AGNES STREET SUBDIVISION, TOWN OF ALTON, ON

FUNCTIONAL SERVICING AND STORMWATER MANAGEMENT REPORT

DECEMBER 20, 2023
PROJECT 20-731

PREPARED BY
Greck and Associates Limited
5770 Highway 7, Unit 3
Woodbridge, ON
L4L 1T8

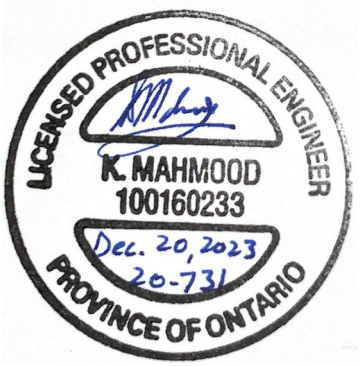
PREPARED FOR
The Alton Development Inc.
1402 Queen Street West,
Alton, Caledon, ON L7K 0C3

Greck

QUALITY ASSURANCE AND QUALITY CONTROL

Greck and Associates Limited (Greck) has a long and proud history of delivering modern and innovative solutions and diversified expertise to our clients. Our Quality Assurance and Quality Control policy ensures our products and services are reviewed internally for quality and conformance with municipal and provincial standards. Our mission of Quality Assurance and Quality Control is to maintain a high level of customer satisfaction through the provision of quality products and continuous review and development of engineering services.

Prepared and Reviewed by:



SIGNATURE

Khalid Mahmood, P.Eng.
Project Manager/Senior Municipal Engineer
kmahmoood@greck.ca

Jennifer Chan, P.Eng.
Water Resources Engineer
jchan@greck.ca

Limitations

This report was prepared by Greck and Associates Limited for The Alton Development Inc.. Any use which a third party makes of this report, or reliance on or decisions to be made based on it, are the responsibility of such third parties. Greck and Associates Limited accepts no responsibility for damages, if suffered by any third party as a result of decisions made or actions based on this project.

TABLE OF CONTENTS

LIST OF TABLES

LIST OF FIGURES

LIST OF APPENDICES

Appendix A: Site Plan, Concept Plan and Topographic Survey
Appendix B: Watermain Calculations and Hydrant Flow Test
Appendix C: Sanitary Design (By Others)
Appendix D: Stormwater Management Calculations
Appendix E: Stormwater Product Specifications
Appendix F: Engineering Drawings

1.0 INTRODUCTION

Greck and Associates Limited has been retained by The Alton Development Inc. (The Client) to prepare a Functional Servicing and Stormwater Management Report (FSSR) for a proposed subdivision on Agnes Street located in village of Alton, ON (Subject Property) in support of the proposed development of a condominium townhouse complex with 14 blocks and 67 units.

This report provides an overview of the proposed development plans and examines their functional serviceability, including requirements and proposed design works related to:

- General site grading
- Water distribution
- Sanitary Servicing
- Major and minor stormwater drainage systems
- Stormwater management; and
- Construction erosion and sediment control

This functional servicing report has been prepared in accordance with accepted engineering practices and criteria from the governing approval agencies, including the Town of Caledon (Town), Region of Peel (Region), Credit Valley Conservation (CVC), and Ministry of Environment, Conservation & Parks (MECP). Following the submission and review of this document, and approval of the current re-zoning and Draft Plan of Subdivision applications, detailed design plans, including supporting reports and drawings, will be prepared and submitted to the above-noted agencies for review and approvals, as required.

In summary, from the completed site servicing, grading, and stormwater management engineering designs, it has determined that the development can be serviced with existing and proposed infrastructure according to policies and guidelines required by the regulating agencies.

1.1 BACKGROUND

1.1.1 SITE LOCATION AND DESCRIPTION

The subject property is located in Alton, Ontario, southwest of the Queen Street West and Agnes Street intersection. The subject property is 4.047ha in size and is mainly comprised of undeveloped meadowlands.

The subject property is an infill development that is bound by the residential dwellings along Queen Street West, Agnes Street, Davis Drive and Emeline Street to the north, east, south, and west respectively. Overall access to the subject property is currently via

an existing driveway on Agnes Street. Tree lines exist along portions of the south and north limits of the property.

A topographic survey conducted by Van Harten Surveying was completed for the proposed development on July 25th, 2018. The existing property slopes from the south limit to the north at an average slope of approximately 2.8%, directing most of the major overland flow towards Agnes Street right-of-way.

The concept plan and topographic survey are provided in **Appendix A**. Please see **Figure 1** for the site location plan.

1.1.2 SOIL CONDITIONS

Terraprobe Inc. (Terraprobe) prepared a Geotechnical Investigation dated March 2019, and a Hydrogeological Investigation and Septic Impact Assessment dated December 2023. The work included drilling eight (8) boreholes equipped with monitoring wells to boreholes 2, 5, and 8 spread throughout the subject property. The soil conditions within the limits of the subject property consist primarily of the following:

- A surficial topsoil layer with a measured thickness of 150mm to 600mm, encountered at eight (8) boreholes.
- Fill consisting predominantly of silt fine sand with trave gravel and topsoil was encountered immediately beneath the ground covers in Boreholes 2,5,6,7, and 8. The fill extended to a depth generally varying from 0.8m to 2.1m below ground.
- Boreholes 1,5, and 6 penetrated a stratum of silty fine sand to depths ranging from 2.1m to 4.0m below ground.
- A deposit of silt sand and gravel with cobbles and boulders was encountered in all boreholes beneath the filly and silty fine sand to depths of about 2.5m to 6.7m below ground.

As shown within the Hydrogeological Investigation, monitoring wells were installed in boreholes 2, 5, and 8, and groundwater measurements were taken from March 4, 2019 to August 9, 2019. The seasonal high groundwater table at the site ranged from 1.1m to 6.4m below ground surface. The groundwater flow direction is easterly towards Shaw's Creek. The groundwater elevation considered for the stormwater design is 414.20m.

The geotechnical and hydrogeological reports prepared by Terraprobe are submitted under separate cover and included in the submission package.

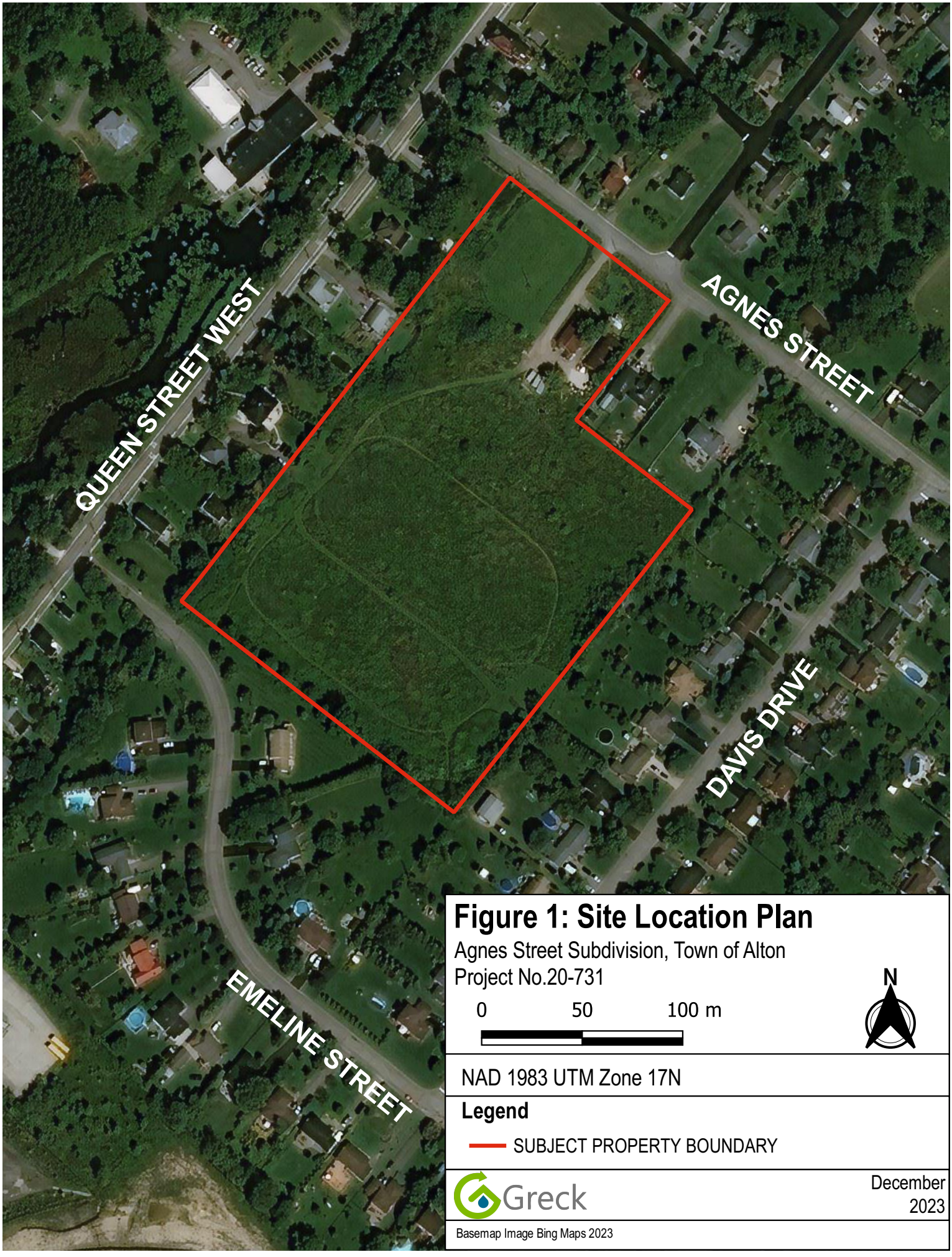


Figure 1: Site Location Plan

Agnes Street Subdivision, Town of Alton
Project No.20-731

0 50 100 m

N

NAD 1983 UTM Zone 17N

Legend

SUBJECT PROPERTY BOUNDARY

Greck

December 2023

Basemap Image Bing Maps 2023

2.0 PROPOSED DEVELOPMENT

The proposed development consists of fourteen (14) blocks of townhomes with a total of sixty-seven (67) units, above ground visitor parking with 14 parking spaces, a 6.0m wide private roadway, combined common amenity/ SWM area, walkway/emergency access block and a 1.5m wide concrete sidewalk to provide pedestrian access. The proposed development will be built on 4.047ha of vacant land. A concept plan of the proposed development prepared by Orchard Design Studio Inc. can be found in **Appendix A**.

As per Region of Peel criteria, the proposed development design population is considered based on the number of units provided in **Table 2-1.**

TABLE 2-1: PROPOSED DEVELOPMENT POPULATION BREAKDOWN

Type of Development	Population Density * (cap/unit)	No. Units	Equivalent Population
Townhouse	3.328	67	223
Total	-	67	223

* As per Region of Peel Development Charged Background Study, December 2020

The total design population is based on the number of units and was calculated to be 223 provided in **Appendix B**.

Currently, there is an existing 150mm diameter watermain located on Agnes Street and Emeline Street. The proposed development will be serviced by a new 200mm diameter PVC looped watermain connecting to the existing 150mm watermain on Emeline Street and to an upgraded 250mm watermain on Agnes Street. Refer to **Drawing SSP** provided in **Appendix F.**

Currently, there is no existing sanitary sewer infrastructure within the municipal right-of-way of the neighboring streets that bound the subject property. The proposed development will be serviced by septic beds and treatment system, for information regarding the sanitary servicing please refer to the septic design prepared by Gunnell Engineering (Gunnell) as shown in **Appendix C**.

For more details on the proposed water and sanitary services, please see Sections 5.0 and 6.0 below. Refer to the preliminary drawings provided in **Appendix F** and the Sewage System Report prepared by Gunnell Engineering in **Appendix C**.

As per the Town of Caledon's Consolidated Linear Infrastructure Environmental Compliant Approval (CLI ECA), a portion of Agnes Street will be urbanized to a 15m right-of-way (ROW). A separate design brief for the urbanization of Agnes Street has been submitted under separate cover.

3.0 SITE GRADING

As is typical with all development projects, earthmoving is required, to varying degrees, to achieve the municipal design criteria and accommodate the development form. Given the existing topography and the proposed development plan, a net fill of approximately 45,000 m^3 is anticipated.

A significant fill is required due to the varying grade changes across the limits of the site, the amount of cover required for the underground infrastructure, and the grading requirements. Surface runoff from the site will drain overland to catch basins into the proposed storm sewer system, ultimately discharging into the existing storm sewer system located on Agnes Street near the Queen Street and Agnes Street intersection. In order to accommodate the proposed site plan and adhere to municipal standards, the proposed grades will match to existing grades at the development limits.

A grading plan has been provided in **Drawing SGP**; see **Appendix F**. The plan will follow municipal design standards, as required considering the following key design factors:

- Provide positive drainage from above ground structures/buildings,
- Match external grades,
- Meet minimum and maximum grades for landscape, hardscape, and roadways.
- Achieve municipal lot grading criteria,
- Provide safe overland flow relief,
- Provide sufficient cover for underground infrastructure,
- Minimize grading and earthworks where necessary.

4.0 ROAD ACCESS

Road access to the proposed development will be facilitated by two (2) individual 6.0m wide one-way roads separated by the vegetated median to accommodate a one-way lane of traffic on each side via Agnes Street connecting to a two-way P-loop. The 6.0m wide roadways will also provide the required fire route for the proposed development. A Traffic Impact Assessment (TIA) by Paradigm Engineering (Paradigm) reviews traffic impacts and the internal circulation. The TIA is submitted under separate cover and included in the submission package.

The proposed development will have sidewalks on one side of each road and have emergency and pedestrian access to Emeline Street with a 4.0 wide concrete walkway to the west of the subject property. The preliminary design concept outlines the integration of a 1.5m wide proposed concrete sidewalk on Emeline Street, serving as a link to connect the walkway with Queen Street. However, the construction of sidewalk not be feasible if there isn't adequate space within the ROW without necessitating a complete

reconstruction of Emiline Street. Additionally, the plan includes connecting the Agnes Street entrance with a sidewalk that extends north to Queen Street and south to the southern limit of the property on Agnes Street. The proposed infrastructure aims to provide accessibility and connectivity for pedestrians. Refer to **Drawing SGP**; see **Appendix F.**

Terraprobe has recommended a pavement design in the Geotechnical Investigation dated March 2019; this report is submitted under separate cover and included in the submission package. The minimum pavement structure for the light duty and the heavy duty pavement will be as follows in **Table 4-1: .**

TABLE 4-1: PAVEMENT STRUCTURE

	Light Duty	Heavy Duty
Material	**Thickness (mm)**	
Asphalt		
Surface Course (HL3)	40	45
Basecourse (HL8)	50	60
Total Asphalt Depth	90	105
Base		
Granular A Base (OPSS 1010) or 19mm Crusher Limestone	150	150
Granular B Type II Sub-Base (OPSS 1010) or 50mm Crusher Run Limestone	300	350
Total Depth	**540**	**605**

5.0 WATER SERVICING

This section serves to provide anticipated water demands and required fire flow calculations in support of functional servicing.

Greck obtained as-built drawings from the Region for the areas adjacent to the subject property. Based on the as-built information, the existing municipal watermain infrastructure is as follows:

- 150mm diameter watermain located in the Agnes Street right-of-way, approximately 1.8 m west from the centerline of the road.
- 150mm diameter watermain located along the south limit of the Emeline Street right-of-way

Existing fire hydrant locations near to the subject property are as follows:

- The nearest existing fire hydrant is located directly in front of subject property on the west side of Agnes Street.

5.1 WATER SUPPLY AND APPURTENANCES

The Region's as-built records indicate that there are 150mm diameter watermains within both the Agnes Street and Emeline Street right-of-ways. As mentioned in Section 2.0, Water servicing for the proposed development will be supplied by a new 200mm diameter PVC looped watermain. The existing watermain from the proposed development to Queen Street will be upgraded from 150mm to 250mm diameter following recommendations of the hydraulic analysis of the proposed watermain network and connected to an existing 250mm watermain on Queen Street. At the subdivision entrance the replacement watermain will be connected to the more southerly stretch of the Agnes Street watermain with a 250x150 reducer.

The proposed 200mm PVC internal watermain will be connected to the upgraded 250mm watermain on Agnes Street and to the existing watermain on Emeline Street via a 250mm watermain under the proposed walkway/emergency access. The two new watermain connections will be accomplished by 250x250mm and 250x150mm cut-in-place tees on Agnes Street and Emeline Street respectively. The new set of 250mm valves to comply with Region's standards for valves at each tee-intersection. Water valves will be provided at the property line for the proposed development.

Four new hydrants are being proposed for 75m radius (minimum) hydrant coverage to provide fire protection for the development. The proposed hydrants will be connected to the proposed 200mm diameter looped watermain.

The nearest existing hydrant is located approximately 12m from the principal entrance of the proposed developed on the west side of Agnes Street. Please see **Drawing SSP** for the Servicing Plan provided in **Appendix F**, for the proposed watermain and hydrant layout.

5.1.1 DOMESTIC WATER DEMANDS

The design criteria used to determine the water demands were based on the Region of Peel Watermain Design Criteria, June 2010 and the Fire Underwriters Survey of Canada, 2020, as required.

Average Day Demand (ADD), Maximum Day Demand (MDD) and Peak Hour Demand (PHD) factors were calculated using demand peaking factors as per Region of Peel, Watermain Design Criteria, Section 2.3 Table 2.

Population values for the proposed development were based on Region of Peel Development Charges Background Study, December 2020, which outlines a population density of 3.328 per townhouse unit.

The estimated domestic water system demands for the proposed development of the subject property are summarized below in **Table 5-1**.

TABLE 5-1: PROJECT DOMESTIC WATER DEMANDS

Water Demand Rate	280 L/capita/day
Theoretical Population	223
Maximum Day Factor	1.8
Peak Hour Factor	3
Average Daily Demand (ADD)	41.81 L/min (0.70 L/s)
Maximum Daily Demand (MDD)	75.26 L/min (1.25 L/s)
Peak Hour Daily Demand (PHD)	125.44 L/min (2.09 L/s)

A detailed breakdown of the calculated demands can be found in **Appendix B**.

5.1.2 FIRE FLOW DEMANDS

Fire demands have been calculated using the *Water Supply for Public Fire Protection* (2020) prepared by Fire Underwriters survey (FUS). In order to keep demand in line with available flows (195 L/s) provided by the Region of Peel's hydraulic modeling assessment, a maximum gross floor area of the buildings between fire breaks or firewalls will be limited to 510 sq. meters. The calculated fire flow demand has been established at 183.33 L/s.

Detailed fire flow calculations are provided in **Appendix B**, and the results are summarized below in **Table 5-2**.

TABLE 5-2: RECOMMENDED FIRE FLOW

Proposed Building	Recommended Fire Flow (L/s)
Residential	183.33

From the fire flow calculations, it was determined that the recommended fire flow of 250.0L/s is required for the proposed development.

5.1.3 WATERMAIN HYDRAULIC ANALYSIS

Hydrant flow tests were conducted by BA Fire Safety at Agnes Street on August 22, 2022, and at Emeline Street on September 07, 2022. The results indicate an actual available maximum flow of 4182GPM (263.84L/s) at a residual pressure of 20psi. The results of the hydrant flow tests can be found in **Appendix B**.

A hydraulic analysis report (dated November 23, 2022) was completed by WSP to achieve the hydraulic requirements as prescribed by the MECP and the Region of Peel's design criteria. The report recommends upsizing of the existing 150mm watermain on Agnes Street that connects the proposed development to Queen Street to the proposed 250mm watermain. The assessment also recommends an additional 250mm connection from Emeline Street to the proposed 200mm looped watermain. The Watermain Hydraulic Analysis report is provided under a separate cover with this submission.

Peel Region's internal modeling with the recommended upgrades indicates a theoretical maximum available fire flow within the system of 195 L/s.

Based on the hydraulic analysis for the watermain network, it is confirmed that the existing 150mm watermain on Emeline Street and upgraded 250mm watermain on Agnes Street will provide sufficient pressure and flow to service the proposed development. Both actual measured flow and the calculated theoretical maximum available flow of 195 L/s are higher than the required fire flow demand of 183.33 L/s and total demand of 184.59 L/s. Therefore, the upgraded watermain network's capacity will be sufficient to meet the proposed development's water demands.

6.0 SANITARY SERVICING

This section summarizes the existing and the proposed sanitary servicing systems in support of functional servicing.

6.1 EXISTING SANITARY SYSTEM

As-built drawings indicate that currently there is no existing sanitary sewer infrastructure within the municipal right-of-way of the neighboring streets that bound the subject property.

6.2 PROPOSED SANITARY SERVICING

Sanitary servicing for the proposed development will be accomplished by individual on-site sewage treatment systems and absorption beds serving each block of townhomes. The sewage treatment design has been completed by Gunnell Engineering for the proposed development. A Sewage System Design Report prepared by Gunnell Engineering, and the Hydrogeological Investigation and Septic Impact Assessment prepared by Terraprobe will be submitted under separate cover.

Refer to **Drawing SSP** for the Servicing Plan provided in **Appendix F** and the proposed sanitary layout is provided in **Drawing SP-1** by Gunnell for the septic design in **Appendix C**.

7.0 UTILITIES

The proposed development is located within the serviced area of the Village of Alton. Electrical, natural gas, and telecommunications infrastructure is available from the adjacent public road allowances. Existing overhead electrical lines traversing the property will need to be relocated as part of the development process. Hydro One Networks has been contacted by the developer to initiate the process.

During the detailed engineering design stage, consultation with each of the service providers will be undertaken to provide them with specific load requirements for the development and proposed service entry locations. Detailed electrical, gas and utility design and coordination will be managed by a qualified engineer.

8.0 FOUNDATION DRAINAGE

A Hydrogeological Investigation and Septic Impact Assessment was prepared by Terraprobe dated December 7, 2023. As per the investigation, eight (8) boreholes were drilled on site to determine the underlying soils and four (4) of the eight boreholes were used for groundwater monitoring. The groundwater table is measured to be between an elevation of 412.8m – 415.8m. Depending on the season and location of the borehole, the groundwater was found range between 1.3m to 6.4m below the existing ground surface.

To keep the proposed block's basements dry from seepage, Terraprobe's investigation recommends perimeter foundation drains consisting of perforated pipe surrounded by a granular filter (minimum 150mm thick). The granular filter should consist of OPSS HL 8 Coarse Aggregate.

Additionally, a sub-floor drainage system to be installed beneath the basement floors of each block is recommended. This sub-floor drainage system may consist of perforated pipes and an appropriately sized sump pump should be provided to accommodate water seepage. The foundation drainage will discharge onto the grassed surface via proposed sump pump.

9.0 SURFACE DRAINAGE

This section provides an outline of the preliminary drainage proposal strategy for the proposed site plan and areas affected by the development. The proposed design will be in accordance with the Town, CVC, and MECP standards and guidelines.

9.1 EXISTING DRAINAGE

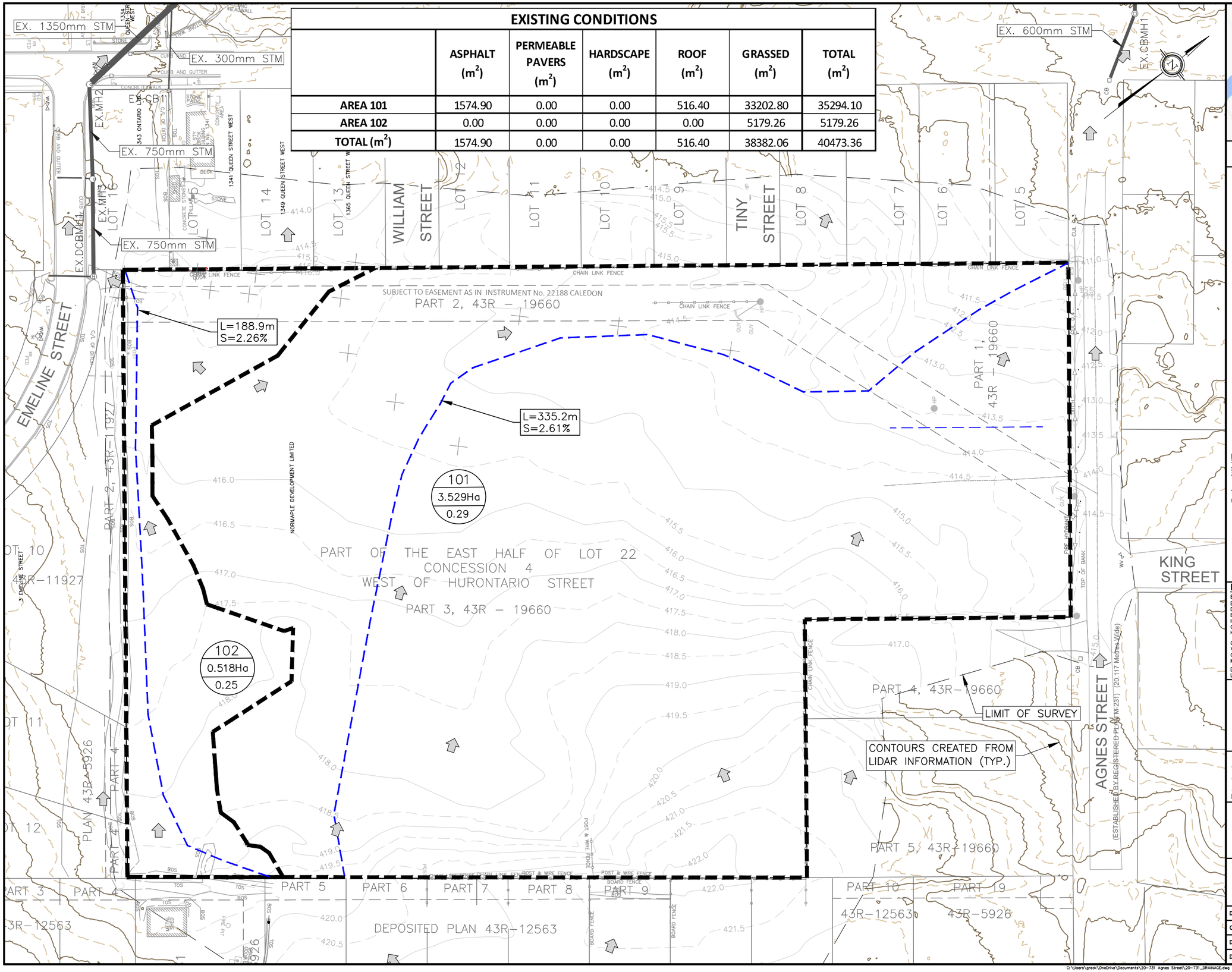
Under existing conditions, the subject site has been delineated into two (2) drainage areas - Area 101 and Area 102:

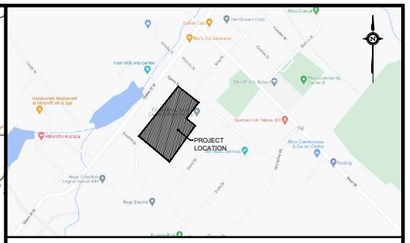
- Area 101 (3.529ha) consists primarily of grassed open field and a driveway area. This catchment drains in the north direction towards Agnes Street and has an average slope of 2.61% along the longest drainage path. Runoff from this catchment discharges to a roadside ditch parallel to Agnes Street. The ditch ultimately discharges to Shaws Creek, downstream of Alton Mill Pond.
- Area 102 (0.518ha) consists of grassed open field. This catchment drains west towards Emeline Street and has an average slope of 2.26% along the longest drainage path. Runoff from this catchment drains to the ditch inlet catchbasin, the runoff is then piped along Queen Street and ultimately discharges to Shaws Creek, downstream of Alton Mill Pond.

Note that Shaws Creek is located approximately 122m northwest of the site. Please see **Figure 2** below for the pre-development drainage area plan.

EXISTING CONDITIONS

	ASPHALT (m^2)	PERMEABLE PAVERS (m^2)	HARDSCAPE (m^2)	ROOF (m^2)	GRASSED (m^2)	TOTAL (m^2)
AREA 101	1574.90	0.00	0.00	516.40	33202.80	35294.10
AREA 102	0.00	0.00	0.00	0.00	5179.26	5179.26
TOTAL (m^2)	1574.90	0.00	0.00	516.40	38382.06	40473.36





KEY PLAN
N.T.S.

LEGEND

EXISTING	PROPOSED	
MH1	MH1	STORM MANHOLE
MH1	MH1	STORM CATCHBASIN MANHOLE
CB	CB	SINGLE CATCHBASIN
DCB	DCB	DOUBLE CATCHBASIN
		STORM SEWER
		LIMIT OF SUBJECT PROPERTY
		EASEMENT
		RIGHT OF WAY
		LOT LINE
–X–	–X–	FENCE LINE
		CURB/SIDEWALK
		BUILDING
		MAJOR CONTOUR LABEL
		MINOR CONTOUR LABEL
		SWALE
		OVERLAND FLOW
		TREE
		STORM DRAINAGE BOUNDARY
		LONGEST TRAVEL PATH
	3 0.023Ha 0.40	DENOTES AREA NUMBER DENOTES AREA IN HECTARES DENOTES RUNOFF COEFFICIENT

NOTES
1. ALL DIMENSIONS ARE IN METRES UNLESS OTHERWISE NOTED.
2. CONTOUR INTERVAL IS 0.50m.
3. ALL DIMENSIONS SHALL BE CHECKED AND VERIFIED IN THE FIELD BY THE CONTRACTOR PRIOR TO ANY CONSTRUCTION, AND ANY DISCREPANCIES SHALL BE REPORTED IMMEDIATELY TO THE ENGINEER.
4. ALL WORK SHALL BE IN ACCORDANCE WITH CURRENT TOWN OF CALEDON STANDARD SPECIFICATIONS AND DRAWINGS UNLESS OTHERWISE NOTED HEREIN.
5. ORDER OF PRECEDENCE OF STANDARDS DRAWINGS IS FIRSTLY TOWN OF CALEDON, AND SECONDLY ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD).

BENCHMARK

BENCHMARK No. N/A
ELEVATION = N/A
DESCRIPTION:
ELEVATIONS ARE BASED ON GPS OBSERVATIONS FROM PERMANENT REFERENCE STATIONS IN THE NAD83 (CSRS–2010) COORDINATE SYSTEM, WITH HEIGHTS CONVERTED TO ORTHOMETRIC ELEVATION ON THE CVGD28 DATUM (1978 ADJUSTMENT) WITH GEOID MODEL HTV2.0, AS SUPPLIED BY NATURAL RESOURCES CANADA.

COMPLETED BY:
VAN HARTEN SURVEYING INC.
COMPLETED ON:
MAY 10, 2018

DEM SOURCE:
LIDAR DTM PEEL 2016 PACKAGE B AVAILABLE FROM LAND INFORMATION ONTARIO

Greck
5770 Highway 7, Woodbridge, Ontario, L4L 1T8 www.greck.ca

CLIENT NAME:

THE ALTON DEVELOPMENTS INC.
1402 QUEEN STREET
ALTON, ON
L7K 0C3

PROJECT NAME:

AGNES STREET SUBDIVISION

AGNES STREET CALEDON, ON

DRAINAGE PLAN EXISTING CONDITIONS

DESIGNED BY:	J.N.	SCALES:		PROJECT No.	20-731
CHECKED BY:	K.M.	HORIZONTAL:	1:1000	DRAWING No.	FIG.2
DRAWN BY:	J.N.	VERTICAL:	N/A	SHEET No.	
DATE:	NOV 27, 2023	SHEET SIZE:	11"x17"		

C:\Users\greck\OneDrive\Documents\20-731 Agnes Street\20-731_DRAINAGE.dwg

Date Plotted: Dec 1, 2023 – 2:04 PM

A summary of the pre-development land cover is provided below in **Table 9-1**.

TABLE 9-1: PREDEVELOPMENT LAND-USE SUMMARY

Surface	Area 101 (m^2)	Area 102 (m^2)	Total (m^2)	Coverage
Driveway & Hardscape	2,091	0	2,091	5%
Grassed	33,203	5,179	38,382	95%
Total	35,294	5,179	40,473	100%
% Impervious	5.9%	0.0%	5.2%	5.2%
Runoff Coefficient	0.29	0.25	0.28	-

The total imperviousness of the existing site was calculated to be 5.2%, and the corresponding runoff coefficient was calculated to be 0.28. The driveway and hardscape were assigned a percent impervious of 100%. The grassed area was assigned a percent impervious of 0%. For detailed calculations, please see **Appendix D**.

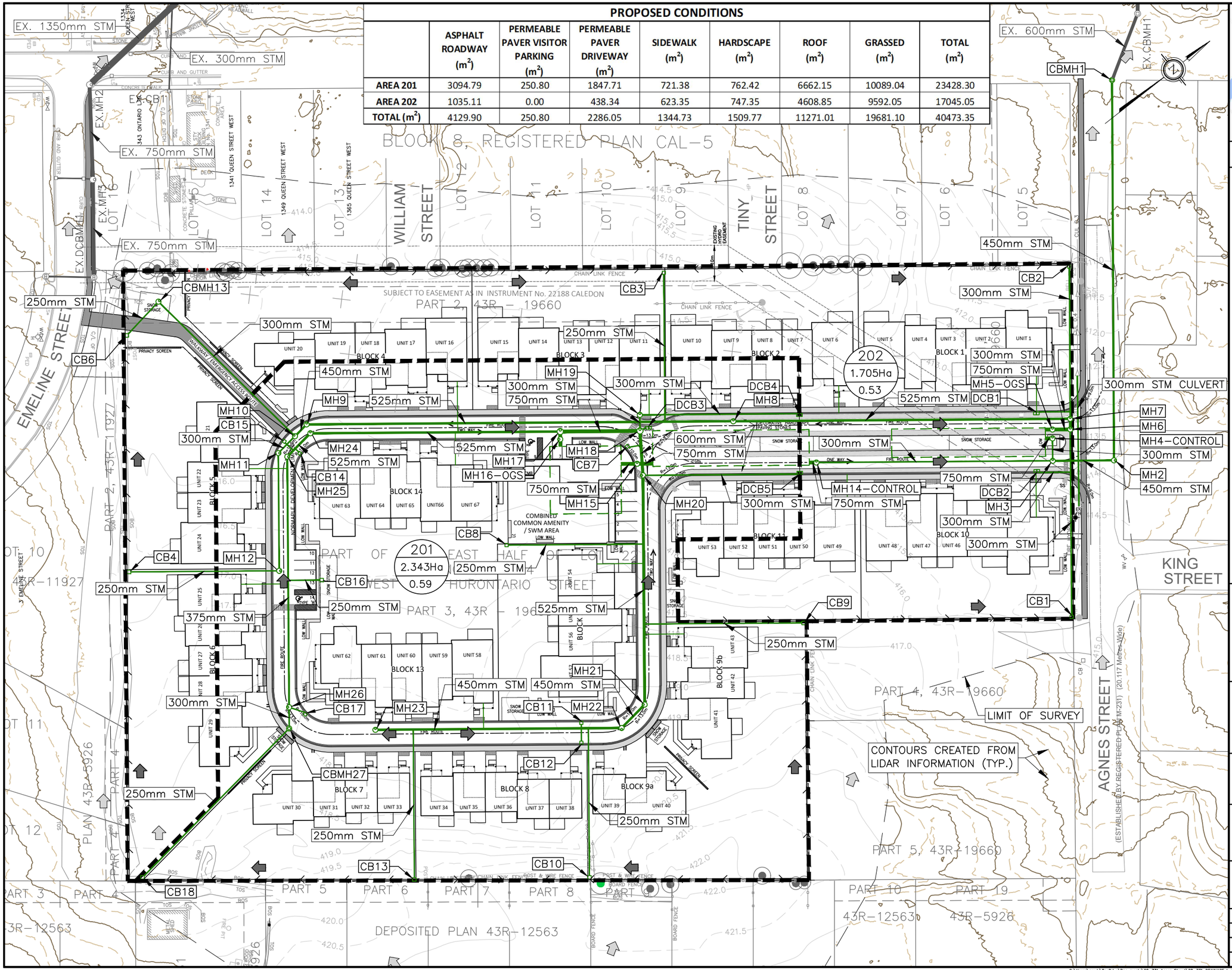
The site currently does not have any internal storm servicing and the portion of Agnes Street adjacent to the site is serviced by a roadside ditch. At detailed design, a subsurface utility investigation will be conducted to determine the location of existing subsurface utilities and pipes.

9.2 PROPOSED DRAINAGE

Under proposed conditions, the subject site has been delineated into two (2) drainage areas: Area 201 and Area 202. Both areas will consist of the right-of-way, townhomes and landscaped areas. Area 201 and Area 202 will be serviced by the proposed storm sewer system. Area 201 will first drain to an infiltration facility and Area 202 will drain directly into a quantity storage chamber. Please see **Figure 3** below for the post-development drainage area plan.

PROPOSED CONDITIONS

	ASPHALT ROADWAY (m^2)	PERMEABLE PAVER VISITOR PARKING (m^2)	PERMEABLE PAVER DRIVEWAY (m^2)	SIDEWALK (m^2)	HARDSCAPE (m^2)	ROOF (m^2)	GRASSED (m^2)	TOTAL (m^2)
AREA 201	3094.79	250.80	1847.71	721.38	762.42	6662.15	10089.04	23428.30
AREA 202	1035.11	0.00	438.34	623.35	747.35	4608.85	9592.05	17045.05
TOTAL (m^2)	4129.90	250.80	2286.05	1344.73	1509.77	11271.01	19681.10	40473.35



KEY PLAN
N.T.S.

LEGEND

EXISTING	PROPOSED	
MH1	MH1	STORM MANHOLE
MH1	MH1	STORM CATCHBASIN MANHOLE
CB	CB	SINGLE CATCHBASIN
DCB	DCB	DOUBLE CATCHBASIN
		STORM SEWER
		LIMIT OF SUBJECT PROPERTY
		EASEMENT
		RIGHT OF WAY
		LOT LINE
-X-	-X-	FENCE LINE
		CURB/SIDEWALK
		BUILDING
		MAJOR CONTOUR LABEL
		MINOR CONTOUR LABEL
		SWALE
		OVERLAND FLOW
		TREE
		STORM DRAINAGE BOUNDARY
		LONGEST TRAVEL PATH
	3	DENOTES AREA NUMBER
	0.023Ha	DENOTES AREA IN HECTARES
	0.40	DENOTES RUNOFF COEFFICIENT

NOTES
1. ALL DIMENSIONS ARE IN METRES UNLESS OTHERWISE NOTED.
2. CONTOUR INTERVAL IS 0.50m.
3. ALL DIMENSIONS SHALL BE CHECKED AND VERIFIED IN THE FIELD BY THE CONTRACTOR PRIOR TO ANY CONSTRUCTION, AND ANY DISCREPANCIES SHALL BE REPORTED IMMEDIATELY TO THE ENGINEER.
4. ALL WORK SHALL BE IN ACCORDANCE WITH CURRENT TOWN OF CALEDON STANDARD SPECIFICATIONS AND DRAWINGS UNLESS OTHERWISE NOTED HEREIN.
5. ORDER OF PRECEDENCE OF STANDARDS DRAWINGS IS FIRSTLY TOWN OF CALEDON, AND SECONDLY ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD).

BENCHMARK

BENCHMARK No. N/A
ELEVATION = N/A
DESCRIPTION:
ELEVATIONS ARE BASED ON GPS OBSERVATIONS FROM PERMANENT REFERENCE STATIONS IN THE NAD83 (CSRS-2010) COORDINATE SYSTEM, WITH HEIGHTS CONVERTED TO ORTHOMETRIC ELEVATION ON THE CVGD28 DATUM (1978 ADJUSTMENT) WITH GEOID MODEL HTV2.0, AS SUPPLIED BY NATURAL RESOURCES CANADA.

COMPLETED BY:
VAN HARTEN SURVEYING INC.
COMPLETED ON:
MAY 10, 2018

DEM SOURCE:
LIDAR DTM PEEL 2016 PACKAGE B AVAILABLE FROM LAND INFORMATION ONTARIO

Greck
5770 Highway 7, Woodbridge, Ontario, L4L 1T8 www.greck.ca

CLIENT NAME:

THE ALTON DEVELOPMENTS INC.
1402 QUEEN STREET
ALTON, ON
L7K 0C3

PROJECT NAME:

AGNES STREET SUBDIVISION

AGNES STREET CALEDON, ON

DRAINAGE PLAN PROPOSED CONDITIONS

DESIGNED BY: A.J.	SCALES:		PROJECT No. 20-731
CHECKED BY: J.C.	HORIZONTAL:	1:1000	DRAWING No. FIG.3
DRAWN BY: A.J.	VERTICAL:	N/A	SHEET No.
DATE: NOV 30, 2023	SHEET SIZE:	11"x17"	

Permeable pavers are proposed for the driveways and visitor's parking areas. A summary of the post-development land cover is provided below in **Table 9-2.**

TABLE 9-2: POST-DEVELOPMENT LAND-USE SUMMARY

Surface	Area 201 (m^2)	Area 202 (m^2)	Total (m^2)	Coverage
Asphalt	3,095	1,035	4,130	10%
Permeable Pavers	2,099	438	2,537	6%
Hardscape	1,484	1,371	2,855	7%
Roof	6,662	4,609	11,271	28%
Landscaped Area	10,089	9,592	19,681	49%
Total	23,428	17,045	40,473	100%
% Impervious	52.5%	42.4%	48.2%	
Runoff Coefficient	0.59	0.53	0.56	-

The total imperviousness of the proposed site was calculated to be 48.2%, and the overall runoff coefficient of the proposed site was calculated to be 0.56. The proposed permeable pavers allow for runoff to infiltrate between gaps and are assigned a percent impervious of 50%. The roof, asphalt, and hardscape areas are assigned a percent impervious of 100%, and the vegetated or lawn areas are assigned a percent impervious of 0%. For detailed calculations, please see **Appendix D**.

The proposed development's storm sewer is to tie into a proposed storm sewer on Agnes Street. The proposed storm sewer on Agnes Street will then tie into an existing 600mm diameter storm sewer located northeast of the property. At detailed design, the proposed storm sewer connection to the existing storm sewer system will be confirmed.

Note that a 152m portion of Agnes Street, south of Queen Street will be reconstructed into an Urban Cross Section. A Stormwater Management Design Brief for the urbanization of Agnes Street has been submitted under separate cover.

10.0 STORMWATER MANAGEMENT

The following stormwater management (SWM) criteria is to be addressed in accordance with regulatory policy:

- Water Quality
- Water Quantity
- Erosion Control
- Water Balance

The proposed SWM strategy for Area 201 and Area 202 includes considerations for water quantity control, water quality control, erosion control, and water balance for the site. The proposed SWM strategy includes a treatment train approach featuring the following SWM controls:

- Area 201 will drain to an oil grit separator (OGS) unit, then to the infiltration facility. Once the infiltration facility fills, runoff will then be piped into a quantity storage chamber.
- Area 202 will drain to an OGS unit, then into a quantity storage chamber.

