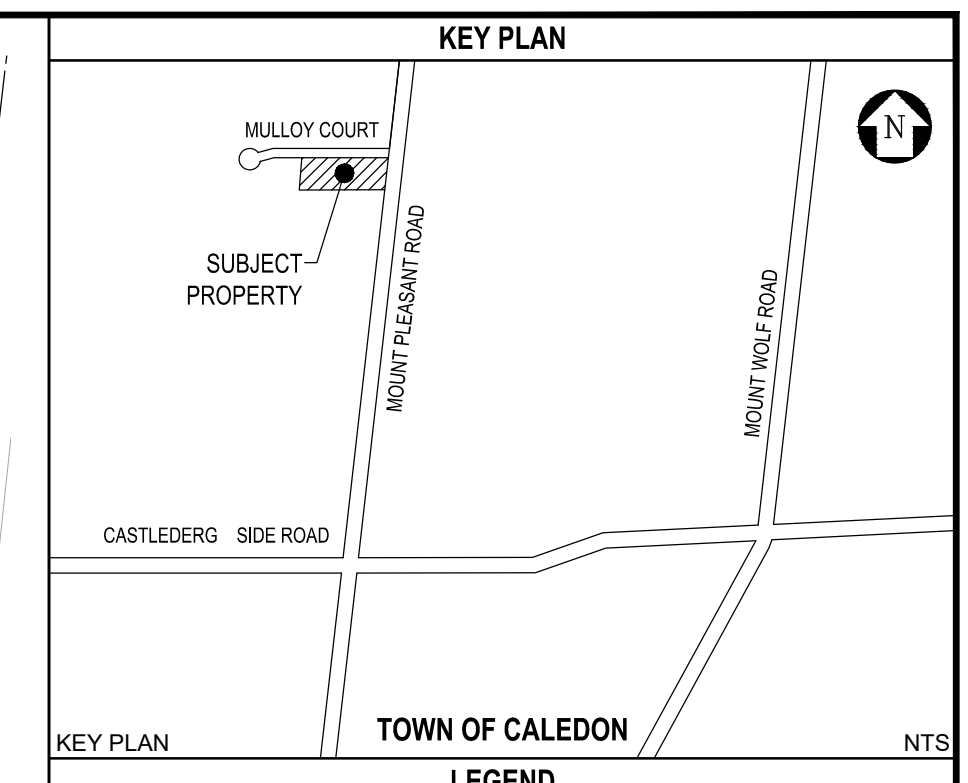
Drawing N^o: **22-3001-07** Sheet N^o: **7 OF 10** Rev. N^o: **③**
 Scale: **1:500**

MIN. 30m LENGTH OF INFILTRATION SWALE TO BE PROVIDED EACH LOT. INFILTRATION SWALE TO BE MAINTAINED BY PROPERTY OWNER. SEE DETAIL '3' THIS SHEET

ROOF LEADERS TO BE DIRECTED TO REAR YARD AREAS AS MUCH AS PRACTICAL

- GRADING NOTES**
1. DOWNSPOUTS TO DISCHARGE TO GROUND VIA SPLASH PADS.
 2. DRIVEWAY GRADES TO BE BETWEEN 2 AND 6%.
 3. ALL SLOPES ARE TO BE 4H:1V MAXIMUM, UNLESS OTHERWISE NOTED.
 4. A MINIMUM OF 1.5m CLEARANCE IS TO BE PROVIDED FROM THE LIMIT OF THE DRIVEWAY TO EXISTING UTILITY STRUCTURES WITHIN THE MUNICIPAL RIGHT-OF-WAY. IF THIS CLEARANCE IS NOT MAINTAINED THEY SHALL BE RELOCATED AT THE APPLICANT'S EXPENSE.
 5. DISTURBED BOULEVARD AREAS TO BE RESTORED WITH MINIMUM 300mm TOPSOIL AND SOD.
 6. DISTURBED SITE AREAS TO BE RESTORED WITH MINIMUM 100mm TOPSOIL AND EITHER SEED OR SOD.
 7. ALL GRADING TO BE IN GENERAL CONFORMANCE WITH THE TOWN OF CALEDON "DEVELOPMENT STANDARDS MANUAL" SECTION 1.12 RESIDENTIAL LOT DRAINAGE AND SODDING.





LEGEND

- PROPERTY LINES (PROPOSED)
- PROPERTY LINES (EXISTING)
- KEY NATURAL HERITAGE FEATURE
- LIMIT OF STRUCTURE ENVELOPE (PROPOSED)
- PROP. GRASSED SWALE
- PROP. ENHANCED GRASS SWALE, MIN. 30.0m / LOT
- PROP. HEAVY DUTY SEDIMENT CONTROL FENCE PER MODIFIED TOWN OF CALEDON STANDARD DRAWING 304
- PROP. DOUBLE ROW HEAVY DUTY SEDIMENT CONTROL FENCE c/w STRAW BALES IN BETWEEN
- PROP. CONSTRUCTION ACCESS AND EGRESS POINT
- PROPOSED MUD MAT ALIGNMENT TO BE FIELD DETERMINED
- PROP. SILT/SOXX CHECK DAM - 450mm PER DETAIL ON SHEET 9

REFER TO TREE PRESERVATION PLAN PREPARED BY AZIMUTH ENVIRONMENTAL CONSULTING INC.

REFER TO GENERAL NOTES AND SPECIFICATIONS ON DWG 22-3001-10

EMERGENCY CONTACT LIST

NAME/AGENCY	PHONE NUMBER
TOWN OF CALEDON	905-584-2272
TORONTO AND REGION CONSERVATION	416-661-6600
MINISTRY OF ENVIRONMENT SPILLS REPORTING	416-325-3000
OWNER - STELLAR HOMES INC.	905-726-7778
PROJECT ENGINEER - ECOMETRIX INCORPORATED	905-794-2325



DESIGNED BY

APPROVED BY

Professional Engineer Seal: Robert Whyte, R. J. WHYTE, 49877509, Apr. 7, 2026, PROVINCE OF ONTARIO

EROSION AND SEDIMENT CONTROL NOTES

SITE MANAGEMENT

- EROSION AND SEDIMENT CONTROL (ESC) MEASURES TO BE IMPLEMENTED PRIOR TO, AND MAINTAINED DURING THE CONSTRUCTION PHASES, TO PREVENT ENTRY OF SEDIMENT INTO THE WATER. ALL DAMAGED EROSION AND SEDIMENT CONTROL MEASURES SHOULD BE REPAIRED AND/OR REPLACED WITHIN 48 HOURS OF INSPECTION. DISTURBED AREAS TO BE MINIMIZED TO THE EXTENT POSSIBLE, AND TEMPORARILY OR PERMANENTLY STABILIZED OR RESTORED AS THE WORK PROGRESSES. AS PER THE ESC GUIDELINE FOR URBAN CONSTRUCTION (2019), ANY DISTURBED AREA LEFT EXPOSED FOR 30 DAYS OR GREATER ARE TO BE STABILIZED. STABILIZATION SHALL BE BY HYDROSEEDING WITH AN APPROVED SEED MIXTURE AND APPLICATION OF MULCH PER OPSS 804 (OR APPROVED EQUIVALENT) TO THE SATISFACTION OF THE TOWN. SEED MIXTURE TO BE COMPRISED OF SPECIES PER THE TRCA'S SEED MIX GUIDELINES SPECIES LIST.
- ALL IN-WATER AND NEAR WATER WORKS TO BE CONDUCTED IN THE DRY WITH APPROPRIATE EROSION AND SEDIMENT CONTROLS.
- THE ESC STRATEGIES OUTLINED ON THE PLANS ARE NOT STATIC AND MAY NEED TO BE UPGRADED/AMENDED AS SITE CONDITIONS CHANGE TO MINIMIZE SEDIMENT LADEN RUNOFF FROM LEAVING THE WORK AREAS. IF THE PRESCRIBED MEASURES ON THE PLANS ARE NOT EFFECTIVE IN PREVENTING THE RELEASE OF A DELETERIOUS SUBSTANCE, INCLUDING SEDIMENT, THEN ALTERNATIVE MEASURES MUST BE IMPLEMENTED IMMEDIATELY TO MINIMIZE POTENTIAL ECOLOGICAL IMPACTS. TRCA ENFORCEMENT OFFICER SHOULD BE IMMEDIATELY CONTACTED. THE TOWN IS TO BE ADVISED OF ANY CHANGES TO ESC MEASURES, AND AT THE DISCRETION OF THE TOWN, UPDATED PLANS MAY BE REQUIRED. ADDITIONAL ESC MEASURES TO BE KEPT ON SITE AND USED AS NECESSARY.
- THE CONTRACTOR IS RESPONSIBLE FOR MAINTAINING ALL ESC MEASURES IN WORKING CONDITION AT ALL TIMES TO THE SATISFACTION OF THE TOWN AND TRCA. ALL DAMAGED ESC MEASURES SHOULD BE REPAIRED AND/OR REPLACED WITHIN 48 HOURS OF INSPECTION.
- THE CONTRACTOR IS TO ASSIGN AN ENVIRONMENTAL MONITOR TO ASSURE CONSTRUCTION ACTIVITIES COMPLY WITH THE ENVIRONMENTAL PROVISIONS AND AGENCY PERMITS. THE ENVIRONMENTAL MONITOR WILL BE A QUALIFIED PERSON AS DETERMINED BY THE TOWN AND TRCA. THE ENVIRONMENTAL MONITOR SHOULD SUBMIT INSPECTION FORMS ELECTRONICALLY TO THE TOWN AND TRCA UPON REQUEST.
- THE ENVIRONMENTAL MONITOR TO ATTEND THE SITE TO INSPECT ALL NEW CONTROLS, AS WELL AS ON A REGULAR BASIS, OR FOLLOWING RAIN/SNOWMELT EVENT, TO MONITOR ALL WORKS, AND IN PARTICULAR WORKS RELATED TO EROSION AND SEDIMENT CONTROLS, DEWATERING OR UNWATERING, RESTORATION AND IN-WATER OR NEAR WATER WORKS. SHOULD CONCERNS ARISE ON SITE THE ENVIRONMENTAL MONITOR SHALL CONTACT THE TRCA ENFORCEMENT OFFICER AS WELL AS THE PROPONENT.
- THE CONTRACTOR SHALL ROUTINELY INSPECT ALL ESC MEASURES TO ENSURE PROPER WORKING ORDER. FREQUENCY OF INSPECTIONS OF ESC MEASURES IS AS FOLLOWS: DURING EARTHWORKS ACTIVITIES:
 - ON A WEEKLY BASIS;
 - PRIOR TO PREDICTED RAINFALL EVENTS;
 - AFTER EVERY RAINFALL EVENT;
 - AFTER SIGNIFICANT SNOWFALL EVENTS, AND
 - DAILY DURING EXTENDED RAIN OR SNOWMELT PERIODS.
 DURING TIMES OF NO EARTHWORKS ACTIVITIES:
 - ONCE EVERY TWO WEEKS;
 - AFTER SIGNIFICANT SNOWMELT EVENTS;
 - AFTER SIGNIFICANT RAINFALL EVENTS (MORE THAN 25mm OF RAINFALL IN A 24-HOUR PERIOD)
- THE PROPONENT/CONTRACTOR SHALL MONITOR THE WEATHER SEVERAL DAYS IN ADVANCE OF THE ONSET OF THE PROJECT TO ENSURE THAT THE WORKS TO BE CONDUCTED DURING FAVOURABLE WEATHER CONDITIONS. SHOULD AN UNEXPECTED STORM ARISE, THE CONTRACTOR SHALL REMOVE ALL UNFIXED ITEMS FROM THE REGIONAL STORM FLOOD PLAN THAT WOULD HAVE THE POTENTIAL TO CAUSE A SPILL OR AN OBSTRUCTION TO FLOW, E.G. FUEL TANKS, PORTA-POTTIES, MACHINERY, EQUIPMENT, CONSTRUCTION MATERIALS, ETC.
- ALL ACTIVITIES, INCLUDING MAINTENANCE PROCEDURES, TO BE CONTROLLED TO PREVENT THE ENTRY OF PETROLEUM PRODUCTS, DEBRIS, RUBBLE, CONCRETE OR OTHER DELETERIOUS SUBSTANCES INTO THE WATER. VEHICULAR REFUELING AND MAINTENANCE TO BE CONDUCTED AT A MINIMUM OF 30 METRES FROM THE WATER. CONTRACTOR SHALL TAKE CARE AND CONTROL SPILLS, FLUIDS AND MATERIALS DURING CONSTRUCTION TO MINIMIZE RISK TO THE ENVIRONMENT.
- ALL CONSTRUCTION VEHICLES MUST ENTER AND EXIT THE SITE ONLY FROM THE APPROVED ACCESS ROUTE(S) AS SHOWN ON THE PLANS. CONSTRUCTION ACCESS WILL BE MAINTAINED TO THE SATISFACTION OF THE TOWN/TRCA. STREET SWEEPING IS REQUIRED AS NEEDED.
- NO CONSTRUCTION ACTIVITY OR MACHINERY SHALL BE ALLOWED BEYOND THE TEMPORARY SEDIMENT CONTROL FENCES OR LIMITS OF THE SITE WORKS.
- ALL DEWATERING/UNWATERING SHALL BE TREATED AND RELEASED TO THE ENVIRONMENT AT LEAST 30 METRES FROM A WATERCOURSE OR WETLAND AND ALLOWED TO DRAIN THROUGH A WELL-VEGETATED AREA. NO DEWATERING EFFLUENT SHALL BE SENT DIRECTLY TO ANY WATERCOURSE, WETLAND OR FOREST, OR ALLOWED TO DRAIN ONTO DISTURBED SOILS WITHIN THE WORK AREA. THESE CONTROL MEASURES SHALL BE MONITORED FOR EFFECTIVENESS AND MAINTAINED OR REVISED TO MEET THE OBJECTIVE OF PREVENTING THE RELEASE OF SEDIMENT LADEN WATER.
- IN ORDER TO COMPLY WITH THE MIGRATORY BIRDS CONVENTION ACT AND BAT HABITAT CONSIDERATIONS, TREE REMOVALS SHOULD BE COMPLETED BETWEEN OCTOBER 1 AND APRIL 1.
- TO PROTECT LOCAL FISH POPULATIONS DURING THEIR SPAWNING, NURSERY AND MIGRATORY PERIODS, IN-WATER NEAR WATER ACTIVITIES MAY ONLY OCCUR DURING THE FOLLOWING TIME PERIOD (TRCA TO CONFIRM TIMING WINDOW DURING REVIEW OF FIRST SUBMISSION):