Downstream of both quantity storage chambers will be a control manhole. Control MH14 will be fitted with an orifice to provide flow control for Area 201 and Control MH4 will be fitted with an orifice to provide flow control for Area 202. A water quality unit will be provided in MH16 and MH5 for Area 201 and Area 202 respectively.

10.1 WATER QUALITY

The required suspended solids removal treatment is MECP Enhanced Protection Level (Level 1). This corresponds to a long-term average removal of 80% total suspended solids (TSS).

Stormwater from the development will be characterized by runoff from roofs, pavers, landscape, and roadway surfaces. The main contaminants of concern are:

- Suspended sediments
- Phosphorous
- Other (oil, grease, gas, temperature)

Water quality controls were considered for both Area 201 and Area 202. The following is proposed for capturing and treating contaminated runoff:

For Area 201, runoff will first be treated by an OGS unit, providing sufficient stormwater treatment by trapping free oils, floatable solids and settling any captured sediment prior to discharge towards the underground infiltration facility. The OGS unit has been sized to provide a TSS removal of 60% and will be installed upstream of the infiltration facility. The infiltration facility will provide stormwater treatment by filtering suspended solids, most metals and hydrocarbons via infiltration. According to the MECP's Stormwater Management Planning and Design Manual (SWMPD, March 2003), infiltration facilities provide 80% TSS removal.

The infiltration facility is sized to accommodate the water quality volume (WQV) to achieve 80% TSS removal. WQV was determined as per Table 3.2 of the MECP SWMPD. Note that while only Area 201 is draining to the infiltration facility, the entire subject property's area was used to calculate the required WQV volume. The infiltration facility will have a volume of 123.7m^3 and a footprint of 368m^2; it will be located within the amenity space.

As per Terraprobe's Hydrogeological Investigation and Septic Impact Assessment dated December 2023, the site's groundwater elevation ranges from 411.5m– 415.8m. As per the groundwater contours shown on the Groundwater Flow Direction Plan, the groundwater at the location of the infiltration gallery is 414.2m. The bottom elevation of the infiltration facility is 415.2m. As such, the minimum 1m separation from the groundwater table requirement is satisfied.

A summary of the required and design WQV is provided below in **Table 10-1**.

TABLE 10-1: WATER QUALITY CONTROL SUMMARY

Drainage Area	40,473.4m^2
Unitary Water Quality Volume (WQV)	28.6m^3/ha
Required WQV	115.7m^3
WQV Provided By Infiltration Facility	123.7m^3

For Area 202, runoff will drain to an OGS unit specified to provide 65% TSS removal. The majority of Area 202 consists of landscaped backyards and building roofs – runoff from these land-uses are considered clean for the purposes of water quality. The permeable pavers will also provide some filtration as runoff infiltrates between the void spaces. Only a minor portion (17%) of Area 202 is hardscape and asphalt road. The OGS unit will be installed upstream of the quantity storage chambers. Due to the high groundwater elevation and grading constraints, infiltration is not possible for Area 202.

Water quality calculations are provided in **Appendix D**. Manufacturer's details regarding the OGS units and infiltration facility can be found in **Appendix E**. The drawings located in **Appendix F**.

10.2 WATER QUANTITY

The proposed storm sewer system will drain to a proposed municipal storm sewer along Agnes Street to service the subject property. As per the Town of Caledon's Development Standards Manual (2019), storm pipes shall be sized to accommodate the 5-year storm event. The proposed SWM facilities will control the 2-100 year post development flow rates down to the 2-year pre-development flow rate.

In existing conditions, Area 102 drains overland to Emeline Street and Area 101 drains overland to Agnes Street. As such, the 2-year pre-development flow rate for Area 101 will dictate the allowable flow rate.

A summary of peak flows and the target release rate is provided in **Table 10-2**, detailed flow calculations can be found in **Appendix D**.

TABLE 10-2: PEAK FLOW RATES

Storm Event	Area 101 Pre-Development Peak Runoff Rate (L/s)	Post-Development Peak Runoff Rate (L/s)		
Area	101	201	202	Total
2-year	111.9	329.7	213.4	543.1
5-year	154.9	421.9	273.1	694.9
10-year	189.4	516.0	334.1	850.1
25-year	253.6	662.0	428.6	1,090.6
50-year	313.8	813.2	526.5	1,339.7
100-year	367.9	944.9	611.7	1,556.6

Runoff from Area 201 will first drain into the infiltration facility, after the infiltration facility fills, runoff will be piped to a quantity storage chamber. The quantity storage chamber will be built using the GreenStorm product and is to be wrapped in an impermeable layer to prevent groundwater from seeping in. Runoff will be attenuated with a 130mm diameter orifice plate fitted in Control MH14. As a conservative measure, the infiltration facility is excluded from the quantity storage and is effectively considered as full at the start of each storm event.

Runoff from Area 202 will drain into a second quantity storage chamber. Due to the site's grading and groundwater constraints, the second storage chamber will be a concrete cistern. This is to ensure that the cistern can withstand the depth of cover and the lateral forces from the groundwater. Runoff will be attenuated with a 100mm diameter orifice plate fitted in Control MH4.

Attenuated flows from Area 201 and Area 202 will then be piped to MH3 where the site's storm sewer system connects to the proposed storm sewer on Agnes Street. The total provided quantity storage is 1,741m^3 and the total controlled discharge rate leaving the site is 107.5L/s which is less than the Area 101 2-year pre-development flow of 111.9L/s.

A summary of the quantity storage chambers is provided in **Table 10-3.**

TABLE 10-3: WATER QUANTITY STORAGE SUMMARY

Drainage Area	201	202
Footprint (m^2)	413	338
Total Storage Provided (m^3)	1,046.2	694.3
100-year Storage Required (m^3)	1017.3	652.1
Orifice Plate Size (mm)	130	100
Orifice Discharge (L/s)	64.33	43.14
Maximum Depth of Cover (m)	1.7	3.15

The provided quantity control storages exceed the required storages. The sizing and configuration of the quantity storage chambers and the orifices will be confirmed and further optimized during detailed design.

Water quantity control calculations are provided in **Appendix D**. The GreenStorm and concrete cistern product sheet is provided in in **Appendix E**. The servicing drawing and layout of the storage facilities can be found in **Appendix F**.

10.3 EROSION CONTROL

The CVC Stormwater Management Guidelines (July 2022) state that "the minimum erosion control requirement for all watercourses within CVC's jurisdiction is retention of the first 5mm of every rainfall event. Industry-standard storage volumes for pervious areas of 5mm were applied, therefore, the erosion control storage volume requirement will be characterized by impervious surfaces.

It is proposed to capture the equivalent of the 5mm event on additional impervious area within Area 201 and Area 202. See **Table 10-4** below for a summary of erosion control volume requirements and the storage provided by the infiltration facility during the 5mm storm event.

TABLE 10-4: EROSION CONTROL VOLUME SUMMARY

Pre-Dev. Impervious Area (m^2)	Post Dev. Impervious Area (m^2)	Post- to Pre-Dev. Added Impervious Area (m^2)	Required Volume (m^3)	Proposed Volume (m^3)
2,091.3	19,523.8	17,432.5	97.6	123.7

During the 5mm event, the proposed infiltration facility will provide 123.7m^3 of subsurface storage. The erosion control storage within the infiltration facility will be provided within

the plastic chamber units below the invert elevation of the inlet and outlet pipe. A total erosion control storage of 123.7m^3 is provided, exceeding the required 97.6m^3.

A maximum 48-hour drawdown time is required for the underground infiltration facility as per MECP criteria. Based on the Hydrogeological Investigation and Septic Impact Assessment dated December 2023 by Terraprobe, the underground infiltration facility will infiltrate into a layer of silt fine sand. Based on the grain size analysis testing, the percolation rate is 12min/cm which is equivalent to an infiltration rate of 50mm/hr.

A drawdown time of 7.0 hours was calculated for the underground infiltration facility. As such, the underground infiltration facility will achieve a maximum drawdown time of less than 48 hours. Erosion control, infiltration facility sizing, and drawdown calculations are provided in **Appendix D**.

10.4 PRELIMINARY STORMWATER MANAGEMENT DESIGN

A summary of the stormwater management facilities servicing Area 201 and Area 202 is provided below:

- Underground quantity storage chambers with a total volume of 1,741m^3 and orifice plates will be used to provide quantity control.
- An OGS unit upstream of the infiltration facility and an OGS unit upstream of both the quantity storage chambers will be used to satisfy the water quality requirement.
- The infiltration facility will provide an infiltration volume of 123.7m^3 which will satisfy the water quality and erosion control volume requirements.
- The design groundwater elevation is 414.2m. The bottom elevation of the infiltration facility is 415.2m. Therefore, the infiltration facility achieves a groundwater separation of 1m.
- A minimum cover of 2.38m from the top of the infiltration facility (415.55m) to the lowest ground elevation (417.93m).

The proposed infiltration facility and quantity storage design details will be confirmed in detail design.

10.5 WATER BALANCE

Urbanization increases impervious cover, which, if left unmitigated, results in a decrease in infiltration. This infiltration reduces groundwater recharge and soil moisture replenishment. It also reduces stream baseflow needed for sustaining aquatic life. Therefore, it is important to maintain the natural hydrologic cycle. Groundwater recharge helps maintain aquifer water levels and supports significant watershed features that are necessary components to the maintenance of a healthy watershed. As a result, a water balance analysis is required to estimate the pre-development and post-development infiltration and runoff.

For water balance criteria, the CVC requires that pre-development infiltration volumes are maintained in the post-development conditions. This typically approximately equates to the retention of the 5mm storm event.

A site-specific water balance was completed for the development area using the MECP's SWMPD (March 2003). This approach uses the method developed by Thornthwaite and Mather.

A summary of the previous and impervious areas is provided below in **Table 10-5**. To be conservative, the proposed permeable pavers were considered as impervious area and will not contribute to water balance targets.

TABLE 10-5: EXISTING AND PROPOSED LAND COVER

Area	Existing (m^2)	Proposed (m^2)
Pervious	38,382	19,524
Impervious	2,091	20,950
Total	40,473	40,473

The parameters used for the water balance analysis are provided in **Table 10-6**.

TABLE 10-6: MECP WATER BALANCE INFILTRATION PARAMETERS

	Comment	Factor
Topography	Hilly Land	0.1
Soils	Open Sandy Loam	0.4
Cover	Cultivated Land	0.1

A total deficit volume of 3,753.8m^3/year will not be infiltrated into the ground given the proposed development plan and resulting change in pervious cover. As such, this annual volume must be balanced and infiltrated back into the ground under proposed conditions.

The water balance target of 3,753.8m^3/year will be provided through the subsurface infiltration facility for the property.

The infiltration facility has been sized to capture the 5mm rainfall event to meet erosion control requirements, which represents approximately 50% of all rainfall events in a given year (City of Toronto WWFMG Figure 1b, November 2006).

An annual precipitation of 902mm was determined (MECP's Orangeville MOE climate station). Assuming that 10% of the rainfall is evaporated, an impervious annual surplus of 811mm was determined and directed towards the infiltration chambers.

Based on an annual impervious surplus of 811mm per year, and assuming 50% of all rainfall events are infiltrated, the annual infiltration volume towards the infiltration facility equates to 9,350m^3, for a total site-wide infiltration of 13,236m^3.

However, for design and conservative purposes, a factor of safety of 1.5 was applied to the total infiltration facility infiltrated volume in the event that infiltration does not occur as efficiently due to soil saturation, partially full infiltration facility from previous rainfall events, or unexpected in-situ soil conditions. This equates to an annual infiltration volume of 6,233m^3, for a total site-wide infiltration of 10,119m^3, therefore exceeding pre-development conditions.

A summary of the infiltration volumes is provided in **Figure 4**.

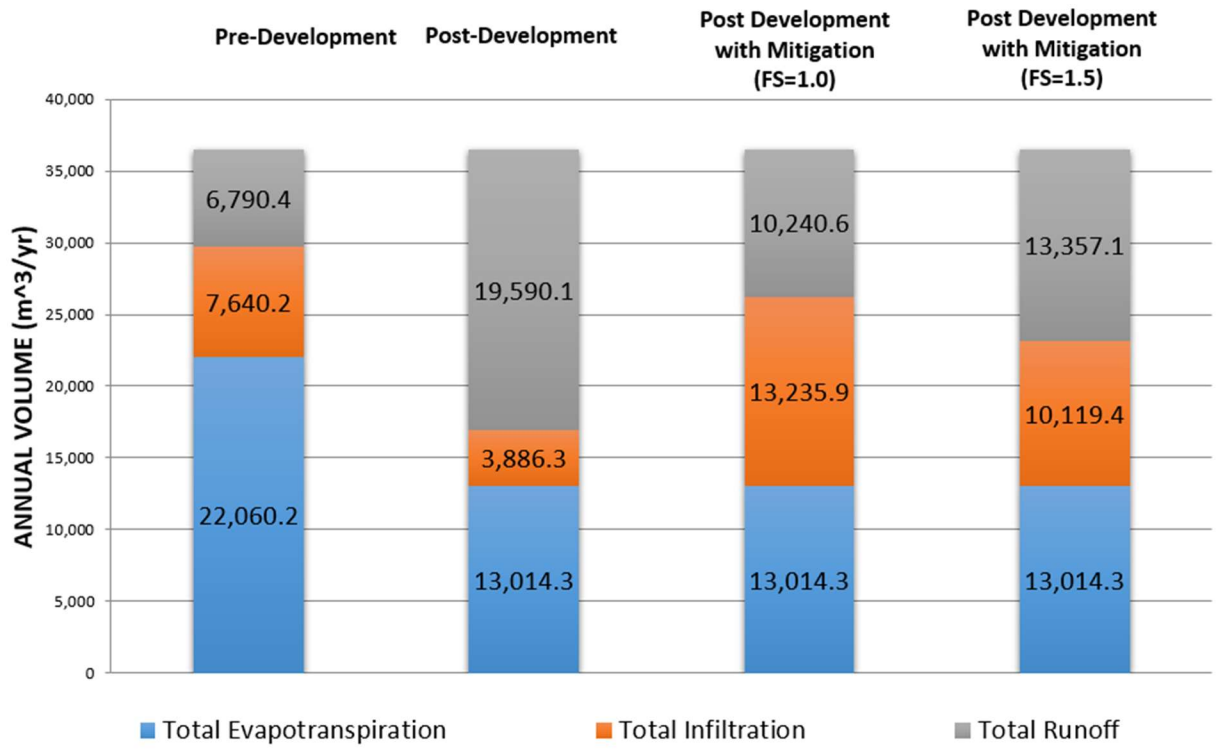


FIGURE 4: WATER BALANCE SUMMARY

As such, the application of the infiltration facility achieves a net increase in overall infiltration, which meets the CVC criteria of maintaining pre-development infiltration levels and providing 5mm of on-site retention. For water balance calculations, please see **Appendix D**.

11.0 EROSION AND SEDIMENT CONTROL

Erosion and sediment controls (ESC) will be implemented for all construction activities, including topsoil striping, material stockpiling, pavement construction, and grading operations. Design details will include a phased approach to minimize disturbance including considerations for restoration. Refer to the Erosion and Sediment Control Plan and Details provided in **Appendix F**.

12.0 CONCLUSIONS

As presented in this report, the proposed development will meet the following municipal and provincial standards and regulations specified for:

- General site grading;
- Water distribution;
- Sanitary sewer servicing;
- Utilities
- Stormwater management; and
- Construction erosion and sediment controls

In summary, it has been determined that the development can be serviced with existing and proposed infrastructure that is in accordance with policies and guidelines required by the Town of Caledon, CVC and other regulating agencies.

13.0 REFERENCES

Credit Valley Conservation – Stormwater Management Guidelines, July 2022

Fire Underwriters Survey – Water Supply for Public Fire Protection – 2020

Ministry of the Environment, Conservation and Parks – Stormwater Management Planning and Design Manual – March 2003

Ministry of the Environment, Conservation and Parks – Design Guidelines for Drinking Water Systems – 2008

Ministry of the Environment, Conservation and Parks – Design Guidelines for Sewage Works – 2008

Region of Peel Development Charges Background Study, December 2020

Region of Peel Watermain Design Criteria, June 2010

Town of Caledon – Development Standards Manual, 2019

APPENDIX A

Site Plan, Concept Plan, and Topographic Survey

QUEEN STREET W.

EMELINE STREET

AGNES STREET

KING ST.

1.5m WIDE WALKWAY EXTENDED TO QUEEN ST.

LOT 16 | LOT 15 | LOT 14 | LOT 13 | LOT 12 | LOT 11 | LOT 10 | LOT 9 | LOT 8 | LOT 7 | LOT 6 | LOT 5

SNOW STORAGE

PRIVACY SCREEN

WALKWAY / EMERGENCY ACCESS ROUTE

BLOCK 1 | BLOCK 2 | BLOCK 3 | BLOCK 4 | BLOCK 5 | BLOCK 6 | BLOCK 7 | BLOCK 8 | BLOCK 9a | BLOCK 9b | BLOCK 10 | BLOCK 11 | BLOCK 12 | BLOCK 13 | BLOCK 14

COMBINED COMMUNITY AMENITY / SWM AREA (1,031 sq.m.)

1.5m SIDEWALK

FIRE ROUTE

TWO WAY

ONE WAY

DECORATIVE HARDSCAPE PAVING STONES

LOW WALL

CMB

TYPE 'A'

TYPE 'B'

SP. = 11.00

SP. = 2.75

SP. = 13.75

R=8.0m

R=10.0m

R=13.0m

99.90

104.72

LOT COVERAGE

BLOCK	COVERAGE
1	35.4%
2	39.6%
3	39.4%
4	32.0%
5	31.5%
6	29.7%
7	23.7%
8	29.7%
9	22.7%
10	35.7%
11	39.9%
12	31.7%
13	37.8%
14	37.2%

LEGEND

- PROPERTY LINE
- 6.0m WIDE FIRE ROUTE
- STOP SIGN
- EXISTING TOPOGRAPHY
- PAINTED STOP BAR
- EXISTING TREE TO REMAIN
- DISPERSAL BED
- PEDESTRIAN CROSSING
- PROPOSED DRY STACK STONE WALL
- PROPOSED 1mX3m WASTE COLLECTION POINT

NOTES:

1. THIS IS A CONCEPT PLAN FOR THE PURPOSE OF GUIDING THE DESIGN OF THE DRAFT PLAN OF SUBDIVISION AND ZONING BY-LAW AMENDMENT. DETAILED SITE PLANS WILL BE PREPARED FOR THE INDIVIDUAL BLOCKS FOR INCLUSION IN BUILDING PERMIT APPLICATIONS.
2. A MODIFIED RT (RESIDENTIAL TOWNHOUSE) ZONE IS PROPOSED BASED ON THE CONCEPT PLAN CONTAINING SITE-SPECIFIC STANDARDS WHERE NECESSARY. SEE THE PROPOSED ZONING MATRIX DETAILED TABLE OUTLINING ALL PROPOSED ZONING STANDARDS.
3. TOPOGRAPHICAL INFORMATION INCLUDING TREE LOCATIONS TAKEN FROM VANHARTEN SURVEY PLAN DATED SEPTEMBER 16, 2022.
4. TREE INVENTORY INFORMATION FROM WILLIAMS & ASSOCIATES ARBORISTS REPORT FEB. 16, 2023 AND UPDATED OCT. 16, 2023. 29 TREES ARE IDENTIFIED FOR RETENTION. GRADING PLAN WILL PROVIDE DETAILS ABOUT TREE PROTECTION MEASURES AT SITE PLAN STAGE.
5. 3-WAY STOP, STOP BARS, PEDESTRIAN CROSSING PAVEMENT MARKINGS AND CHICANE FEATURE AS RECOMMENDED IN TRAFFIC IMPACT STUDY BY PARADIGM ENGINEERING. TO BE DETAILED DURING DETAILED SUBDIVISION DESIGN PROCESS IN ACCORDANCE WITH ONTARIO TRAFFIC MANUAL BOOK 11.
6. WALLS AND PRIVACY SCREEN LOCATIONS ARE APPROXIMATE ONLY AND WILL BE FINALIZED DURING THE DETAILED SUBDIVISION/CONDOMINIUM PROCESS(ES). THESE ELEMENTS WILL BE MAINTAINED BY THE CONDOMINIUM CORPORATION(S).
7. ACCESSIBLE SPACES INCLUDE ONE TYPE 'A' SPACE AND ONE TYPE 'B' SPACE.

SITE DATA

REGULATION	PROPOSED
LOT FRONTAGE (ON AGNES STREET)	99.90 m
SITE AREA (ha)	40,445.80 sq.m. (4.04ha)
# UNITS WITH DOUBLE GARAGES	41
# UNITS WITH SINGLE GARAGEGS	26
TOTAL UNITS	67
DENSITY	16.58 Upha
# OF RESIDENTIAL BLOCKS	14
# OF UNITS PER BLOCK (MAX.)	5
BUILDING HEIGHT	10.5 m
MINIMUM SETBACK TO AGNES STREET	6.0 m
MIM. SETBACK FROM REAR OF DWELLINGS TO ABUTTING RESIDENTIAL PROPERTIES	13.07 m
AREA TABLE	
RESIDENTIAL BLOCKS	3.319 ha
COMMON ROAD AND PARKING	0.435 ha
COMMON AMENITY AND WALKWAY	0.291 ha
TOTAL	4.045 ha
OPEN SPACE and COVERAGE	
YARDS, ABSORPTION BEDS, COMMON AMENITY AREAS	2.001 ha (49.4%)
HARD SURFACE AREAS (BUILDINGS, PATIOS, ROADS, WALKWAYS, SIDEWALKS, DRIVWAYS)	2.044 ha (50.6%)
TOTAL	4.045 ha
PARKING PROVIDED	TOTAL
PRIVATE PARKING WITHIN GARAGES	108
PRIVATE PARKING IN DRIVEWAYS	108
COMMON VISITOR PARKING	14
TOTAL	230

ORCHARD DESIGN STUDIO INC.
marketingmeetsarchitecture

User Defined

Project Information

SEATON GROUP

BUNGALOW TOWNHOMES WITH LOFTS

Agnes Street, Caledon, ON.

Set Issuance

No.	Date	Description

Sheet Information

SITE PLAN

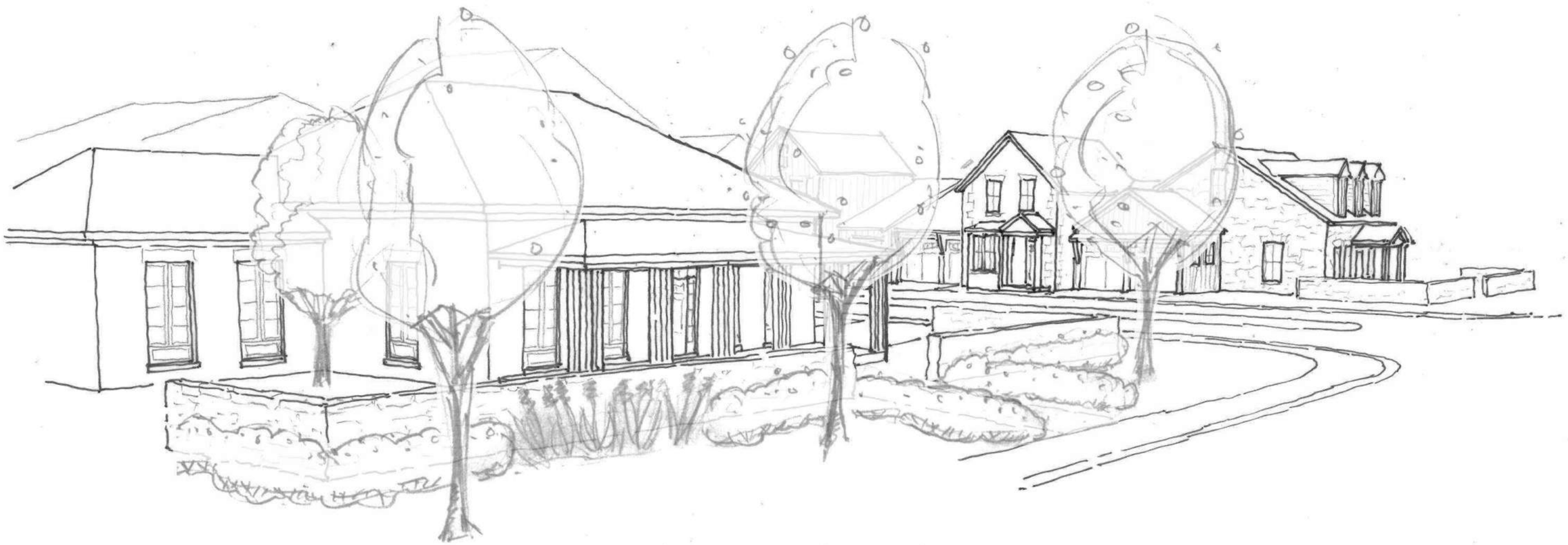
Project No. 14948
Project Start Date: 2023.11.01
File: Agnes Street - Site Plan.dwg
Drawn by: KBR
Scale: 1:400

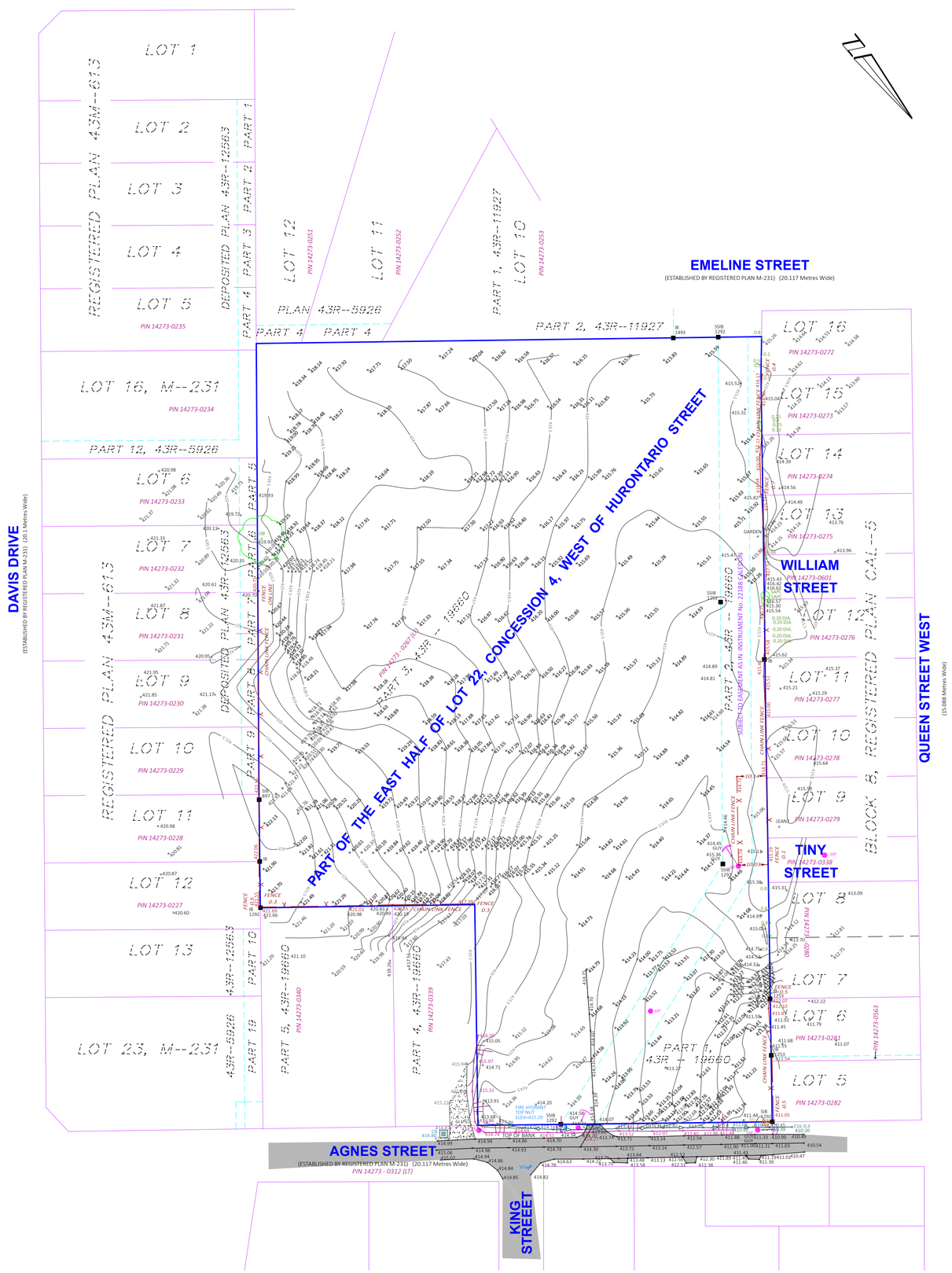
PRELIMINARY

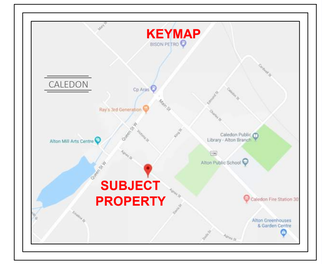
A1.01

Plot Date|Time - 11/9/2023 10:50:45 AM

P:\1-Projects\Seaton Group\14948_Agnes st\2-Drawings\







TOPOGRAPHIC SURVEY OF PART OF EAST HALF OF LOT 22, CONCESSION 4, WEST OF HURONTARIO STREET

GEOGRAPHIC TOWNSHIP OF CALEDON, COUNTY OF PEEL

TOWN OF CALEDON

REGIONAL MUNICIPALITY OF PEEL

SCALE 1 : 750

0 5 10 20 30 40 50 metres

750

VAN HARTEN SURVEYING INC.

LEGEND

⊡	DENOTES SURVEY MONUMENT SET
■	DENOTES SURVEY MONUMENT FOUND
SIB	DENOTES .025 x .025 x 1.20 STANDARD IRON BAR
IB	DENOTES .015 x .015 x 0.60 IRON BAR
SSIB	DENOTES .025 x .025 x 0.60 SHORT STANDARD IRON BAR
RP	DENOTES .015 DIA. X 0.07 ROUND IRON BAR WITH STAMPED WASHER
PB	DENOTES .025 x .025 x 0.30 PLASTIC BAR
CC	DENOTES CUT CROSS
WIT	DENOTES WITNESS
OU	DENOTES ORIGIN UNKNOWN
VH	DENOTES VAN HARTEN SURVEYING INC., O.L.S.'s
1292	DENOTES WM. E. BENNETT SURVEYING LTD., O.L.S.'s
897	DENOTES WILLIAM J. QUINSEY, O.L.S.'s
1493	DENOTES YOUNG AND YOUNG SURVEYORS INC., O.L.S.
375	DENOTES D.J. CULLEN LTD., O.L.S.

EXISTING ELEVATION × 206.55

GUY WIRE — GUY

HYDRO POLE — HP

FIRE HYDRANT — FH

CATCHBASIN — CB

BELL PEDESTAL — BELL

LINETYPES

OVERHEAD HYDRO — OH

FENCELINE — X

DITCH/SWALE

CENTRELINE OF ROAD

TOP OF BANK

HATCHES

ASPHALT

GRAVEL

BENCHMARK:

ELEVATIONS ARE BASED ON GPS OBSERVATIONS FROM PERMANENT REFERENCE STATIONS IN THE NAD83 (CSRS-2010) COORDINATE SYSTEM, WITH HEIGHTS CONVERTED TO ORTHOMETRIC ELEVATIONS ON THE CVGD28 DATUM (1978 ADJUSTMENT) WITH GEOID MODEL HTv2.0, AS SUPPLIED BY NATURAL RESOURCES CANADA.

REFERENCE:

1. BEARINGS ARE GRID BEARINGS AND ARE DERIVED FROM GPS OBSERVATIONS AND ARE REFERRED TO THE UTM PROJECTION, ZONE 17. NAD 83-CSRS (2010) ADJUSTMENT.
2. DISTANCES SHOWN ON THE PLAN ARE ADJUSTED GROUND DISTANCES AND CAN BE CONVERTED TO UTM GRID DISTANCES BY MULTIPLYING BY AN AVERAGED COMBINED SCALE FACTOR OF 0.9996086

NOTE:

BOUNDARY INFORMATION SHOWN ON THIS PLAN WAS COMPILED FROM REGISTRY OFFICE INFORMATION AND PLAN FOR THE SUBJECT PROPERTY: 43R-19660

FIELD WORK FOR THIS SURVEY WAS COMPLETED ON THE 10th DAY OF MAY , 2018

JAMES M. LAWS

ONTARIO LAND SURVEYOR

METRIC:

DISTANCES SHOWN ON THIS PLAN ARE IN METRES AND CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048.

REVISION SCHEDULE

No.	DATE	BY	COMMENTS
1	7/25/18	S.J.	INITIAL SUBMISSION

Van Harten SURVEYING INC.
LAND SURVEYORS and ENGINEERS

Kitchener Ph: 519-742-8371 | Guelph Ph: 519-821-2763 | Orangeville Ph: 519-940-4110

www.vanharten.com info@vanharten.com

DRAWN BY: S.J. | CHECKED BY: JML | PROJECT No. 25228-17

SEATON GROUP

Jul 25,2018-4:41pm
G:\CALEDON\CON4WHS\AGNES ST DEVELPOMENT\ACAD\TOPO-R08B UTM 2010 NR.dwg

APPENDIX B

Watermain Calculations and Hydrant Flow Test

HYDRANT FLOW TEST REPORT

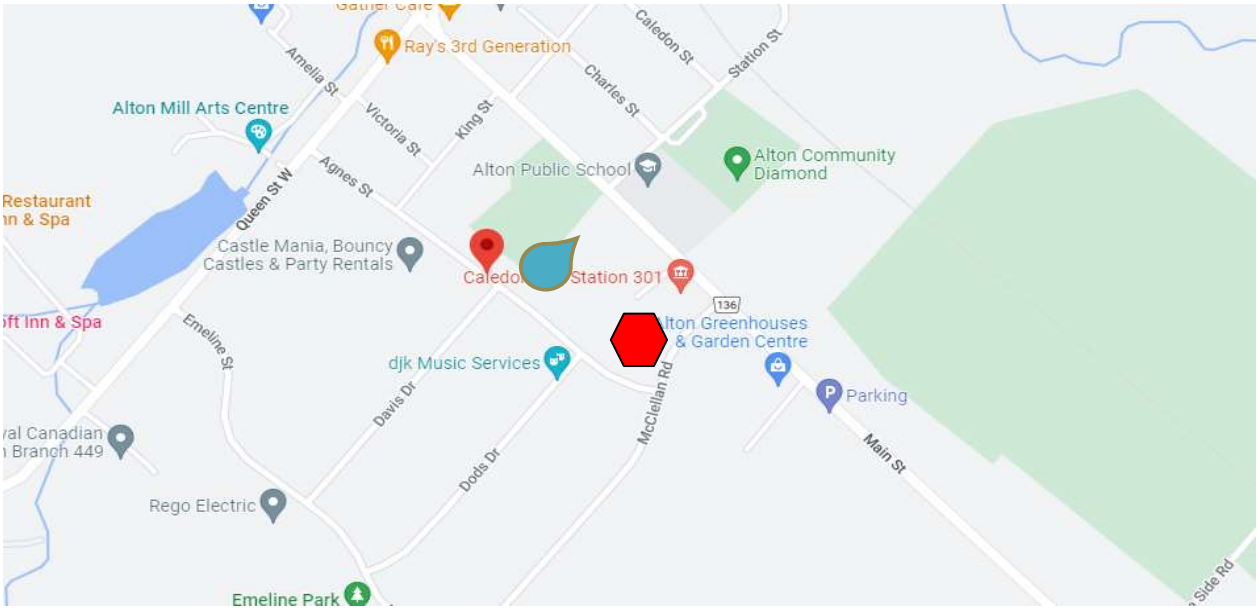
GENERAL INFORMATION:

PROJECT ID	**105-22**	TESTED BY:	AA/RS
PROJECT NAME	**Agnes Street - Hydrant Flow Test #1**	DATE	**August 22-22**
BUILDING ADDRESS	**Agnes Street**	TIME	**2:00:00 PM**
	Alton, Ontario		

WATER MAIN INFORMATION:

MAIN SIZE / MATERIAL	**150MM**
CONFIGURATION	**Looped**

HYDRANT LOCATION:



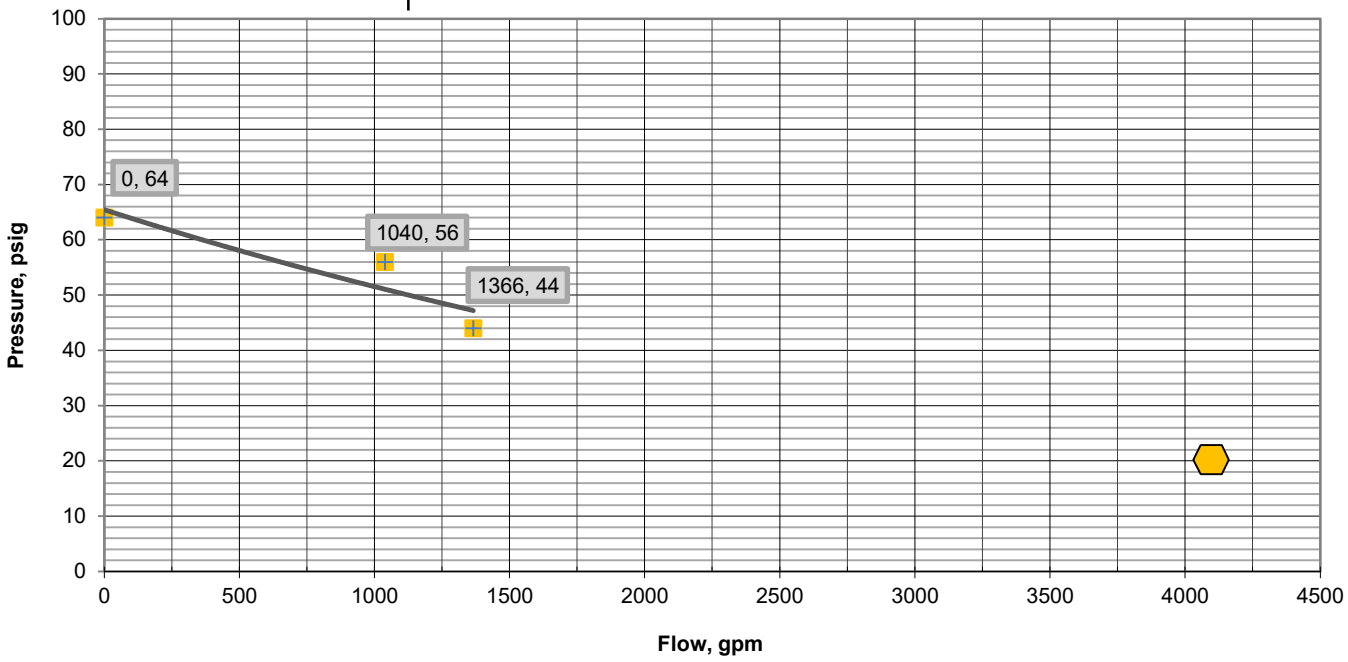
LEGEND: STATIC HYDRANT RESIDUAL HYDRANT

FINAL RESULTS:

Test #	Number of Outlets	Orifice Size (in)	Pitot Reading (psig)	EquivInt Flow (usgpm)	Total Flow (usgpm)	Projected flow at 20psi	Gauge Pressure (psig)	Discharge Coef'nt
Static	N/A	N/A	N/A	N/A	**0**	N/A	**64**	N/A
1	1	2.47	51	1040	**1040**	2610	**56**	0.8
2	2	2.47	22	683	**1366**	2091	**44**	0.8

FLOW AT 20PSI (140kPa) :

SINGLE OUTLET **2610 GPM (2 1/2 NOZZLE)**
DOUBLE OUTLET **2091 GPM (2 1/2 NOZZLE) - Combined = 4182 GPM**



HYDRANT INFORMATION:

HYDRANT DETAILS **CLASS C (RED)**
LISTED FLOW **500GPM @ 20PSI**

HYDRANT FLOW TEST REPORT

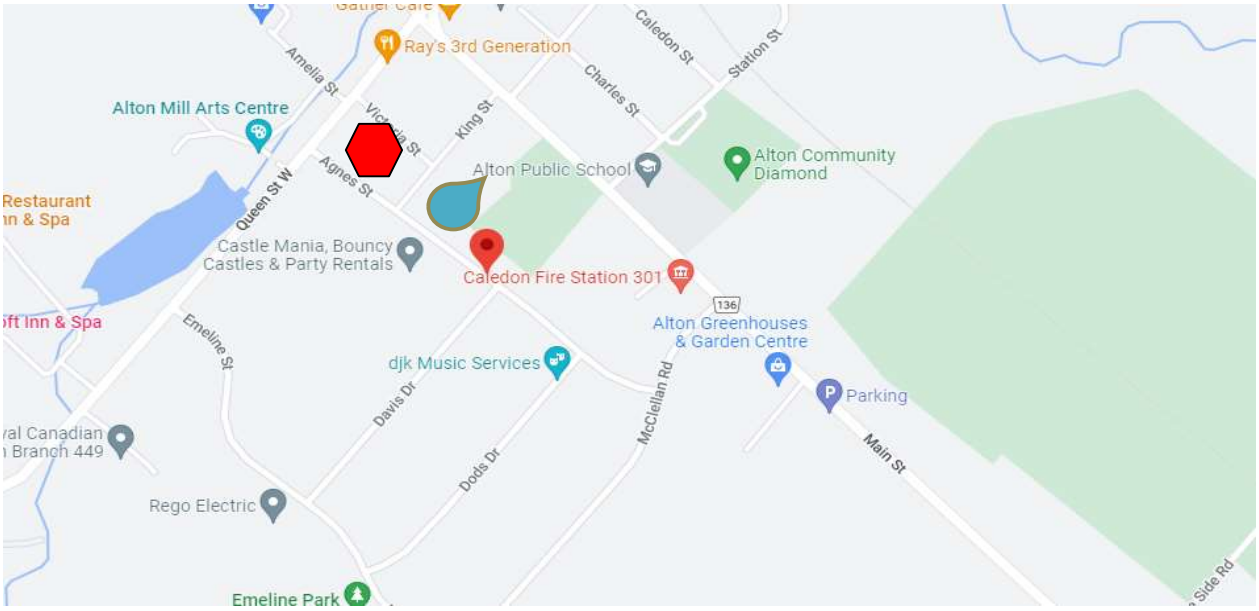
GENERAL INFORMATION:

PROJECT ID	**105-22**	TESTED BY:	AA/RS
PROJECT NAME	**Agnes Street - Hydrant Flow Test #2**	DATE	**August 22-22**
BUILDING ADDRESS	**Agnes Street**	TIME	**2:00:00 PM**
	Alton, Ontario		