ENVIRONMENTAL COMPLIANCE
- PLEASE NOTIFY THE TRCA AT 416-661-6000 48 HOURS PRIOR TO COMMENCING CONSTRUCTION.
- AN ENVIRONMENTAL MONITOR TO BE ON SITE, AND PROVIDE ADVICE, TO ENSURE THAT ACTIVITIES THAT COULD HAVE A NEGATIVE IMPACT TO THE NATURAL ENVIRONMENT ARE EFFECTIVELY MITIGATED AS CONSTRUCTION PROCEEDS. THE ENVIRONMENTAL MONITOR SHALL NOTIFY THE TRCA ENFORCEMENT OFFICER AND PROJECT MANAGER IF AN ISSUE ARISES.
- TEMPORARY EROSION AND SEDIMENT CONTROLS**
- MUD MAT TO BE PROVIDED ON SITE AT ALL LOCATIONS WHERE CONSTRUCTION VEHICLES EXIT THE SITE. MUD MAT(S) SHALL BE A MINIMUM OF 5m WIDE, 30m LONG AND 0.45m DEEP. THE MUD MAT(S) SHALL CONSIST OF 50-100mm CLEAR STONE MATERIAL OR APPROVED EQUIVALENT EXCEPT FOR THE FIRST 15m WHICH SHALL BE 50mm CLEAR STONE. CONTRACTOR TO ENSURE ALL VEHICLES LEAVE THE SITE VIA THE MUD MAT AND THAT THE MUD MAT IS MAINTAINED IN A MANNER TO MAXIMIZE EFFECTIVE NESS AT ALL TIMES.
- THE CONTRACTOR IS RESPONSIBLE TO IMPLEMENT DUST CONTROL MEASURES AND CONSTRUCTION BEST PRACTICE GUIDELINES AS APPROVED BY THE TOWN AND TRCA.
- TOPSOIL AND MATERIAL STOCKPILES TO BE ENCLOSED WITH SEDIMENT CONTROL FENCE. SEDIMENT CONTROL FENCE FOR STOCKPILES TO BE TERRAFIX TERRAFENCE OR APPROVED EQUIVALENT. THE MAXIMUM SIDE SLOPE SHALL BE 1.5H:1V. ONCE TOPSOIL STRIPPING IS COMPLETED, THE STOCKPILE SHALL BE VEGETATED, SUBJECT TO WEATHER CONDITIONS, BY HYDROSEEDING OR AN APPROVED EQUIVALENT, TO THE SATISFACTION OF THE TOWN.
- REMOVE TEMPORARY SEDIMENT CONTROLS FOLLOWING COMPLETION OF CONSTRUCTION AND SITE STABILIZATION AND REINSTATE AFFECTED AREAS TO EXISTING CONDITIONS OR BETTER. TIMING OF REMOVAL OF TEMPORARY SEDIMENT CONTROLS TO BE APPROVED BY TOWN STAFF.
- SEDIMENT CONTROL FENCING ON LOTS TO REMAIN IN PLACE UNTIL BUILDER HOME CONSTRUCTION THEN EITHER BE MAINTAINED, REMOVED OR AUGMENTED. SEDIMENT CONTROL FENCE TO BE REMOVED BY BUILDER ON COMPLETION OF HOUSE CONSTRUCTION AND LOT RESTORATION.

N°	Date	Revisions	Dwn.	Dsg'd.	Chk'd.
③	07/APR/2026	FOURTH SUBMISSION	AAF	AAF	RJW
②	21/NOV/2025	THIRD SUBMISSION	AAF	AAF	RJW
①	17/JAN/2025	SECOND SUBMISSION	AAF	AAF	RJW
①	26/JAN/2024	DPA APPLICATION	AAF	AAF	RJW

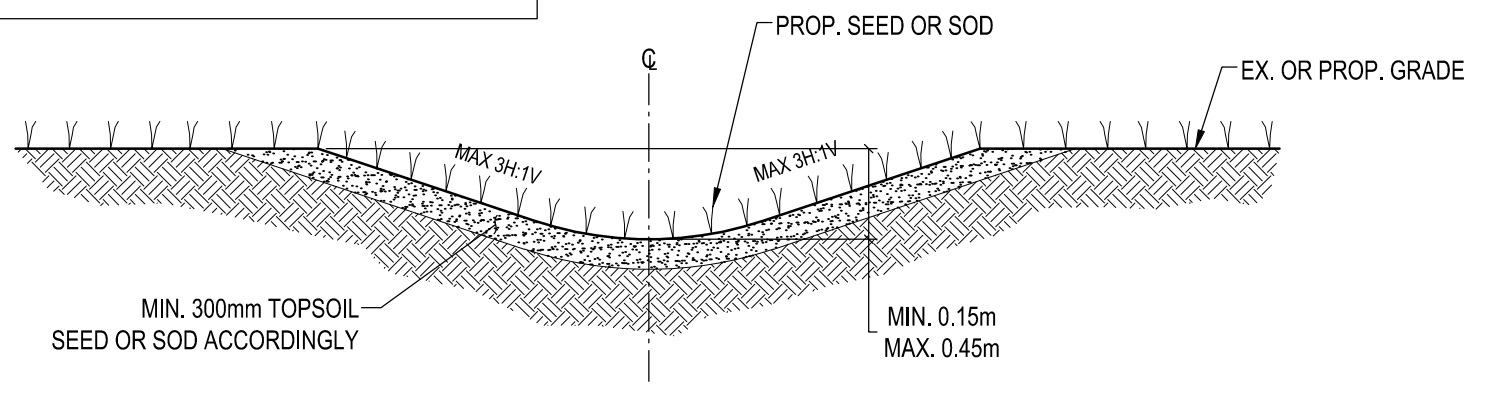
STELLAR HOMES INC.

Project Name: **STELLAR ESTATES PHASE 2
MULLOY COURT, TOWN OF CALEDON**

Title Name: **EROSION AND SEDIMENT
CONTROL PLAN**

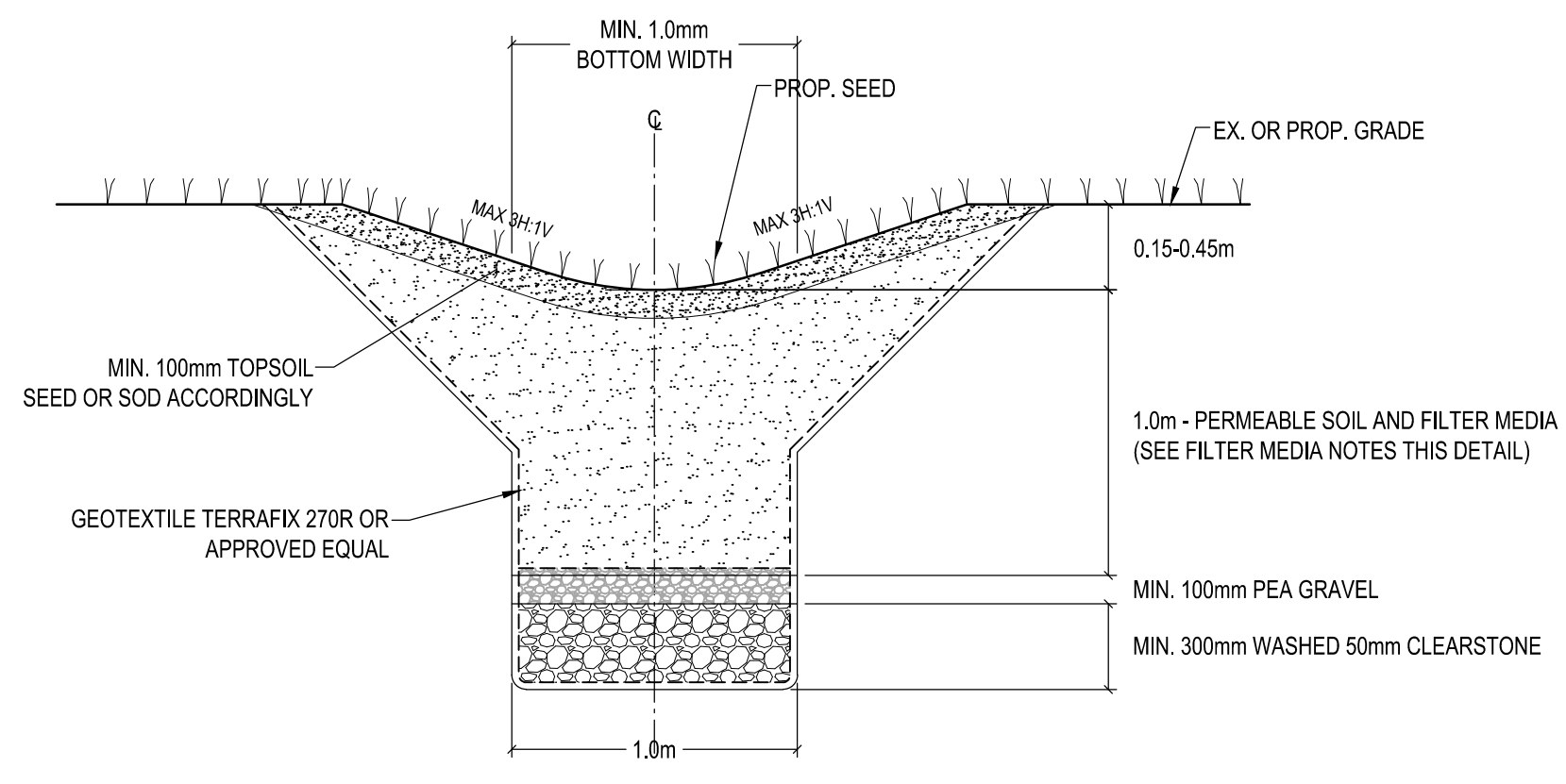
Drawing N°: **22-3001-08** Sheet N°: **8 OF 10** Rev. N°: **③**
Scale: **AS NOTED**

SWALES TO BE MAINTAINED BY OWNER SUCH THAT THEY FUNCTION AS INTENDED. SWALES TO BE MAINTAINED CLEAR OF OBSTRUCTIONS



SWALE DETAIL (TYP.)
SCALE: N.T.S. 07

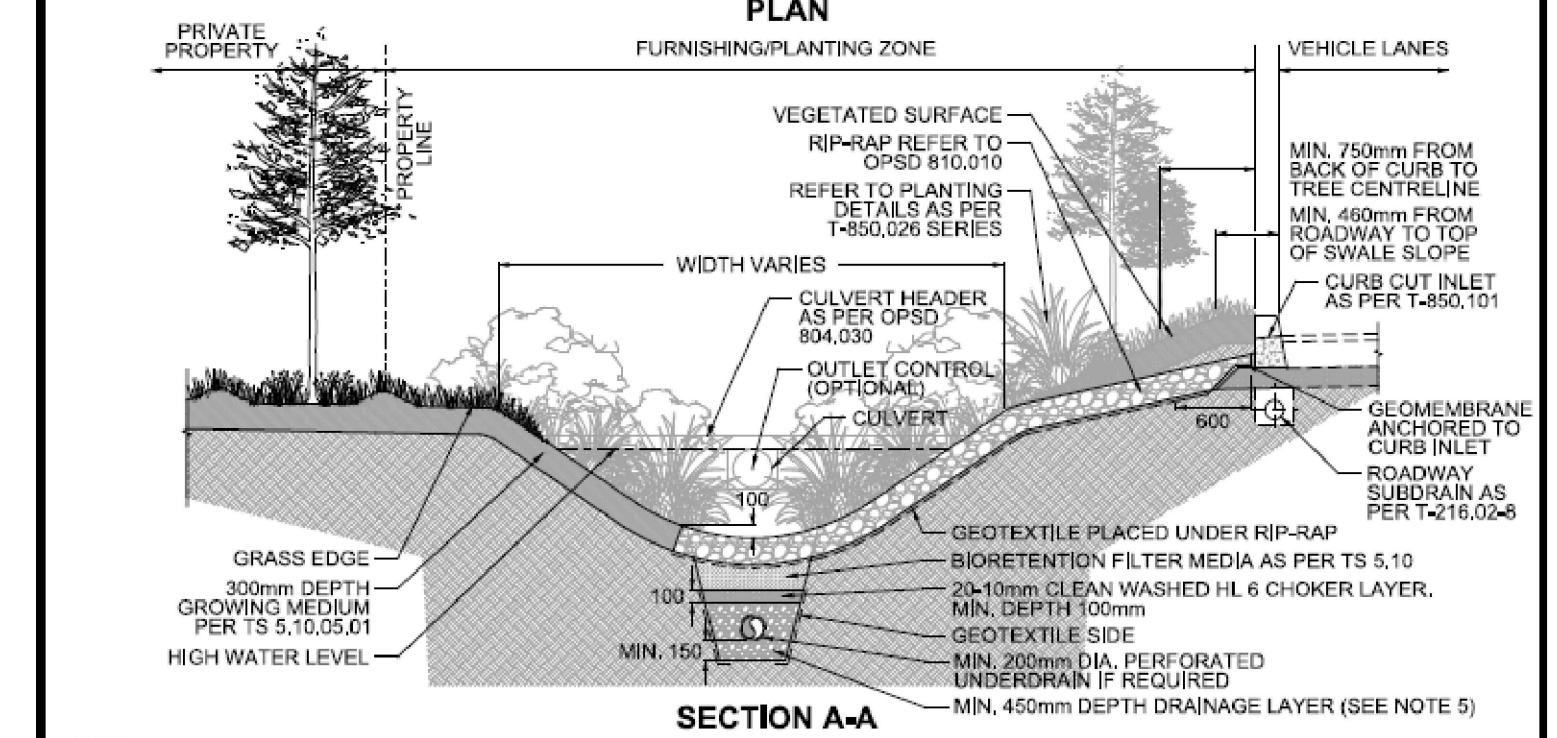
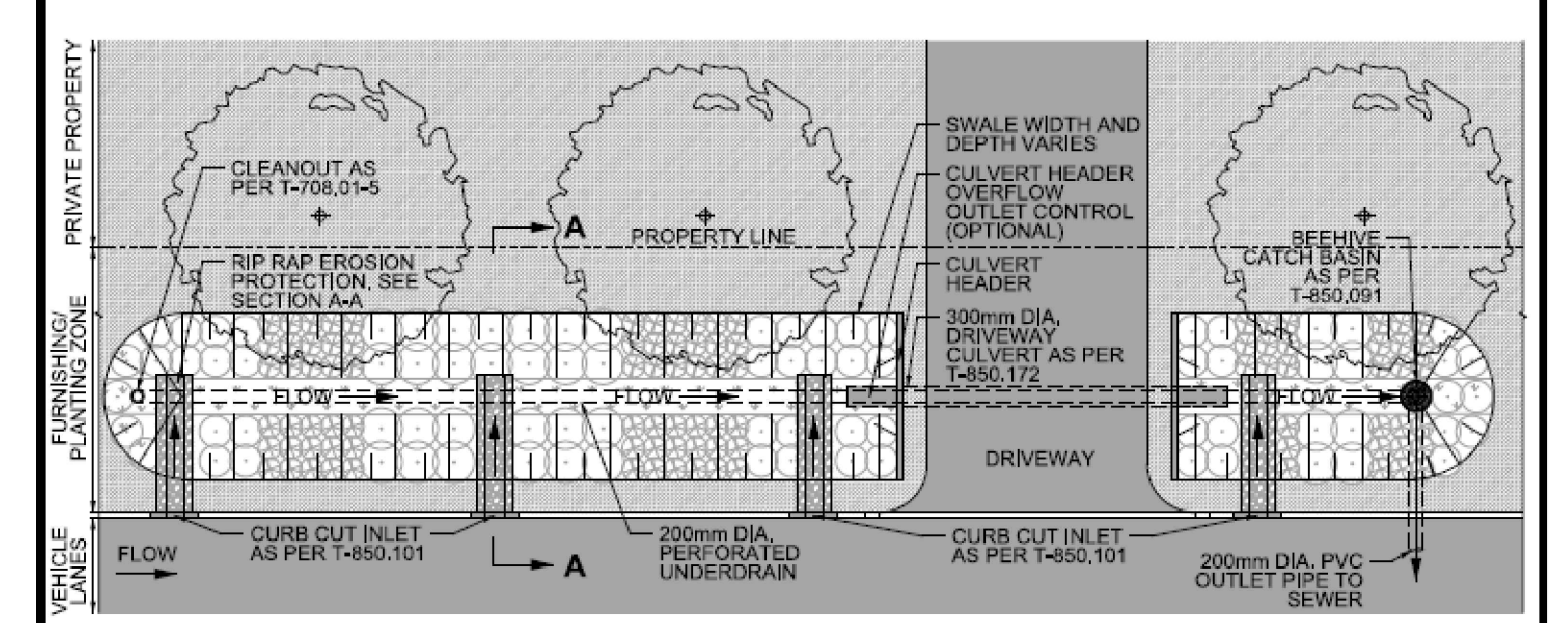
ENHANCED GRASS SWALES TO BE MAINTAINED BY OWNER SUCH THAT THEY FUNCTION AS INTENDED. SWALES TO BE MAINTAINED CLEAR OF OBSTRUCTIONS