WATER MAIN INFORMATION:

MAIN SIZE / MATERIAL	**150MM**
CONFIGURATION	**Looped**

HYDRANT LOCATION:



LEGEND: STATIC HYDRANT RESIDUAL HYDRANT

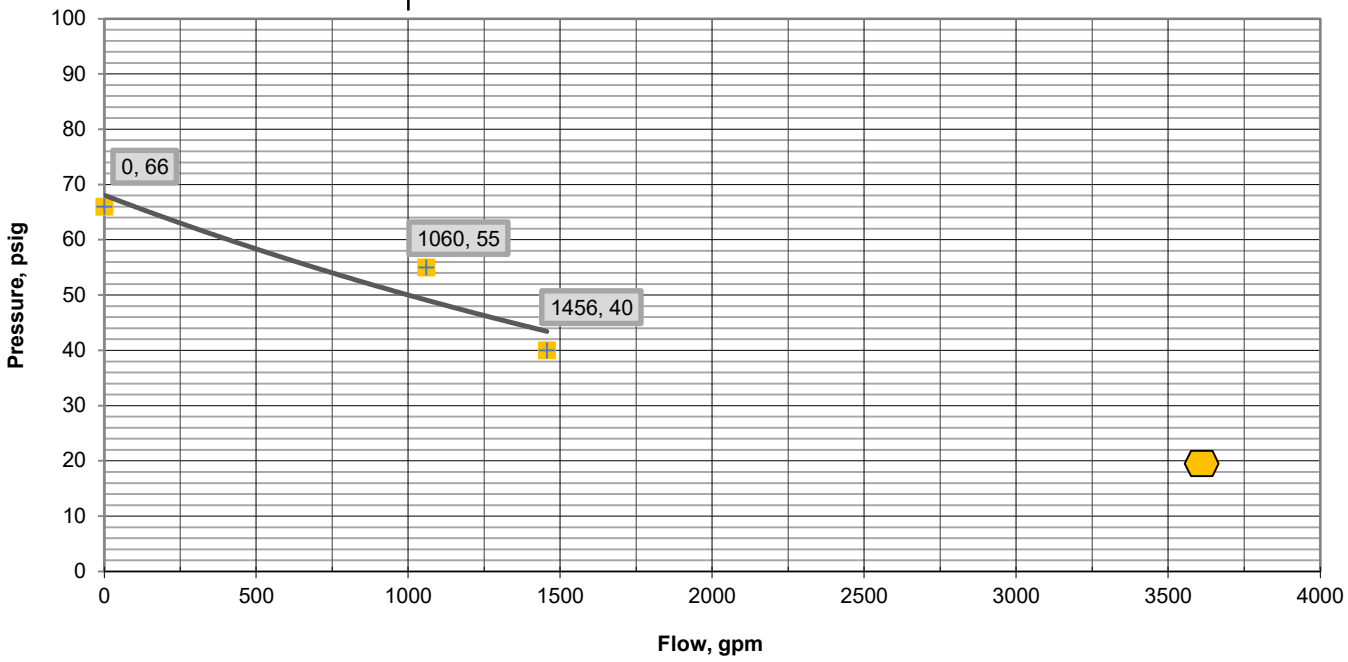
FINAL RESULTS:

Test #	Number of Outlets	Orifice Size (in)	Pitot Reading (psig)	EquivInt Flow (usgpm)	Total Flow (usgpm)	Projected flow at 20psi	Gauge Pressure (psig)	Discharge Coef'nt
Static	N/A	N/A	N/A	N/A	**0**	N/A	**66**	N/A
1	1	2.47	53	1060	**1060**	2295	**55**	0.8
2	2	2.47	25	728	**1456**	1981	**40**	0.8

FLOW AT 20PSI (140kPa) :

SINGLE OUTLET **2295 GPM (2 1/2 NOZZLE)**

DOUBLE OUTLET **1981 GPM (2 1/2 NOZZLE) Combined = 3962 GPM**



HYDRANT INFORMATION:

HYDRANT DETAILS **CLASS C (RED)**

LISTED FLOW **500GPM @ 20PSI**

HYDRANT FLOW TEST REPORT

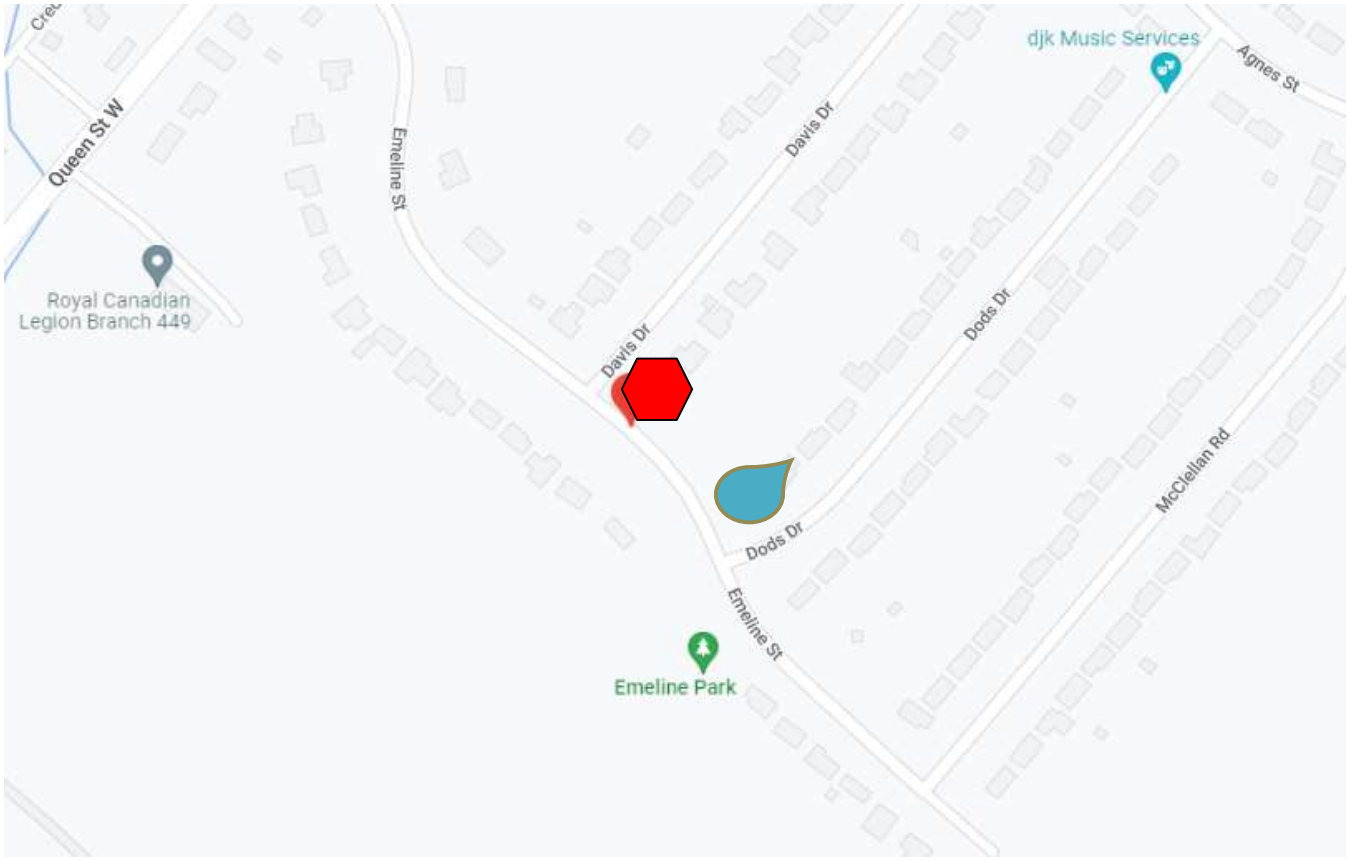
GENERAL INFORMATION:

PROJECT ID	**116-22**	TESTED BY:	RS
PROJECT NAME	**Emeline Street Flow Test**	DATE	**Sept 7-22**
BUILDING ADDRESS	**Emeline Street and Dods Drive Alton, Ontario**	TIME	**2:00:00 PM**

WATER MAIN INFORMATION:

MAIN SIZE / MATERIAL	**150MM**
CONFIGURATION	**Looped**

HYDRANT LOCATION:



LEGEND: STATIC HYDRANT RESIDUAL HYDRANT

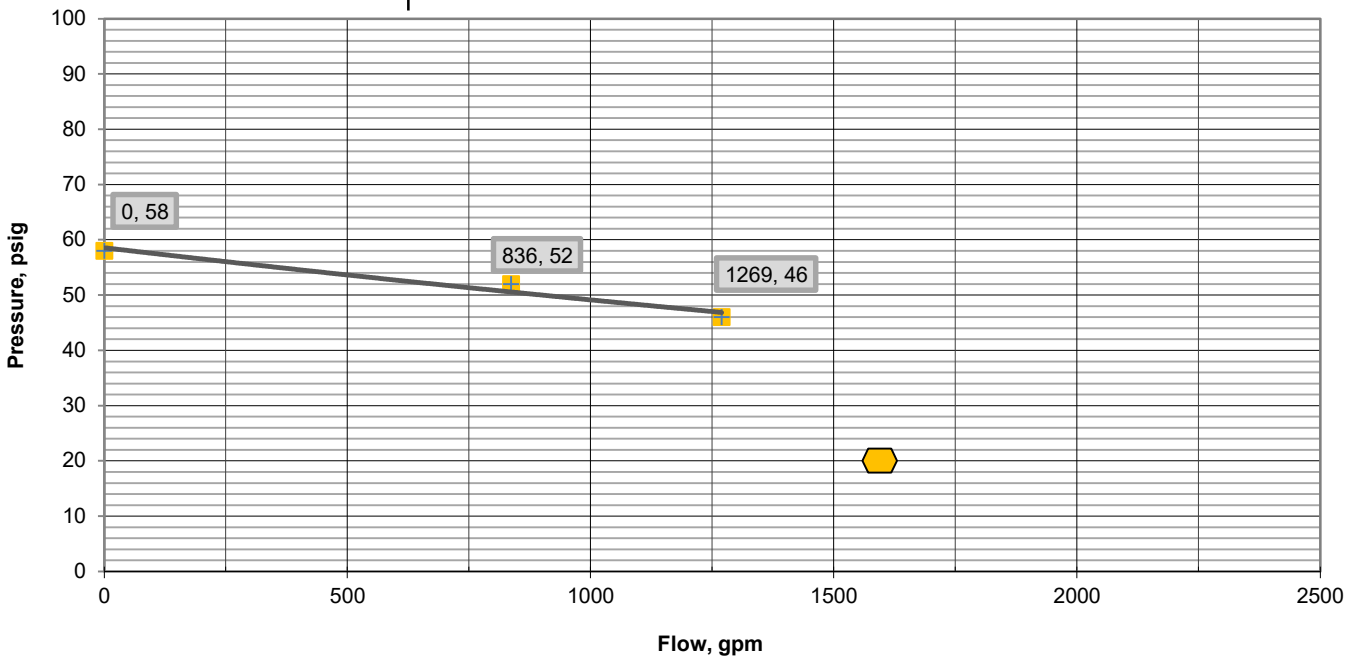
FINAL RESULTS:

Test #	Number of Outlets	Orifice Size (in)	Pitot Reading (psig)	EquivInt Flow (usgpm)	Total Flow (usgpm)	Projected flow at 20psi	Gauge Pressure (psig)	Discharge Coef'nt
Static	N/A	N/A	N/A	N/A	**0**	N/A	**58**	N/A
1	1	2.47	33	836	**836**	2266	**52**	0.8
2	2	2.47	19	635	**1269**	2365	**46**	0.8

FLOW AT 20PSI (140kPa) :

SINGLE OUTLET **1269 GPM (2 1/2 NOZZLE)**

DOUBLE OUTLET **836 GPM (2 1/2 NOZZLE)- Combined = 1672 GPM**



HYDRANT INFORMATION:

HYDRANT DETAILS **CLASS C (RED)**

LISTED FLOW **500GPM @ 20PSI**

THEORETCIAL FIRE FLOW CALCULATIONS

PROJECT: Agnes Street Subdivision
PROJECT No: 20-731
LOCATION: Caledon, ON
DATE: October 18, 2023

DESIGNED BY: Deven Verma, EIT.
REVIEWED BY:Khalid Mahmood, P. Eng

$$F = 220C\sqrt{A}$$

F = The required Fire Flow in litres per minute

C = Coefficient related to the type of construction

A = The tatal floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered

Total Floor Area (A) considered for fire flow (m2) 510.0

NOTES

- Table below is based on procedures and figures from the Water Supply for Public Fire Protection - Fire Underwriters Survey of Canada, 2020.
- Exposure distance factor max adjustment is 75%.
- Type of building construction is wood frame as confirmed by the architect.

Manual Input

PROPOSED RESIDENTIAL UNIT

Step	Description	Term	Options		Multiplier Associated with Option	Value used	Unit	Total Fire Flow (L/min)
1	Frame Use for Construction of Unit	**Building Material**						
		Coefficient related to type of construction (C)	Wood Frame		1.5	1.5	N/A	N/A
			Ordinary Construction		1			
			Non-Combustible Construction		0.8			
			Fire Resistive materials (<2hrs)		0.7			
			Fire Resistive materials (>2hrs)		0.6			
2	Number of Storeys	Number of floors not inlcuding basement				2	N/A	N/A
3	Floor Area (A)	Total Floor Area (A) - for all stories exluding basement (m²)				510.0	(m²)	N/A
		Average Floor Measurements	Square Feet (ft²)		0.093	255.0		
			Square Metres (m²)		1			
			Hectares (ha)		10,000			
4	Fire Flow	Required fire flow without reductions or increases (rounded to the nearest 1000 L/min:					L/min	7,000
5	Combustibility of Building Contents	**Reductions / Increases From Factors Affecting Burning**						
		Occupancy content hazard reduction or surcharge Factor	Non-Combustible		-0.25	-0.15	N/A	-1,050
			Limited Combustible		-0.15			
			Combustible		0.00			
			Free Burning		0.15			
			Rapid Burning		0.25			
6	Building Equipped with Sprinklers	Sprinkler Reduction Factor	Complete Automatic Sprinklers		-0.50	0.00	N/A	0
			Adequate Automatic Sprinklers		-0.30			
			None		0.00			
7	Separation Distance Between Buildings	Exposure Distance Factor *	North Separation	20.1 - 30m	0.10	0.65	N/A	4,550
			South Separation	20.1 - 30m	0.10			
			East Separation	0 to 3m	0.25			
			West Separation	3.1 to 10m	0.20			
8	Required Fire Flow						**Total Required Fire Flow Rounded to the Nearest 1000 L/min:**	**11,000**
							Total Required Fire Flow in L/s:	183.3
							Duration of Fire Flow (hrs):	2
							Required Volume of Fire Flow (m³):	1,485

*Floor areas confirmed with the architect (ORCHARD Design Studio Inc.). Coefficient for type of construciton (C) is for non-conbustible construction as confimred by the architect.

Separation Distance Factor as per Fire Underwriters Survey of Canada, 2020

Seperation	*Charge*	*Seperation*	*Charge*
0 to 3m	*25%*	*20.1 to 30m*	*10%*
3.1 to 10m	*20%*	*30.1 to 45m*	*5%*
10.1m to 20m	*15%*		

Acceptable Fire Flow ranges as per Fire Underwriters Survey of Canada, 2020

2,000 Lpm < F < 45,000 Lpm; therefore acceptable

Note: For types of construction that do not fall within the categories given, coefficients shall not be greater than 1.5 nor less than 0.6 and may be determined by interpolation between consecutive construction types as listed above. Construction types are defined in the Appendix.

NOTE: THIS IS ONLY PRELIMINARY AND SUBJECT TO CHANGE BASED ON ARCHITECTURAL AND MECHANICAL DESIGN. THIS IS ONLY FOR AN ESTIMATE AS WE DO NOT CLAIM TO BE FIRE PROTECTION EXPERTS.

THEORETICAL WATER DEMAND CALCULATIONS

PROJECT: Agnes Street Subdivision
PROJECT No: 20-731
LOCATION: Caledon, ON
DATE: December 19, 2023

DESIGNED BY: Deven Verma, EIT.
REVIEWED BY: Khalid Mahmood, P. Eng

Manual Input
Automatic Output
Total Demand

Design Parameters

Residential		
Persons Per Unit (Townhouses):	3.328	(Region of Peel, Development Charges Background Study, December 2020)
Townhouse Units (ea.)	67	
Total Population	223	
Average Day Residential flow (L/cap/day):	270	(Region of Peel, Development Charges Background Study, December 2020)
Maximum Day Factor:	1.8	(Region of Peel, Development Charges Background Study, December 2020)
Peak Hour Factor:	3	(Region of Peel, Watermain Design Criteria, June 2010)
Fire Flow for Single detached dwelling: (L/min)	11000	Calculated (Fire underwriters survey, 2000)
Fire Flow for Single detached dwelling: (L/s)	183.33	

Total Water Demands (TWD):

Total Population	Average Daily Demand (ADD)		Max. Daily Demand (MDD)		Peak Hour Demand (PHD)		Fire Flow Demand (FFD)		MDD +FFD	Total Water Demand*	
#	(L/day)	(L/min)	(L/day)	(L/min)	(L/day)	(L/min)	(L/Min)	(L/s)	(L/min)	(L/min)	(L/s)
223	**60,210.00**	**41.81**	**108,378.00**	**75.26**	**180,630.00**	**125.44**	**11,000.00**	**183.33**	**11,075.26**	**11,075.26**	**184.59**

* Total water demand is the higher of MDD+Fire flow or Peak Hour Demand

APPENDIX C

Sanitary Design (By Others)

GUNNELL ENGINEERING LTD.
Municipal & Environmental Engineering

March 14, 2023
(Revised December 7, 2023)

Mr. Jeremy Grant
The Alton Development Inc.
1402 Queen Street
Caledon, Ontario
L7K 0C3

Re: Agnes Street Residential Development – Town of Caledon
Functional Servicing Report: Ontario Building Code Sewage Systems
Our File: D3082

Dear Mr. Grant,

The proposed residential development is to consist of 67 townhouse units, which are to be developed into fourteen (14) condominium blocks, with each condominium block under separate land ownership. Each condominium block will include for 4 or 5 townhouse units.

Municipal sanitary sewers are not available to service the proposed development, however municipal water is to be provided. Wastewater servicing for each residential block (4 or 5 townhouse units) will be serviced with an on-site sewage system. Each condominium Townhouse Block (Blocks 1 to 14) will each be serviced by one Ontario Building Code (OBC) compliant Class IV Tertiary Sewage Treatment System and a Type 'A' Dispersal Bed, with each of the 14 sewage systems having a daily design sewage flow of less than 10,000 L/day. Refer to attached Drawing SP-1 for the Townhouse Condominium Block layout and dispersal / septic bed locations. The permitting jurisdiction for these proposed Ontario Building Code (OBC) sewage systems will fall under the jurisdiction of the Town of Caledon Building Department (i.e. not the Ministry of the Environment, Conservation and Parks). In addition, and since the maximum number of residential units for each condominium block / land ownership is five, a Municipal Responsibility Assessment (MRA) in not required. We note that condominium townhouse blocks will be managed by the respective condominium association, to include for on-going service and maintenance, and funding for upgrades and component replacement within their designated reserve funds.

A septic test pit investigation was undertaken on August 11, 2022, with test pit locations shown on attached Drawing SP-1. The scope of the test pit investigation included identification of native soil type & percolation rate, as well as groundwater elevation observations in the area of each sewage system Type 'A' Dispersal Bed. The test pit results concluded that the native soils were coarse sand, with a percolation rate ranging between 6-10 mins/cm. Groundwater was not encountered in any test pit during the investigation. In addition, there was no soil staining that would be indicative of a seasonal high groundwater elevation. Preliminary design drawings have been prepared for the proposed on-site sewage treatment and effluent dispersal systems for the proposed Agnes Street residential development, Town of Caledon. Based on the soil percolation rates of the native soil, site topography and layout, and absence of groundwater, soil staining that would be indicative of a seasonal high groundwater elevation, in the septic test pits; Waterloo Biofilter tertiary treatment sewage systems, complete with Type 'A' Dispersal Beds, for each residential Condominium Block, has been proposed. There are 14 on-site sewage systems in total.

The configuration of the typical proposed sanitary servicing system is shown on the attached preliminary site plan Drawings, SP1-1, SP5-1 and SP9-1, as described below:

Design Sanitary Flows

The sewage treatment plant and effluent dispersal system servicing each of the 14 residential Blocks will have daily design flow sewage capacities ranging from 7,700 to of 9,900 L/day. Each Block includes 4 or 5 three (3)-bedroom townhouse units.

Individual townhouse daily design sewage flows for these 3-bedroom units are based on OBC Table 8.2.1.3.A. The size of the Type 'A' Dispersal Beds is based on OBC Section 8.7.7. Detailed calculations are illustrated on the preliminary sewage system layouts (Drawings SP1-1, SP5-1 and SP9-1), complete with our Ontario Building Code Compliance Analysis.

Proposed Sewage Treatment System

The proposed sewage treatment system for each residential townhouse condominium Block will include a Class IV tertiary treatment system (Waterloo Biofilter). The Waterloo Biofilter sewage treatment system meets Ontario Building Code Level IV (tertiary) quality effluent ($CBOD_5 \leq 10$ mg/L and TSS $\leq$ 10 mg/L), and is certified under the CAN/BNQ 3680-600 testing protocol per OBC Table 8.6.2.2. The Waterloo Biofilter sewage treatment system will each consist of a 22,500 L (5,000 gal) W.B. Anaerobic Digester with gravity flow to a 9,000 L Pump Station. Sewage effluent will be time dosed to a BT-22500 22,500 L (5,000 gal.) basket Biofilter tank. The Biofilter tank, c/w two (2) pumps; one pump to re-circulate to the W.B. Anaerobic Digester, the second pump to demand dose to the 18,000 L (4,000 gal.) WaterNox Tank (LS-18000), for nitrate treatment to 5 mg/L, as detailed in the Terraprobe hydro-geological report. Sewage from the WaterNox Tank will be demand dosed to the Type 'A' Dispersal Bed (timed dosed via the Pump Station).

The Waterloo Biofilter WaterNOx-LS Denitrification Unit underwent BNQ 3680-600 testing in 2016 for nitrogen removal. The test results are attached to this report. During the CAN/BNQ 3680-600 protocol Period A (based on NSF-40), the total nitrogen removal of the system was 92% with an average effluent concentration of 4.8 mg/L (TKN was 4.6 mg/L and NO3-N + NO2-N was 0.20 mg/L). During the CAN/BNQ 3680-600 protocol Period B (strenuous working parent schedule), the total nitrogen removal of the system was 80% with an average effluent concentration of 11.9 mg/L (TKN was 8.5 mg/L and NO3-N + NO2-N was 3.38 mg/L). The testing results indicated that the WaterNOx-LS system can successfully remove very high levels of total nitrogen passively, while buffering pH to neutral and keeping $CBOD_5$ and TSS levels below 10 mg/L.

Effluent Dispersal Systems

Treated effluent from the sewage treatment plant, servicing each townhouse Block, will be discharged to a Type 'A' Dispersal Bed, with a daily design sewage flow ranging from 7,700 to 9,900 L/day. Preliminary design calculations for the effluent dispersal systems are outlined on the sewage system design details on attached site plan drawings (i.e. typical sewage system preliminary layouts for Townshouse Blocks 1, 5, and 9). Specified OBC clearance distances for

the Type 'A' dispersal bed stone layers are shown on the attached drawings. The native sand soils were assessed with a soil percolation rate of T = 6 – 10 min/cm.

Summary

In summary, the property is able to accommodate the proposed domestic sewage treatment and on-site disposal from the proposed residential townhouse development, with the detailed 14 sewage treatment / dispersal bed systems. The sewage systems will be designed in accordance with the Ontario Building Code (OBC), to treat the effluent from the proposed residential development, for each of the 14 townhouse condominium block sewage systems.

We trust that the above description of the on-site sewage systems meets your requirements. Please do not hesitate to contact us if you have any questions.

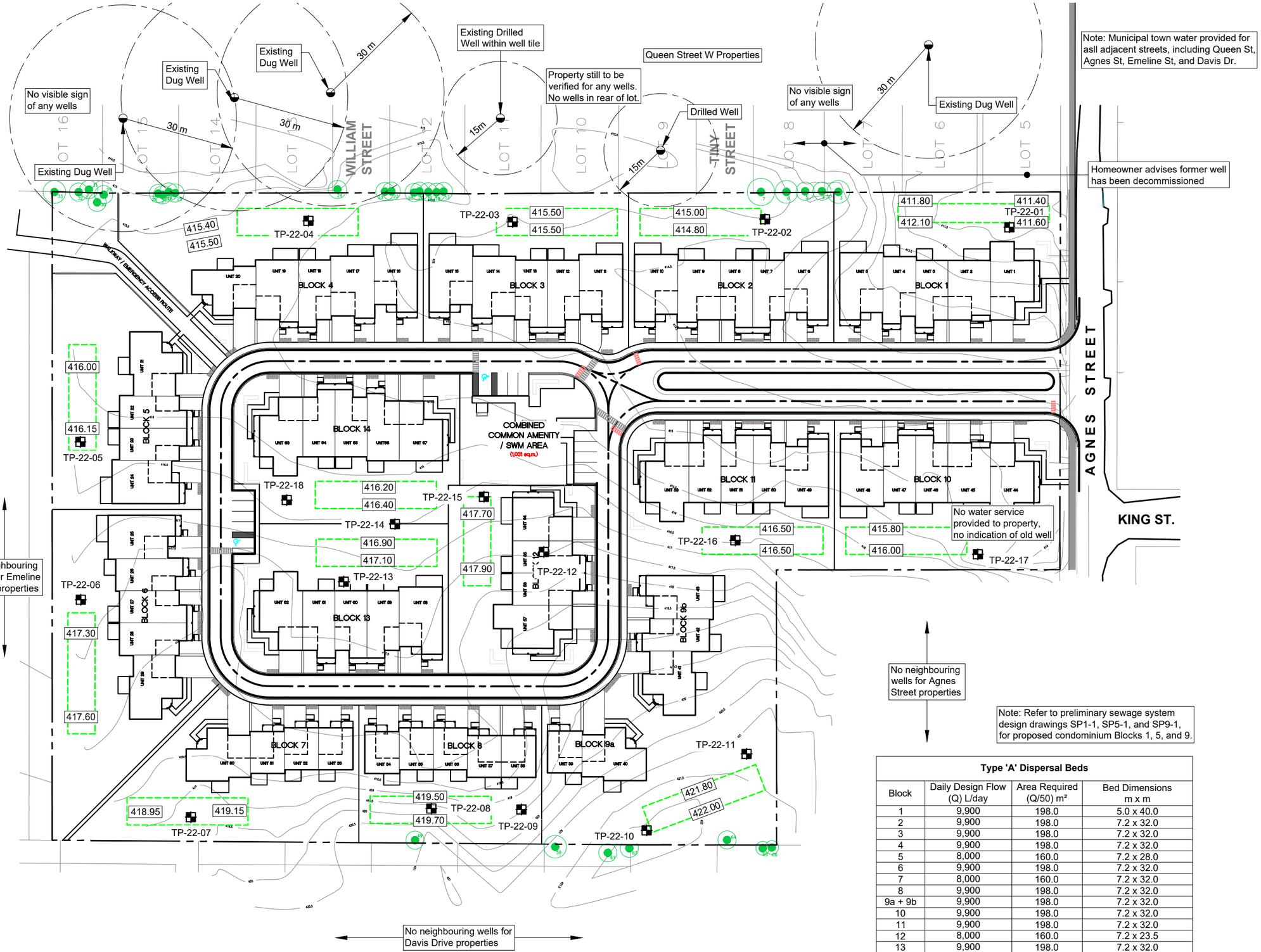
Yours truly,
GUNNELL ENGINEERING LTD.

Teika Zilans
Environmental Technician

Eric Gunnell, P.Eng

Attachments:

- Gunnell Engineering Ltd Preliminary. Drawings SP-1, SP1-1, SP5-1, SP9-1, DT-1, DT-2 and DT-3
- Waterloo Biofilter WaterNOx-LS Third Party Testing Summary



Note: Refer to preliminary sewage system design drawings SP1-1, SP5-1, and SP9-1, for proposed condominium Blocks 1, 5, and 9.

Type 'A' Dispersal Beds

Block	Daily Design Flow (Q) L/day	Area Required (Q/50) m²	Bed Dimensions m x m
1	9,900	198.0	5.0 x 40.0
2	9,900	198.0	7.2 x 32.0
3	9,900	198.0	7.2 x 32.0
4	9,900	198.0	7.2 x 32.0
5	8,000	160.0	7.2 x 28.0
6	9,900	198.0	7.2 x 32.0
7	8,000	160.0	7.2 x 32.0
8	9,900	198.0	7.2 x 32.0
9a + 9b	9,900	198.0	7.2 x 32.0
10	9,900	198.0	7.2 x 32.0
11	9,900	198.0	7.2 x 32.0
12	8,000	160.0	7.2 x 23.5
13	9,900	198.0	7.2 x 32.0
14	9,900	198.0	7.2 x 32.0

Gunnell Engineering Ltd.
1110 Stellar Drive, Unit 106
Newmarket, ON L3Y 7B7
bus: 905-868-9400
fax: 905-853-5734
www.septicdesign.ca

LEGEND

- Existing Known Wells
- Test Pit Locations
- Type 'A' Dispersal Beds (14)

Preliminary

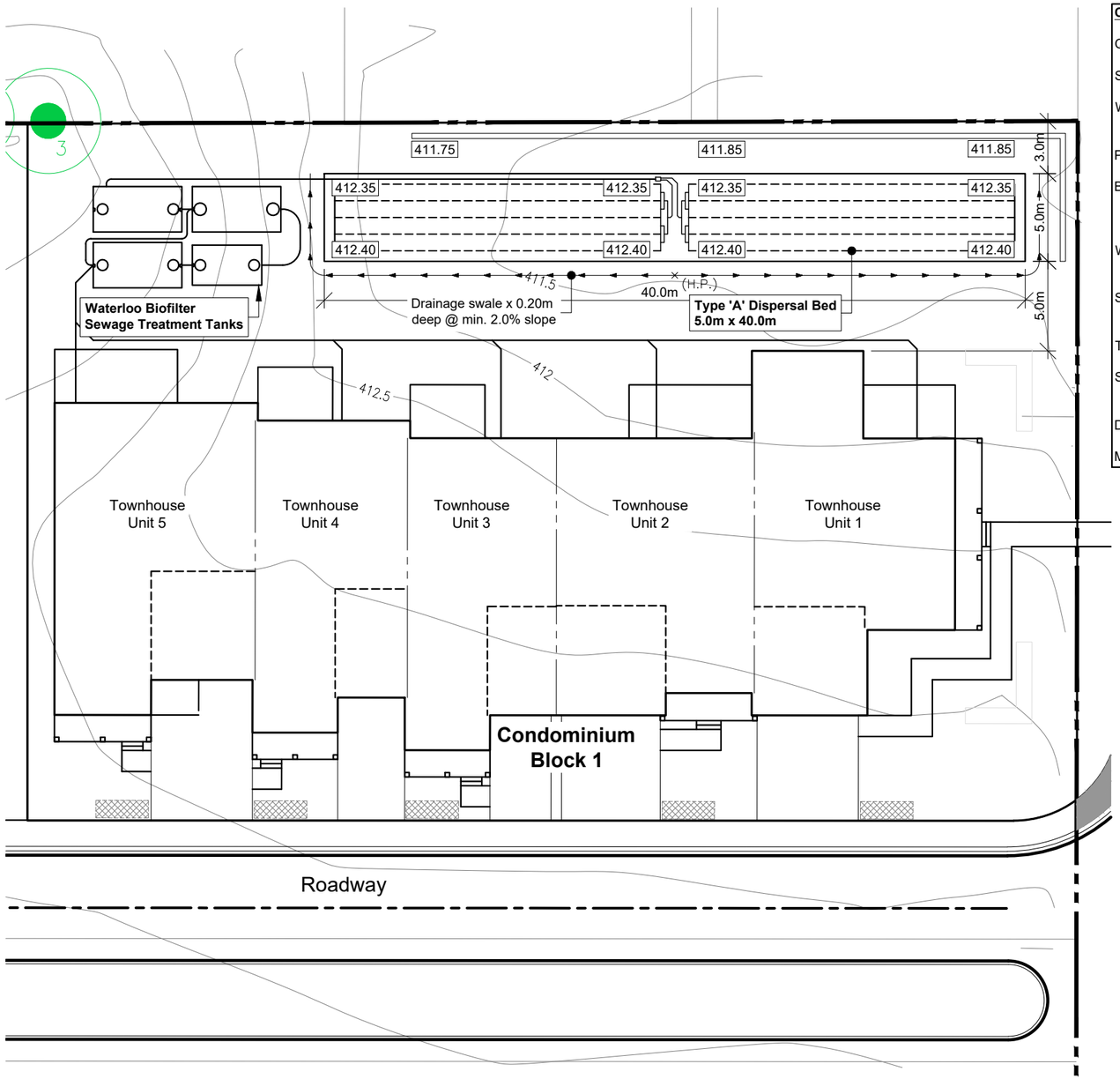
Rev. No.	Date	Description	CAD
Rev. 1	25-Jul-2022	Updated Well Locations	KD
Rev. 2	7-Mar-2023	Updated Site Plan	JK
Rev. 3	28-NOV-2023	Town Comments	JK

Agnes Street Townhouse Residential Development Town of Caledon

Overall Site Plan: Neighbouring Well Locations Test Pit Locations Septic Field Locations

Scale: 1:1,000	Designed By: EG
Date: 21-JUL-2022	Drawn By: JK
Project No.: D3082	Checked By: EG
	Drawing No.: SP-1

File: \\Gunnell\NAP\Shared\Gunnell Engineering AutoCAD\D3000 - PROJECTS\D3082 - Alton Residential Infill\CAD\-BC- Updated Site Plan\D3082BC-SP1.dwg
Plotted On: Thu, 30 Nov 2023 - 4:26pm



Class IV Tertiary Treatment System: Waterloo Biofilter - Preliminary Design: Block 1

Q = 9,900 L/day (Five 3-bedroom, 3-bathroom Townhouses, each at 1,980 L/day)

Sewage Treatment: CBOD5 ≤ 10 mg/L, TSS ≤ 10 mg/L, Nitrates ≤ 5 mg/L

W.B. Anaerobic Digester: 1.89 x daily flow = 1.89 x Q = 1.89 x 9,900 L = 18,711 L
Provide Waterloo Biofilter Anaerobic Digester: 22,500 L (5,000 gal.) with gravity flow to Pump Station.

Pump Station: Provide 9,000 L (PT-9000) pump tank to time dose to BT-22500 Biofilter Tank.

Biofilter Tank: Provide 22,500 L (5,000 gal.) BT22500 Basket Biofilter tank, provided by Waterloo Biofilter. Biofilter Tank to have two pumps; one pump to re-circulate to W.B. Anaerobic Digester, second pump to demand dose to WaterNox Tank (advanced nitrate treatment).

WaterNox-LS Tank: Provide 18,000 L (4,000 gal.) LS-18000 Tank (to Waterloo Biofilter Specifications), to dose on a demand basis to Type 'A' Dispersal bed.

Soil Percolation: T = 6 min/cm. Test Pit Investigation Undertaken on August 11, 2022 by Gunnell Engineering identified Sand Soils.

Type 'A' Dispersal Bed (Based on Q = 9,900 L/day & T = 6 min/cm)

Stone Layer: Maximum loading = 50 L/sm/day (i.e.: Q ≥ 3,000 L/day); 9,900 / 50 = 198.0 sm.
Provide Stone Layer Area = 200.0 sm. (5.0m x 40.0m)

Dispersal Bed Area: QT/850: 9,900 x 6 / 850 = 69.8m^2. Provide Dispersal Bed Area: 5.0m x 40.0m = 200 m^2

Mantle - N/A (i.e. T < 15 min/cm).

Stone Layer (c/w distribution piping) is to be a minimum of:
- 15.0m from drilled wells
- 30.0m from dug wells
- 3.0m from property lines
- 5.0m from townhouses

Note: Type 'A' Dispersal Bed is not raised above finished grade, therefore no increase to setbacks to stone layer.

Sewage System / Adjacent Grading Design Criteria:

1. 4:1 max. down slopes away from septic field.
2. No slopes directly down to septic fields (direct surface water around field with swales).
3. Swales are to be min. 0.15m deep with max. 4:1 side slopes adjacent to septic fields.
4. Septic fields are to be min. 3.0m from property lines and 5.0m from residences and installed at existing grades.
5. Septic tanks are to be min. 3.0m from property lines and 1.5m from residences.
6. No retaining walls constructed adjacent to septic fields.

Gunnell Engineering Ltd.
1110 Stellar Drive, Unit 106
Newmarket, ON L3Y 7B7
bus: 905-868-9400
fax: 905-853-5734
www.septicdesign.ca

LEGEND

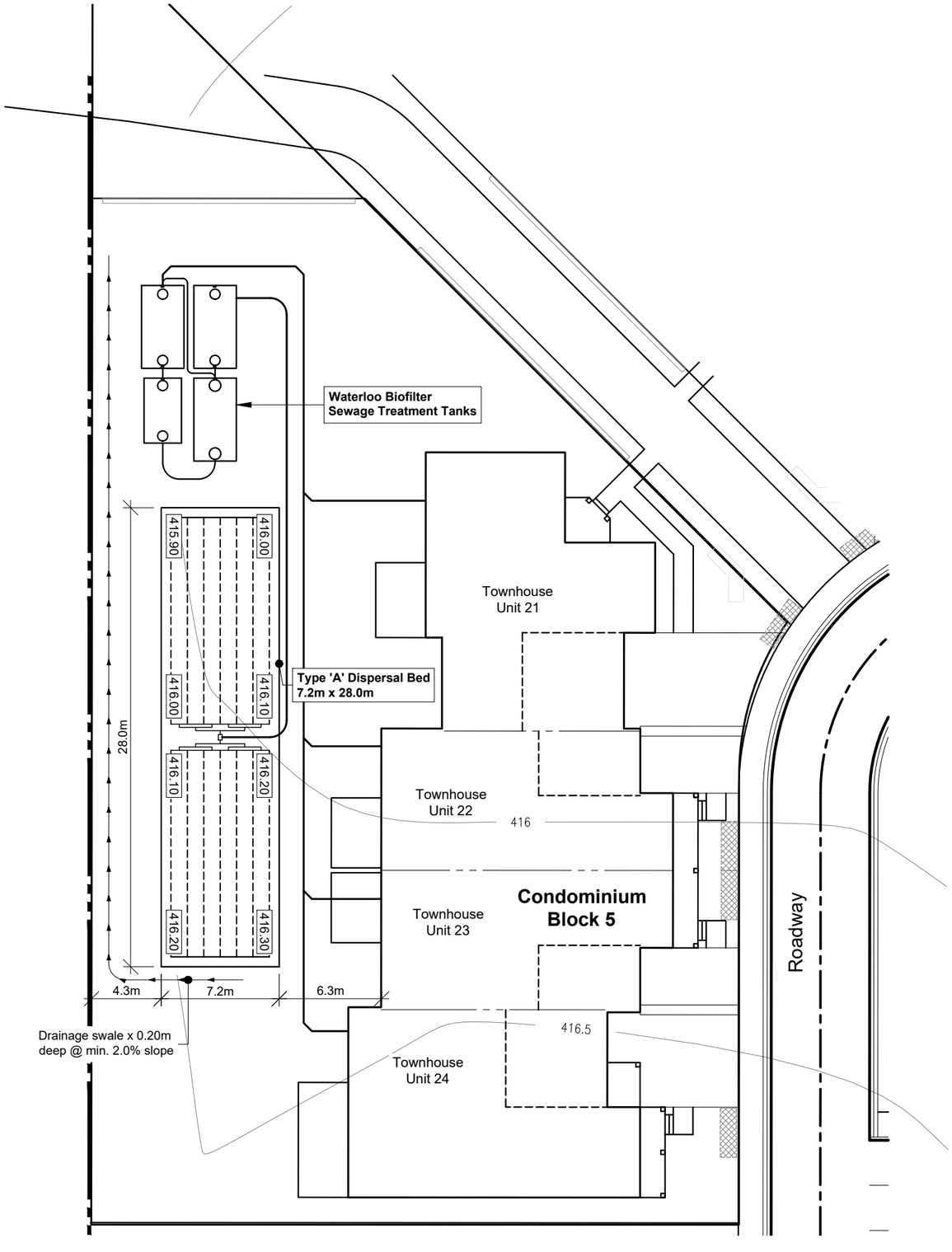
Preliminary

Agnes Street Townhouse Residential Development Town of Caledon

Typical Sewage System Layout: Block 1

Scale: 1:300	Designed By: EG
Date: 7-Mar-2023	Drawn By: JK
Project No.: D3082	Checked By: EG
	Drawing No.: SP1-1

File: \\GunnellQNAP\Shared\Gunnell Engineering AutoCAD\D3000 - PROJECTS\D3082 - Alton Residential Infill\CAD\-BC- Updated Site Plan\D3082BC-SP1-1.dwg
Plotted On: Thu, 30 Nov 2023 - 4:26pm



Class IV Tertiary Treatment System: Waterloo Biofilter - Preliminary Design: Block 5

Q = 8,000 L/day (Four 3-bedroom, 3-bathroom Townhouses, each at 2,000 L/day)

Sewage Treatment: CBOD5 ≤ 10 mg/L, TSS ≤ 10 mg/L, Nitrates ≤ 5 mg/L

W.B. Anaerobic Digester: 1.89 x daily flow = 1.89 x Q = 1.89 x 8,000 L = 15,120 L
Provide Waterloo Biofilter Anaerobic Digester: 18,000 L (4,000 gal.) with gravity flow to Pump Station.

Pump Station: Provide 6,800 L (PT-6800) pump tank to time dose to BT-18000 Biofilter Tank.

Biofilter Tank: Provide 18,000 L (4,000 gal.) BT-18000 Basket Biofilter tank, provided by Waterloo Biofilter. Biofilter Tank to have two pumps; one pump to re-circulate to W.B. Anaerobic Digester, second pump to demand dose to WaterNox Tank (advanced nitrate treatment).

WaterNox-LS Tank: Provide 13,500 L (3,000 gal.) LS-13500 Tank (to Waterloo Biofilter Specifications), to dose on a demand basis to Type 'A' Dispersal bed.

Soil Percolation: T = 6 min/cm. Test Pit Investigation Undertaken on August 11, 2022 by Gunnell Engineering identified Sand Soils.