PROPOSED ENHANCED GRASS SWALE (TYP.) ON LOTS
SCALE: 1:20 07

- FILTER MEDIA NOTES**
- SOIL MIXTURE TO CONTAIN:
 - 85 - 88% COARSE SAND
 - 8 - 12% SOIL FINES
 - 3 - 5% ORGANIC MATTER (LEAF COMPOST)
 - PHOSPHORUS SOIL TEST INDEX (P-INDEX) VALUE: 10-30 ppm
 - CATIONIC EXCHANGE CAPACITY: GRATER THAN 10 meq/100g
 - FILTER MEDIA FREE OF STONES, STUMPS, ROOTS AND OTHER LARGE DEBRIS
 - pH: 5.5 TO 7.5

- NOTES**
- ENHANCED GRASS SWALE TO BE DESIGNED IN GENERAL CONFORMANCE WITH INDUSTRY STANDARDS.
 - CHECK DAMS TO BE USED WHEN LONGITUDINAL SWALE SLOPES EXCEED 3%.
 - GRAVEL/CLEARSTONE LAYER TO TERMINATE AT GRADE AT END OF SWALE WITH A BLIND DRAIN.

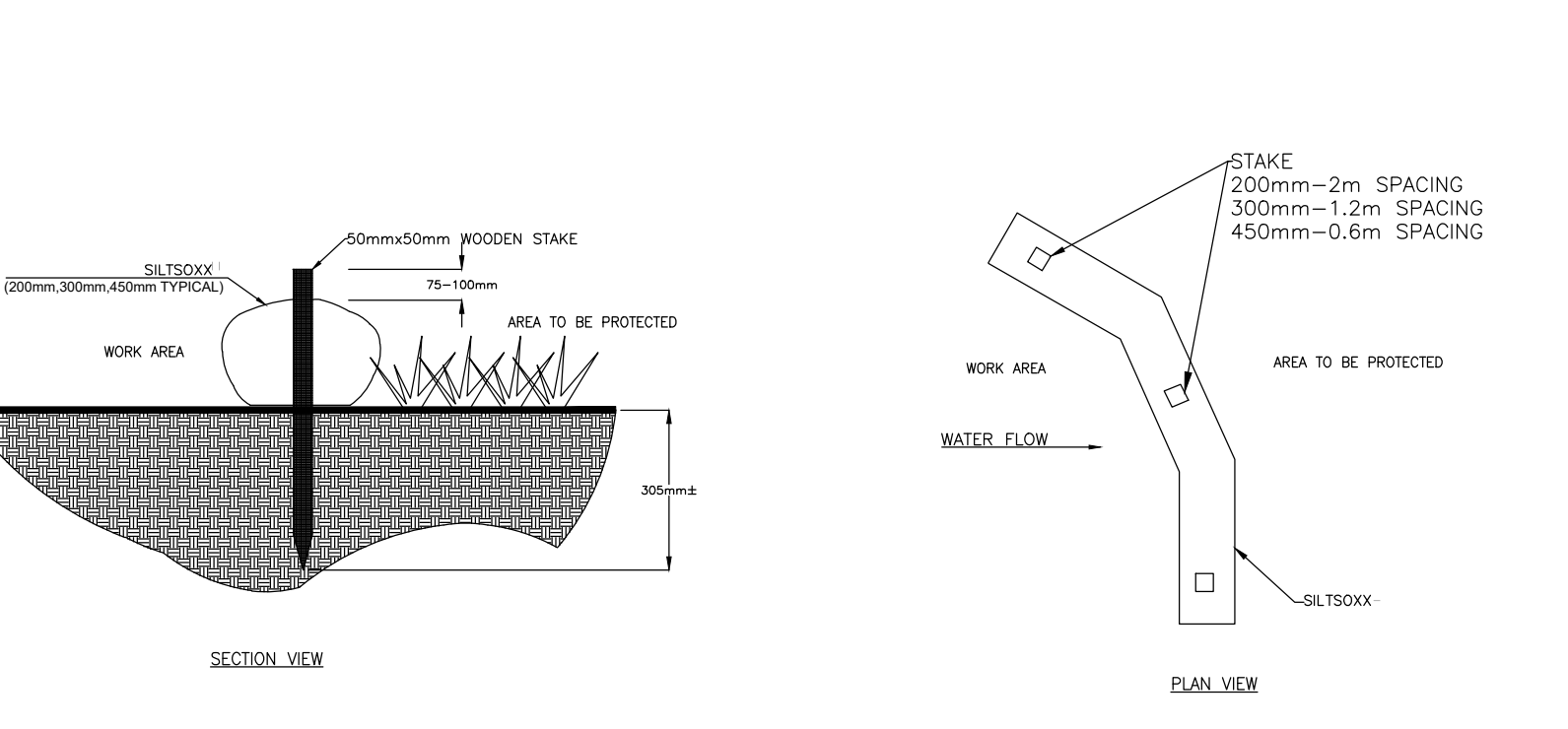


- NOTES:**
- BIOSWALE WIDTH AND DEPTH VARIES BASED ON DESIRED STORAGE CAPACITY, MAXIMUM PONDING DEPTH FROM SWALE SURFACE TO TOP OF DRIVEWAY CULVERTS TO BE 300mm. MINIMUM LENGTH BETWEEN DRIVEWAYS IS 5m.
 - SIDE SLOPES OF SWALE SURFACE 3H:1V MAXIMUM, 4H:1V PREFERRED.
 - LONGITUDINAL SLOPE DESIGNED TO ALLOW A MAXIMUM VELOCITY OF 1.5m/s. BEYOND WHICH SPECIFIC EROSION CONTROL MEASURES ARE REQUIRED (CHECK DAMS AS PER T-850.031, T-850.032, T-850.033 AND OPSD 212.010). SLOPE RANGE FROM 0.3% TO 4%.
 - CLEANOUTS TO BE CONNECTED TO PERFORATED UNDERDRAIN WITH 90 OR 45 DEGREE ELBOW ORIENTED TOWARDS THE MONITORING WELL. CLEANOUTS TO BE PROVIDED AT MAX. 30m SPACING. UNDERDRAIN TO BE MIN. 200mm DIA. HDPE OR EQUIVALENT SMOOTH INTERIOR WALLED PERFORATED PIPE. PERFORATIONS TO BE ON THE BOTTOM SIDE OF THE PIPE. ANY PERFORATIONS ON THE TOP SIDE OF THE UNDERDRAIN PIPE, TO BE TAPED OFF WITH MEMBRANE STRIPS.
 - GRAVEL USED FOR DRAINAGE LAYER TO BE 20 TO 50mm UNIFORMLY-GRADED, CLEAN (MAXIMUM WASH LOSS OF 0.5%), CRUSHED ANGULAR STONE THAT HAS A POROSITY OF 0.4.

All dimensions are in millimetres unless otherwise shown.

	ENGINEERING & CONSTRUCTION SERVICES STANDARD DRAWING	REV 0	SEP 2021
	BIOSWALE IN SOFTSCAPE	T-850.111	
	LAYOUT AND SECTION	NTS	SHEET 1

PROPOSED BIOSWALE (TYP.) IN BOULEVARD
SCALE: N.T.S. 07

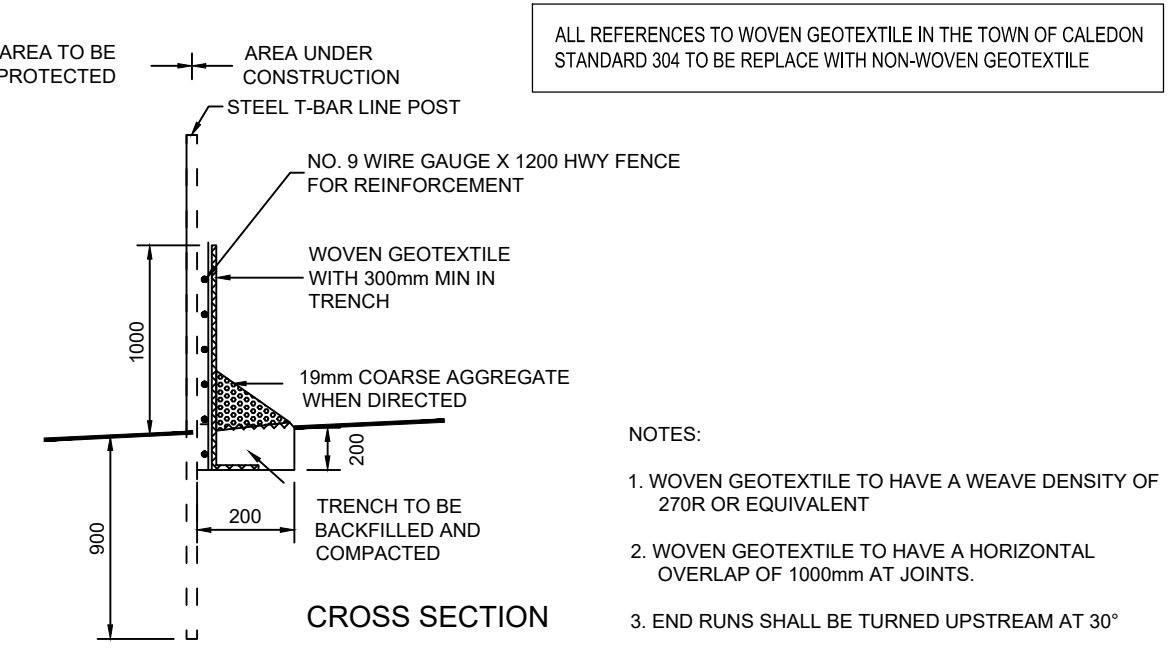
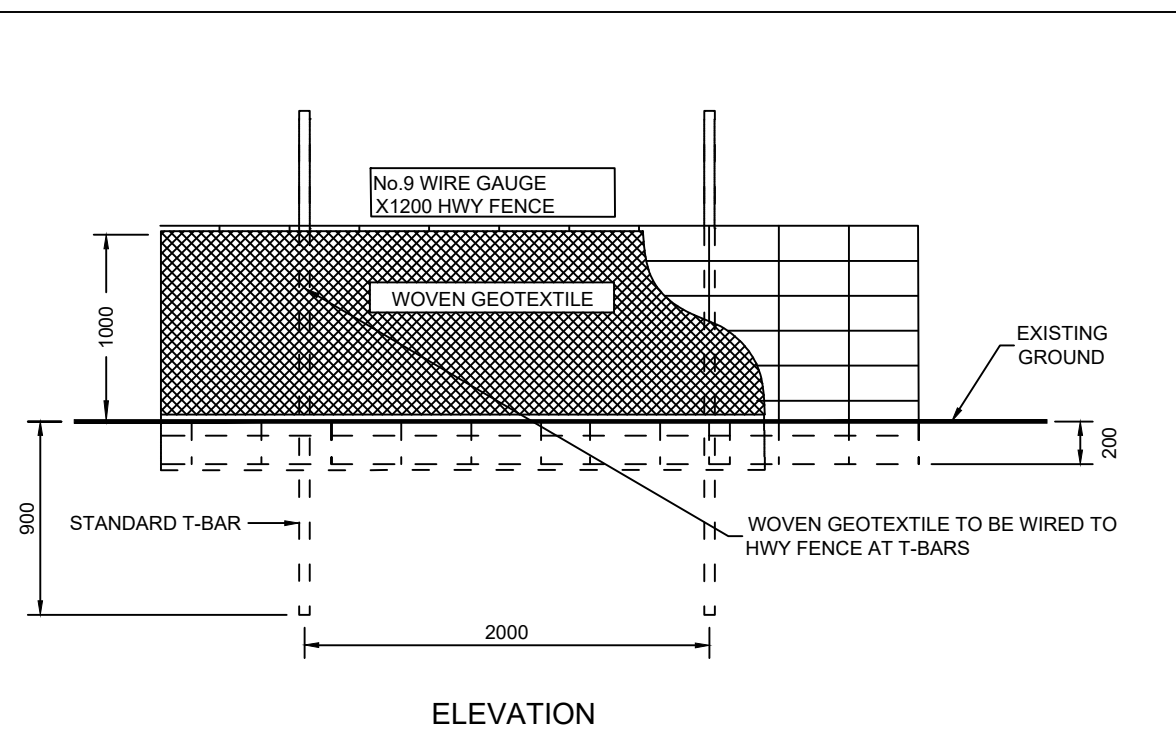