Type 'A' Dispersal Bed (Based on Q = 8,000 L/day & T = 6 min/cm)

Stone Layer: Maximum loading = 50 L/sm/day (i.e.: Q ≥ 3,000 L/day); 8,000 / 50 = 160.0 sm.
Provide Stone Layer Area = 201.6 sm. (7.2m x 28.0m)

Dispersal Bed Area: QT/850: 8,000 x 6 / 850 = 56.5m^2. Provide Dispersal Bed Area: 7.2m x 28.0m = 201.6 m^2

Mantle - N/A (i.e. T < 15 min/cm).

Stone Layer (c/w distribution piping) is to be a minimum of:
- 15.0m from drilled wells
- 30.0m from dug wells
- 3.0m from property lines
- 5.0m from townhouses

Note: Type 'A' Dispersal Bed is not raised above finished grade, therefore no increase to setbacks to stone layer.

Sewage System / Adjacent Grading Design Criteria:

1. 4:1 max. down slopes away from septic field.
2. No slopes directly down to septic fields (direct surface water around field with swales).
3. Swales are to be min. 0.15m deep with max. 4:1 side slopes adjacent to septic fields.
4. Septic fields are to be min. 3.0m from property lines and 5.0m from residences and installed at existing grades.
5. Septic tanks are to be min. 3.0m from property lines and 1.5m from residences.
6. No retaining walls constructed adjacent to septic fields.

Gunnell Engineering Ltd.
1110 Stellar Drive, Unit 106
Newmarket, ON L3Y 7B7
bus: 905-868-9400
fax: 905-853-5734
www.septicdesign.ca

LEGEND

Preliminary

Rev. No.	Date	Description	CAD
Rev. 1	28-NOV-2023	Town Comments	JK

Agnes Street Townhouse Residential Development Town of Caledon

Typical Sewage System Layout: Block 5

Scale: 1:300	Designed By: EG
Date: 7-Mar-2023	Drawn By: JK
Project No.: D3082	Checked By: EG
	Drawing No.: SP5-1

Sewage System / Adjacent Grading Design Criteria:

1. 4:1 max. down slopes away from septic field.
2. No slopes directly down to septic fields (direct surface water around field with swales).
3. Swales are to be min. 0.15m deep with max. 4:1 side slopes adjacent to septic fields.
4. Septic fields are to be min. 3.0m from property lines and 5.0m from residences and installed at existing grades.
5. Septic tanks are to be min. 3.0m from property lines and 1.5m from residences.
6. No retaining walls constructed adjacent to septic fields.

Stone Layer (c/w distribution piping) is to be a minimum of:
- 15.0m from drilled wells
- 30.0m from dug wells
- 3.0m from property lines
- 5.0m from townhouses

Note: Type 'A' Dispersal Bed is not raised above finished grade, therefore no increase to setbacks to stone layer.

Class IV Tertiary Treatment System: Waterloo Biofilter - Preliminary Design: Block 9

Q = 9,900 L/day (Five 3-bedroom, 3-bathroom Townhouses, each at 1,980 L/day)

Sewage Treatment: CBOD5 ≤ 10 mg/L, TSS ≤ 10 mg/L, Nitrates ≤ 5 mg/L

W.B. Anaerobic Digester: 1.89 x daily flow = 1.89 x Q = 1.89 x 9,900 L = 18,711 L
Provide Waterloo Biofilter Anaerobic Digester: 22,500 L (5,000 gal.) with gravity flow to Pump Station.

Pump Station: Provide 9,000 L (PT-9000) pump tank to time dose to BT-22500 Biofilter Tank.

Biofilter Tank: Provide 22,500 L (5,000 gal.) BT22500 Basket Biofilter tank, provided by Waterloo Biofilter. Biofilter Tank to have two pumps; one pump to re-circulate to W.B. Anaerobic Digester, second pump to demand dose to WaterNox Tank (advanced nitrate treatment tank).

WaterNox-LS Tank: Provide 18,000 L (4,000 gal.) LS-18000 Tank (to Waterloo Biofilter Specifications), to dose on a demand basis to Type 'A' Dispersal bed.

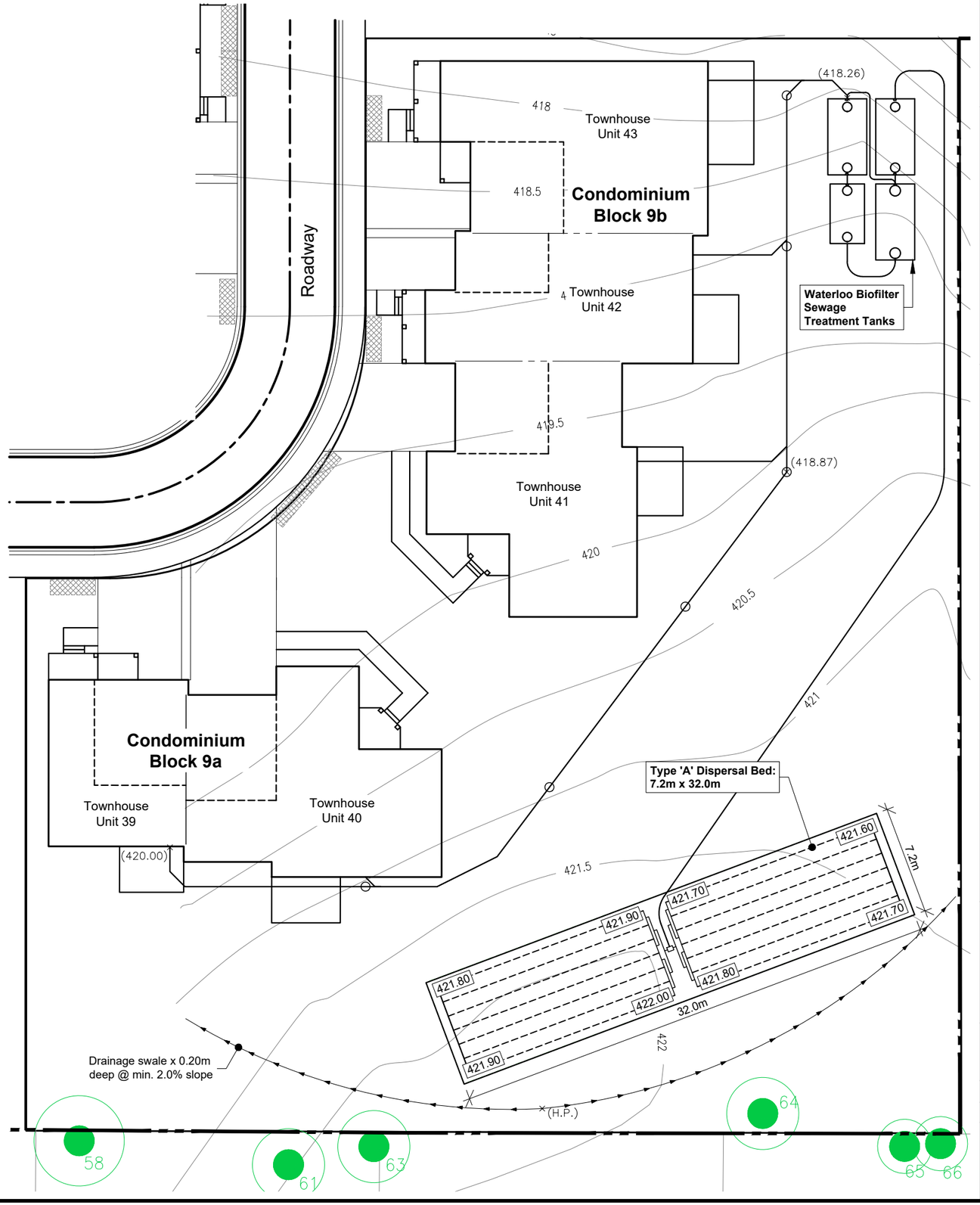
Soil Percolation: T = 8 min/cm. Test Pit Investigation Undertaken on August 11, 2022 by Gunnell Engineering identified Sand Soils.

Type 'A' Dispersal Bed (Based on Q = 9,900 L/day & T = 8 min/cm)

Stone Layer: Maximum loading = 50 L/sm/day (i.e.: Q ≥ 3,000 L/day); 9,900 / 50 = 198.0 sm.
Provide Stone Layer Area = 200.0 sm. (5.0m x 40.0m)

Dispersal Bed Area: QT/850: 9,900 x 8 / 850 = 93.2m^2. Provide Dispersal Bed Area: 7.2m x 32.0m = 230.4 m^2

Mantle - N/A (i.e. T < 15 min/cm).



Gunnell Engineering Ltd.
1110 Stellar Drive, Unit 106
Newmarket, ON L3Y 7B7
bus: 905-868-9400
fax: 905-853-5734
www.septicdesign.ca

LEGEND

Preliminary

Rev. No.	Date	Description	CAD
Rev. 1	28-NOV-2023	Town Comments	JK

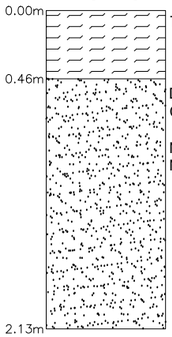
Agnes Street Townhouse Residential Development Town of Caledon

Typical Sewage System Layout: Block 9

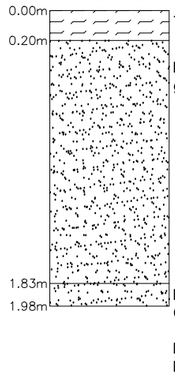
Scale: 1:300	Designed By: EG
Date: 7-Mar-2023	Drawn By: JK
Project No.: D3082	Checked By: EG
	Drawing No.: SP9-1

Gunnell Engineering Ltd.
1110 Stellar Drive, Unit 106
Newmarket, ON L3Y 7B7
bus: 905-868-9400
fax: 905-853-5734
www.septicdesign.ca

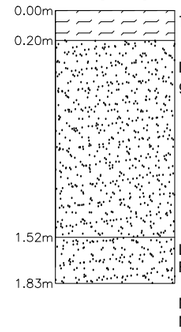
Test Pit
TP[22-01]



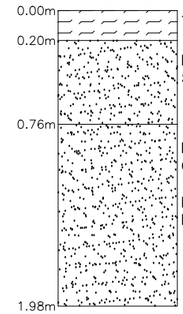
Test Pit
TP[22-02]



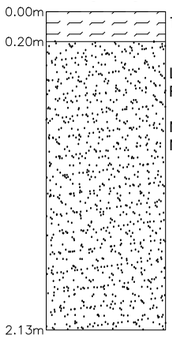
Test Pit
TP[22-03]



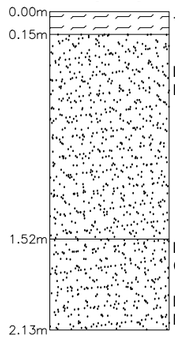
Test Pit
TP[22-04]



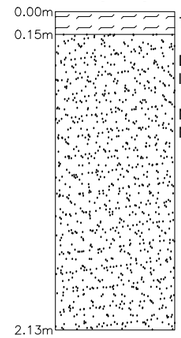
Test Pit
TP[22-05]



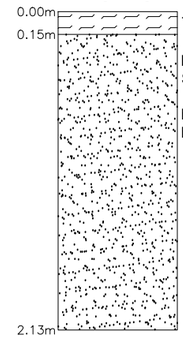
Test Pit
TP[22-06]



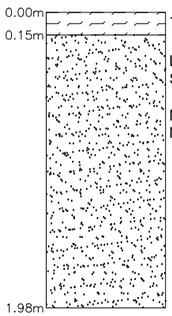
Test Pit
TP[22-07]



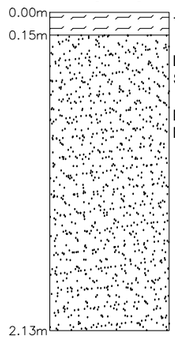
Test Pit
TP[22-08]



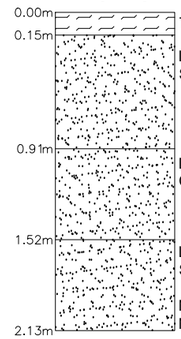
Test Pit
TP[22-09]



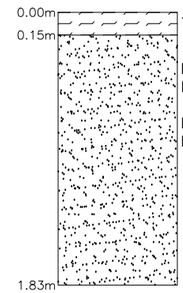
Test Pit
TP[22-10]



Test Pit
TP[22-11]



Test Pit
TP[22-12]



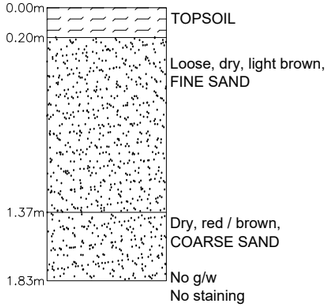
Alton Residential Infill
Agnes Street
Town of Caledon

Test Pit Soil Profiles

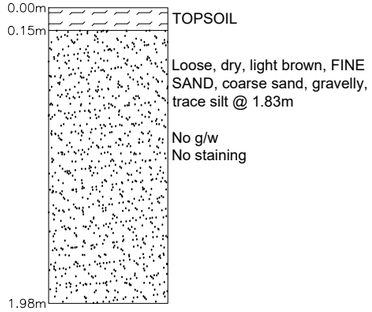
Scale: N.T.S.	Designed By: KD
Date: 19-AUG-2022	Drawn By: KD
Project No.: **D3082**	Checked By: EG
	Drawing No.: **DT-1**

Gunnell Engineering Ltd.
1110 Stellar Drive, Unit 106
Newmarket, ON L3Y 7B7
bus: 905-868-9400
fax: 905-853-5734
www.septicdesign.ca

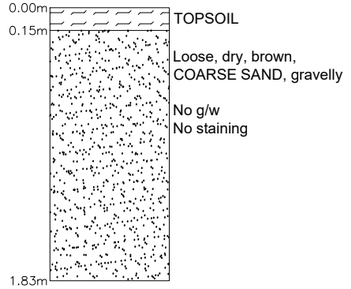
Test Pit
TP[22-13]



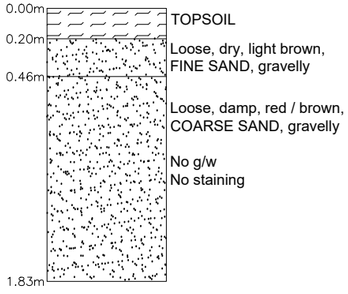
Test Pit
TP[22-14]



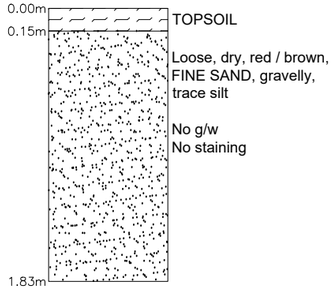
Test Pit
TP[22-15]



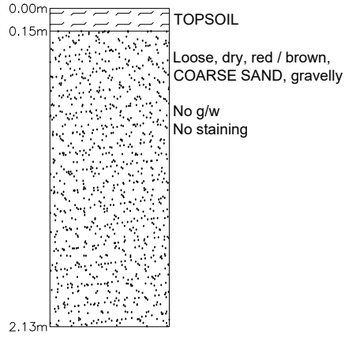
Test Pit
TP[22-16]



Test Pit
TP[22-17]



Test Pit
TP[22-18]



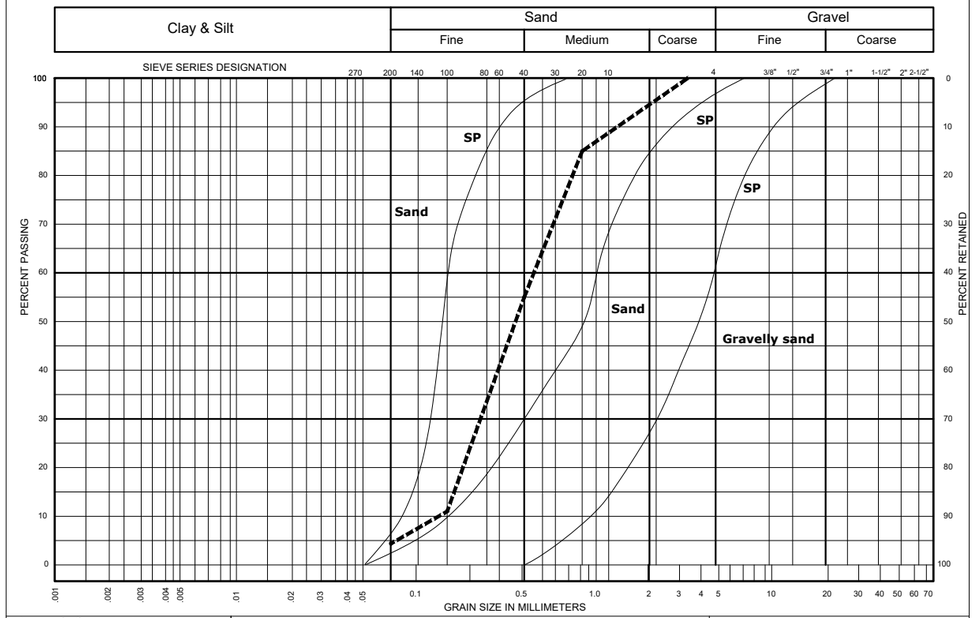
Alton Residential Infill
Agnes Street
Town of Caledon

Test Pit Soil Profiles

Scale: N.T.S.	Designed By: KD
Date: 19-AUG-2022	Drawn By: KD
Project No.: D3082	Checked By: EG
	Drawing No.: DT-2

File: \\GunnellQNAP\Shared\Gunnell Engineering AutoCAD\D3000 - PROJECTS\D3082 - Alton Residential Infill\CAD\-BC- Updated Site Plan\D3082BC-DT2.dwg
Plotted On: Thu, 30 Nov 2023 - 4:26pm

UNIFIED SOIL CLASSIFICATION SYSTEM



Prepared for Gunnell Engineering Ltd.

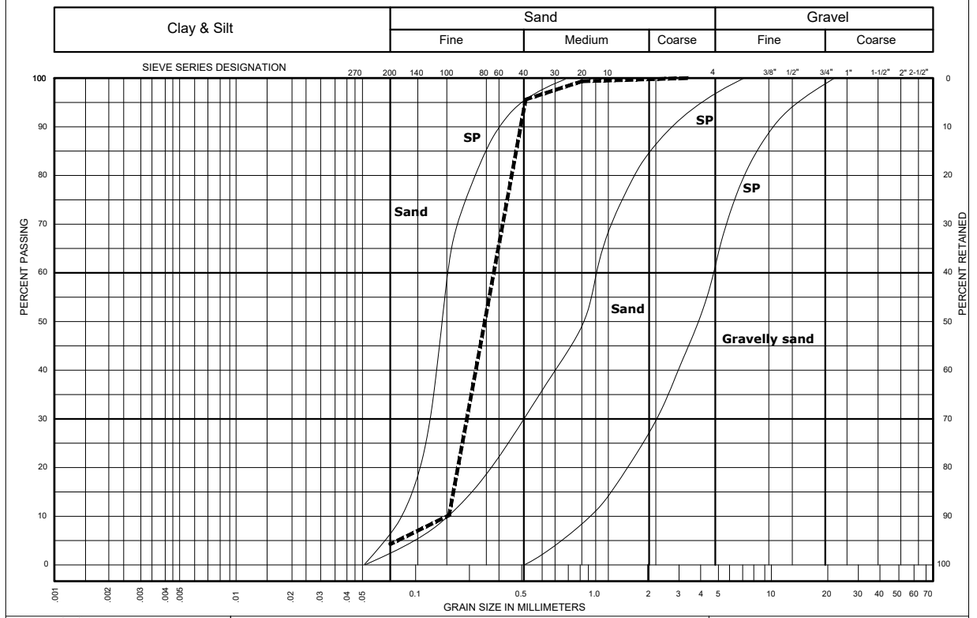
Project: D3082
Sample: TP22-1
Depth: 2.13m
Date Sampled: Aug 11, 2022

USCS
Coarse Grained Soils
Poorly-graded sands (SP)

Poorly-graded sands & gravelly-sands
Little or no fines (< 5% passing
No. 200 sieve (0.074mm)

Percolation Time
: T = 6 mins/cm

UNIFIED SOIL CLASSIFICATION SYSTEM



Prepared for Gunnell Engineering Ltd.

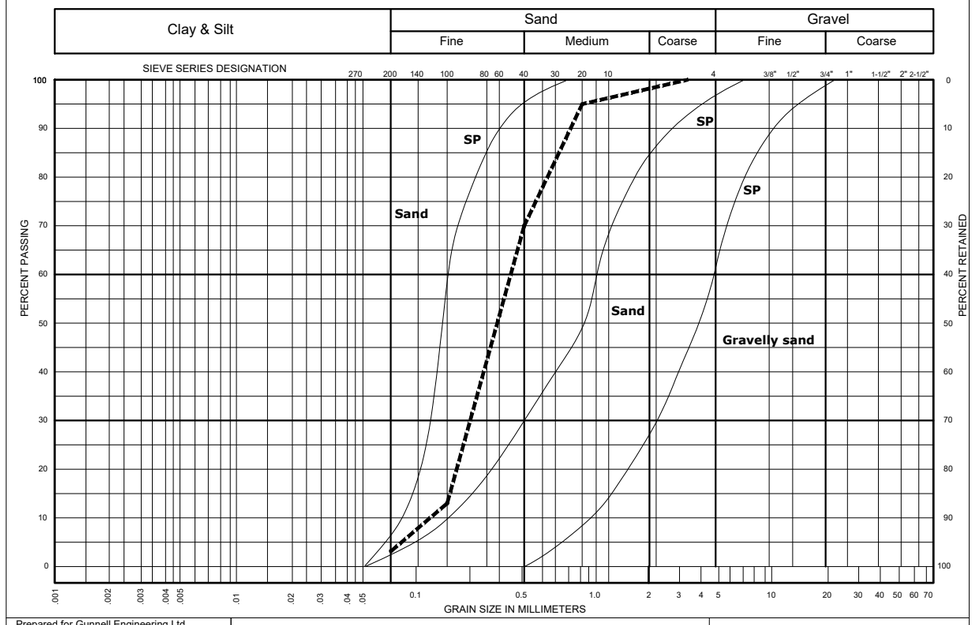
Project: D3082
Sample: TP22-7
Depth: 2.13m
Date Sampled: Aug 11, 2022

USCS
Coarse Grained Soils
Poorly-graded sands (SP)

Poorly-graded sands & gravelly-sands
Little or no fines (< 5% passing
No. 200 sieve (0.074mm)

Percolation Time
: T = 8 mins/cm

UNIFIED SOIL CLASSIFICATION SYSTEM



Prepared for Gunnell Engineering Ltd.

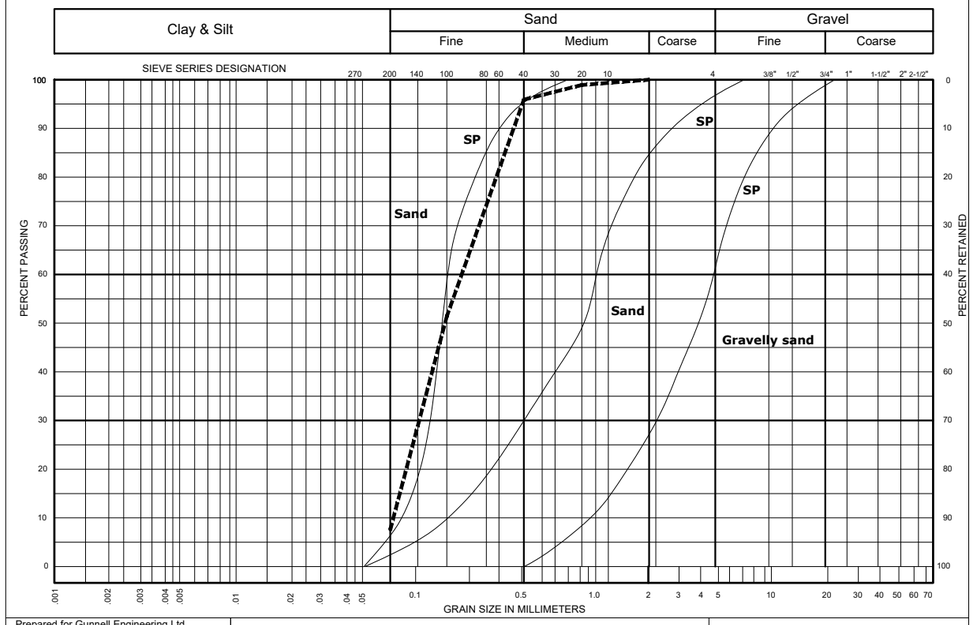
Project: D3082
Sample: TP22-13
Depth: 1.83m
Date Sampled: Aug 11, 2022

USCS
Coarse Grained Soils
Poorly-graded sands (SP)

Poorly-graded sands & gravelly-sands
Little or no fines (< 5% passing
No. 200 sieve (0.074mm)

Percolation Time
: T = 6 mins/cm

UNIFIED SOIL CLASSIFICATION SYSTEM



Prepared for Gunnell Engineering Ltd.

Project: D3082
Sample: TP22-4
Depth: 1.98m
Date Sampled: Aug 11, 2022

USCS
Coarse Grained Soils
Poorly-graded sands (SP)

Poorly-graded sands & gravelly-sands
Little or no fines (< 5% passing
No. 200 sieve (0.074mm)

Percolation Time
: T = 10 mins/cm

Gunnell Engineering Ltd.
1110 Stellar Drive, Unit 106
Newmarket, ON L3Y 7B7
bus: 905-868-9400
www.septicdesign.ca

Alton Residential Infill
Agnes Street
Town of Caledon

Soil Laboratory Analysis

Scale: N.T.S.	Designed By: --
Date: 7-MAR-2023	Drawn By: JK
Project No.: D3082	Checked By: --
	Drawing No.: DT-3

WaterNOx-LS Third Party Testing Summary

In the fall of 2016, Waterloo Biofilter Systems Inc. installed their WaterNOx-LS™ denitrification unit at the Bureau de Normalisation du Quebec (BNQ) test site located in Quebec City. The system underwent BNQ 3680-600 test protocol which includes two parts - Period A and Period B. Period A is based on the methodology of NSF/ANSI Standards 40 and 245, containing the same flow patterns and stress tests. Period B provides for a further 6 months of seasonal reliability testing to ensure that the test includes cold weather results.

The WaterNOx-LS is a passive autotrophic denitrification process using sulphur-limestone minerals in a submerged, up-flow configuration. The WaterNOx-LS, which was sized for 1,600 L/day (350 gpd) followed a Waterloo Biofilter nitrifying treatment unit.

Period A Test Results

During Period A wastewater is dosed according to the hydraulic loading specified in NSF-40. Period A includes the wash-day, working-parent, power failure, and vacation period stress tests. All sample results taken during stress tests are included in the analysis. Influent wastewater temperature values ranged from 10.0 °C (50 °F) to 16.5 °C (62 °F) with an average value of 13.3 °C (56 °F). Influent pH averaged 7.9 and effluent pH averaged 7.2.

Table 1 – Period A Results for the WaterNOx-LS

Parameters	Influent	Effluent	Removal
(c)BOD_5	260	6	97.6%
TSS	312	3	99.2%
Fecal Coliforms	2,403,000	4,900	99.8%
$NO_{2,3}$	0.08	0.20	
TKN	57.1	4.6	92.0%
TN	57.1	4.8	91.6%

n = 123; n = 357 for fecals

All parameters in mg/L except Fecal Coliforms in cfu/100mL

All values arithmetic averages except Fecal Coliforms in geometric average

Weekly influent total nitrogen concentrations ranged from 43.0 mg/L to 68.8 mg/L with a six-month average concentration of 57.1 mg/L.

Weekly effluent $NO_{2,3}$ concentrations ranged from < 0.02 mg/L to 3.33 mg/L with a six-month average of 0.20 mg/L. Weekly effluent TKN concentrations ranged from 1.5 mg/L to 16.9 mg/L with a six-month average of 4.6 mg/L. Weekly effluent total nitrogen concentrations ranged from 1.7 mg/L to 17.1 mg/L with a six-month average of 4.8 mg/L. The total nitrogen reduction over the six-month period was 91.6%.

65 Massey Road, Suite C, Guelph ON N1H 7M6 T: 519 856-0757 1-866-366-4329 F: 519 856-0759 www.waterloo-biofilter.com

Period B Test Results

Weekday hydraulic loading is modified during Period B to a strenuous 'working parent' schedule where 40% of the flow is delivered over three hours in the morning, and 60% is delivered over three hours in the evening. All samples taken during Period B are included in the analysis. Influent wastewater temperature values ranged from 10.1 °C (50 °F) to 15.8 °C (60 °F) with an average value of 12.3 °C (54 °F). Influent pH averaged 8.0 and effluent pH averaged 7.1.

Table 2 – Period B Results for the WaterNOx-LS

Parameters	Influent	Effluent	Removal
(c)BOD_5	248	4	98.2%
TSS	304	3	99.1%
Fecal Coliforms	2,142,000	2,800	99.9%
$NO_{2,3}$	0.17	3.38	
TKN	60.3	8.5	85.9%
TN	60.4	11.9	80.3%

n = 59 except Fecal Coliforms n = 118

All parameters in mg/L except Fecal Coliforms in cfu/100mL

All values arithmetic averages except Fecal Coliforms in geometric average

Weekly influent total nitrogen concentrations ranged from 21.2 mg/L to 85.6 mg/L with a six-month average concentration of 60.4 mg/L.

Weekly effluent $NO_{2,3}$ concentrations ranged from < 0.04 mg/L to 15.2 mg/L with a six-month average of 3.38 mg/L. Weekly effluent TKN concentrations ranged from 1.2 mg/L to 21.2 mg/L with a weekly average of 8.5 mg/L. Weekly effluent total nitrogen concentrations ranged from 3.7 mg/L to 22.2 mg/L with a six-month average of 11.9 mg/L. The total nitrogen reduction over the six-month period was 80.3%.

Conclusion

In summary, the WaterNOx-LS system can successfully remove very high levels of total nitrogen passively, while buffering pH to neutral and keeping $cBOD_5$ and TSS levels below 10 mg/L.

65 Massey Road, Suite C, Guelph ON N1H 7M6 T: 519 856-0757 1-866-366-4329 F: 519 856-0759 www.waterloo-biofilter.com

APPENDIX D

Stormwater Management Calculations

Site Characteristics
Site: Agnes Street Infill Subdivision, Alton, Ontario
December 20, 2023

Pre-Development

Land-Use	Impervious Ratio	Area 101 (m^2)	Area 102 (m^2)	Total (m^2)	Coverage
Driveway & Hardscape	1.00	2,091.3	0.0	2,091.3	5%
Grassed Area	0.00	33,202.8	5,179.3	38,382.0	95%
Total		35,294.1	5,179.3	40,473.3	100%
	% Impervious =	5.9%	0.0%	5.2%	
	Runoff Coefficient* =	0.29	0.25	0.28	

*Pervious areas were assigned a runoff coefficient of 0.25 and impervious areas were assigned a runoff coefficient of 0.90

Post-Development

Land-Use	Impervious Ratio	Area 201 (m^2)	Area 202 (m^2)	Total (m^2)	Coverage
Asphalt	1.00	3,094.8	1,035.1	4,129.9	10%
Permeable Pavers	0.50	2,098.5	438.3	2,536.9	6%
Hardscape	1.00	1,483.8	1,370.7	2,854.5	7%
Roof	1.00	6,662.2	4,608.9	11,271.0	28%
Landscaped Area	0.00	10,089.0	9,592.1	19,681.1	49%
Total		23,428.3	17,045.1	40,473.3	100%
	% Impervious =	52.5%	42.4%	48.2%	
	Runoff Coefficient* =	0.59	0.53	0.56	

*Pervious areas were assigned a runoff coefficient of 0.25 and impervious areas were assigned a runoff coefficient of 0.90

Peak Runoff Assessment
Site: Agnes Street Infill Subdivision, Alton, Ontario
December 20, 2023

The subject property is part of the Shaw's Creek subwatershed in the CVC's jurisdiction which requires post-development flows to be controlled to pre-development levels for the 2-100year storm events.

Peak Runoff Assessment

Town of Caledon Intensity-Duration Frequency Curves (from Development Standards Manual 2019)

Return Period	A	B	C
2	1,070	0.8759	7.85
5	1,593	0.8789	11
10	2,221	0.908	12
25	3,158	0.9335	15
50	3,886	0.9495	16
100	4,688	0.9624	17

$$I = \frac{A}{(t + C)^B}$$

a, b, c = IDF Parameters
I = Intensity (mm/h)
t = Storm Duration, 10 minutes minimum (min)

Time of Concentration

Airport
If Runoff Coefficient < 0.4

$$T_c = \frac{3.26\,(1.1 - C)\,L^{0.5}}{S_w^{0.33}}$$

where, L = Flow length (m)
Sw = slope (%)
C = Runoff Coefficient

Bransby
If Runoff Coefficient > 0.4

$$T_c = \frac{0.057\,L}{S_w^{0.2}\,A^{0.1}}$$

where, L = Flow length (m)
Sw = slope (%)

Parameter	Existing 101	Existing 102	Proposed 201	Proposed 202
C	0.29	0.25	0.59	0.53
L	335.2	188.9	233.5	194
A	3.529	0.518	2.343	1.705
S_w	2.61	2.26	0.81	2.74
Method	Airport	Airport	Bransby	Bransby
T =	35	29	10	10

**10 minute time of concentration used for proposed catchments as a conservative measure*

Rational Method

Return Period	Existing 101		Existing 102		Proposed 201		Proposed 202		Total Runoff (L/s)
	Intensity (mm/hr)	Runoff (L/s)	Intensity (mm/hr)	Runoff (L/s)	Intensity (mm/hr)	Runoff (L/s)	Intensity (mm/hr)	Runoff (L/s)	
2	39.6	111.9	45.3	16.3	85.7	329.7	85.7	213.4	543.1
5	54.8	154.9	62.1	22.3	109.7	421.9	109.7	273.1	694.9
10	67.0	189.4	76.1	27.4	134.2	516.0	134.2	334.1	850.1
25*	81.5	253.6	92.1	36.4	156.5	662.0	156.5	428.6	1,090.6
50*	92.4	313.8	104.4	45.1	176.2	813.2	176.2	526.5	1,339.7
100*	104.0	367.9	117.4	52.8	196.5	944.9	196.5	611.7	1,556.6

*Incorporates Runoff coefficient adjustment factor of: 25 year = 1.1, 50 year = 1.2, 100 year = 1.25

Area 201 Chamber Storage Calculations (100 year post to 2 year pre)

The quantity storage chamber will provide quantity control for Area 201

100-Year Post Development Required Discharge = 64.8 L/s *Area 201 occupies 58% of the total site, required discharge is 58% of 2-year existing peak flow* for Area 101
Outlet Discharge= 64.3 L/s

Starting Time 60 min
Time Step 1 min
Area 201, A 2.34 ha
Runoff Coefficient 0.74 (including 1.25 Correction factor)

Time (min)	100 Year Intensity (mm/h)	Inflow (m^3/s)	Outflow (m^3/s)	Storage Required (m^3)
60	72	0.345	0.064	1009.1
61	71	0.340	0.064	1010.4
62	70	0.336	0.064	1011.5
63	69	0.332	0.064	1012.6
64	68	0.328	0.064	1013.5
65	67	0.324	0.064	1014.3
66	67	0.321	0.064	1015.0
67	66	0.317	0.064	1015.6
68	65	0.313	0.064	1016.1
69	64	0.310	0.064	1016.5
70	64	0.306	0.064	1016.8
71	63	0.303	0.064	1017.1
72	62	0.300	0.064	1017.3
73	62	0.297	0.064	1017.3
74	61	0.293	0.064	1017.3
75	60	0.290	0.064	1017.3
76	60	0.287	0.064	1017.1
77	59	0.284	0.064	1016.9
78	59	0.282	0.064	1016.6
79	58	0.279	0.064	1016.3
80	57	0.276	0.064	1015.9

Therefore the storage required to attenuate peak flows = **1017.3** m^3 *Active storage*

Quantity Control Orifice Sizing for Area 201

Orifice Equation: $Q = C\,A\,(2\,g\,h)^{0.5}$
Orifice Diameter = 130 mm
Orifice Invert = 413.93 m
HGL = 417.11 m *Assuming a maximum head is from the RIM of the control MH to the orifice invert.*
Orifice Coefficient, C = 0.62 *0.62 for plate, 0.83 for tube*
Orifice Area, A = 0.0133 m^2
g = 9.81 m/s^2
h = 3.12 m
Orifice Q = 0.064 m^3/s
Orifice Q = 64.33 L/s

Area 202 Chamber Storage Calculations (100 year post to 2 year pre)

The quantity storage chamber will provide quantity control for Area 202

100-Year Post Development Required Discharge = 47.1 L/s Area 202 occupies 42% of the total site, required discharge is 42% of 2-year existing peak flow of Area 101

Outlet Discharge= 43.1 L/s

Starting Time	60	min	Area 202, A	1.70	ha
Time Step	1	min	Runoff Coefficient	0.66	(including 1.25 Correction factor)

Time (min)	100 Year Intensity (mm/h)	Inflow (m^3/s)	Outflow (m^3/s)	Storage Required (m^3)
60	72	0.223	0.043	647.9
61	71	0.220	0.043	648.7
62	70	0.218	0.043	649.3
63	69	0.215	0.043	649.9
64	68	0.213	0.043	650.4
65	67	0.210	0.043	650.8
66	67	0.208	0.043	651.2
67	66	0.205	0.043	651.5
68	65	0.203	0.043	651.7
69	64	0.201	0.043	651.9
70	64	0.198	0.043	652.0
71	63	0.196	0.043	652.1
72	62	0.194	0.043	652.1
73	62	0.192	0.043	652.1
74	61	0.190	0.043	652.0
75	60	0.188	0.043	651.9
76	60	0.186	0.043	651.7
77	59	0.184	0.043	651.4
78	59	0.182	0.043	651.2
79	58	0.180	0.043	650.9
80	57	0.179	0.043	650.5

Therefore the storage required to attenuate peak flows = **652.1** m^3 Quantity Control storage

Quantity Control Orifice Sizing for Area 202

Orifice Equation:	$Q = C A (2 g h)^{0.5}$		
Orifice Diameter =	100	mm	
Orifice Invert =	409.29	m	
HGL =	413.34	m	*Assuming a maximum head is from the RIM of the control MH to the orifice invert.*
Orifice Coefficient, C =	0.62		*0.62 for plate, 0.83 for tube*
Orifice Area, A =	0.0079	m^2	
g =	9.81	m/s^2	
h =	4.00	m	
Orifice Q =	0.0431	m^3/s	
Orifice Q =	43.14	L/s	

Water Balance/Infiltration Targets
Site: Agnes Street Infill Subdivision, Alton, Ontario
December 20, 2023

Infiltration Target Volume

Controlled at-grade areas are to be directed to the subsurface infiltration facility which are sized to meet the water quality and balance targets.

Development Area (201+202)=	**40,473.3**	**m^2**
% Impervious =	**48%**	
Impervious Area =	**19,523.8**	**m^2**

Table 3.2 of the MECP Stormwater Management Planning and Design Manual will guide the required water quality volume. Subject property is required to provide an Enhanced Protection Level.

Impervious Level (%)	35	55	70	85
Storage Volume (m^3/ha)	25	30	35	40

Required Unitary Quality Volume =	28.6	m^3/ha
Required Quality Volume =	115.7	m^3

As per the Town of Caledon Design Standards Manual 2019, the infiltration chamber should be sized to infiltrate the 5 mm event for water balance over impervious surfaces as pervious surfaces have an initial abstraction of 5mm.

Rainfall Depth =	5	mm
Required Infiltration Volume =	97.6	m^3

Therefore the infiltration gallery will be designed to infiltrate 115.7 m3. This will be the minimum void volume in the base stone.