- NOTE:**
- ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SHOWN.
 - NOT TO SCALE.
 - ALL MATERIALS TO MEET TOWN OF CALEDON SPECIFICATIONS.
 - DISSECTION DEPICTED IS FOR MINIMUM SLOPES. GREATER SLOPES MAY REQUIRE LARGER SIZES FOR THE PRODUCTS.
 - CONTRACT MATERIAL TO BE DELIVERED ON SITE, AS DETERMINED BY ENGINEER.

SILTSOXX™

APPLICATION DETAIL 1 OF 1

REVISIONS / ISSUE	DATE	BY	CHKD



- NOTES:**
- WOVEN GEOTEXTILE TO HAVE A WEAVE DENSITY OF 270R OR EQUIVALENT
 - WOVEN GEOTEXTILE TO HAVE A HORIZONTAL OVERLAP OF 1000mm AT JOINTS.
 - END RUNS SHALL BE TURNED UPSTREAM AT 30°

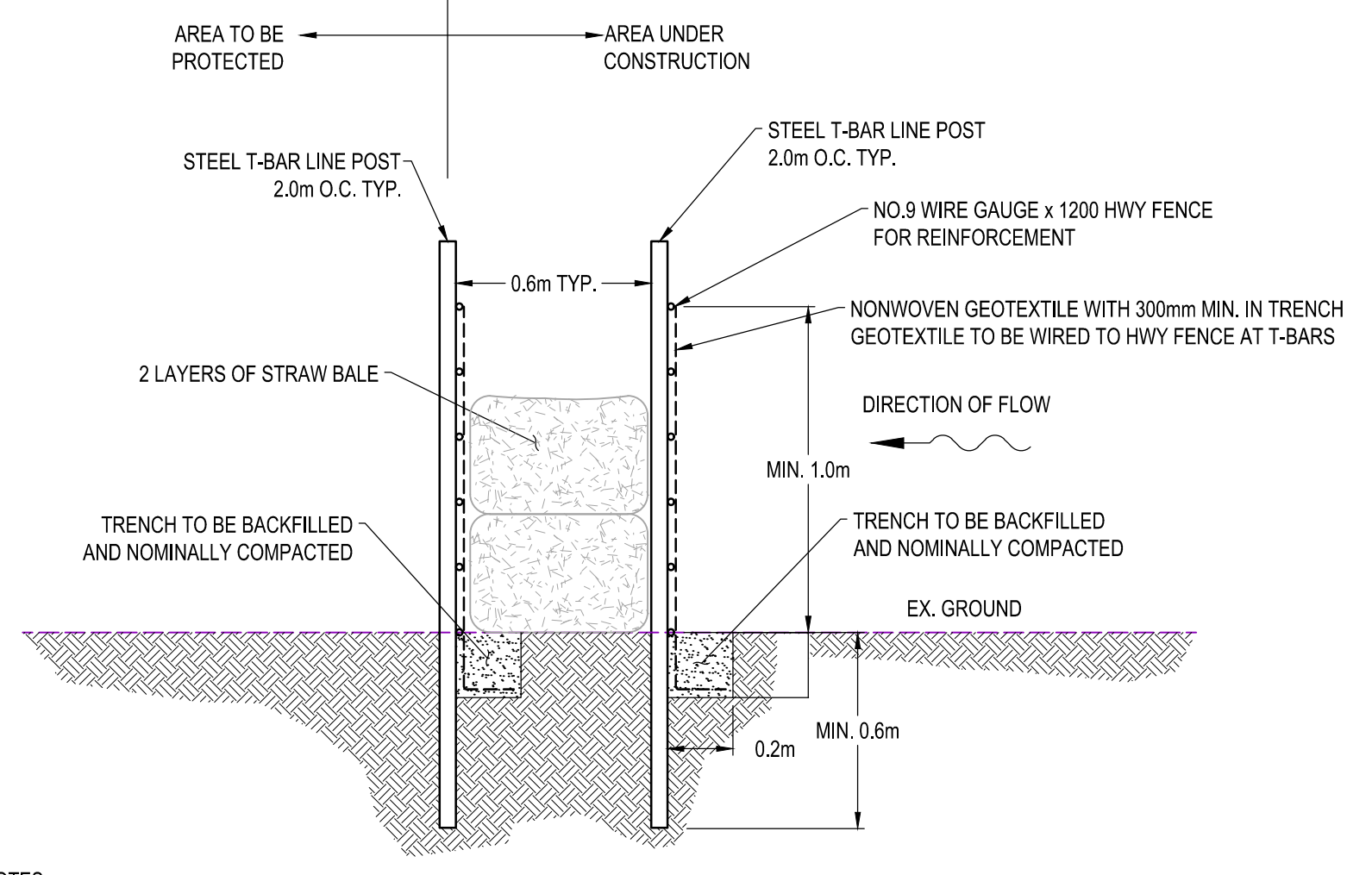
NO.	REVISION	APRD	DATE
2	NAME CHANGED, STANDARD No. 325.01 NOW 304		JUNE 08
1	SUPPORT FENCING CHANGED TO HWY FENCE		OCT 02