Infiltration Facility Drawdown

Req. Water Balance Volume (5mm Event)	97.6	m^3
Req. Water Quality Volume:	115.7	m^3
Target volume is the greater of water balance and quality, V =	**115.7**	m^3

Maximum Allowable Depth

$d_{c\,max}$ =	$i\,(t_s - d_p/i) / V_r$		Percolation Time =	12	min/cm *from Terraprobe HydroG Report
$d_{c\,max}$ =	6000	mm	I = infiltration rate =	50	mm/hr
			ts = time to drain =	48	hours
Height of Infiltration Gallery =	350	mm	Vr = void ratio =	0.4	
Proposed Depth =	350	mm	Groundwater Elevation =	414.2	m *from Terraprobe HydroG Report
			dp = Depth of ponding =	0	
Prop. Drawdown (Subsurface)=	7.00	hours			
Safety Factor =	6.86				

Required Footprint

Af =	V / d Vr	
WQV	115.7	m^3
d =	0.35	m
Required Footprint =	330.5	m^2
Proposed Area =	368.0	m^2
Subsurface Storage Volume =	123.7	m^3
Separation from GW table =	1.00	m

Climate Data								Pervious Area			Impervious Area		
Month	**Days in the month**	**Hours of Sunlight* ****	**Mean Temperature ****	**Heat Index**	**Potential Evapo-transpiration***	**Daylight Correction Value**	**Total Precipitation* ***	**Adjusted Potential Evapo-transpiration**	**Surplus**	**Deficit**	**Evaporation**	**Surplus**	**Deficit**
			(T) #	**I**	**mm/month**		**mm**	**mm**	**mm**	**mm**	**mm**	**mm**	**mm**
January	31	9.3	-7.5	0.00	0.0	0.80	64.3	0.00	64.3	0.0	6.4	57.9	0.0
February	28	10.5	-6.5	0.00	0.0	0.82	54.5	0.00	54.5	0.0	5.5	49.1	0.0
March	31	12.1	-2.1	0.00	0.0	1.04	60.9	0.00	60.9	0.0	6.1	54.8	0.0
April	30	13.6	5.3	1.09	25.9	1.13	70.1	29.36	40.7	0.0	7.0	63.1	0.0
May	31	14.7	11.7	3.62	58.4	1.27	86.6	73.91	12.7	0.0	8.7	77.9	0.0
June	30	15.0	16.9	6.32	85.1	1.25	81.3	106.44	0.0	25.1	8.1	73.2	0.0
July	31	14.8	19.4	7.79	98.1	1.27	80.8	125.02	0.0	44.2	8.1	72.7	0.0
August	31	14.2	18.4	7.19	92.9	1.22	88.2	113.61	0.0	25.4	8.8	79.4	0.0
September	30	13.1	14.3	4.91	71.7	1.09	87.0	78.31	8.7	0.0	8.7	78.3	0.0
October	31	10.7	7.8	1.96	38.5	0.92	76.6	35.49	41.1	0.0	7.7	68.9	0.0
November	30	9.7	2.0	0.25	9.5	0.81	87.1	7.70	79.4	0.0	8.7	78.4	0.0
December	31	8.8	-4.1	0.00	0.0	0.76	64.2	0.00	64.2	0.0	6.42	57.8	0.0
TOTAL	365			33.1	480.2		**901.6**	**570**	**426.5**	**95**	**90.2**	**811.4**	**0**

Notes

* PET = 16 [10 T / I]$^{\alpha}$

where, $\alpha = (675 * 10^{-9} * I^3) - (771 * 10^{-7} * I^2) + (1792 * 10^{-5} * I) + 0.49239 = 1.112$

**Canadian Climate Normals 1981-2010 Station Data - Orangeville MOE - located 9 km nor th of the site
https://climate.weather.gc.ca/climate_normals/results_1981_2010_e.html?searchType=stnName&txtStationName=orangeville&searchMethod=contains&txtCentralLatMin=0&txtCentralLatSec=0&txtCentralLongMin=0&txtCentralLongSec=0&stnID=4991&dispBack=1

***Canadian Climate Normals 1981-2010 Station Data - Toronto Lester B Pearson Int'l A -located 59 km southwest of the site
https://climate.weather.gc.ca/climate_normals/results_1981_2010_e.html?searchType=stnName&txtStationName=pearson&searchMethod=contains&txtCentralLatMin=0&txtCentralLatSec=0&txtCentralLongMin=0&txtCentralLongSec=0&stnID=5097&dispBack=1

Pervious Surplus: **331.8** **mm**

Impervious Surplus: **811.4** **mm**

Assumes 10% of rainfall is evaporated (no evapotranspiration occurs)

Impervious Factor = 0.10

Water Balance Design Sheet **Pre-Development**

Site: Agnes Street Infill Subdivision, Alton, ON

December 20, 2023

Existing Drainage Area 101

Catchment Parameter	Units	Perv	Imperv	Total
Area	m^2	38,382	2,091	40,473
Pervious Area	m^2	38,382	0	38,382
Impervious Area	m^2	0	2,091	2,091
Infiltration Factors				
Topography		0.1	0.1	0.10
Soil		0.4	0.4	0.40
Land Cover		0.1	0.1	0.10
MECP Infiltration Factor		0.60	0.60	0.60
Actual Infiltration Factor		0.60	0.00	0.57
Runoff Coefficient		0.25	0.95	0.29
Runoff from Impervious Surfaces*		0%	0%	0%
Inputs (per Unit Area)				
Precipitation	mm/yr	902	902	902
Run- on	mm/yr	0	0	0
Other	mm/yr	0	0	0
Total Inputs	mm/yr	902	902	902
Outputs (per Unit Area)				
Precipitation Surplus	mm/yr	332	811	
Net Surplus	mm/yr	0	0	
Total Evapotranspiration	**mm/yr**	**570**	**90**	
Infiltration	mm/yr	199	0	
Rooftop Infiltration	mm/yr	0	0	
Total Infiltration	**mm/yr**	**199**	**0**	
Runoff Pervious Areas	mm/yr	133	811	
Runoff Impervious Areas	mm/yr	0	0	
Total Runoff	**mm/yr**	**133**	**811**	
Total Outputs	**mm/yr**	**902**	**902**	
Difference (input - output)	mm/yr	0	0	
Inputs (Volumes)				
Precipitation	m^3/yr	34,605	1,886	36,491
Run-on	m^3/yr	0	0	0
Other Inputs	m^3/yr	0	0	0
Total Inputs	m^3/yr	34,605	1,886	36,491
Outputs (Volumes)				
Precipitation Surplus	m^3/yr	12,734	1,697	14,431
Net Surplus	m^3/yr	0	0	0
Total Evapotranspiration	**m^3/yr**	**21,872**	**189**	**22,060**
Infiltration	m^3/yr	7,640	0	7,640
Rooftop Infiltration	m^3/yr	0	0	0
Total Infiltration	**m^3/yr**	**7,640**	**0**	**7,640**
Runoff Pervious Areas	m^3/yr	5,093	1,697	6,790
Runoff Impervious Areas	m^3/yr	0	0	0
Total Runoff	**m^3/yr**	**5,093**	**1,697**	**6,790**
Total Outputs	**m^3/yr**	**34,605**	**1,886**	**36,491**
Difference (input - output)	m^3/yr	0	0	0

Water Balance Design Sheet		**Post Development**		
Site: Agnes Street Infill Subdivision, Alton, ON				
December 20, 2023				
		Proposed Drainage Area 201 & 202		
Catchment Parameter	**Units**	**Perv**	**Imperv**	**Total**
Area	m^2	19,524	20,950	40,473
Pervious Area	m^2	19,524	0	19,524
Impervious Area	m^2	0	20,950	20,950
Infiltration Factors				
Topography		0.1	0.1	0.10
Soil		0.4	0.4	0.40
Land Cover		0.1	0.1	0.10
MECP Infiltration Factor		0.60	0.60	0.60
% Impervious		0%	100%	52%
Actual Imperv Factor		0.60	0.00	0.29
Inputs (per Unit Area)				
Precipitation	mm/yr	902	902	
Run- on	mm/yr	0	0	
Other	mm/yr	0	0	
Total Inputs	mm/yr	902	902	
Outputs (per Unit Area)				
Precipitation Surplus	mm/yr	332	811	
Net Surplus	mm/yr	332	811	
Total Evapotranspiration	**mm/yr**	**570**	**90**	
Infiltration	mm/yr	199	0	
LID Infiltration	mm/yr	0	0	
Total Infiltration	**mm/yr**	**199**	**0**	
Runoff Pervious Areas	mm/yr	133	0	
Runoff Impervious Areas	mm/yr	0	811	
Total Runoff	**mm/yr**	**133**	**811**	
Total Outputs	**mm/yr**	**902**	**902**	
Difference (input - output)	mm/yr	0	0	
Inputs (Volumes)				
Precipitation	m^3/yr	17603	18888	36491
Run-on	m^3/yr	0	0	0
Other Inputs	m^3/yr	0	0	0
Total Inputs	m^3/yr	17,603	18,888	36,491
Outputs (Volumes)				
Precipitation Surplus	m^3/yr	6,477	16,999	23,476
Net Surplus	m^3/yr	6,477	16,999	23,476
Total Evapotranspiration	**m^3/yr**	**11,125**	**1,889**	**13,014**
Infiltration	m^3/yr	3,886	0	3,886
Rooftop Infiltration	m^3/yr	0	0	0
Total Infiltration	**m^3/yr**	**3,886**	**0**	**3,886**
Runoff Pervious Areas	m^3/yr	2,591	0	2,591
Runoff Impervious Areas	m^3/yr	0	16,999	16,999
Total Runoff	**m^3/yr**	**2,591**	**16,999**	**19,590**
Total Outputs	**m^3/yr**	**17,603**	**18,888**	**36,491**
Difference (input - output)	m^3/yr	0	0	0

Water Balance Design Sheet		**Post Development with SWM, FS = 1.0**		
Site: Agnes Street Infill Subdivision, Alton, ON				
December 20, 2023				
		Proposed Drainage Area A1		
Catchment Parameter	**Units**	**Perv**	**Imperv**	**Total**
Area	m^2	19,524	20,950	40,473
Pervious Area	m^2	19,524	0	19,524
Impervious Area	m^2	0	20,950	20,950
Infiltration Factors				
Topography		0.1	0.1	0.10
Soil		0.4	0.4	0.40
Land Cover		0.1	0.1	0.10
MECP Infiltration Factor		0.60	0.60	0.60
% Impervious		0%	100%	52%
Actual Imperv Factor		0.60	0.00	0.29
Inputs (per Unit Area)				
Precipitation	mm/yr	902	902	
Run- on	mm/yr	0	0	
Other	mm/yr	0	0	
Total Inputs	mm/yr	902	902	
Outputs (per Unit Area)				
Precipitation Surplus	mm/yr	332	811	
Net Surplus	mm/yr	332	811	
Total Evapotranspiration	**mm/yr**	**570**	**90**	
Infiltration	mm/yr	199	0	
LID Infiltration*	mm/yr	0	446	
Total Infiltration	**mm/yr**	**199**	**446**	
Runoff Pervious Areas	mm/yr	133	0	
Runoff Impervious Areas	mm/yr	0	365	
Total Runoff	**mm/yr**	**133**	**365**	
Total Outputs	**mm/yr**	**902**	**902**	
Difference (input - output)	mm/yr	0	0	
Inputs (Volumes)				
Precipitation	m^3/yr	17,603	18,888	36,491
Run-on	m^3/yr	0	0	0
Other Inputs	m^3/yr	0	0	0
Total Inputs	m^3/yr	17,603	18,888	36,491
Outputs (Volumes)				
Precipitation Surplus	m^3/yr	6,477	16,999	23,476
Net Surplus	m^3/yr	6,477	16,999	23,476
Total Evapotranspiration	**m^3/yr**	**11,125**	**1,889**	**13,014**
Infiltration	m^3/yr	3,886	0	3,886
LID Infiltration*	m3/yr	0	9,350	9,350
Total Infiltration	**m^3/yr**	**3,886**	**9,350**	**13,236**
Runoff Pervious Areas	m^3/yr	2,591	0	2,591
Runoff Impervious Areas	m^3/yr	0	7,650	7,650
Total Runoff	**m^3/yr**	**2,591**	**7,650**	**10,241**
Total Outputs	**m^3/yr**	**17,603**	**18,888**	**36,491**
Difference (input - output)	m^3/yr	0	0	0

*5mm of rainfall to be retained. 55% of rainfall events are less than 5mm, therefore it is assumed 55% of annual precipitation surplus is infiltrated

Water Balance Design Sheet		**Post Development with SWM, FS = 1.5**		
Site: Agnes Street Infill Subdivision, Alton, ON				
December 20, 2023				
		Proposed Drainage Area A1		
Catchment Parameter	**Units**	**Perv**	**Imperv**	**Total**
Area	m^2	19,524	20,950	40,473
Pervious Area	m^2	19,524	0	19,524
Impervious Area	m^2	0	20,950	20,950
Infiltration Factors				
Topography		0.1	0.1	0.10
Soil		0.4	0.4	0.40
Land Cover		0.1	0.1	0.10
MECP Infiltration Factor		0.60	0.60	0.60
% Impervious		0%	100%	52%
Actual Imperv Factor		0.60	0.00	0.29
Inputs (per Unit Area)				
Precipitation	mm/yr	902	902	
Run- on	mm/yr	0	0	
Other	mm/yr	0	0	
Total Inputs	mm/yr	902	902	
Outputs (per Unit Area)				
Precipitation Surplus	mm/yr	332	811	
Net Surplus	mm/yr	332	811	
Total Evapotranspiration	**mm/yr**	**570**	**90**	
Infiltration	mm/yr	199	0	
LID Infiltration*	mm/yr	0	298	
Total Infiltration	**mm/yr**	**199**	**298**	
Runoff Pervious Areas	mm/yr	133	0	
Runoff Impervious Areas	mm/yr	0	514	
Total Runoff	**mm/yr**	**133**	**514**	
Total Outputs	**mm/yr**	**902**	**902**	
Difference (input - output)	mm/yr	0	0	
Inputs (Volumes)				
Precipitation	m^3/yr	17,603	18,888	36,491
Run-on	m^3/yr	0	0	0
Other Inputs	m^3/yr	0	0	0
Total Inputs	m^3/yr	17,603	18,888	36,491
Outputs (Volumes)				
Precipitation Surplus	m^3/yr	6,477	16,999	23,476
Net Surplus	m^3/yr	6,477	16,999	23,476
Total Evapotranspiration	**m^3/yr**	**11,125**	**1,889**	**13,014**
Infiltration	m^3/yr	3,886	0	3,886
LID Infiltration*	m3/yr	0	6,233	6,233
Total Infiltration	**m^3/yr**	**3,886**	**6,233**	**10,119**
Runoff Pervious Areas	m^3/yr	2,591	0	2,591
Runoff Impervious Areas	m^3/yr	0	10,766	10,766
Total Runoff	**m^3/yr**	**2,591**	**10,766**	**13,357**
Total Outputs	**m^3/yr**	**17,603**	**18,888**	**36,491**
Difference (input - output)	m^3/yr	0	0	0

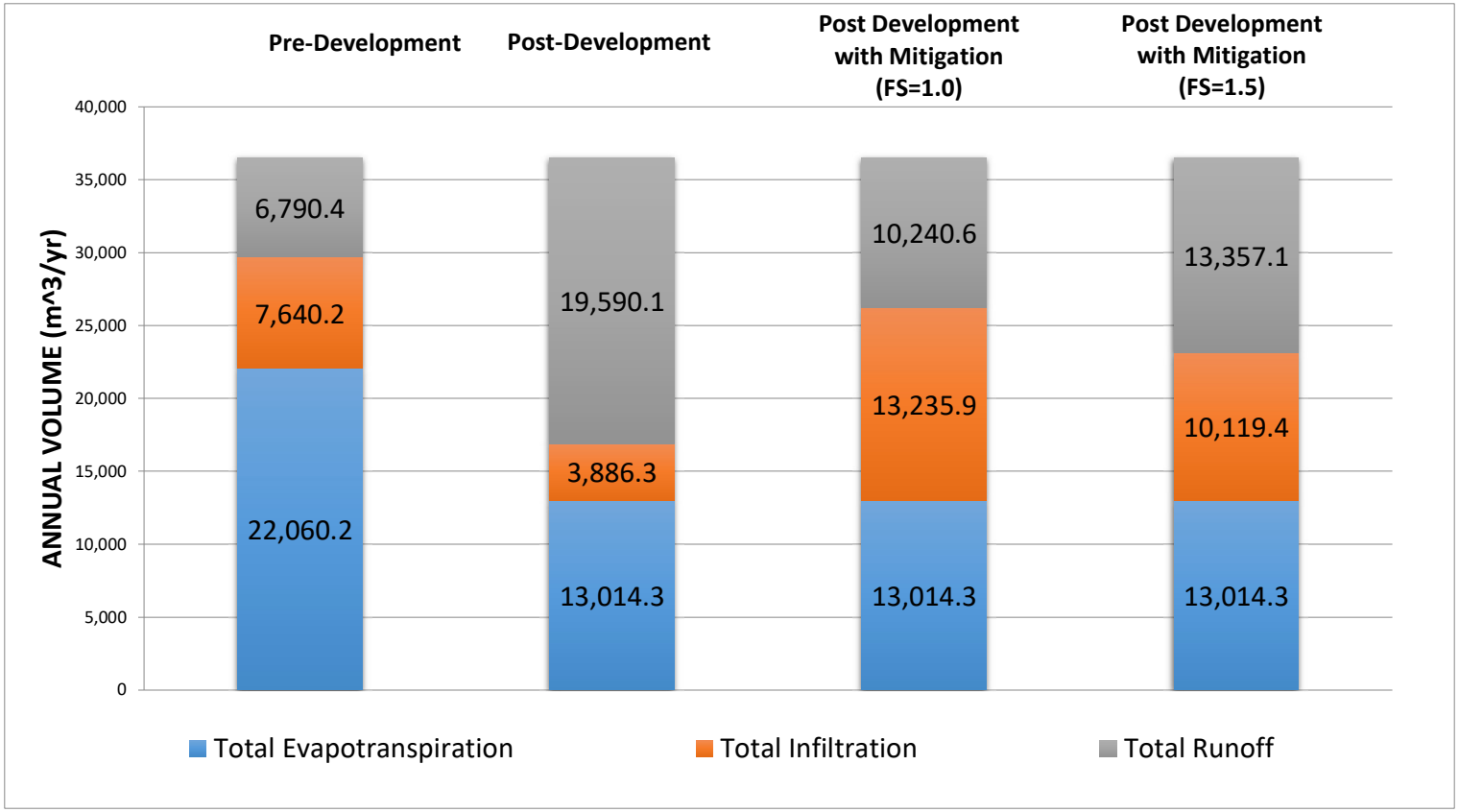
*5mm of rainfall to be retained. 55% of rainfall events are less than 5mm, therefore it is assumed 55% of annual precipitation surplus is infiltrated. Assuming a factor of safety of 1.5, this equates to 37% of rainfall events

Water Balance Summary Sheet
Site: Agnes Street Infill Subdivision, Alton, ON
December 20, 2023

Mean Temperature **

Potential Evapo-transpiration*

	Units	Pre-Development	Post-Development	Change (Pre- to Post-)	Post Development with Mitigation (FS=1.0)	Post Development with Mitigation (FS=1.5)	Change (Pre- to Post-Mitigation)
Inputs (Volumes)							
Precipitation	m^3/yr	36,490.8	36,490.7	0%	36,490.7	36,490.7	0%
Run-on	m^3/yr	0.0	0.0	0%	0.0	0.0	0%
Other Inputs	m^3/yr	0.0	0.0	0%	0.0	0.0	0%
Total Inputs		**36,490.77**	**36,490.73**	0%	**36,490.7**	**36,490.7**	0%
Outputs (Volumes)							
Precipitation Surplus	m^3/yr	14,430.6	23,476.5	63%	23,476.5	23,476.5	63%
Net Surplus	m^3/yr	0.0	23,476.5	0%	23,476.5	23,476.5	0%
Total Evapotranspiration	**m^3/yr**	22,060.2	13,014.3	-41%	13,014.3	13,014.3	-41%
Infiltration	m^3/yr	7,640.2	3,886.3	-49%	3,886.3	3,886.3	-49%
LID Infiltration	m^3/yr	0.0	0.0	0%	9,349.6	6,233.1	0%
Total Infiltration	**m^3/yr**	**7,640.2**	**3,886.3**	-49%	**13,235.9**	**10,119.4**	73%
Runoff Pervious Areas	m^3/yr	6,790.4	2,590.9	-62%	2,590.9	2,590.9	-62%
Runoff Impervious Areas	m^3/yr	0.0	16,999.3	0%	7,649.7	10,766.2	0%
Total Runoff	**m^3/yr**	**6,790.4**	**19,590.1**	188%	**10,240.6**	**13,357.1**	51%
Total Outputs	**m^3/yr**	36,490.8	36,490.7	0%	36,490.7	36,490.7	0%



TOWN OF CALEDON
STORM SEWER DESIGN SHEET

Project / Subdivision : Agnes Street Subdivision

Consulting Engineer : Greck and Associates
Project No.: 20-731

Prepared by: James Norris

Checked by: Khalid Mahmood

Last Revised: December 1, 2023

Design Parameters (5 Year Storm)

A = drainage area (ha)	T_{init}(hr)= 0.167
C = runoff coefficient	A= 1593
T_c = time of concentration	B= 11.000
	C= 0.879

Manning's (n): 0.013
System to be Designed for: 5 Year Storm

Design Equations

$$I = \frac{A}{(t + B)^C}$$

$$Q = 2.78 \times A \times C \times I$$

Location			Drainage Area Characteristics						Rainfall / Runoff			Sewer Data								
Street	From	To	Area	Area	Cum. Area	Runoff Coeff. R	AR in Section	Cum. AR	Time of Concentration	Rainfall Intensity	Runoff Q	Pipe Diameter	Pipe Length	Grade	Material	Total Flow (Q Max)	% FULL	Full Flow Velocity	V (Actual)	Sect. Time	Accum. Time
	MH #	MH #	(m2)	(ha)	(ha)				(min)	(mm/hr)	m3/sec	(mm)	(m)	(%)		(m3/s)	%	(m/s)	(m/s)	(Min)	(Min)
	CBMH13	MH10	3604	0.360	0.360	0.43	0.154	0.154	10.00	109.68	0.047	300	53.90	1.47	PVC	0.120	39.2%	1.68	1.49	0.60	10.60
	MH12	MH11	3406	0.341	0.341	0.43	0.148	0.148	10.00	109.68	0.045	300	33.10	2.78	PVC	0.120	37.6%	2.31	2.01	0.27	10.27
	MH11	MH10	0	0.000	0.341	0.00	0.000	0.148	10.27	108.43	0.045	300	6.66	5.00	PVC	0.120	37.2%	3.09	2.68	0.04	10.32
	MH10	MH9	0	0.000	0.701	0.00	0.000	0.302	10.60	106.99	0.090	450	4.65	0.50	PVC	0.210	42.8%	1.28	1.19	0.06	10.67
	MH9	MH8	2890	0.289	0.990	0.53	0.154	0.456	10.67	106.71	0.135	525	120.00	0.50	PVC	0.317	42.7%	1.42	1.32	1.52	12.18
	MH8	MH7	0	0.000	0.990	0.00	0.000	0.456	12.18	100.55	0.128	525	94.75	2.18	PVC	0.470	27.1%	2.96	2.17	0.73	12.91
	MH7	MH6	3584	0.358	1.348	0.60	0.216	0.673	12.91	97.85	0.183	600	2.98	0.50	PVC	0.453	40.4%	1.55	1.40	0.04	12.95
	MH6	MH5-OGS	4195	0.419	1.768	0.58	0.244	0.916	12.95	97.73	0.249	750	5.00	0.50	PVC	0.821	30.3%	1.80	1.40	0.06	13.01
	MH5-OGS	SWM FACILITY202	0	0.000	1.768	0.00	0.000	0.916	13.01	97.51	0.248	750	2.00	0.50	PVC	0.821	30.2%	1.80	1.40	0.02	13.03
	CBMH27	MH26	1552	0.155	0.155	0.38	0.059	0.059	10.00	109.68	0.018	300	5.98	0.50	PVC	0.071	25.2%	0.98	0.68	0.15	10.15
	MH26	MH25	1368	0.137	0.292	0.50	0.068	0.127	10.15	109.01	0.039	375	70.43	0.50	PVC	0.129	29.9%	1.13	0.88	1.34	11.49
	MH25	MH24	3571	0.357	0.649	0.76	0.270	0.397	11.49	103.28	0.114	525	9.24	0.50	PVC	0.317	36.0%	1.42	1.21	0.13	11.61
	MH24	MH17	0	0.000	0.649	0.00	0.000	0.397	11.61	102.77	0.114	525	70.27	0.50	PVC	0.317	35.8%	1.42	1.21	0.97	12.58
	MH23	MH22	6176	0.618	0.618	0.59	0.365	0.365	10.00	109.68	0.111	375	69.23	0.50	PVC	0.129	86.0%	1.13	1.29	0.90	10.90
	MH22	MH21	0	0.000	0.618	0.00	0.000	0.365	10.90	105.73	0.107	375	9.24	0.50	PVC	0.129	82.9%	1.13	1.29	0.12	11.01
	MH21	MH20	3406	0.341	0.958	0.43	0.148	0.513	11.01	105.22	0.150	525	64.46	0.50	PVC	0.317	47.3%	1.42	1.39	0.78	11.79
	MH20	MH18	867	0.087	1.045	0.81	0.070	0.583	11.79	102.07	0.165	600	12.52	0.50	PVC	0.453	36.5%	1.55	1.34	0.16	11.95

Location			Drainage Area Characteristics						Rainfall / Runoff			Sewer Data								
Street	From	To	Area	Area	Cum. Area	Runoff Coeff. R	AR in Section	Cum. AR	Time of Concentration	Rainfall Intensity	Runoff Q	Pipe Diameter	Pipe Length	Grade	Material	Total Flow (Q Max)	% FULL	Full Flow Velocity	V (Actual)	Sect. Time	Accum. Time
	MH #	MH #	(m2)	(ha)	(ha)				(min)	(mm/hr)	m3/sec	(mm)	(m)	(%)		(m3/s)	%	(m/s)	(m/s)	(Min)	(Min)
	MH19	MH18	739	0.074	0.074	0.78	0.057	0.057	10.00	109.68	0.017	300	4.50	0.50	PVC	0.071	24.5%	0.98	0.68	0.11	10.11
	MH18	MH17	4300	0.430	1.549	0.66	0.285	0.925	11.95	101.46	0.261	750	22.43	0.50	PVC	0.821	31.8%	1.80	1.44	0.26	12.21
	MH17	MH16-OGS	0	0.000	2.198	0.00	0.000	1.322	12.58	99.06	0.364	750	2.18	0.50	PVC	0.821	44.3%	1.80	1.71	0.02	12.60
	MH16-OGS	INFILTRATION FACILITY	0	0.000	2.198	0.00	0.000	1.322	12.60	98.98	0.364	750	2.00	0.50	PVC	0.821	44.3%	1.80	1.71	0.02	12.62
	INFILTRATION FACILI	MH15	0	0.000	2.198	0.00	0.000	1.322	12.62	98.91	0.364	750	4.50	2.00	PVC	1.100	33.1%	3.60	2.94	0.03	12.65
	MH15	SWM FACILITY201	0	0.000	2.198	0.00	0.000	1.322	12.65	98.81	0.363	750	4.42	2.00	PVC	1.100	33.0%	3.60	2.94	0.03	12.67
	SWM FACILITY201	MH14-CONTROL	0	0.000	2.198	0.00	0.000	1.322	12.67	98.72	0.363	750	2.00	2.00	PVC	1.100	33.0%	3.60	2.93	0.01	12.68
	MH14-CONTROL	MH3	0	0.000	2.198	0.00	0.000	1.322	12.68	98.68	0.064	300	66.46	7.21	PVC	0.120	53.6%	3.71	3.82	0.29	12.97
	SWM FACILITY202	MH4-CONTROL	0	0.000	1.768	0.00	0.000	0.916	12.97	97.63	0.249	750	2.00	0.50	PVC	0.821	30.3%	1.80	1.40	0.02	13.00
	MH4-CONTROL	MH3	0	0.000	1.768	0.00	0.000	0.916	-	-	0.043	375	6.31	0.50	PVC	0.129	33.3%	1.13	0.93	0.11	-
	MH3	MH2	0	0.000	3.966	0.00	0.000	2.239	-	-	0.107	450	17.24	0.50	PVC	0.210	51.1%	1.28	1.29	0.22	-
	MH2	CBMH1	0	0.000	3.966	0.00	0.000	2.239	-	-	0.107	450	106.96	0.50	PVC	0.210	51.1%	1.28	1.29	1.38	-
											Orifice Discharge										

APPENDIX E

Stormwater Management Product Specifications

◆ Verification Statement ◆ Verification Statement ◆ Verification Statement ◆

VERIFICATION STATEMENT

GLOBE Performance Solutions

Verifies the performance of

Stormceptor® EF and EFO Oil-Grit Separators

Developed by Imbrium Systems, Inc.,
Whitby, Ontario, Canada

Registration: GPS-ETV_VR2020-11-15_Imbrium-SC

In accordance with

ISO 14034:2016

Environmental management —
Environmental technology verification (ETV)

John D. Wiebe, PhD
Executive Chairman
GLOBE Performance Solutions

November 15, 2020
Vancouver, BC, Canada

Verification Body
GLOBE Performance Solutions
404 – 999 Canada Place | Vancouver, B.C | Canada |V6C 3E2

Technology description and application

The Stormceptor® EF and EFO are treatment devices designed to remove oil, sediment, trash, debris, and pollutants attached to particulates from Stormwater and snowmelt runoff. The device takes the place of a conventional manhole within a storm drain system and offers design flexibility that works with various site constraints. The EFO is designed with a shorter bypass weir height, which accepts lower surface loading rate into the sump, thereby reducing re-entrainment of captured free floating light liquids.

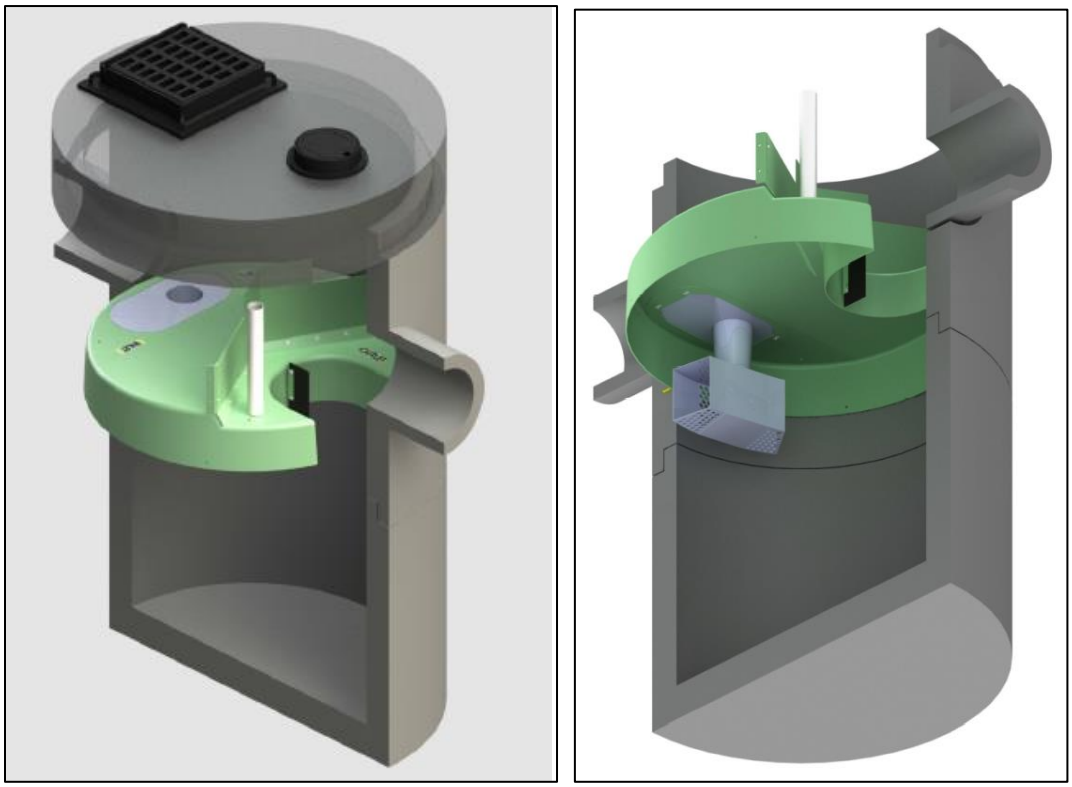


Figure 1. Graphic of typical inline Stormceptor® unit and core components.

Stormwater and snowmelt runoff enters the Stormceptor® EF/EFO's upper chamber through the inlet pipe(s) or a surface inlet grate. An insert divides the unit into lower and upper chambers and incorporates a weir to reduce influent velocity and separate influent (untreated) from effluent (treated) flows. Influent water ponds upstream of the insert's weir providing driving head for the water flowing downwards into the drop pipe where a vortex pulls the water into the lower chamber. The water diffuses at lower velocities in multiple directions through the drop pipe outlet openings. Oil and other floatables rise up and are trapped beneath the insert, while sediments undergo gravitational settling to the sump's bottom. Water from the sump can exit by flowing upward to the outlet riser onto the top side of the insert and downstream of the weir, where it discharges through the outlet pipe.

Maximum flow rate into the lower chamber is a function of weir height and drop pipe orifice diameter. The Stormceptor® EF and EFO are designed to allow a surface loading rate of 1135 L/min/m^2 (27.9 gal/min/ft^2) and 535 L/min/m^2 (13.1 gal/min/ft^2) into the lower chamber, respectively. When prescribed surface loading rates are exceeded, ponding water can overtop the weir height and bypass the lower treatment chamber, exiting directly through the outlet pipe. Hydraulic testing and scour testing demonstrate that the internal bypass effectively prevents scour at all bypass flow rates. Increasing the bypass flow rate does not increase the orifice-controlled flow rate into the lower treatment chamber where sediment is stored. This internal bypass feature allows for in-line installation, avoiding the cost of

additional bypass structures. During bypass, treatment continues in the lower chamber at the maximum flow rate. The Stormceptor® EFO's lower design surface loading rate is favorable for minimizing re-entrainment and washout of captured light liquids. Inspection of Stormceptor® EF and EFO devices is performed from grade by inserting a sediment probe through the outlet riser and an oil dipstick through the oil inspection pipe. The unit can be maintained by using a vacuum hose through the outlet riser.

Performance conditions

The data and results published in this Technology Fact Sheet were obtained from the testing program conducted on the Imbrium Systems Inc.'s Stormceptor® EF4 and EFO4 Oil-Grit Separators, in accordance with the Procedure for Laboratory Testing of Oil-Grit Separators (Version 3.0, June 2014). The Procedure was prepared by the Toronto and Region Conservation Authority (TRCA) for Environment Canada's Environmental Technology Verification (ETV) Program. A copy of the Procedure may be accessed on the Canadian ETV website at www.etvcanada.ca.

Performance claim(s)

Capture test[a]:

During the capture test, the Stormceptor® EF4 OGS device, with a false floor set to 50% of the manufacturer's recommended maximum sediment storage depth and a constant influent test sediment concentration of 200 mg/L, removes 70, 64, 54, 48, 46, 44, and 49 percent of influent sediment by mass at surface loading rates of 40, 80, 200, 400, 600, 1000, and 1400 L/min/m^2, respectively.

Stormceptor® EFO4, with a false floor set to 50% of the manufacturer's recommended maximum sediment storage depth and a constant influent test sediment concentration of 200 mg/L, removes 70, 64, 54, 48, 42, 40, and 34 percent of influent sediment by mass at surface loading rates of 40, 80, 200, 400, 600, 1000, and 1400 L/min/m^2, respectively.

Scour test[a]:

During the scour test, the Stormceptor® EF4 and Stormceptor® EFO4 OGS devices, with 10.2 cm (4 inches) of test sediment pre-loaded onto a false floor reaching 50% of the manufacturer's recommended maximum sediment storage depth, generate corrected effluent concentrations of 4.6, 0.7, 0, 0.2, and 0.4 mg/L at 5-minute duration surface loading rates of 200, 800, 1400, 2000, and 2600 L/min/m^2, respectively.

Light liquid re-entrainment test[a]:

During the light liquid re-entrainment test, the Stormceptor® EFO4 OGS device with surrogate low-density polyethylene beads preloaded within the lower chamber oil collection zone, representing a floating light liquid volume equal to a depth of 50.8 mm over the sedimentation area, retained 100, 99.5, 99.8, 99.8, and 99.9 percent of loaded beads by mass during the 5-minute duration surface loading rates of 200, 800, 1400, 2000, and 2600 L/min/m^2.

[a] The claim can be applied to other units smaller or larger than the tested unit as long as the untested units meet the scaling rule specified in the Procedure for Laboratory of Testing of Oil Grit Separators (Version 3.0, June 2014)

Performance results

The test sediment consisted of ground silica (1 – 1000 micron) with a specific gravity of 2.65, uniformly mixed to meet the particle size distribution specified in the testing procedure. The *Procedure for Laboratory Testing of Oil Grit Separators* requires that the three sample average of the test sediment particle size distribution (PSD) meet the specified PSD percent less than values within a boundary threshold of 6%. The comparison of the average test sediment PSD to the CETV specified PSD in Figure 2 indicates that the test sediment used for the capture and scour tests met this condition.

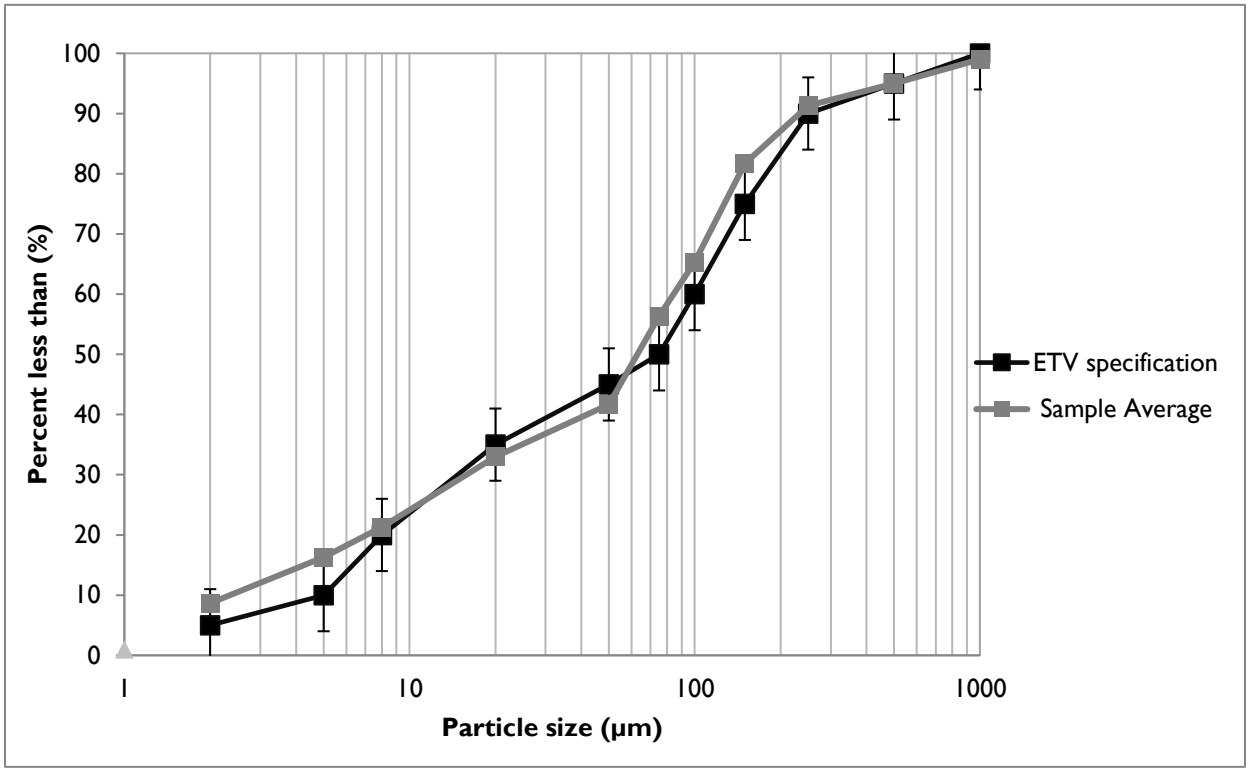


Figure 2. The three sample average particle size distribution (PSD) of the test sediment used for the capture and scour test compared to the specified PSD.

The capacity of the device to retain sediment was determined at seven surface loading rates using the modified mass balance method. This method involved measuring the mass and particle size distribution of the injected and retained sediment for each test run. Performance was evaluated with a false floor simulating the technology filled to 50% of the manufacturer's recommended maximum sediment storage depth. The test was carried out with clean water that maintained a sediment concentration below 20 mg/L. Based on these conditions, removal efficiencies for individual particle size classes and for the test sediment as a whole were determined for each of the tested surface loading rates (Table 1). Since the EF and EFO models are identical except for the weir height, which bypasses flows from the EFO model at a surface loading rate of 535 L/min/m^2 (13.1 gpm/ft^2), sediment capture tests at surface loading rates from 40 to 400 L/min/m^2 were only performed on the EF unit. Surface loading rates of 600, 1000, and 1400 L/min/m^2 were tested on both units separately. Results for the EFO model at these higher flow rates are presented in Table 2.

In some instances, the removal efficiencies were above 100% for certain particle size fractions. These discrepancies are not unique to any one test laboratory and may be attributed to errors relating to the blending of sediment, collection of representative samples for laboratory submission, and laboratory

analysis of PSD. Due to these errors, caution should be exercised in applying the removal efficiencies by particle size fraction for the purposes of sizing the tested device (see Bulletin # CETV 2016-11-0001). The results for "all particle sizes by mass balance" (see Table 1 and 2) are based on measurements of the total injected and retained sediment mass, and are therefore not subject to blending, sampling or PSD analysis errors.

Table 1. Removal efficiencies (%) of the EF4 at specified surface loading rates

Particle size fraction (µm)	**Surface loading rate (L/min/m²)**						
	40	80	200	400	600	1000	1400
>500	90	58	58	100*	86	72	100*
250 - 500	100*	100*	100	100*	100*	100*	100*
150 - 250	90	82	26	100*	100*	67	90
105 - 150	100*	100*	100*	100*	100*	100*	100
75 - 105	100*	92	74	82	77	68	76
53 - 75	Undefined [a]	56	100*	72	69	50	80
20 - 53	54	100*	54	33	36	40	31
8 - 20	67	52	25	21	17	20	20
5 – 8	33	29	11	12	9	7	19
<5	13	0	0	0	0	0	4
All particle sizes by mass balance	**70.4**	**63.8**	**53.9**	**47.5**	**46.0**	**43.7**	**49.0**

[a] An outlier in the feed sample sieve data resulted in a negative removal efficiency for this size fraction.
* Removal efficiencies were calculated to be above 100%. Calculated values ranged between 101 and 171% (average 128%). See text and Bulletin # CETV 2016-11-0001 for more information.

Table 2. Removal efficiencies (%) of the EFO4 at surface loading rates above the bypass rate of 535 L/min/m²

Particle size fraction (µm)	**Surface loading rate (L/min/m²)**		
	600	1000	1400
>500	89	83	100*
250 - 500	90	100*	92
150 - 250	90	67	100*
105 - 150	85	92	77
75 - 105	80	71	65
53 - 75	60	31	36
20 - 53	33	43	23
8 - 20	17	23	15
5 – 8	10	3	3
<5	0	0	0
All particle sizes by mass balance	**41.7**	**39.7**	**34.2**

* Removal efficiencies were calculated to be above 100%. Calculated values ranged between 103 and 111% (average 107%). See text and Bulletin # CETV 2016-11-0001 for more information.

Figure 3 compares the particle size distribution (PSD) of the three sample average of the test sediment to the PSD of the sediment retained by the EF4 at each of the tested surface loading rates. Figure 4 shows the same graph for the EFO4 unit at surface loading rates above the bypass rate of 535 L/min/m².

As expected, the capture efficiency for fine particles in both units was generally found to decrease as surface loading rates increased.

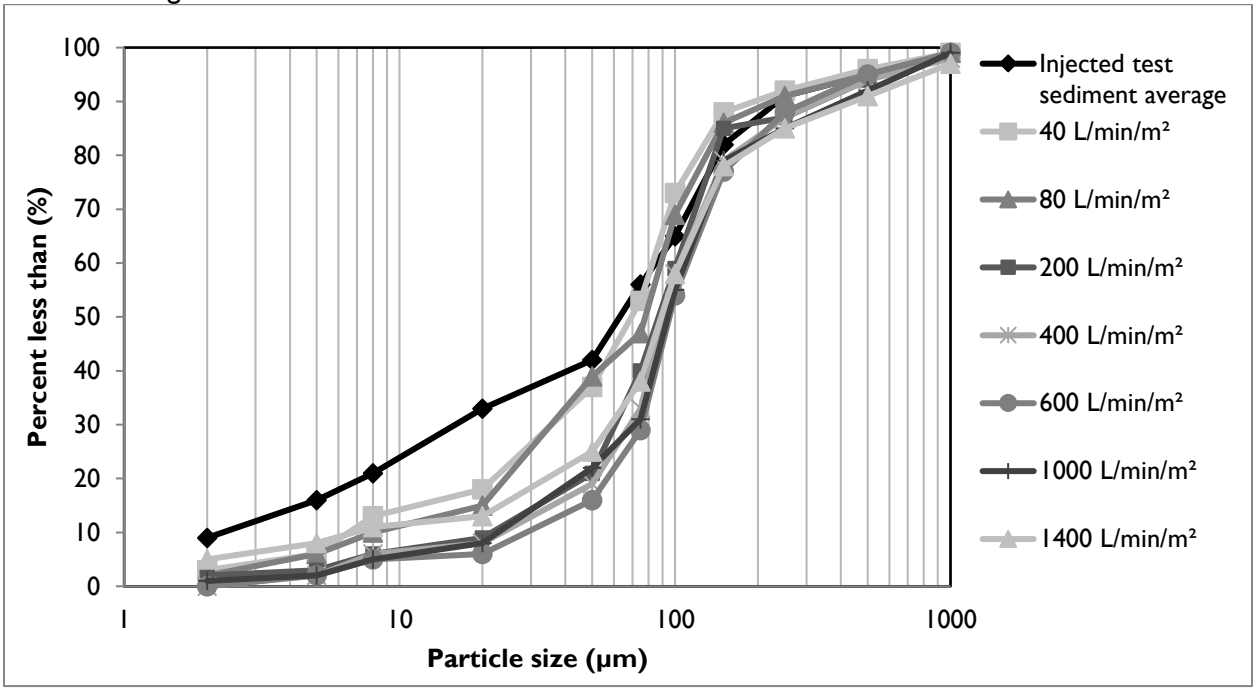


Figure 3. Particle size distribution of sediment retained in the EF4 in relation to the injected test sediment average.

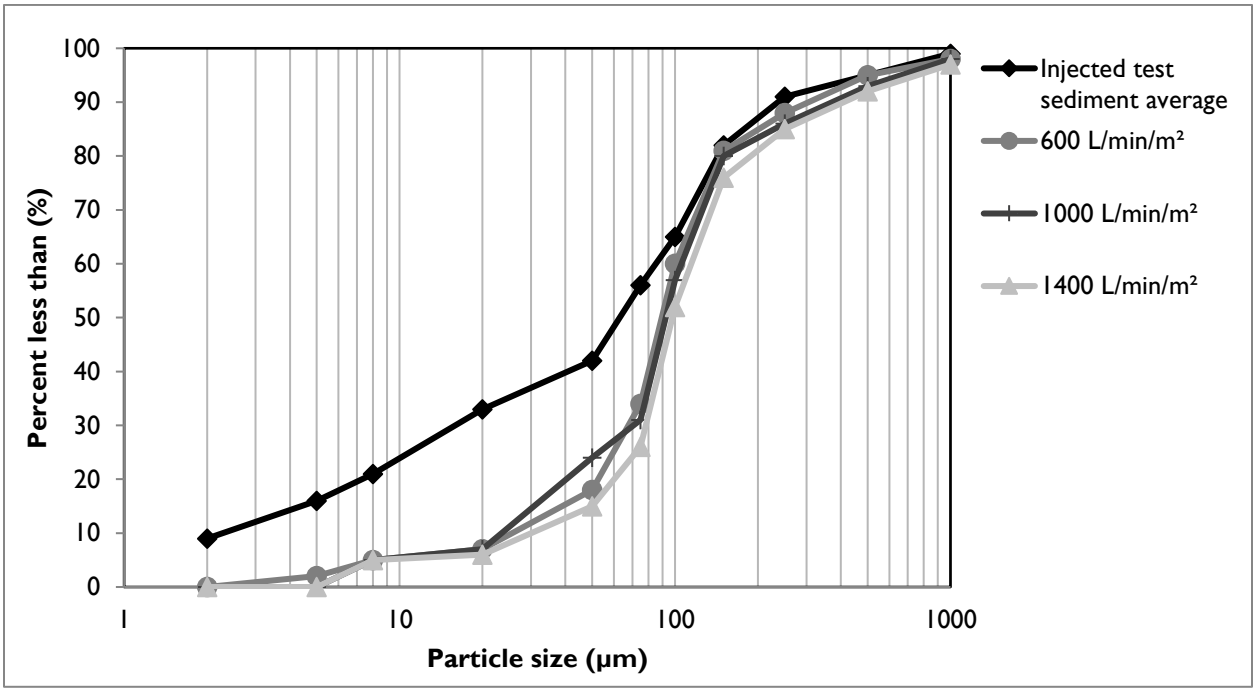


Figure 4. Particle size distribution of sediment retained in the EFO4 in relation to the injected test sediment average at surface loading rates above the bypass rate of 535 L/min/m²

Table 4 shows the results of the sediment scour and re-suspension test for the EF4 unit. The EFO4 was not tested as it was reasonably assumed that scour rates would be lower given that flow bypass occurs at a lower surface loading rate. The scour test involved preloading 10.2 cm of fresh test sediment into

the sedimentation sump of the device. The sediment was placed on a false floor to mimic a device filled to 50% of the maximum recommended sediment storage depth. Clean water was run through the device at five surface loading rates over a 30 minute period. Each flow rate was maintained for 5 minutes with a one minute transition time between flow rates. Effluent samples were collected at one minute sampling intervals and analyzed for Suspended Sediment Concentration (SSC) and PSD by recognized methods. The effluent samples were subsequently adjusted based on the background concentration of the influent water. Typically, the smallest 5% of particles captured during the 40 L/min/m^2 sediment capture test is also used to adjust the concentration, as per the method described in Bulletin # CETV 2016-09-0001. However, since the composites of effluent concentrations were below the Reporting Detection Limit of the Laser Diffraction PSD methodology, this adjustment was not made. Results showed average adjusted effluent sediment concentrations below 5 mg/L at all tested surface loading rates.

It should be noted that the EF4 starts to internally bypass water at 1135 L/min/m^2, potentially resulting in the dilution of effluent concentrations, which would not normally occur under typical field conditions because the field influent concentration would contain a much higher sediment concentration than during the lab test. Recalculation of effluent concentrations to account for dilution at surface loading rates above the bypass rate showed sediment effluent concentrations to be below 1.6 mg/L.

Table 4. Scour test adjusted effluent sediment concentration.

Run	Surface loading rate (L/min/m^2)	Run time (min)	Background sample concentration (mg/L)	Adjusted effluent suspended sediment concentration (mg/L) [a]	Average (mg/L)
1	200	1:00	<RDL	11.9	4.6
		2:00		7.0	
		3:00		4.4	
		4:00		2.2	
		5:00		1.0	
		6:00		1.2	
2	800	7:00	<RDL	1.1	0.7
		8:00		0.9	
		9:00		0.6	
		10:00		1.4	
		11:00		0.1	
		12:00		0	
3	1400	13:00	<RDL	0	0
		14:00		0.1	
		15:00		0	
		16:00		0	
		17:00		0	
		18:00		0	
4	2000	19:00	1.2	0.2	0.2
		20:00		0	
		21:00		0	
		22:00		0.7	
		23:00		0	
		24:00		0.4	

5	2600	25:00	1.6	0.3	0.4
		26:00		0.4	
		27:00		0.7	
		28:00		0.4	
		29:00		0.2	
		30:00		0.4	

[a] The adjusted effluent suspended sediment concentration represents the actual measured effluent concentration minus the background concentration. For more information see Bulletin # CETV 2016-09-0001.

The results of the light liquid re-entrainment test used to evaluate the unit's capacity to prevent re-entrainment of light liquids are reported in Table 5. The test involved preloading 58.3 L (corresponding to a 5 cm depth over the collection sump area of 1.17m^2) of surrogate low-density polyethylene beads within the oil collection skirt and running clean water through the device continuously at five surface loading rates (200, 800, 1400, 2000, and 2600 L/min/m^2). Each flow rate was maintained for 5 minutes with approximately 1 minute transition time between flow rates. The effluent flow was screened to capture all re-entrained pellets throughout the test.

Table 5. Light liquid re-entrainment test results for the EFO4.

Surface Loading Rate (L/min/m2)	Time Stamp	Amount of Beads Re-entrained			
		Mass (g)	Volume (L)[a]	% of Pre-loaded Mass Re-entrained	% of Pre-loaded Mass Retained
200	62	0	0	0.00	100
800	247	168.45	0.3	0.52	99.48
1400	432	51.88	0.09	0.16	99.83
2000	617	55.54	0.1	0.17	99.84
2600	802	19.73	0.035	0.06	99.94
Total Re-entrained		295.60	0.525	0.91	--
Total Retained		32403	57.78	--	99.09
Total Loaded		32699	58.3	--	--

[a] Determined from bead bulk density of 0.56074 g/cm^3

Variances from testing Procedure

The following minor deviations from the *Procedure for Laboratory Testing of Oil-Grit Separators* (Version 3.0, June 2014) have been noted:

1. During the capture test, the 40 L/min/m^2 and 80 L/min/m^2 surface loading rates were evaluated over 3 and 2 days respectively due to the long duration needed to feed the required minimum of 11.3 kg of test sediment into the unit at these lower flow rates. Pumps were shut down at the end of each intermediate day, and turned on again the following morning. The target flow rate was re-established within 30 seconds of switching on the pump. This procedure may have allowed sediments to be captured that otherwise may have exited the unit if the test was continuous. On the basis of practical considerations, this variance was approved by the verifier prior to testing.

2. During the scour test, the coefficient of variation (COV) for the lowest flow rate tested (200 L/min/m^2) was 0.07, which exceeded the specified limit of 0.04 target specified in the OGS Procedure. A pump capable of attaining the highest flow rate of 3036 L/min had difficulty maintaining the lowest flow of 234 L/min but still remained within +/- 10% of the target flow and is viewed as having very little impact on the observed results. Similarly, for the light liquid re-entrainment test the COV for the flow rate of the 200 L/min/m^2 run was 0.049, exceeding the limit of 0.04, but is believed to introduce negligible bias.

3. Due to pressure build up in the filters, the runs at 1000 L/min/m^2 for the Stormceptor® EF4 and 1000 and 1400 L/min/m^2 for the Stormceptor® EFO4 were slightly shorter than the target. The run times were 54, 59 and 43 minutes respectively, versus targets of 60 and 50 minutes. The final feed samples were timed to coincide with the end of the run. Since >25 lbs of sediment was fed, the shortened time did not invalidate the runs.

Verification

The verification was completed by the Verification Expert, Toronto and Region Conservation Authority, contracted by GLOBE Performance Solutions, using the International Standard ***ISO 14034:2016 Environmental management -- Environmental technology verification (ETV)***. Data and information provided by Imbrium Systems Inc. to support the performance claim included the following: Performance test report prepared by Good Harbour Laboratories, and dated September 8, 2017; the report is based on testing completed in accordance with the Procedure for Laboratory Testing of Oil-Grit Separators (Version 3.0, June 2014).

What is ISO14034:2016 Environmental management – Environmental technology verification (ETV)?

ISO 14034:2016 specifies principles, procedures and requirements for environmental technology verification (ETV), and was developed and published by the *International Organization for Standardization (ISO)*. The objective of ETV is to provide credible, reliable and independent verification of the performance of environmental technologies. An environmental technology is a technology that either results in an environmental added value or measures parameters that indicate an environmental impact. Such technologies have an increasingly important role in addressing environmental challenges and achieving sustainable development.

For more information on the Stormceptor® EF and EFO OGS please contact:

Imbrium Systems, Inc.
407 Fairview Drive
Whitby, ON
L1N 3A9, Canada
Tel: 416-960-9900
info@imbriumsystems.com

For more information on ISO 14034:2016 / ETV please contact:

GLOBE Performance Solutions
World Trade Centre
404 – 999 Canada Place
Vancouver, BC
V6C 3E2 Canada
Tel: 604-695-5018 / Toll Free: 1-855-695-5018
etv@globeperformance.com

STORMCEPTOR®
ESTIMATED NET ANNUAL SEDIMENT (TSS) LOAD REDUCTION

03/14/2023

Province:	Ontario
City:	Alton
Nearest Rainfall Station:	TORONTO INTL AP
Climate Station Id:	6158731
Years of Rainfall Data:	20

Site Name:	Agnes St Area 201
Drainage Area (ha):	2.343
% Imperviousness:	52.50

Runoff Coefficient 'c': 0.61

Particle Size Distribution:	CA ETV
Target TSS Removal (%):	60.0

Required Water Quality Runoff Volume Capture (%):	90.00
Estimated Water Quality Flow Rate (L/s):	44.81
Oil / Fuel Spill Risk Site?	Yes
Upstream Flow Control?	No
Peak Conveyance (maximum) Flow Rate (L/s):	
Site Sediment Transport Rate (kg/ha/yr):	

Project Name:	Agnes Street
Project Number:	20-731
Designer Name:	Jennifer Chan
Designer Company:	Greck
Designer Email:	jchan@greck.ca
Designer Phone:	289-657-9797
EOR Name:	
EOR Company:	
EOR Email:	
EOR Phone:	

Net Annual Sediment (TSS) Load Reduction Sizing Summary

Stormceptor Model	TSS Removal Provided (%)
EFO4	42
EFO6	52
EFO8	58
EFO10	61
EFO12	64

Recommended Stormceptor EFO Model: EFO10

Estimated Net Annual Sediment (TSS) Load Reduction (%): 61

Water Quality Runoff Volume Capture (%): > 90

imbrium

THIRD-PARTY TESTING AND VERIFICATION

►**Stormceptor® EF and Stormceptor® EFO** are the latest evolutions in the Stormceptor® oil-grit separator (OGS) technology series, and are designed to remove a wide variety of pollutants from stormwater and snowmelt runoff. These technologies have been third-party tested in accordance with the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators** and performance has been third-party verified in accordance with the **ISO 14034 Environmental Technology Verification (ETV)** protocol.

PERFORMANCE

►**Stormceptor® EF and EFO** remove stormwater pollutants through gravity separation and floatation, and feature a patent-pending design that generates positive removal of total suspended solids (TSS) throughout each storm event, including high-intensity storms. Captured pollutants include sediment, free oils, and sediment-bound pollutants such as nutrients, heavy metals, and petroleum hydrocarbons. Stormceptor is sized to remove a high level of TSS from the frequent rainfall events that contribute the vast majority of annual runoff volume and pollutant load. The technology incorporates an internal bypass to convey excessive stormwater flows from high-intensity storms through the device without resuspension and washout (scour) of previously captured pollutants. Proper routine maintenance ensures high pollutant removal performance and protection of downstream waterwavs.

PARTICLE SIZE DISTRIBUTION (PSD)

►The **Canadian ETV PSD** shown in the table below was used, or in part, for this sizing. This is the identical PSD that is referenced in the Canadian ETV ***Procedure for Laboratory Testing of Oil-Grit Separators*** for both sediment removal testing and scour testing. The Canadian ETV PSD contains a wide range of particle sizes in the sand and silt fractions, and is considered reasonably representative of the particle size fractions found in typical urban stormwater runoff.

Particle Size (µm)	Percent Less Than	Particle Size Fraction (µm)	Percent
1000	100	500-1000	5
500	95	250-500	5
250	90	150-250	15
150	75	100-150	15
100	60	75-100	10
75	50	50-75	5
50	45	20-50	10
20	35	8-20	15
8	20	5-8	10
5	10	2-5	5
2	5	<2	5

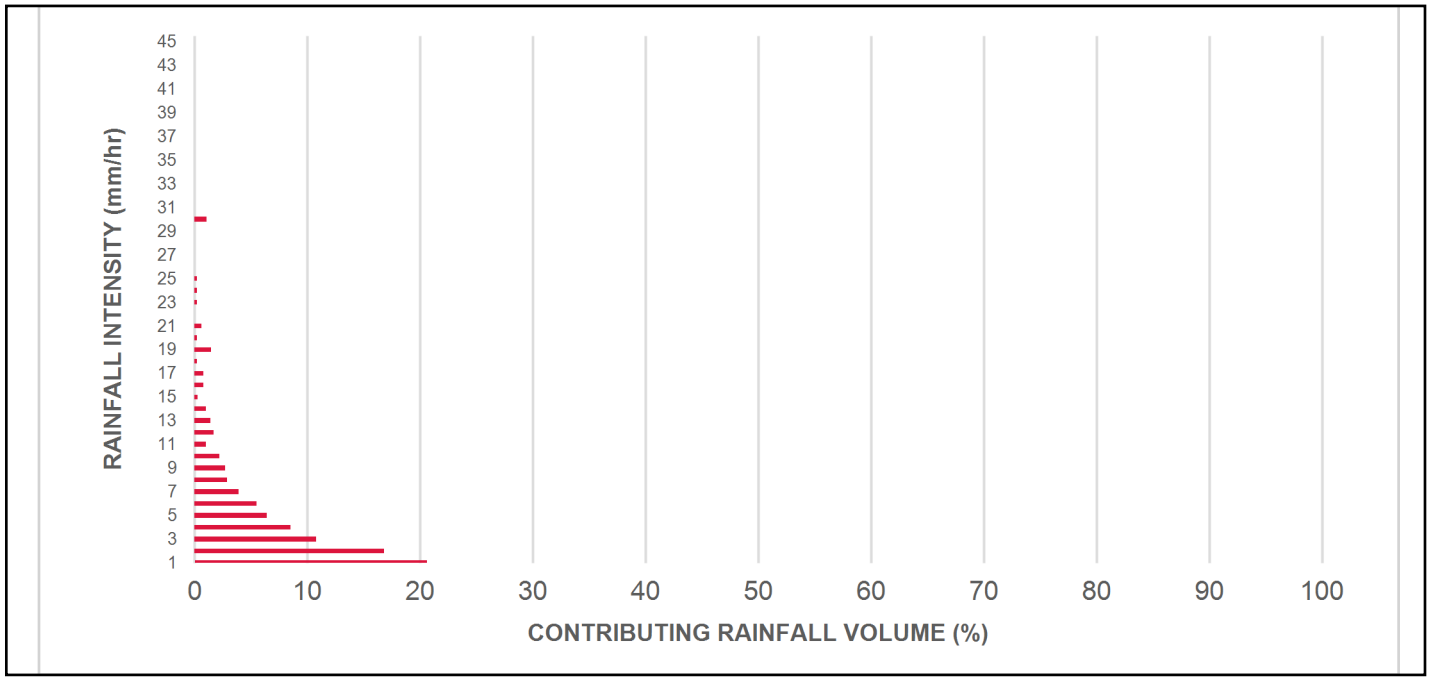
imbrium

Stormceptor® EF Sizing Report

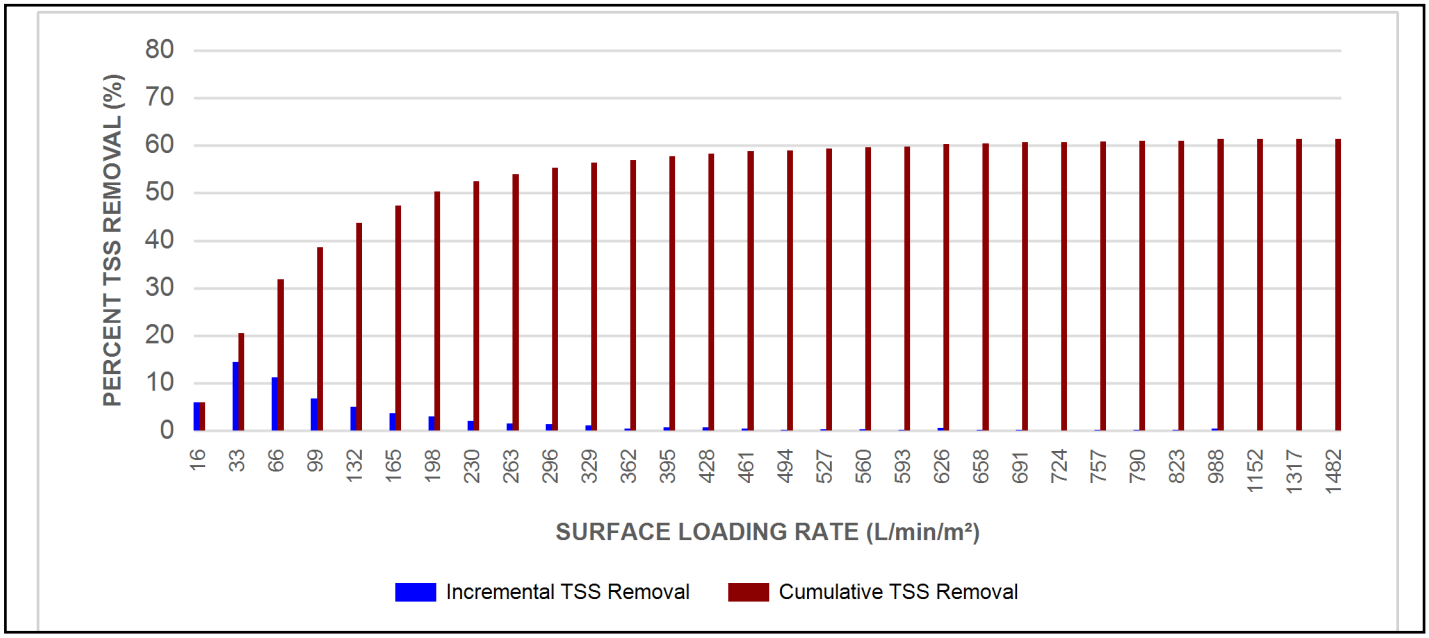
Rainfall Intensity (mm / hr)	Percent Rainfall Volume (%)	Cumulative Rainfall Volume (%)	Flow Rate (L/s)	Flow Rate (L/min)	Surface Loading Rate (L/min/m²)	Removal Efficiency (%)	Incremental Removal (%)	Cumulative Removal (%)
0.5	8.5	8.5	2.00	120.0	16.0	70	6.0	6.0
1	20.6	29.1	4.01	240.0	33.0	70	14.5	20.5
2	16.8	45.9	8.01	481.0	66.0	67	11.3	31.8
3	10.8	56.7	12.02	721.0	99.0	63	6.8	38.6
4	8.5	65.2	16.02	961.0	132.0	60	5.1	43.7
5	6.4	71.6	20.03	1202.0	165.0	57	3.7	47.3
6	5.5	77.0	24.03	1442.0	198.0	55	3.0	50.3
7	3.9	81.0	28.04	1682.0	230.0	53	2.1	52.4
8	2.9	83.9	32.05	1923.0	263.0	52	1.5	53.9
9	2.7	86.5	36.05	2163.0	296.0	51	1.4	55.3
10	2.2	88.7	40.06	2403.0	329.0	50	1.1	56.4
11	1.0	89.7	44.06	2644.0	362.0	49	0.5	56.9
12	1.7	91.3	48.07	2884.0	395.0	48	0.8	57.7
13	1.4	92.8	52.08	3125.0	428.0	47	0.7	58.3
14	1.0	93.7	56.08	3365.0	461.0	46	0.4	58.8
15	0.3	94.0	60.09	3605.0	494.0	45	0.1	58.9
16	0.8	94.8	64.09	3846.0	527.0	44	0.4	59.3
17	0.8	95.7	68.10	4086.0	560.0	43	0.4	59.6
18	0.2	95.8	72.10	4326.0	593.0	42	0.1	59.7
19	1.5	97.3	76.11	4567.0	626.0	42	0.6	60.3
20	0.2	97.5	80.12	4807.0	658.0	42	0.1	60.4
21	0.6	98.2	84.12	5047.0	691.0	42	0.3	60.7
22	0.0	98.2	88.13	5288.0	724.0	41	0.0	60.7
23	0.2	98.4	92.13	5528.0	757.0	41	0.1	60.8
24	0.2	98.6	96.14	5768.0	790.0	41	0.1	60.9
25	0.2	98.9	100.15	6009.0	823.0	41	0.1	61.0
30	1.1	100.0	120.17	7210.0	988.0	40	0.5	61.4
35	0.0	100.0	140.20	8412.0	1152.0	38	0.0	61.4
40	0.0	100.0	160.23	9614.0	1317.0	35	0.0	61.4
45	0.0	100.0	180.26	10816.0	1482.0	32	0.0	61.4
Estimated Net Annual Sediment (TSS) Load Reduction =								**61 %**

Climate Station ID: 6158731 *Years of Rainfall Data*: 20

RAINFALL DATA FROM TORONTO INTL AP RAINFALL STATION



INCREMENTAL AND CUMULATIVE TSS REMOVAL FOR THE RECOMMENDED STORMCEPTOR® MODEL



Maximum Pipe Diameter / Peak Conveyance

Stormceptor EF / EFO	Model Diameter		Min Angle Inlet / Outlet Pipes	Max Inlet Pipe Diameter		Max Outlet Pipe Diameter		Peak Conveyance Flow Rate	
	(m)	(ft)		(mm)	(in)	(mm)	(in)	(L/s)	(cfs)
EF4 / EFO4	1.2	4	90	609	24	609	24	425	15
EF6 / EFO6	1.8	6	90	914	36	914	36	990	35
EF8 / EFO8	2.4	8	90	1219	48	1219	48	1700	60
EF10 / EFO10	3.0	10	90	1828	72	1828	72	2830	100
EF12 / EFO12	3.6	12	90	1828	72	1828	72	2830	100

SCOUR PREVENTION AND ONLINE CONFIGURATION

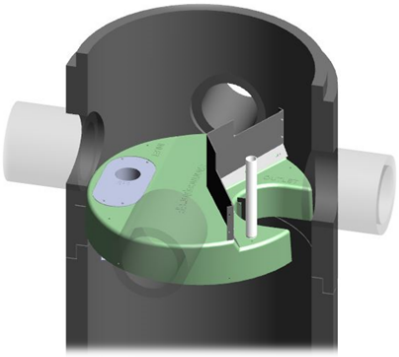
►**Stormceptor® EF and EFO** feature an internal bypass and superior scour prevention technology that have been demonstrated in third-party testing according to the scour testing provisions of the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators**, and the exceptional scour test performance has been third-party verified in accordance with the ISO 14034 ETV protocol. As a result, Stormceptor EF and EFO are approved for online installation, eliminating the need for costly additional bypass structures, piping, and installation expense.

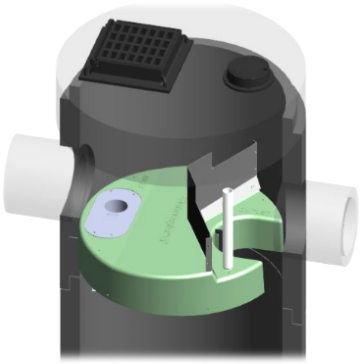
DESIGN FLEXIBILITY

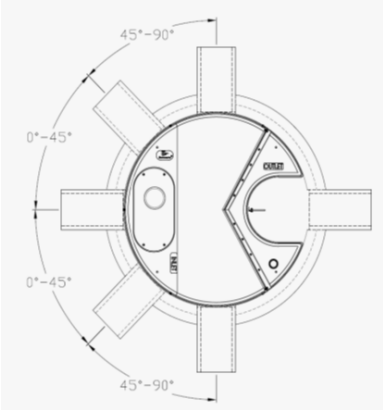
►**Stormceptor® EF** and **EFO** offers design flexibility in one simplified platform, accepting stormwater flow from a single inlet pipe or multiple inlet pipes, and/or surface runoff through an inlet grate. The device can also serve as a junction structure, accommodate a 90-degree inlet-to-outlet bend angle, and can be modified to ensure performance in submerged conditions.

OIL CAPTURE AND RETENTION

►While Stormceptor® EF will capture and retain oil from dry weather spills and low intensity runoff, **Stormceptor® EFO** has demonstrated superior oil capture and greater than 99% oil retention in third-party testing according to the light liquid re-entrainment testing provisions of the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators**. Stormceptor EFO is recommended for sites where oil capture and retention is a requirement.







INLET-TO-OUTLET DROP

Elevation differential between inlet and outlet pipe inverts is dictated by the angle at which the inlet pipe(s) enters the unit.

0° - 45° : The inlet pipe is 1-inch (25mm) higher than the outlet pipe.

45° - 90° : The inlet pipe is 2-inches (50mm) higher than the outlet pipe.

HEAD LOSS

The head loss through Stormceptor EF is similar to that of a 60-degree bend structure. The applicable K value for calculating minor losses through the unit is 1.1. For submerged conditions the applicable K value is 3.0.

Pollutant Capacity

Stormceptor EF / EFO	Model Diameter		Depth (Outlet Pipe Invert to Sump Floor)		Oil Volume		Recommended Sediment Maintenance Depth *		Maximum Sediment Volume *		Maximum Sediment Mass **	
	(m)	(ft)	(m)	(ft)	(L)	(Gal)	(mm)	(in)	(L)	(ft^3)	(kg)	(lb)
EF4 / EFO4	1.2	4	1.52	5.0	265	70	203	8	1190	42	1904	5250
EF6 / EFO6	1.8	6	1.93	6.3	610	160	305	12	3470	123	5552	15375
EF8 / EFO8	2.4	8	2.59	8.5	1070	280	610	24	8780	310	14048	38750
EF10 / EFO10	3.0	10	3.25	10.7	1670	440	610	24	17790	628	28464	78500
EF12 / EFO12	3.6	12	3.89	12.8	2475	655	610	24	31220	1103	49952	137875

*Increased sump depth may be added to increase sediment storage capacity

** Average density of wet packed sediment in sump = 1.6 kg/L (100 lb/ft^3)

Feature	Benefit	Feature Appeals To
Patent-pending enhanced flow treatment and scour prevention technology	Superior, verified third-party performance	Regulator, Specifying & Design Engineer
Third-party verified light liquid capture and retention for EFO version	Proven performance for fuel/oil hotspot locations	Regulator, Specifying & Design Engineer, Site Owner
Functions as bend, junction or inlet structure	Design flexibility	Specifying & Design Engineer
Minimal drop between inlet and outlet	Site installation ease	Contractor
Large diameter outlet riser for inspection and maintenance	Easy maintenance access from grade	Maintenance Contractor & Site Owner

STANDARD STORMCEPTOR EF/EFO DRAWINGS

For standard details, please visit http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef

STANDARD STORMCEPTOR EF/EFO SPECIFICATION

For specifications, please visit http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef

Table of TSS Removal vs Surface Loading Rate Based on Third-Party Test Results
Stormceptor® EFO

SLR (L/min/m²)	TSS % REMOVAL	SLR (L/min/m²)	TSS % REMOVAL	SLR (L/min/m²)	TSS % REMOVAL	SLR (L/min/m²)	TSS % REMOVAL
1	70	660	42	1320	35	1980	24
30	70	690	42	1350	35	2010	24
60	67	720	41	1380	34	2040	23
90	63	750	41	1410	34	2070	23
120	61	780	41	1440	33	2100	23
150	58	810	41	1470	32	2130	22
180	56	840	41	1500	32	2160	22
210	54	870	41	1530	31	2190	22
240	53	900	41	1560	31	2220	21
270	52	930	40	1590	30	2250	21
300	51	960	40	1620	29	2280	21
330	50	990	40	1650	29	2310	21
360	49	1020	40	1680	28	2340	20
390	48	1050	39	1710	28	2370	20
420	47	1080	39	1740	27	2400	20
450	47	1110	38	1770	27	2430	20
480	46	1140	38	1800	26	2460	19
510	45	1170	37	1830	26	2490	19
540	44	1200	37	1860	26	2520	19
570	43	1230	37	1890	25	2550	19
600	42	1260	36	1920	25	2580	18
630	42	1290	36	1950	24		

STANDARD PERFORMANCE SPECIFICATION FOR "OIL GRIT SEPARATOR" (OGS) STORMWATER QUALITY TREATMENT DEVICE

PART 1 – GENERAL

1.1 WORK INCLUDED

This section specifies requirements for selecting, sizing, and designing an underground Oil Grit Separator (OGS) device for stormwater quality treatment, with third-party testing results and a Statement of Verification in accordance with ISO 14034 Environmental Management – Environmental Technology Verification (ETV).

1.2 REFERENCE STANDARDS & PROCEDURES

ISO 14034:2016 Environmental management – Environmental technology verification (ETV)

Canadian Environmental Technology Verification (ETV) Program's **Procedure for Laboratory Testing of Oil-Grit Separators**

1.3 SUBMITTALS

1.3.1 All submittals, including sizing reports & shop drawings, shall be submitted upon request with each order to the contractor then forwarded to the Engineer of Record for review and acceptance. Shop drawings shall detail all OGS components, elevations, and sequence of construction.

1.3.2 Alternative devices shall have features identical to or greater than the specified device, including: treatment chamber diameter, treatment chamber wet volume, sediment storage volume, and oil storage volume.

1.3.3 Unless directed otherwise by the Engineer of Record, OGS stormwater quality treatment product substitutions or alternatives submitted within ten days prior to project bid shall not be accepted. All alternatives or substitutions submitted shall be signed and sealed by a local registered Professional Engineer, based on the exact same criteria detailed in Section 3, in entirety, subject to review and approval by the Engineer of Record.

PART 2 – PRODUCTS

2.1 OGS POLLUTANT STORAGE

The OGS device shall include a sump for sediment storage, and a protected volume for the capture and storage of petroleum hydrocarbons and buoyant gross pollutants. The minimum sediment & petroleum hydrocarbon storage capacity shall be as follows:

2.1.1	4 ft (1219 mm) Diameter OGS Units:	1.19 m^3 sediment / 265 L oil
	6 ft (1829 mm) Diameter OGS Units:	3.48 m^3 sediment / 609 L oil
	8 ft (2438 mm) Diameter OGS Units:	8.78 m^3 sediment / 1,071 L oil
	10 ft (3048 mm) Diameter OGS Units:	17.78 m^3 sediment / 1,673 L oil
	12 ft (3657 mm) Diameter OGS Units:	31.23 m^3 sediment / 2,476 L oil

PART 3 – PERFORMANCE & DESIGN

3.1 GENERAL

The OGS stormwater quality treatment device shall be verified in accordance with ISO 14034:2016 Environmental management – Environmental technology verification (ETV). The OGS stormwater quality treatment device shall

remove oil, sediment and gross pollutants from stormwater runoff during frequent wet weather events, and retain these pollutants during less frequent high flow wet weather events below the insert within the OGS for later removal during maintenance. The Manufacturer shall have at least ten (10) years of local experience, history and success in engineering design, manufacturing and production and supply of OGS stormwater quality treatment device systems, acceptable to the Engineer of Record.

3.2 SIZING METHODOLOGY

The OGS device shall be engineered, designed and sized to provide stormwater quality treatment based on treating a minimum of 90 percent of the average annual runoff volume and a minimum removal of an annual average 60% of the sediment (TSS) load based on the Particle Size Distribution (PSD) specified in the sizing report for the specified device. Sizing of the OGS shall be determined by use of a minimum ten (10) years of local historical rainfall data provided by Environment Canada. Sizing shall also be determined by use of the sediment removal performance data derived from the ISO 14034 ETV third-party verified laboratory testing data from testing conducted in accordance with the Canadian ETV protocol Procedure for Laboratory Testing of Oil-Grit Separators, as follows:

3.2.1 Sediment removal efficiency for a given surface loading rate and its associated flow rate shall be based on sediment removal efficiency demonstrated at the seven (7) tested surface loading rates specified in the protocol, ranging 40 L/min/m^2 to 1400 L/min/m^2, and as stated in the ISO 14034 ETV Verification Statement for the OGS device.

3.2.2 Sediment removal efficiency for surface loading rates between 40 L/min/m^2 and 1400 L/min/m^2 shall be based on linear interpolation of data between consecutive tested surface loading rates.

3.2.3 Sediment removal efficiency for surface loading rates less than the lowest tested surface loading rate of 40 L/min/m^2 shall be assumed to be identical to the sediment removal efficiency at 40 L/min/m^2. No extrapolation shall be allowed that results in a sediment removal efficiency that is greater than that demonstrated at 40 L/min/m^2.

3.2.4 Sediment removal efficiency for surface loading rates greater than the highest tested surface loading rate of 1400 L/min/m^2 shall assume zero sediment removal for the portion of flow that exceeds 1400 L/min/m^2, and shall be calculated using a simple proportioning formula, with 1400 L/min/m^2 in the numerator and the higher surface loading rate in the denominator, and multiplying the resulting fraction times the sediment removal efficiency at 1400 L/min/m^2.

The OGS device shall also have sufficient annual sediment storage capacity as specified and calculated in Section 2.1.

3.3 CANADIAN ETV or ISO 14034 ETV VERIFICATION OF SCOUR TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of third-party scour testing conducted in accordance with the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators.**

3.3.1 To be acceptable for on-line installation, the OGS device must demonstrate an average scour test effluent concentration less than 10 mg/L at each surface loading rate tested, up to and including 2600 L/min/m^2.

3.4 LIGHT LIQUID RE-ENTRAINMENT SIMULATION TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of completed third-party Light Liquid Re-entrainment Simulation Testing in accordance with the Canadian ETV **Program's Procedure for Laboratory Testing of Oil-Grit Separators,** with results reported within the Canadian ETV or ISO 14034 ETV verification. This re-entrainment testing is conducted with the device pre-loaded with low density polyethylene (LDPE) plastic beads as a surrogate for light liquids such as oil and fuel. Testing is conducted on the same OGS unit tested for sediment removal to

assess whether light liquids captured after a spill are effectively retained at high flow rates.

3.4.1 For an OGS device to be an acceptable stormwater treatment device on a site where vehicular traffic occurs and the potential for an oil or fuel spill exists, the OGS device must have reported verified performance results of greater than 99% cumulative retention of LDPE plastic beads for the five specified surface loading rates (ranging 200 L/min/m^2 to 2600 L/min/m^2) in accordance with the Light Liquid Re-entrainment Simulation Testing within the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators.** However, an OGS device shall not be allowed if the Light Liquid Re-entrainment Simulation Testing was performed with screening components within the OGS device that are effective at retaining the LDPE plastic beads, but would not be expected to retain light liquids such as oil and fuel.

Stormceptor®

FORTERRA

Stormceptor® EF Sizing Report

STORMCEPTOR®
ESTIMATED NET ANNUAL SEDIMENT (TSS) LOAD REDUCTION

03/14/2023

Province:	Ontario
City:	Alton
Nearest Rainfall Station:	TORONTO INTL AP
Climate Station Id:	6158731
Years of Rainfall Data:	20

Site Name:	Agnes St Area 202
Drainage Area (ha):	1.705
% Imperviousness:	42.40

Runoff Coefficient 'c': 0.55

Particle Size Distribution:	CA ETV
Target TSS Removal (%):	65.0

Required Water Quality Runoff Volume Capture (%):	90.00
Estimated Water Quality Flow Rate (L/s):	29.39
Oil / Fuel Spill Risk Site?	Yes
Upstream Flow Control?	No
Peak Conveyance (maximum) Flow Rate (L/s):	
Site Sediment Transport Rate (kg/ha/yr):	

Project Name:	Agnes Street
Project Number:	20-731
Designer Name:	Jennifer Chan
Designer Company:	Greck
Designer Email:	jchan@greck.ca
Designer Phone:	289-657-9797
EOR Name:	
EOR Company:	
EOR Email:	
EOR Phone:	

Net Annual Sediment (TSS) Load Reduction Sizing Summary

Stormceptor Model	TSS Removal Provided (%)
EFO4	48
EFO6	56
EFO8	61
EFO10	64
EFO12	66

Recommended Stormceptor EFO Model: EFO12

Estimated Net Annual Sediment (TSS) Load Reduction (%): 66

Water Quality Runoff Volume Capture (%): > 90

imbrium

THIRD-PARTY TESTING AND VERIFICATION

►**Stormceptor® EF and Stormceptor® EFO** are the latest evolutions in the Stormceptor® oil-grit separator (OGS) technology series, and are designed to remove a wide variety of pollutants from stormwater and snowmelt runoff. These technologies have been third-party tested in accordance with the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators** and performance has been third-party verified in accordance with the **ISO 14034 Environmental Technology Verification (ETV)** protocol.

PERFORMANCE

►**Stormceptor® EF and EFO** remove stormwater pollutants through gravity separation and floatation, and feature a patent-pending design that generates positive removal of total suspended solids (TSS) throughout each storm event, including high-intensity storms. Captured pollutants include sediment, free oils, and sediment-bound pollutants such as nutrients, heavy metals, and petroleum hydrocarbons. Stormceptor is sized to remove a high level of TSS from the frequent rainfall events that contribute the vast majority of annual runoff volume and pollutant load. The technology incorporates an internal bypass to convey excessive stormwater flows from high-intensity storms through the device without resuspension and washout (scour) of previously captured pollutants. Proper routine maintenance ensures high pollutant removal performance and protection of downstream waterwavs.

PARTICLE SIZE DISTRIBUTION (PSD)

►The **Canadian ETV PSD** shown in the table below was used, or in part, for this sizing. This is the identical PSD that is referenced in the Canadian ETV ***Procedure for Laboratory Testing of Oil-Grit Separators*** for both sediment removal testing and scour testing. The Canadian ETV PSD contains a wide range of particle sizes in the sand and silt fractions, and is considered reasonably representative of the particle size fractions found in typical urban stormwater runoff.