TOWN OF CALEDON

APRD: C.C. DATE: APRIL 2000

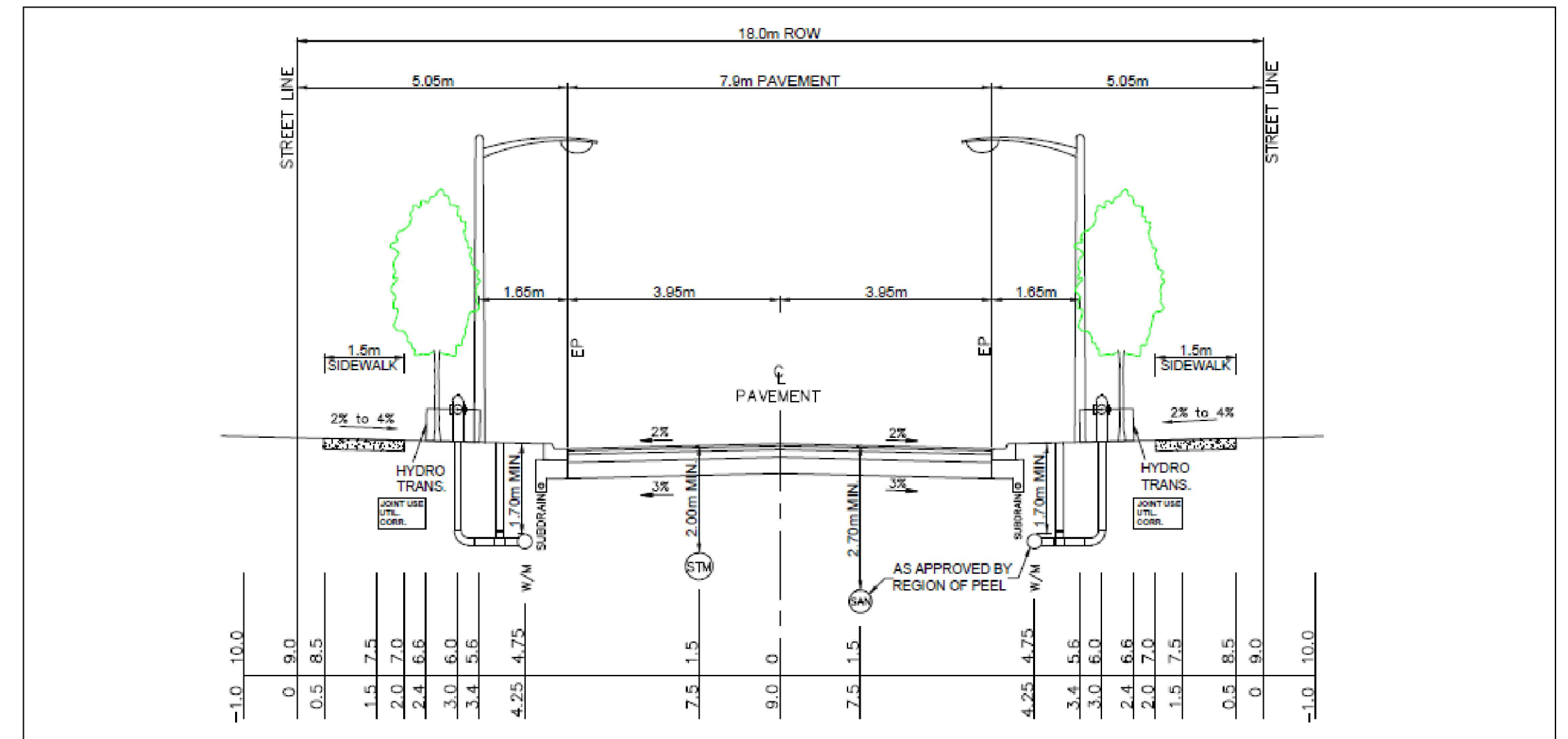
DRAWN: BJM SCALE: N.T.S.

STANDARD No. 304



- NOTES:**
- NONWOVEN GEOTEXTILE TO HAVE A HORIZONTAL OVERLAP OF 1000mm AT JOINTS.
 - END RUNS SHALL BE TURNED UPSTREAM AT 30°.
 - STRAW BALES TO BE PLACED CONTINUOUSLY END TO END BETWEEN SEDIMENT CONTROL FENCE.

DOUBLE SEDIMENT CONTROL FENCE WITH STRAW BALES (TYP.)
SCALE: N.T.S. 08



- NOTES:**
- WATERMAIN TO HAVE MINIMUM COVER OF 1.7m.
 - UTILITY CORRIDOR TO HAVE A MINIMUM COVER OF 0.9m.
 - TREES TO BE PLACED IN LOCATIONS PER APPROVED LANDSCAPE PLAN.
 - STREETLIGHT FIXTURE PER APPROVED TOWN STANDARD.
 - THE FOLLOWING IS A MINIMUM ROAD BASE AND WILL REQUIRE A SOILS REPORT VERIFICATION:
 - 40 mm HL3
 - 65 mm HL8
 - 150 mm GRANULAR "A"
 - 300 mm GRANULAR "B"
 - THE BOULEVARDS REQUIRE A MINIMUM OF 300mm OF TOPSOIL AND NURSERY SOIL.
 - ON A CRESCENT THE WATERMAIN SHALL BE PLACED ON THE OUTSIDE.
 - FULL LENGTH MINIMUM 100 MM DIA. SUB-DRAINS CW FILTER CLOTH SHALL BE INSTALLED, AS PER APPROVED TOWN OF CALEDON STANDARD ING. 216.
 - SUB-GRADE SHALL BE COMPACTED TO A MINIMUM 95% OF S.P.D. AT OPTIMUM MOISTURE CONTENT.
 - WHERE POSSIBLE MANHOLE LIDS TO BE LOCATED OUT OF THE LANE OF TRAFFIC.
 - LONG DIMENSION OF TRANSFORMER TO BE PARALLEL TO STREETLINE.

TOWN OF CALEDON	4	TEXT AND SLOPE REVISIONS	MAY 19	APRD: C.C.	DATE: JUNE 08
	3	DIMENSION AND TEXT REVISION	JAN 09		
	2	DIMENSION AND LAYOUT REVISION	JULY 08	DRAWN: C.C.	SCALE: N.T.S.
	1	DIMENSION EDIT	JUNE 08		

18.0m LOCAL ROAD
8.5m ROADWAY (7.9m PAVEMENT)

NO.	REVISION	APRD	DATE
4	TEXT AND SLOPE REVISIONS	MAY 19	APRD: C.C. DATE: JUNE 08
3	DIMENSION AND TEXT REVISION	JAN 09	
2	DIMENSION AND LAYOUT REVISION	JULY 08	DRAWN: C.C. SCALE: N.T.S.
1	DIMENSION EDIT	JUNE 08	

STANDARD No. 202

Ecometrix | Environmental INTELLIGENCE

DESIGNED BY: R. J. WHYTE 49877509

APPROVED BY: [Signature]

PROVINCE OF ONTARIO

NO.	Date	Revisions	Dwn.	Dsg'd.	Chk'd.
③	07/APR/2026	FOURTH SUBMISSION	AAF	AAF	RJW
②	21/NOV/2025	THIRD SUBMISSION	AAF	AAF	RJW
①	17/JAN/2025	SECOND SUBMISSION	AAF	AAF	RJW
①	26/JAN/2024	DPA APPLICATION	AAF	AAF	RJW

STELLAR HOMES INC.

Project Name: **STELLAR ESTATES PHASE 2**
MULLOY COURT, TOWN OF CALEDON

Title Name: **CONSTRUCTION DETAILS**

Drawing No.: **22-3001-09**

Sheet No.: 9 OF 10

Scale: AS NOTED