Particle Size (µm)	Percent Less Than	Particle Size Fraction (µm)	Percent
1000	100	500-1000	5
500	95	250-500	5
250	90	150-250	15
150	75	100-150	15
100	60	75-100	10
75	50	50-75	5
50	45	20-50	10
20	35	8-20	15
8	20	5-8	10
5	10	2-5	5
2	5	<2	5

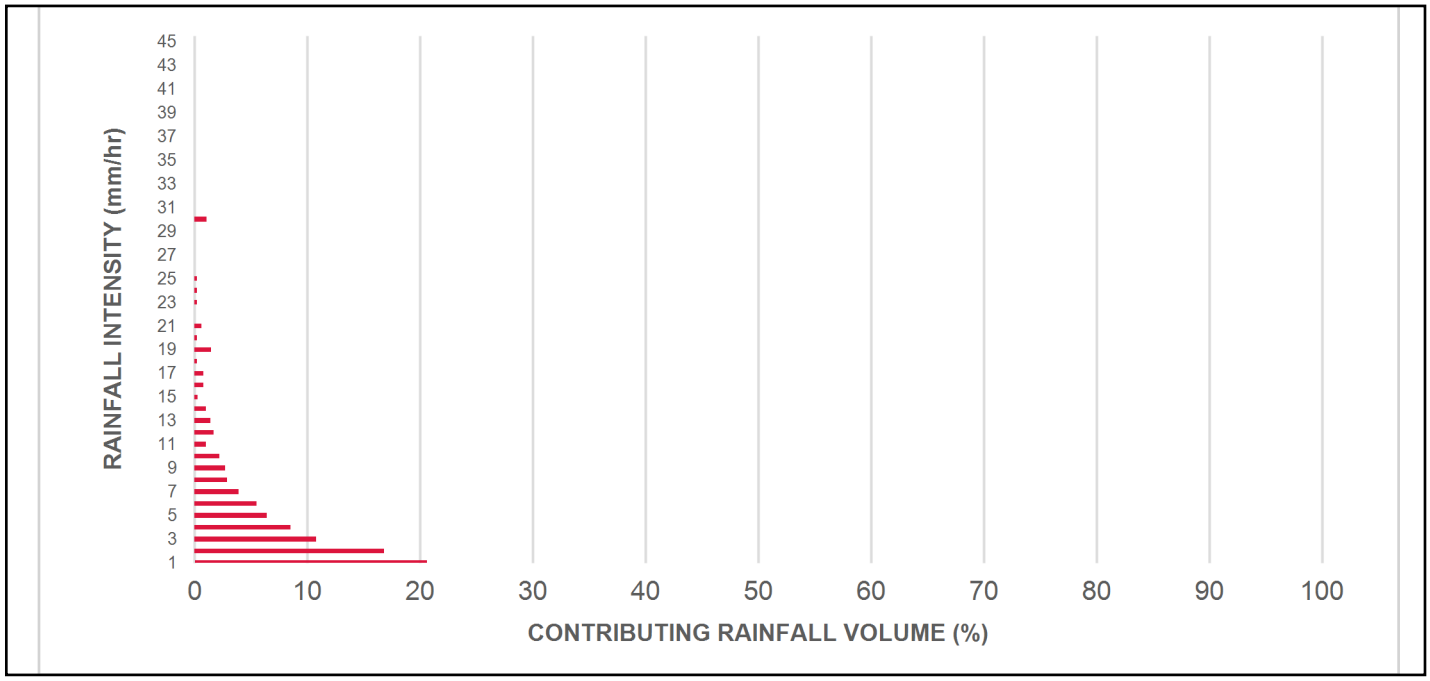
imbrium

Stormceptor® EF Sizing Report

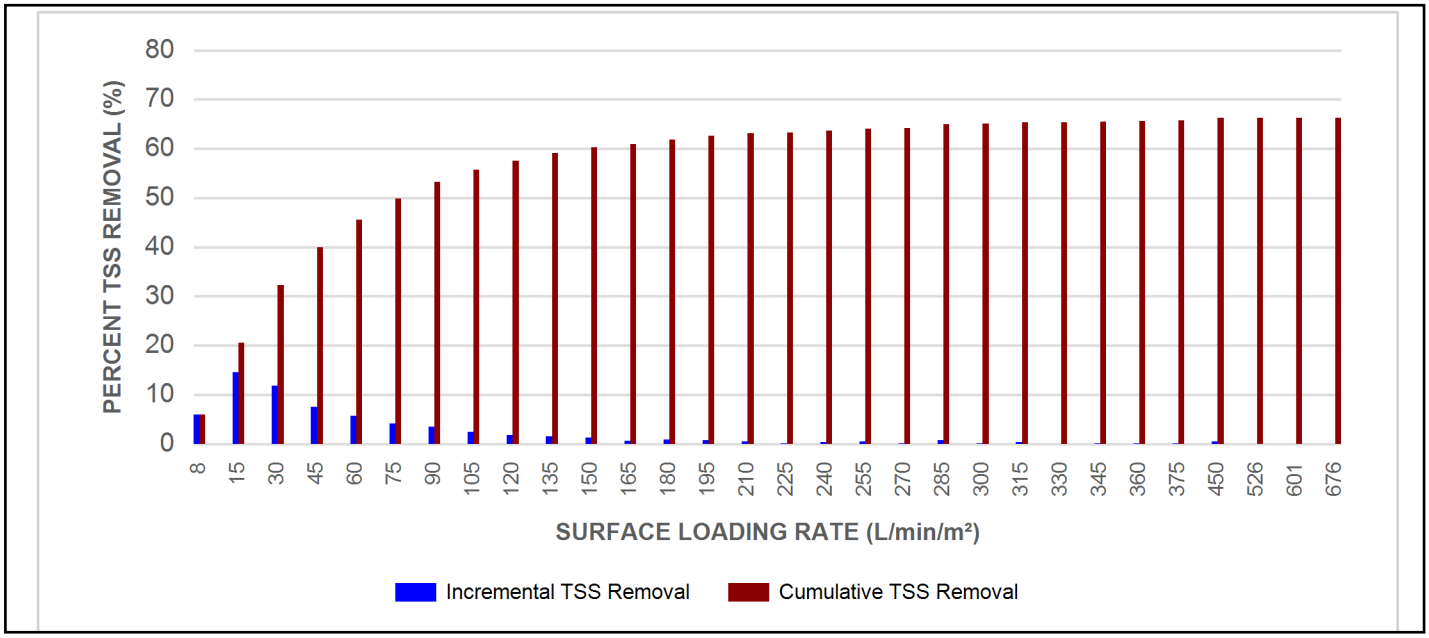
Rainfall Intensity (mm / hr)	Percent Rainfall Volume (%)	Cumulative Rainfall Volume (%)	Flow Rate (L/s)	Flow Rate (L/min)	Surface Loading Rate (L/min/m²)	Removal Efficiency (%)	Incremental Removal (%)	Cumulative Removal (%)
0.5	8.5	8.5	1.31	79.0	8.0	70	6.0	6.0
1	20.6	29.1	2.63	158.0	15.0	70	14.5	20.5
2	16.8	45.9	5.26	315.0	30.0	70	11.8	32.3
3	10.8	56.7	7.88	473.0	45.0	70	7.6	39.9
4	8.5	65.2	10.51	631.0	60.0	67	5.7	45.6
5	6.4	71.6	13.14	788.0	75.0	66	4.2	49.8
6	5.5	77.0	15.77	946.0	90.0	63	3.4	53.2
7	3.9	81.0	18.39	1104.0	105.0	62	2.5	55.7
8	2.9	83.9	21.02	1261.0	120.0	61	1.8	57.5
9	2.7	86.5	23.65	1419.0	135.0	60	1.6	59.1
10	2.2	88.7	26.28	1577.0	150.0	58	1.3	60.3
11	1.0	89.7	28.91	1734.0	165.0	57	0.6	60.9
12	1.7	91.3	31.53	1892.0	180.0	56	0.9	61.8
13	1.4	92.8	34.16	2050.0	195.0	55	0.8	62.6
14	1.0	93.7	36.79	2207.0	210.0	54	0.5	63.1
15	0.3	94.0	39.42	2365.0	225.0	53	0.2	63.3
16	0.8	94.8	42.04	2523.0	240.0	53	0.4	63.7
17	0.8	95.7	44.67	2680.0	255.0	53	0.4	64.1
18	0.2	95.8	47.30	2838.0	270.0	52	0.1	64.2
19	1.5	97.3	49.93	2996.0	285.0	52	0.8	65.0
20	0.2	97.5	52.56	3153.0	300.0	51	0.1	65.1
21	0.6	98.2	55.18	3311.0	315.0	51	0.3	65.4
22	0.0	98.2	57.81	3469.0	330.0	50	0.0	65.4
23	0.2	98.4	60.44	3626.0	345.0	50	0.1	65.5
24	0.2	98.6	63.07	3784.0	360.0	49	0.1	65.6
25	0.2	98.9	65.70	3942.0	375.0	49	0.1	65.8
30	1.1	100.0	78.83	4730.0	450.0	47	0.5	66.3
35	0.0	100.0	91.97	5518.0	526.0	44	0.0	66.3
40	0.0	100.0	105.11	6307.0	601.0	42	0.0	66.3
45	0.0	100.0	118.25	7095.0	676.0	42	0.0	66.3
Estimated Net Annual Sediment (TSS) Load Reduction =								**66 %**

Climate Station ID: 6158731 *Years of Rainfall Data*: 20

RAINFALL DATA FROM TORONTO INTL AP RAINFALL STATION



INCREMENTAL AND CUMULATIVE TSS REMOVAL FOR THE RECOMMENDED STORMCEPTOR® MODEL



Maximum Pipe Diameter / Peak Conveyance

Stormceptor EF / EFO	Model Diameter		Min Angle Inlet / Outlet Pipes	Max Inlet Pipe Diameter		Max Outlet Pipe Diameter		Peak Conveyance Flow Rate	
	(m)	(ft)		(mm)	(in)	(mm)	(in)	(L/s)	(cfs)
EF4 / EFO4	1.2	4	90	609	24	609	24	425	15
EF6 / EFO6	1.8	6	90	914	36	914	36	990	35
EF8 / EFO8	2.4	8	90	1219	48	1219	48	1700	60
EF10 / EFO10	3.0	10	90	1828	72	1828	72	2830	100
EF12 / EFO12	3.6	12	90	1828	72	1828	72	2830	100

SCOUR PREVENTION AND ONLINE CONFIGURATION

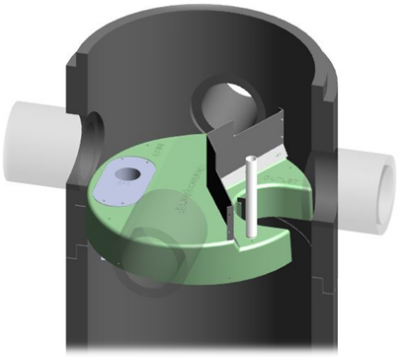
►**Stormceptor® EF and EFO** feature an internal bypass and superior scour prevention technology that have been demonstrated in third-party testing according to the scour testing provisions of the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators**, and the exceptional scour test performance has been third-party verified in accordance with the ISO 14034 ETV protocol. As a result, Stormceptor EF and EFO are approved for online installation, eliminating the need for costly additional bypass structures, piping, and installation expense.

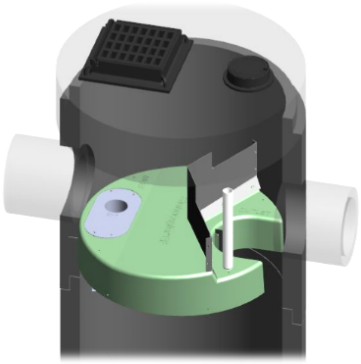
DESIGN FLEXIBILITY

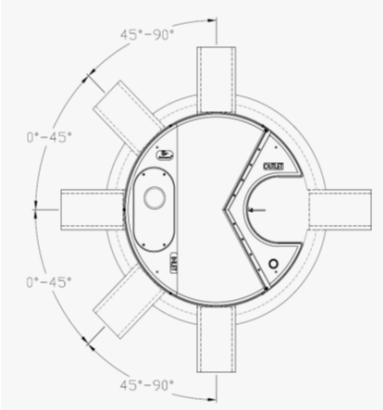
►**Stormceptor® EF** and **EFO** offers design flexibility in one simplified platform, accepting stormwater flow from a single inlet pipe or multiple inlet pipes, and/or surface runoff through an inlet grate. The device can also serve as a junction structure, accommodate a 90-degree inlet-to-outlet bend angle, and can be modified to ensure performance in submerged conditions.

OIL CAPTURE AND RETENTION

►While Stormceptor® EF will capture and retain oil from dry weather spills and low intensity runoff, **Stormceptor® EFO** has demonstrated superior oil capture and greater than 99% oil retention in third-party testing according to the light liquid re-entrainment testing provisions of the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators**. Stormceptor EFO is recommended for sites where oil capture and retention is a requirement.







INLET-TO-OUTLET DROP

Elevation differential between inlet and outlet pipe inverts is dictated by the angle at which the inlet pipe(s) enters the unit.

0° - 45° : The inlet pipe is 1-inch (25mm) higher than the outlet pipe.

45° - 90° : The inlet pipe is 2-inches (50mm) higher than the outlet pipe.

HEAD LOSS

The head loss through Stormceptor EF is similar to that of a 60-degree bend structure. The applicable K value for calculating minor losses through the unit is 1.1. For submerged conditions the applicable K value is 3.0.

Pollutant Capacity

Stormceptor EF / EFO	Model Diameter		Depth (Outlet Pipe Invert to Sump Floor)		Oil Volume		Recommended Sediment Maintenance Depth *		Maximum Sediment Volume *		Maximum Sediment Mass **	
	(m)	(ft)	(m)	(ft)	(L)	(Gal)	(mm)	(in)	(L)	(ft^3)	(kg)	(lb)
EF4 / EFO4	1.2	4	1.52	5.0	265	70	203	8	1190	42	1904	5250
EF6 / EFO6	1.8	6	1.93	6.3	610	160	305	12	3470	123	5552	15375
EF8 / EFO8	2.4	8	2.59	8.5	1070	280	610	24	8780	310	14048	38750
EF10 / EFO10	3.0	10	3.25	10.7	1670	440	610	24	17790	628	28464	78500
EF12 / EFO12	3.6	12	3.89	12.8	2475	655	610	24	31220	1103	49952	137875

*Increased sump depth may be added to increase sediment storage capacity

** Average density of wet packed sediment in sump = 1.6 kg/L (100 lb/ft^3)

Feature	Benefit	Feature Appeals To
Patent-pending enhanced flow treatment and scour prevention technology	Superior, verified third-party performance	Regulator, Specifying & Design Engineer
Third-party verified light liquid capture and retention for EFO version	Proven performance for fuel/oil hotspot locations	Regulator, Specifying & Design Engineer, Site Owner
Functions as bend, junction or inlet structure	Design flexibility	Specifying & Design Engineer
Minimal drop between inlet and outlet	Site installation ease	Contractor
Large diameter outlet riser for inspection and maintenance	Easy maintenance access from grade	Maintenance Contractor & Site Owner

STANDARD STORMCEPTOR EF/EFO DRAWINGS

For standard details, please visit http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef

STANDARD STORMCEPTOR EF/EFO SPECIFICATION

For specifications, please visit http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef

Table of TSS Removal vs Surface Loading Rate Based on Third-Party Test Results
Stormceptor® EFO

SLR (L/min/m²)	TSS % REMOVAL	SLR (L/min/m²)	TSS % REMOVAL	SLR (L/min/m²)	TSS % REMOVAL	SLR (L/min/m²)	TSS % REMOVAL
1	70	660	42	1320	35	1980	24
30	70	690	42	1350	35	2010	24
60	67	720	41	1380	34	2040	23
90	63	750	41	1410	34	2070	23
120	61	780	41	1440	33	2100	23
150	58	810	41	1470	32	2130	22
180	56	840	41	1500	32	2160	22
210	54	870	41	1530	31	2190	22
240	53	900	41	1560	31	2220	21
270	52	930	40	1590	30	2250	21
300	51	960	40	1620	29	2280	21
330	50	990	40	1650	29	2310	21
360	49	1020	40	1680	28	2340	20
390	48	1050	39	1710	28	2370	20
420	47	1080	39	1740	27	2400	20
450	47	1110	38	1770	27	2430	20
480	46	1140	38	1800	26	2460	19
510	45	1170	37	1830	26	2490	19
540	44	1200	37	1860	26	2520	19
570	43	1230	37	1890	25	2550	19
600	42	1260	36	1920	25	2580	18
630	42	1290	36	1950	24		

STANDARD PERFORMANCE SPECIFICATION FOR "OIL GRIT SEPARATOR" (OGS) STORMWATER QUALITY TREATMENT DEVICE

PART 1 – GENERAL

1.1 WORK INCLUDED

This section specifies requirements for selecting, sizing, and designing an underground Oil Grit Separator (OGS) device for stormwater quality treatment, with third-party testing results and a Statement of Verification in accordance with ISO 14034 Environmental Management – Environmental Technology Verification (ETV).

1.2 REFERENCE STANDARDS & PROCEDURES

ISO 14034:2016 Environmental management – Environmental technology verification (ETV)

Canadian Environmental Technology Verification (ETV) Program's **Procedure for Laboratory Testing of Oil-Grit Separators**

1.3 SUBMITTALS

1.3.1 All submittals, including sizing reports & shop drawings, shall be submitted upon request with each order to the contractor then forwarded to the Engineer of Record for review and acceptance. Shop drawings shall detail all OGS components, elevations, and sequence of construction.

1.3.2 Alternative devices shall have features identical to or greater than the specified device, including: treatment chamber diameter, treatment chamber wet volume, sediment storage volume, and oil storage volume.

1.3.3 Unless directed otherwise by the Engineer of Record, OGS stormwater quality treatment product substitutions or alternatives submitted within ten days prior to project bid shall not be accepted. All alternatives or substitutions submitted shall be signed and sealed by a local registered Professional Engineer, based on the exact same criteria detailed in Section 3, in entirety, subject to review and approval by the Engineer of Record.

PART 2 – PRODUCTS

2.1 OGS POLLUTANT STORAGE

The OGS device shall include a sump for sediment storage, and a protected volume for the capture and storage of petroleum hydrocarbons and buoyant gross pollutants. The minimum sediment & petroleum hydrocarbon storage capacity shall be as follows:

2.1.1	4 ft (1219 mm) Diameter OGS Units:	1.19 m^3 sediment / 265 L oil
	6 ft (1829 mm) Diameter OGS Units:	3.48 m^3 sediment / 609 L oil
	8 ft (2438 mm) Diameter OGS Units:	8.78 m^3 sediment / 1,071 L oil
	10 ft (3048 mm) Diameter OGS Units:	17.78 m^3 sediment / 1,673 L oil
	12 ft (3657 mm) Diameter OGS Units:	31.23 m^3 sediment / 2,476 L oil

PART 3 – PERFORMANCE & DESIGN

3.1 GENERAL

The OGS stormwater quality treatment device shall be verified in accordance with ISO 14034:2016 Environmental management – Environmental technology verification (ETV). The OGS stormwater quality treatment device shall

remove oil, sediment and gross pollutants from stormwater runoff during frequent wet weather events, and retain these pollutants during less frequent high flow wet weather events below the insert within the OGS for later removal during maintenance. The Manufacturer shall have at least ten (10) years of local experience, history and success in engineering design, manufacturing and production and supply of OGS stormwater quality treatment device systems, acceptable to the Engineer of Record.

3.2 SIZING METHODOLOGY

The OGS device shall be engineered, designed and sized to provide stormwater quality treatment based on treating a minimum of 90 percent of the average annual runoff volume and a minimum removal of an annual average 60% of the sediment (TSS) load based on the Particle Size Distribution (PSD) specified in the sizing report for the specified device. Sizing of the OGS shall be determined by use of a minimum ten (10) years of local historical rainfall data provided by Environment Canada. Sizing shall also be determined by use of the sediment removal performance data derived from the ISO 14034 ETV third-party verified laboratory testing data from testing conducted in accordance with the Canadian ETV protocol Procedure for Laboratory Testing of Oil-Grit Separators, as follows:

3.2.1 Sediment removal efficiency for a given surface loading rate and its associated flow rate shall be based on sediment removal efficiency demonstrated at the seven (7) tested surface loading rates specified in the protocol, ranging 40 L/min/m^2 to 1400 L/min/m^2, and as stated in the ISO 14034 ETV Verification Statement for the OGS device.

3.2.2 Sediment removal efficiency for surface loading rates between 40 L/min/m^2 and 1400 L/min/m^2 shall be based on linear interpolation of data between consecutive tested surface loading rates.

3.2.3 Sediment removal efficiency for surface loading rates less than the lowest tested surface loading rate of 40 L/min/m^2 shall be assumed to be identical to the sediment removal efficiency at 40 L/min/m^2. No extrapolation shall be allowed that results in a sediment removal efficiency that is greater than that demonstrated at 40 L/min/m^2.

3.2.4 Sediment removal efficiency for surface loading rates greater than the highest tested surface loading rate of 1400 L/min/m^2 shall assume zero sediment removal for the portion of flow that exceeds 1400 L/min/m^2, and shall be calculated using a simple proportioning formula, with 1400 L/min/m^2 in the numerator and the higher surface loading rate in the denominator, and multiplying the resulting fraction times the sediment removal efficiency at 1400 L/min/m^2.

The OGS device shall also have sufficient annual sediment storage capacity as specified and calculated in Section 2.1.

3.3 CANADIAN ETV or ISO 14034 ETV VERIFICATION OF SCOUR TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of third-party scour testing conducted in accordance with the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators.**

3.3.1 To be acceptable for on-line installation, the OGS device must demonstrate an average scour test effluent concentration less than 10 mg/L at each surface loading rate tested, up to and including 2600 L/min/m^2.

3.4 LIGHT LIQUID RE-ENTRAINMENT SIMULATION TESTING

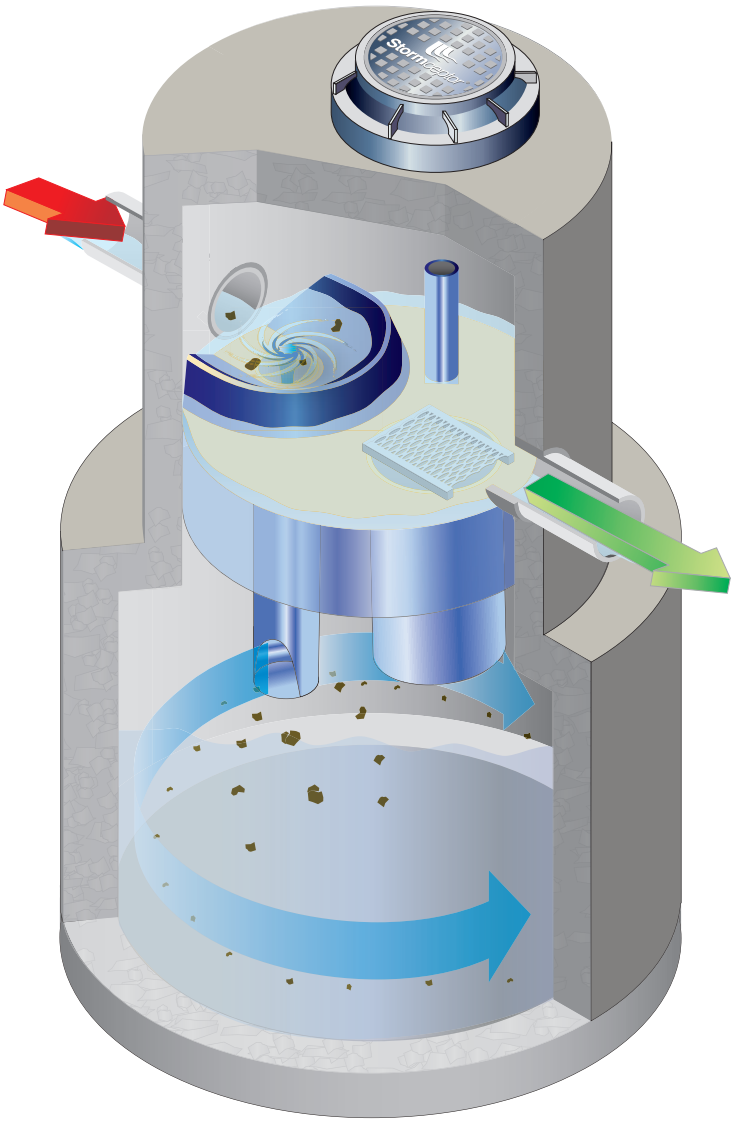
The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of completed third-party Light Liquid Re-entrainment Simulation Testing in accordance with the Canadian ETV **Program's Procedure for Laboratory Testing of Oil-Grit Separators,** with results reported within the Canadian ETV or ISO 14034 ETV verification. This re-entrainment testing is conducted with the device pre-loaded with low density polyethylene (LDPE) plastic beads as a surrogate for light liquids such as oil and fuel. Testing is conducted on the same OGS unit tested for sediment removal to

assess whether light liquids captured after a spill are effectively retained at high flow rates.

3.4.1 For an OGS device to be an acceptable stormwater treatment device on a site where vehicular traffic occurs and the potential for an oil or fuel spill exists, the OGS device must have reported verified performance results of greater than 99% cumulative retention of LDPE plastic beads for the five specified surface loading rates (ranging 200 L/min/m^2 to 2600 L/min/m^2) in accordance with the Light Liquid Re-entrainment Simulation Testing within the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators.** However, an OGS device shall not be allowed if the Light Liquid Re-entrainment Simulation Testing was performed with screening components within the OGS device that are effective at retaining the LDPE plastic beads, but would not be expected to retain light liquids such as oil and fuel.

Stormceptor®

Owner's Manual



Stormceptor is protected by one or more of the following patents:

Canadian Patent No. 2,137,942
Canadian Patent No. 2,175,277
Canadian Patent No. 2,180,305
Canadian Patent No. 2,180,338
Canadian Patent No. 2,206,338
Canadian Patent No. 2,327,768
U.S. Patent No. 5,753,115
U.S. Patent No. 5,849,181
U.S. Patent No. 6,068,765
U.S. Patent No. 6,371,690
U.S. Patent No. 7,582,216
U.S. Patent No. 7,666,303
Australia Patent No. 693.164
Australia Patent No. 707,133
Australia Patent No. 729,096
Australia Patent No. 779,401
Australia Patent No. 2008,279,378
Australia Patent No. 2008,288,900
Indonesia Patent No. 0007058
Japan Patent No. 3581233
Japan Patent No. 9-11476
Korean Patent No. 0519212
Malaysia Patent No. 118987
New Zealand Patent No. 314,646
New Zealand Patent No. 583,008
New Zealand Patent No. 583,583
South African Patent No. 2010/00682
South African Patent No. 2010/01796
Other Patents Pending

Table of Contents

Congratulations!

Your selection of a Stormceptor® means that you have chosen the most recognized and efficient stormwater oil/sediment separator available for protecting the environment. Stormceptor is a pollution control device often referred to as a “Hydrodynamic Separator (HDS)” or an “Oil Grit Separator (OGS)”, engineered to remove and retain pollutants from stormwater runoff to protect our lakes, rivers and streams from the harmful effects of non-point source pollution.

1 – Stormceptor Overview

Stormceptor is a patented stormwater quality structure most often utilized as a treatment component of the underground storm drain network for stormwater pollution prevention. Stormceptor is designed to remove sediment, total suspended solids (TSS), other pollutants attached to sediment, hydrocarbons and free oil from stormwater runoff. Collectively the Stormceptor provides spill protection and prevents non-point source pollution from entering downstream waterways.

Key benefits of Stormceptor include:

- Removes sediment, suspended solids, debris, nutrients, heavy metals, and hydrocarbons (oil and grease) from runoff and snowmelt.
- Will not scour or re-suspend trapped pollutants.
- Provides sediment and oil storage.
- Provides spill control for accidents, commercial and industrial developments.
- Easy to inspect and maintain (vacuum truck).
- “STORMCEPTOR” is *clearly* marked on the access cover (excluding inlet designs).
- Relatively small footprint.
- 3rd Party tested and independently verified.
- Dedicated team of experts available to provide support.

Model Types:

- STC (Standard)
- STF (Fiberglass)
- EOS (Extended Oil Storage)
- OSR (Oil and Sand Removal)
- MAX (Custom designed unit, specific to site)

Configuration Types:

- Inlet unit (accommodates inlet flow entry, and multi-pipe entry)
- In-Line (accommodates multi-pipe entry)
- Submerged Unit (accommodates the site’s tailwater conditions)
- Series Unit (combines treatment in two systems)

Please Maintain Your Stormceptor

To ensure long-term environmental protection through continued performance as originally designed for your site, **Stormceptor must be maintained**, as any stormwater treatment practice does. The need for maintenance is determined through inspection of the Stormceptor. Procedures for inspection are provided within this document. Maintenance of the Stormceptor is performed from the surface via vacuum truck.

If you require information about Stormceptor, or assistance in finding resources to facilitate inspections or maintenance of your Stormceptor please call your local Stormceptor Licensee or Imbrium® Systems.

2 – Stormceptor Operation & Components

Stormceptor is a flexibly designed underground stormwater quality treatment device that is unparalleled in its effectiveness for pollutant capture and retention using patented flow separation technology.

Stormceptor creates a non-turbulent treatment environment below the insert platform within the system. The insert diverts water into the lower chamber, allowing free oils and debris to rise, and sediment to settle under relatively low velocity conditions. These pollutants are trapped and stored below the insert and protected from large runoff events for later removal during the maintenance procedure.

With thousands of units operating worldwide, Stormceptor delivers reliable protection every day, in every storm. The patented Stormceptor design prohibits the scour and release of captured pollutants, ensuring superior water quality treatment and protection during even the most extreme storm events. Stormceptor's proven performance is backed by the longest record of lab and field verification in the industry.

Stormceptor Schematic and Component Functions

Below are schematics of two common Stormceptor configurations with key components identified and their functions briefly described.

Figure 1.

Inline Stormceptor

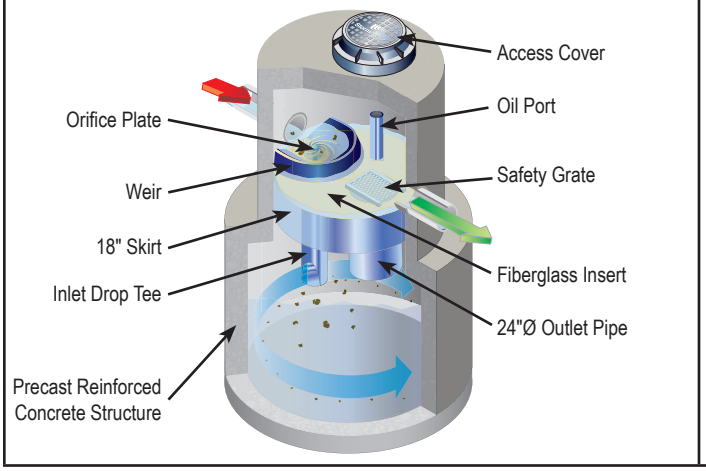
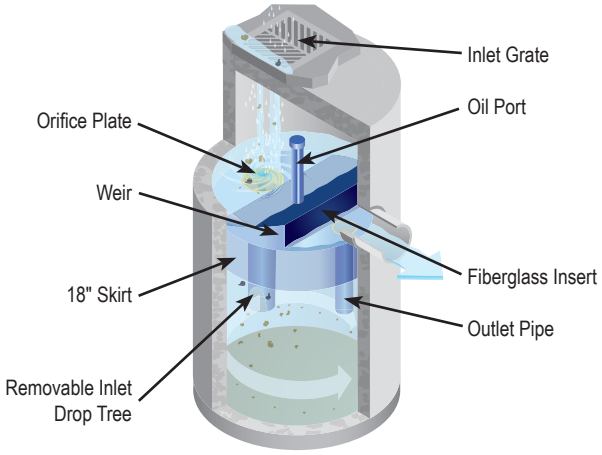


Figure 2.

Inlet Stormceptor



- **Manhole access cover** – provides access to the subsurface components
- **Precast reinforced concrete structure** – provides the vessel's watertight structural support
- **Fiberglass insert** – separates vessel into upper and lower chambers
- **Weir** – directs incoming stormwater and oil spills into the lower chamber
- **Orifice plate** – prevents scour of accumulated pollutants
- **Inlet drop tee** – conveys stormwater into the lower chamber
- **Fiberglass skirt** – provides double-wall containment of hydrocarbons
- **Outlet riser pipe** – conveys treated water to the upper chamber; primary vacuum line access port for sediment removal
- **Oil inspection port** – primary access for measuring oil depth and oil removal
- **Safety grate** – safety measure to cover riser pipe in the event of manned entry into vessel

3 – Stormceptor Identification

Stormceptor is available in both precast concrete and fiberglass vessels, with precast concrete often being the dominant material of construction.

In the Stormceptor, a patented, engineered fiberglass insert separates the structure into an upper chamber and lower chamber. The lower chamber will remain full of water, as this is where the pollutants are sequestered for later removal. Multiple Stormceptor model (STC, OSR, EOS, MAX and STF) configurations exist, each to be inspected and maintained in a similar fashion.

Each unit is easily identifiable as a Stormceptor by the trade name "Stormceptor" embossed on each access cover at the surface. To determine the location of "inlet" Stormceptor units with horizontal catch basin inlet, look down into the grate as the Stormceptor insert will be visible. The name "Stormceptor" is not embossed on inlet models due to the variability of inlet grates used/ approved across North America.

Once the location of the Stormceptor is determined, the model number may be identified by comparing the measured depth from the fiberglass insert level at the outlet pipe's invert (water level) to the bottom of the tank using **Table 1**.

In addition, starting in 1996 a metal serial number tag containing the model number has been affixed to the inside of the unit, on the fiberglass insert. If the unit does not have a serial number, or if there is any uncertainty regarding the size of the unit using depth measurements, please contact your local Stormceptor Representative for assistance.

Sizes/Models

Typical general dimensions and capacities of the standard precast STC, EOS & OSR Stormceptor models in both USA and Canada/International (excluding South East Asia and Australia) are provided in **Tables 1 and 2**. Typical rim to invert measurements are provided later in this document. The total depth for cleaning will be the sum of the depth from outlet pipe invert (generally the water level) to rim (grade) and the depth from outlet pipe invert to the precast bottom of the unit. Note that depths and capacities may vary slightly between regions.

Table 1A. (US) Stormceptor Dimensions – Insert to Base of Structure

STC Model	Insert to Base (in.)
450	60
900	55
1200	71
1800	105
2400	94
3600	134
4800	128
6000	150
7200	134
11000*	128
13000*	150
16000*	134

EOS Model	Insert to Base (in.)
4-175	60
9-365	55
12-590	71
18-1000	105
24-1400	94
36-1700	134
48-2000	128
60-2500	150
72-3400	134
110-5000*	128
130-6000*	150
160-7800*	134

OSR Model	Insert to Base (in.)
65	60
140	55
250	94
390	128
560	134
780*	128
1125*	134

Typical STF m (in.)
1.5 (60)
1.5 (61)
1.8 (73)
2.9 (115)
2.3 (89)
3.2 (127)
2.9 (113)
3.5 (138)
3.3 (128)

Notes:

1. *Depth Below Pipe Inlet Invert to the Bottom of Base Slab can vary slightly by manufacturing facility, and can be modified to accommodate specific site designs, pollutant loads or site conditions. Contact your local representative for assistance.*

**Consist of two chamber structures in series.*

Table 1B. (CA & Int'l) Stormceptor Dimensions – Insert to Base of Structure

STC Model	Insert to Base (m)
300	1.5
750	1.5
1000	1.8
1500	2.8
2000	2.8
3000	3.7
4000	3.4
5000	4.0
6000	3.7
9000*	3.4
11000*	4.0
14000*	3.7

EOS Model	Insert to Base (m)
300	1.5
750	1.5
1000	1.8
2000	2.8
3000	3.7
4000	3.4
5000	4.0
6000	3.7
9000*	3.4
10000*	4.0
14000*	3.7

OSR Model	Insert to Base (m)
300	1.7
750	1.6
2000	2.6
4000	3.6
6000	3.7
9000*	3.6
14000*	3.7

Typical STF m (in.)
1.5 (60)
1.5 (61)
1.8 (73)
2.9 (115)
2.3 (89)
3.2 (127)
2.9 (113)
3.5 (138)
3.3 (128)

Notes:

1. *Depth Below Pipe Inlet Invert to the Bottom of Base Slab can vary slightly by manufacturing facility, and can be modified to accommodate specific site designs, pollutant loads or site conditions. Contact your local representative for assistance.*

**Consist of two chamber structures in series.*

Table 2A. (US) Storage Capacities

STC Model	Hydrocarbon Storage Capacity gal	Sediment Capacity ft^3	**EOS Model**	Hydrocarbon Storage Capacity gal	**OSR Model**	Hydrocarbon Storage Capacity gal	Sediment Capacity ft^3
450	86	46	**4-175**	175	**065**	115	46
900	251	89	**9-365**	365	**140**	233	58
1200	251	127	**12-590**	591			
1800	251	207	**18-1000**	1198			
2400	840	205	**24-1400**	1457	**250**	792	156
3600	840	373	**36-1700**	1773			
4800	909	543	**48-2000**	2005	**390**	1233	465
6000	909	687	**60-2500**	2514			
7200	1059	839	**72-3400**	3418	**560**	1384	690
11000*	2797	1089	**110-5000***	5023	**780***	2430	930
13000*	2797	1374	**130-6000***	6041			
16000*	3055	1677	**160-7800***	7850	**1125***	2689	1378

Notes:

1. *Hydrocarbon & Sediment capacities can be modified to accommodate specific site design requirements, contact your local representative for assistance.*

**Consist of two chamber structures in series.*

Table 2B. (CA & Int'l) Storage Capacities

STC Model	Hydrocarbon Storage Capacity L	Sediment Capacity L	EOS Model	Hydrocarbon Storage Capacity L	OSR Model	Hydrocarbon Storage Capacity L	Sediment Capacity L
300	300	1450	**300**	662	**300**	300	1500
750	915	3000	**750**	1380	**750**	900	3000
1000	915	3800	**1000**	2235			
1500	915	6205					
2000	2890	7700	**2000**	5515	**2000**	2790	7700
3000	2890	11965	**3000**	6710			
4000	3360	16490	**4000**	7585	**4000**	4700	22200
5000	3360	20940	**5000**	9515			
6000	3930	26945	**6000**	12940	**6000**	5200	26900
9000*	10555	32980	**9000***	19010	**9000***	9300	33000
11000*	10555	37415	**10000***	22865			
14000*	11700	53890	**14000***	29715	**14000***	10500	53900

Notes:

1. *Hydrocarbon & Sediment capacities can be modified to accommodate specific site design requirements, contact your local representative for assistance.*

**Consist of two chamber structures in series.*

4 – Stormceptor Inspection & Maintenance

Regular inspection and maintenance is a proven, cost-effective way to maximize water resource protection for all stormwater pollution control practices, and is required to insure proper functioning of the Stormceptor. Both inspection and maintenance of the Stormceptor is easily performed from the surface. Stormceptor's patented technology has no moving parts, simplifying the inspection and maintenance process.

Please refer to the following information and guidelines before conducting inspection and maintenance activities.

When is inspection needed?

- Post-construction inspection is required prior to putting the Stormceptor into service.
- Routine inspections are recommended during the first year of operation to accurately assess the sediment accumulation.
- Inspection frequency in subsequent years is based on the maintenance plan developed in the first year.
- Inspections should also be performed immediately after oil, fuel, or other chemical spills.

When is maintenance cleaning needed?

- For optimum performance, the unit should be cleaned out once the sediment depth reaches the recommended maintenance sediment depth, which is approximately 15% of the unit's total storage capacity (see **Table 2**). The frequency should be adjusted based on historical inspection results due to variable site pollutant loading.

- Sediment removal is easier when removed on a regular basis at or prior to the recommended maintenance sediment depths, as sediment build-up can compact making removal more difficult.
- The unit should be cleaned out immediately after an oil, fuel or chemical spill.

What conditions can compromise Stormceptor performance?

- If construction sediment and debris is not removed prior to activating the Stormceptor unit, maintenance frequency may be reduced.
- If the system is not maintained regularly and fills with sediment and debris beyond the capacity as indicated in **Table 2**, pollutant removal efficiency may be reduced.
- If an oil spill(s) exceeds the oil capacity of the system, subsequent spills may not be captured.
- If debris clogs the inlet of the system, removal efficiency of sediment and hydrocarbons may be reduced.
- If a downstream blockage occurs, a backwater condition may occur for the Stormceptor and removal efficiency of sediment and hydrocarbons may be reduced.

What training is required?

The Stormceptor is to be inspected and maintained by professional vacuum cleaning service providers with experience in the maintenance of underground tanks, sewers and catch basins. For typical inspection and maintenance activities, no specific supplemental training is required for the Stormceptor. Information provided within this Manual (provided to the site owner) contains sufficient guidance to maintain the system properly.

In unusual circumstances, such as if a damaged component needs replacement or some other condition requires manned entry into the vessel, confined space entry procedures must be followed. Only professional maintenance service providers trained in these procedures should enter the vessel. Service provider companies typically have personnel who are trained and certified in confined space entry procedures according to local, state, and federal standards.

What equipment is typically required for inspection?

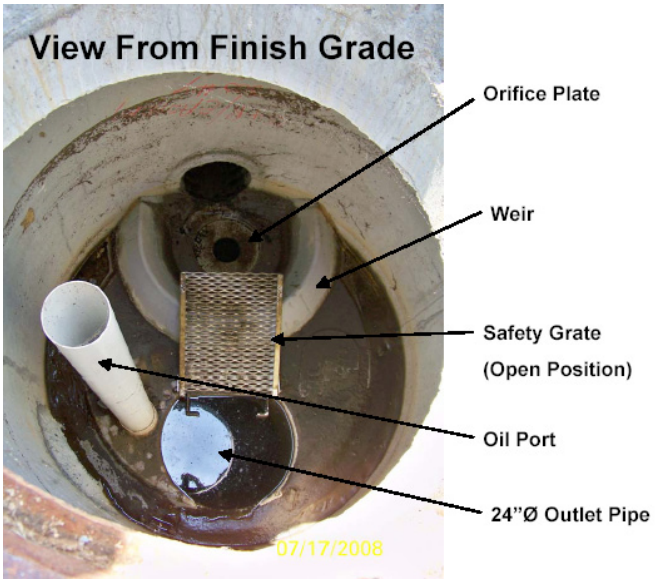
- Manhole access cover lifting tool
- Oil dipstick / Sediment probe with ball valve (typically ¾-inch to 1-inch diameter)
- Flashlight
- Camera
- Data log / Inspection Report
- Safety cones and caution tape
- Hard hat, safety shoes, safety glasses, and chemical-resistant gloves

Recommended Stormceptor Inspection Procedure:

- Stormceptor is to be inspected from grade through a standard surface manhole access cover.
- Sediment and oil depth inspections are performed with a sediment probe and oil dipstick.
- Oil depth is measured through the oil inspection port, either a 4-inch (100 mm) or 6-inch (150 mm) diameter port.
- Sediment depth can be measured through the oil inspection port or the 24-inch (610 mm) diameter outlet riser pipe.
- Inspections also involve a visual inspection of the internal components of the system.

Figure 3.

Figure 4.



What equipment is typically required for maintenance?

- Vacuum truck equipped with water hose and jet nozzle
- Small pump and tubing for oil removal
- Manhole access cover lifting tool
- Oil dipstick / Sediment probe with ball valve (typically ¾-inch to 1-inch diameter)
- Flashlight
- Camera
- Data log / Inspection Report
- Safety cones
- Hard hats, safety shoes, safety glasses, chemical-resistant gloves, and hearing protection for service providers
- Gas analyzer, respiratory gear, and safety harness for specially trained personnel if confined space entry is required

Recommended Stormceptor Maintenance Procedure

Maintenance of Stormceptor is performed using a vacuum truck.

No entry into the unit is required for maintenance. ***DO NOT ENTER THE STORMCEPTOR CHAMBER*** unless you have the proper personal safety equipment, have been trained and are qualified to enter a confined space, as identified by local Occupational Safety and Health Regulations (e.g. 29 CFR 1910.146 or Canada Occupational Safety and Health Regulations – SOR/86-304). Without the proper equipment, training and permit, entry into confined spaces can result in serious bodily harm and potentially death. Consult local, provincial, and/or state regulations to determine the requirements for confined space entry. Be aware, and take precaution that the Stormceptor fiberglass insert may be slippery. In addition, be aware that some units do not have a safety grate to cover the outlet riser pipe that leads to the submerged, lower chamber.

- Ideally maintenance should be conducted during dry weather conditions when no flow is entering the unit.
- Stormceptor is to be maintained through a standard surface manhole access cover.
- Insert the oil dipstick into the oil inspection port. If oil is present, pump off the oil layer into separate containment using a small pump and tubing.
- Maintenance cleaning of accumulated sediment is performed with a vacuum truck.
    - For 6-ft (1800 mm) diameter models and larger, the vacuum hose is inserted into the lower chamber via the 24-inch (610 mm) outlet riser pipe.
    - For 4-ft (1200 mm) diameter model, the removable drop tee is lifted out, and the vacuum hose is inserted into the lower chamber via the 12-inch (305 mm) drop tee hole.

Figure 5.

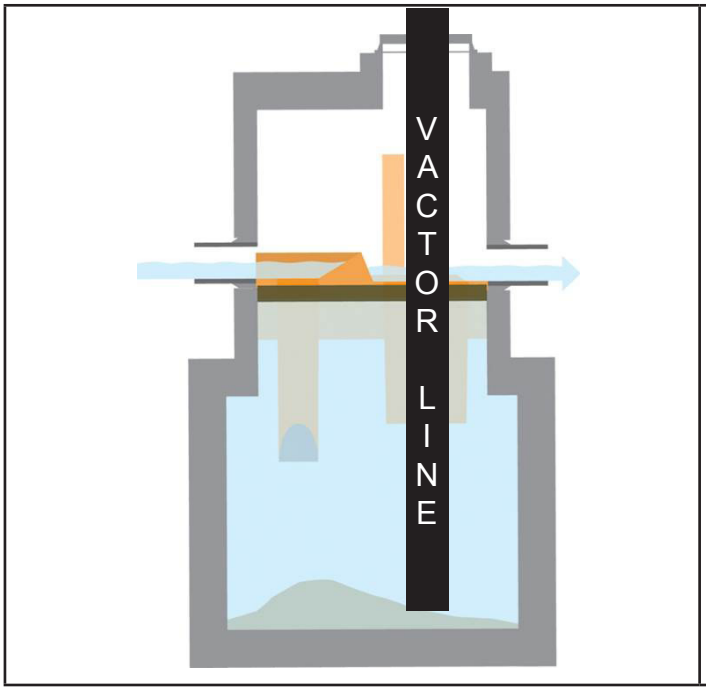
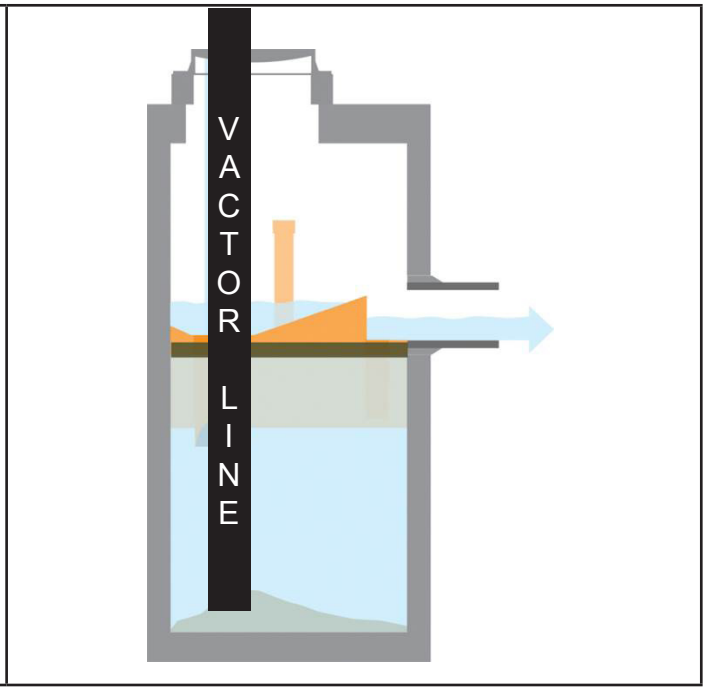


Figure 6.



- Using the vacuum hose, decant the water from the lower chamber into a separate containment tank or to the sanitary sewer, if permitted by the local regulating authority.
- Remove the sediment sludge from the bottom of the unit using the vacuum hose. For large Stormceptor units, a flexible hose is often connected to the primary vacuum line for ease of movement in the lower chamber.
- Units that have not been maintained regularly, have surpassed the maximum recommended sediment capacity, or contain damaged components may require manned entry by trained personnel using safe and proper confined space entry procedures.

Figure 7.

Figure 8.

A maintenance worker stationed at the above ground surface uses a vacuum hose to evacuate water, sediment, and debris from the system.

What is required for proper disposal?

The requirements for the disposal of material removed from Stormceptor units are similar to that of any other stormwater treatment Best Management Practices (BMP). Local guidelines should be consulted prior to disposal of the separator contents. In most areas the sediment, once dewatered, can be disposed of in a sanitary landfill. It is not anticipated that the sediment would be classified as hazardous waste. This could be site and pollutant dependent. In some cases, approval from the disposal facility operator/agency may be required.

What about oil spills?

Stormceptor is often implemented in areas where there is high potential for oil, fuel or other hydrocarbon or chemical spills. Stormceptor units should be cleaned immediately after a spill occurs by a licensed liquid waste hauler. You should also notify the appropriate regulatory agencies as required in the event of a spill.

What if I see an oil rainbow or sheen at the Stormceptor outlet?

With a steady influx of water with high concentrations of oil, a sheen may be noticeable at the Stormceptor outlet. This may occur because a hydrocarbon rainbow or sheen can be seen at

very small oil concentrations (< 10 ppm). Stormceptor is effective at removing 95% of free oil, and the appearance of a sheen at the outlet with high influent oil concentrations does not mean that the unit is not working to this level of removal. In addition, if the influent oil is emulsified, the Stormceptor will not be able to remove it. The Stormceptor is designed for free oil removal and not emulsified or dissolved oil conditions.

What factors affect the costs involved with inspection/maintenance?
The Vacuum Service Industry for stormwater drainage and sewer systems is a well-established sector of the service industry that cleans underground tanks, sewers and catch basins. Costs to clean Stormceptor units will vary. Inspection and maintenance costs are most often based on unit size, the number of units on a site, sediment/oil/hazardous material loads, transportation distances, tipping fees, disposal requirements and other local regulations.

What factors predict maintenance frequency?
Maintenance frequency will vary with the amount of pollution on your site (number of hydrocarbon spills, amount of sediment, site activity and use, etc.). It is recommended that the frequency of maintenance be increased or reduced based on local conditions. If the sediment load is high from an unstable site or sediment loads transported from upstream catchments, maintenance may be required semi-annually. Conversely once a site has stabilized, maintenance may be required less frequently (for example: two to seven year, site and situation dependent). Maintenance should be performed immediately after an oil spill or once the sediment depth in Stormceptor reaches the value specified in **Table 3** based on the unit size.

Table 3A. (US) Recommended Sediment Depths Indicating Maintenance

STC Model	Maintenance Sediment depth (in)	EOS Model	Maintenance Sediment depth (in)	Oil Storage Depth (in)	OSR Model	Maintenance Sediment depth (in)
450	8	**4-175**	9	24	**065**	8
900	8	**9-365**	9	24	**140**	8
1200	10	**12-590**	11	39		
1800	15					
2400	12	**24-1400**	14	68	**250**	12
3600	17	**36-1700**	19	79		
4800	15	**48-2000**	16	68	**390**	17
6000	18	**60-2500**	20	79		
7200	15	**72-3400**	17	79	**560**	17
11000*	17	**110-5000***	16	68	**780***	17
13000*	20	**130-6000***	20	79		
16000*	17	**160-7800***	17	79	**1125***	17

Note:

1. *The values above are for typical standard units.*

**Per structure.*

Table 3B. (CA & Int'l) Recommended Sediment Depths Indicating Maintenance

STC Model	Maintenance Sediment depth (mm)	EOS Model	Maintenance Sediment depth (mm)	Oil Storage Depth (mm)	OSR Model	Maintenance Sediment depth (mm)
300	225	**300**	225	610	**300**	200
750	230	**750**	230	610	**750**	200
1000	275	**1000**	275	990		
1500	400					
2000	350	**2000**	350	1727	**2000**	300
3000	475	**3000**	475	2006		
4000	400	**4000**	400	1727	**4000**	375
5000	500	**5000**	500	2006		
6000	425	**6000**	425	2006	**6000**	375
9000*	400	**9000***	400	1727	**9000***	425
11000*	500	**10000***	500	2006		
14000*	425	**14000***	425	2006	**14000***	425

Note:

1. *The values above are for typical standard units.*

   **Per structure.*

Replacement parts

Since there are no moving parts during operation in a Stormceptor, broken, damaged, or worn parts are not typically encountered. Therefore, inspection and maintenance activities are generally focused on pollutant removal. However, if replacements parts are necessary, they may be purchased by contacting your local Stormceptor Representative, or Imbrium Systems.

The benefits of regular inspection and maintenance are many – from ensuring maximum operation efficiency, to keeping maintenance costs low, to the continued protection of natural waterways – and provide the key to Stormceptor's long and effective service life.

Stormceptor Inspection and Maintenance Log

Stormceptor Model No: _____

Allowable Sediment Depth: _____

Serial Number: _____

Installation Date: _____

Location Description of Unit: _____

Other Comments: _____

Contact Information

Questions regarding the Stormceptor can be addressed by contacting your area Stormceptor Licensee, Imbrium Systems, or visit our website at www.stormceptor.com.

Stormceptor Licensees:

CANADA

Lafarge Canada Inc.
www.lafargepipe.com

403-292-9502 / 1-888-422-4022	Calgary, AB
780-468-5910	Edmonton, AB
204-958-6348	Winnipeg, MB, NW. ON, SK

Langley Concrete Group
www.langleyconcretegroup.com

604-502-5236	BC

Hanson Pipe & Precast Inc.
www.hansonpipeandprecast.com

519-622-7574 / 1-888-888-3222	ON

Lécuyer et Fils Ltée.
www.lecuyerbeton.com

450-454-3928 / 1-800-561-0970	QC

Strescon Limited
www.strescon.com

902-494-7400	NS, NF
506-633-8877	NB, PE

UNITED STATES

Rinker Materials
www.rinkerstormceptor.com
1-800-909-7763

AUSTRALIA & SOUTHEAST ASIA, including New Zealand & Japan

Humes Water Solutions
www.humes.com.au
+61 7 3364 2894

Imbrium Systems Inc. & Imbrium Systems LLC

Canada	1-416-960-9900 / 1-800-565-4801
United States	1-301-279-8827 / 1-888-279-8826
International	+1-416-960-9900 / +1-301-279-8827
Email	info@imbriumsystems.com

www.imbriumsystems.com
www.stormceptor.com

STORMCON
STORMWATER MANAGEMENT SOLUTIONS.

GreenStorm ST

Rigofill ST product by FRÄNKISCHE

Underground storage infiltration modules

www.stormcon.ca

Table of contents

*Rigofill ST product by FRÄNKISCHE

Storing stormwater with storage/infiltration systems

Basic element for underground water storage facilities

GreenStorm ST* are plastic tanks to be installed underground (storage/ infiltration modules) in which water is collected and stored. Storage/infiltration systems temporarily collect stormwater and discharge it later. In addition to infiltration using underdrained swale systems, pipe swales, and gravel swales common in the past, increasingly more storage/infiltration systems are being built today.

The storage space of the storage/ infiltration system consists of numerous GreenStorm ST* modules which can be combined three-dimensionally to form large systems.

The advantage of this method is that the void ratio is up to three times larger in these infiltration systems than in gravel swales which saves space and excavation work.

GreenStorm ST* is a modular system which is characterised by high flexibility, rapid installation and a high level of user-friendliness.

*Rigofill ST product by FRÄNKISCHE

Application – infiltration

Stormwater infiltration – giving back to nature

Large amounts of stormwater can reduce the performance of wastewater treatment systems. Infiltrating unpolluted stormwater nearby has therefore several advantages.

A constant growth in built-up areas and increase in impervious surfaces prevent natural infiltration of stormwater into the soil. Special infiltration systems are used in order to discharge it to the water cycle. In addition to infiltration using pipe swales, increasingly more storage/infiltration systems are being built.

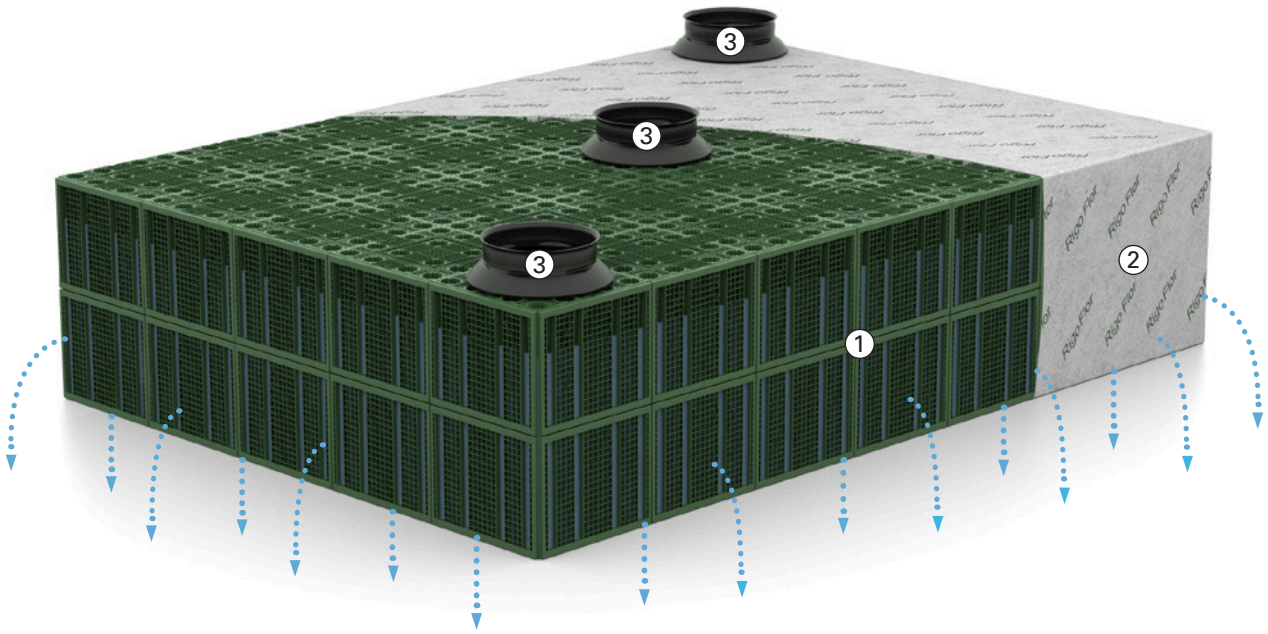
The advantage of this method is that the storage volume of the infiltration system is increased, and space and excavation are saved as compared to gravel swales. Stormwater is thus returned to the natural water cycle and can contribute to producing new groundwater. Infiltration systems are subject to very high requirements. Consequently, they have become an important component of urban drainage.

Storage/infiltration systems considerably increase the underground storage volume. High-performance storage/infiltration systems can be installed even in confined space.

In particular in urban construction no additional space is required and precious building ground is saved.

Légende

1. GreenStorm ST* storage /infiltration module
2. Geotextile
3. QuadroControl ST system shaft



*Rigofill ST product by FRÄNKISCHE

Application – retention

Retaining stormwater – instead of flooding

If subsoil conditions are unfavourable to infiltration, the goal is to retain the stormwater and ensure a retarded, timelagged discharge. Exposure to impulsive stress can be eliminated or reduced in sewer networks, wastewater treatment systems and waterbodies.

Stormwater retention systems retard the infiltration of stormwater. They are comprised of a watertight retaining element, an inlet and a vortex outlet.

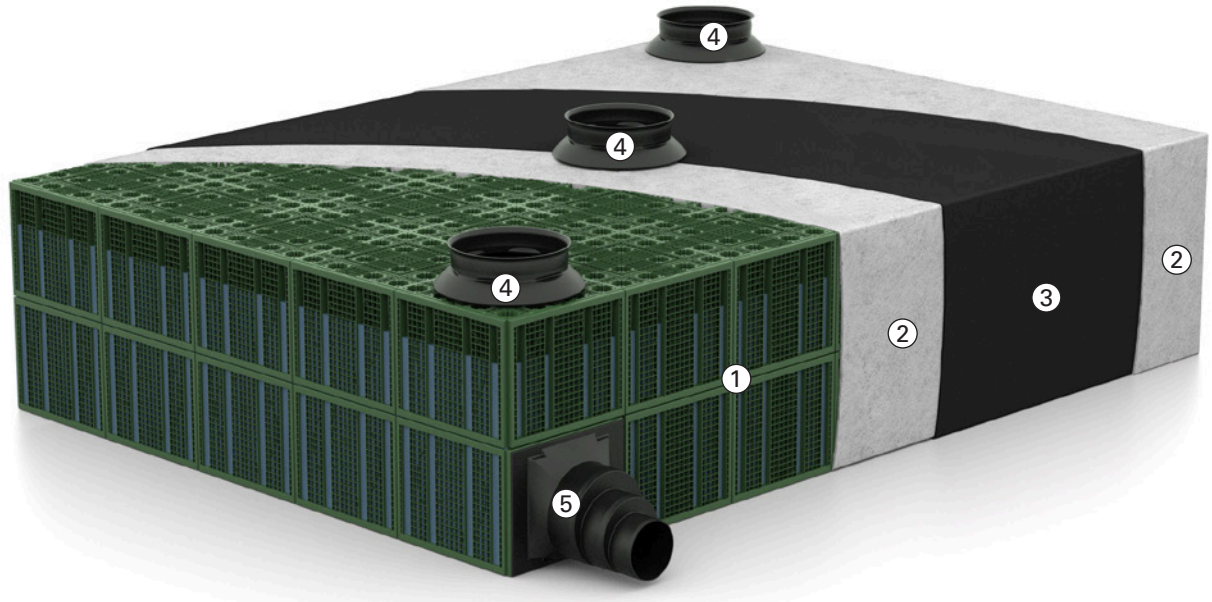
The stormwater distributes evenly in the system where it can be stored and is then discharged in a controlled manner through throttle shafts. If infiltration must be avoided or to prevent unintended discharge of groundwater or strata water (e.g., in case of contaminated soil), it is necessary to waterproof the retention system.

Stormwater runoff from impervious surfaces that cannot infiltrate naturally leads to peak loads in sewer systems.

Stormwater retention facilities collect stormwater in an underground storage tank and discharge it in a retarded manner but continuously. Their very short construction times make storage/ infiltration systems an inexpensive alternative to conventional retention facilities such as retention channels or underground concrete tanks.

Légende

1. GreenStorm ST* storage /infiltration module
2. Geotextile
3. Impermeable membrane
4. QuadroControl ST system shaft
5. Adapter



*Rigofill ST product by FRÄNKISCHE

Application – harvesting / fire water storage

Harvesting stormwater – saving drinking water

Water – particularly drinking water – is a priceless resource which should be treated responsibly and used sparingly. It is therefore wise to collect, store and use stormwater if the water must not necessarily be suitable for drinking purposes, instead of allowing the water to infiltrate into the soil unused or diverting it into the sewer system.

There are many examples: irrigation for greens, car wash, use in toilets, etc.

Water is diverted into a waterproof storage/infiltration system and can be supplied for use via a pumping system.

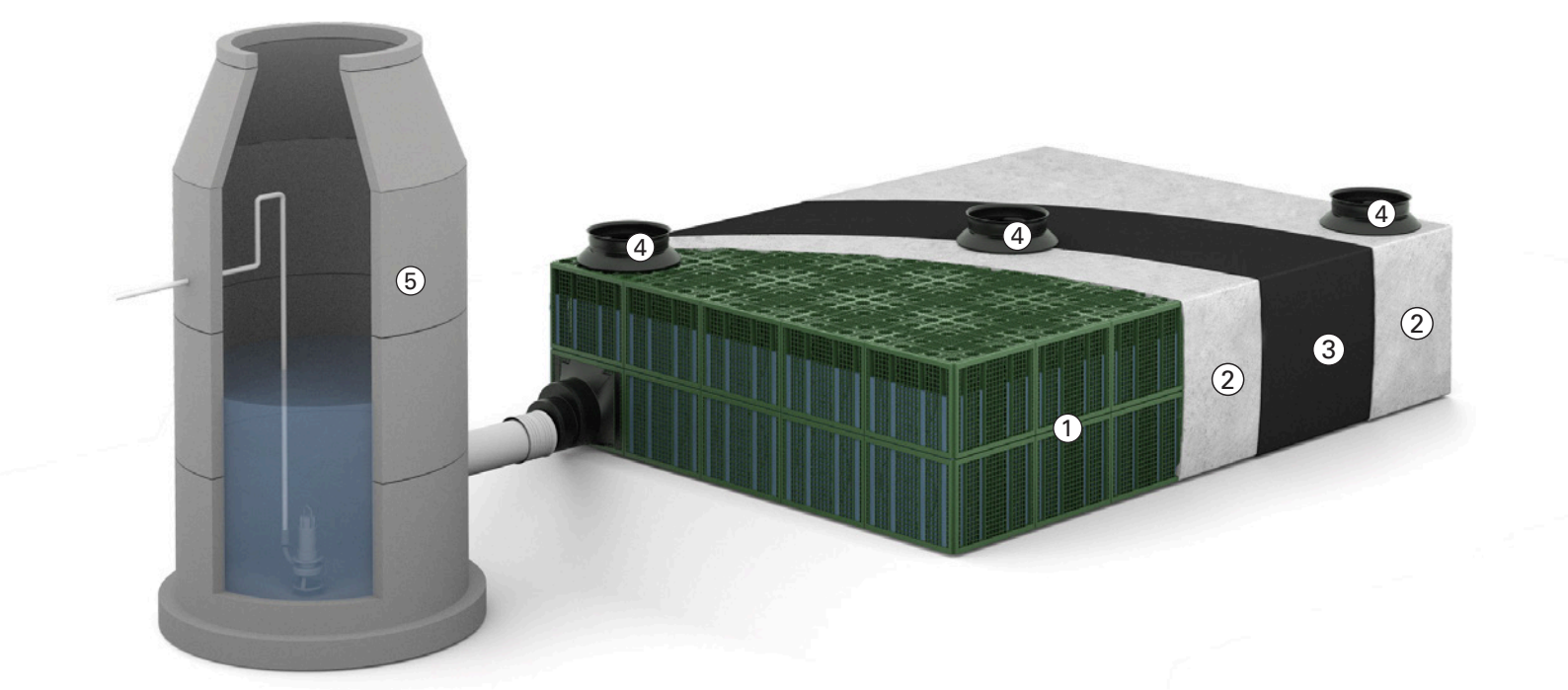
The use of the GreenStorm inspect system allows for finding solutions that fit project-specific requirements – even under the most difficult conditions such as very tight space, narrow conditions, low cover, high groundwater level, etc.

Stormwater harvesting systems provide water for different domestic and industrial water uses. They comprise a watertight retaining element, an inlet with upstream stormwater treatment system, a pump shaft and a system control.

Using GreenStorm ST* for fire water storage also saves water, since system checks can be made in a filled state and water does not have to be pumped out as is the case with conventional concrete tanks.

Légende

1. GreenStorm ST* storage/infiltration module
2. Geotextile
3. Impermeable membrane
4. QuadroControl ST system shaft
5. Tapping shaft (on-site)



*Rigofill ST product by FRÄNKISCHE

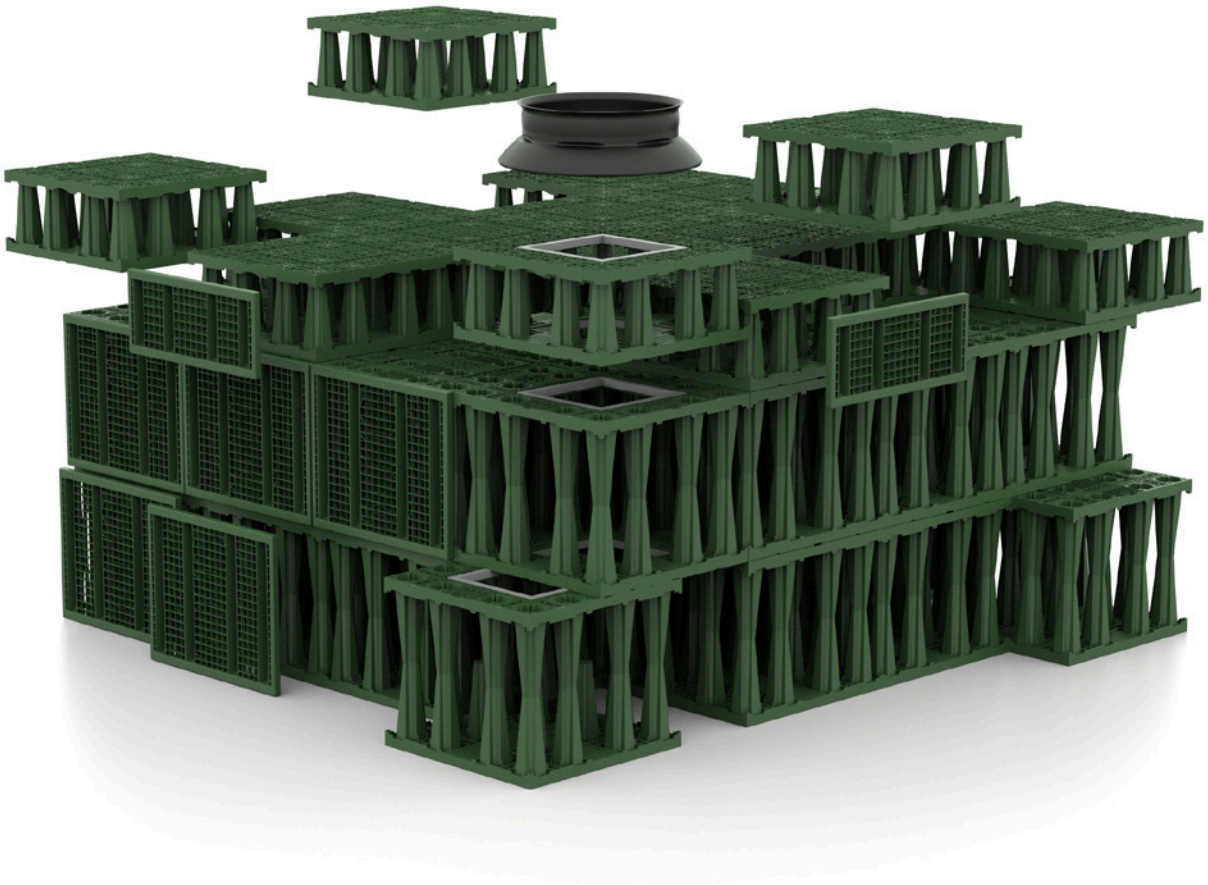
Modular design

Individual system geometries due to modular design

Sizes (length and width) of GreenStorm ST*orage/infiltration systems can be freely designed with hardly any limitations. The 800 mm cellular block type structure can easily be adapted to fit nearly any layout.

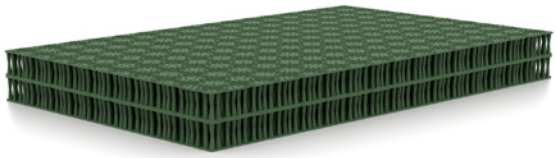
With heights of 660 mm (full block) and 350 mm (half block), systems can be built in various sizes to accommodate any single- or multi-layer combination. Therefore, the system can very easily be adapted to on-site requirements. Under high groundwater conditions or low permeability of backfill soil, for example, rather shallow depth systems are to be preferred.

For soils with good permeability, however, high and compact systems are favourable and may be built accordingly. The maximum space available is used.

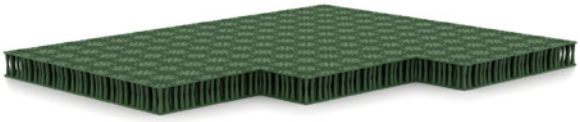


*Rigofill ST product by FRÄNKISCHE

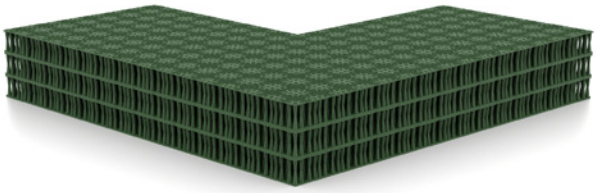
Possible system geometries



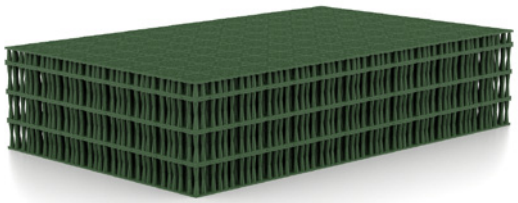
GreenStorm ST*
2-layer



GreenStorm ST*
1-layer



GreenStorm ST*
3-layer



GreenStorm ST*
3 1/2-layer

*Rigofill ST product by FRÄNKISCHE

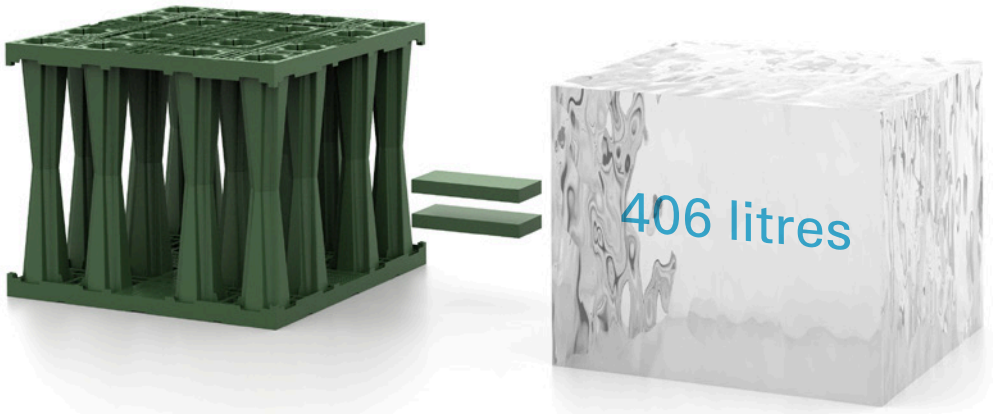
Storage volume

Extremely high volume

The GreenStorm ST* full block provides a storage volume of 406 litres with a gross volume of 422 litres. With a storage volume of more than 96 %, it stores three times as much water as gravel swales.

The half block has a height of 350 mm and is used if shallow systems are required, e.g., in case of high groundwater levels. With a gross volume of 224 litres, it offers a storage volume of 212 litres.

Column void
The column void of the storage/infiltration module is 100 % available as storage space. Large openings at the column base and at the column connection allow unrestricted filling and emptying of the columns.

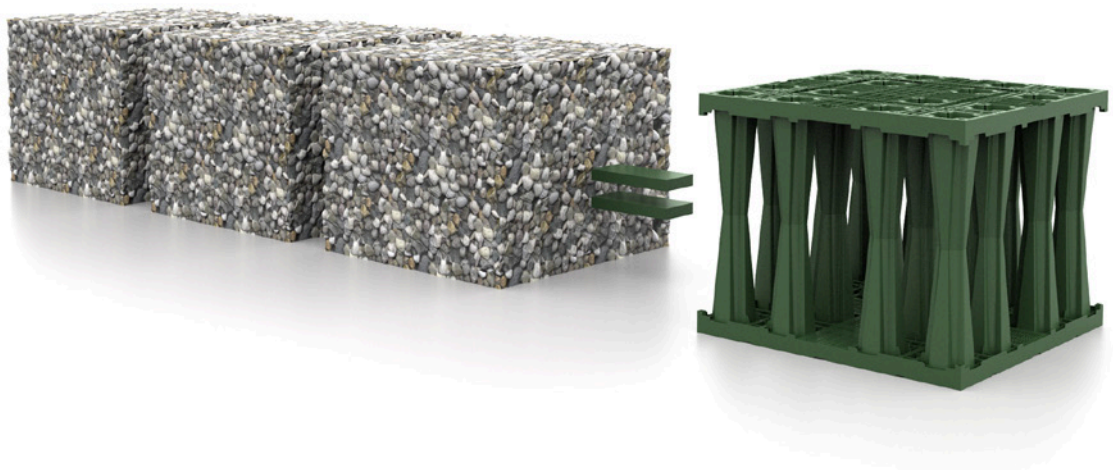


Storage/infiltration systems as compared to gravel swales

Pipe and gravel swales only use approx. 30 % of their volume to store water. Therefore, three times the required water storage volume must be provided by excavation. This requires lots of space which is frequently not available in urban areas.

GreenStorm ST* storage/infiltration systems save an enormous amount of space and excavation work. Thus, subsoil storage spaces for stormwater can be built in a very efficient and cost-saving way.

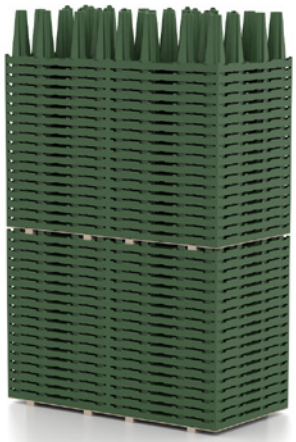
Storage/infiltration systems considerably increase the storage space. High-performance storage/infiltration systems can be installed even in confined space.



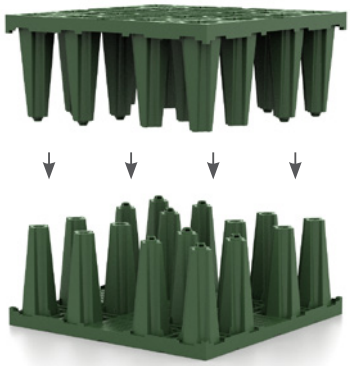
*Rigofill ST product by FRÄNKISCHE

Installation

Easy construction site handling



Requires little space for storage
The storage/infiltration modules are delivered in compact, stacked units with 17 modules per pallet.
The easy stackability of the GreenStorm ST* and ST-B modules allows them to be stored even in confined construction space, even outside the excavation pit.
This facilitates installation, since no additional storage space must be provided in the excavation pit. Installation is neither impeded nor constrained.



Pre-assembly
Depending on the requirements, GreenStorm
ST and GreenStorm ST*-B modules can be pre-assembled in no time at all, both outside and inside the excavation pit with just one easy move. Easy high tensile strength snap connections allow for combining two half elements to create a reliable unit in only a short period of time. This can easily be done by one person alone without requiring any additional tools. The moveable parts of the snap connection are recessed and thus protected from damage.

Easy assembly
There is no need to adhere to any complex installation pattern – the pre-assembled modules or half blocks can just as well be connected to create a single unit.
The low weight allows this to be done by one person only. Connectors establish firm connections between the individual modules. The surface can be accessed immediately without any risk of accidents, since the hole size of the columns is dimensioned respectively (< 100 mm). Thus, no additional covers of column holes are required.

Montage dans la fouille

Up to

88 %

storage space saved as compared to unstackable storage/infiltration modules

*Rigofill ST product by FRÄNKISCHE

Inspection

CCTV inspection even when filled

Storage/infiltration systems are durable structures for urban drainage; they must work reliably for decades. Durability and reliability are essential requirements.
The best way to inspect the state of a system using state-of-the-art technology is CCTV inspection. Thus, a storage/infiltration system can be inspected excellently – for final acceptance or later. This provides safety for authorities, engineers, construction companies, customers, and operators.

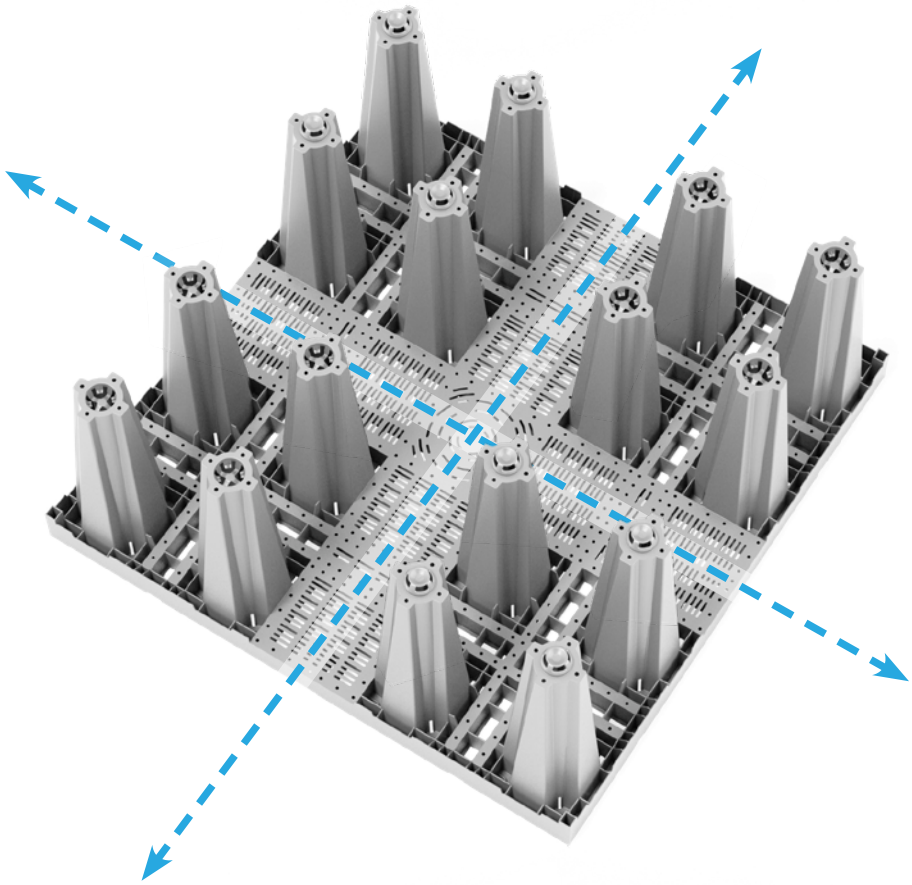
Cross-shaped inspection tunnel

GreenStorm ST* modules have a cross-shaped tunnel which makes the storage/infiltration system camera-accessible and flushable in two axes and thus in four dimensions.
The special and open design of the inspection tunnel allows for an unobstructed view of the entire interior and not only the inspection tunnel.

For example, the statically relevant load-bearing elements, the condition of the geotextile and the entire soil area can be viewed. GreenStorm ST* and GreenStorm ST*-B thus provide excellent options to control the "inner life" of a storage/infiltration system at any time.

The ideal, level and vibration-free running surface and the slim column structure allow for an unobstructed view of the entire module volume. The Quadro Control ST shaft for GreenStorm ST*, which can be integrated, allows for easy access of the automotive dolly for both professional final acceptance inspection and flushing technology.

100 %
inspectable



*Rigofill ST product by FRÄNKISCHE

Inspection

Recommended camera equipment

A standard sewer camera is sufficient for camera inspection.
A rotatable and height-adjustable camera head allows for an optimal view of the lateral soil area, a controllable carriage ensures a centred positioning, and high-performance optics together with lighting allow for a perfect picture.

Certified CCTV accessibility

GreenStorm ST* has been designed for the use of modern CCTV inspection technology.
The inspectability of the GreenStorm ST* and QuadroControl ST system unit has been tested and confirmed by leading manufacturers of pipe CCTV inspection technology!

Recommended: tender invitation for final acceptance inspection

Final acceptance of sewers using camera inspection has long since become a matter of course in sewer construction.
Also in the construction of storage/ infiltration systems, the final acceptance inspection is important! Planning engineers should absolutely include this in their tender documents. For instructions on the professional system configuration of the CCTV inspection technology, please refer to **www.fraenkische.com**

*Rigofill ST product by FRÄNKISCHE

Loading

GreenStorm ST* Heavy traffic

Storage/infiltration systems are subsoil structures and must have sufficient load-carrying capacity against impacting soil and traffic loads.

GreenStorm ST* storage/ infiltration systems are extremely strong and have been designed with various applications in mind:
While GreenStorm ST* has been designed in
particular for traffic loads of up to 13 tons axle load.

Certification CSTB

High resistance

When installed under traffic areas, relevant national guidelines must be observed.

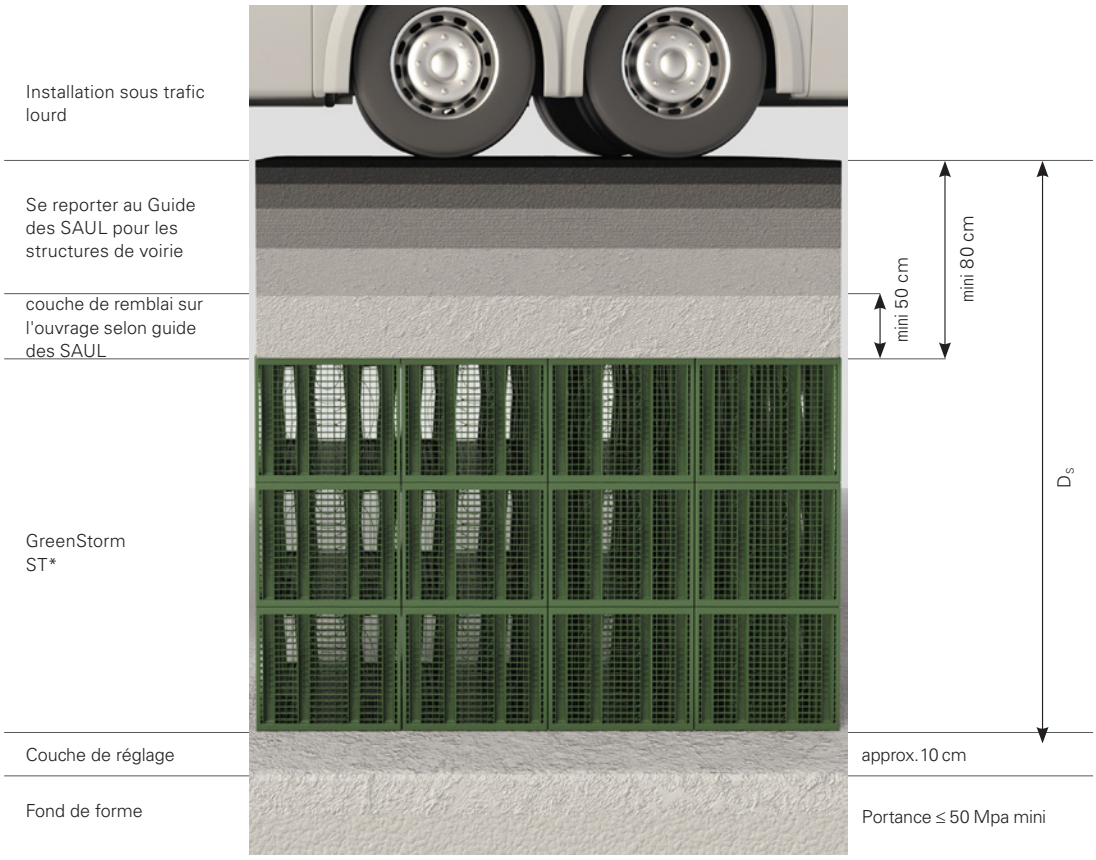
To build the planum for the road construction, an upper levelling layer must be provided. It should preferably be built as a gravel sub-base with a thickness of at least 350 mm, other materials usually result in larger covers.

Generally, a uniform modulus of deformation EV2 ≥ 45 MN/m² must be proven on the planum.

Installation under traffic area

The subsoil structures must have sufficient load-carrying capacity against impacting soil and traffic loads to ensure reliable stability.

This is why GreenStorm ST* is suitable for traffic loads of up to 15 tons axle load (20 tons possible, please refer to our technical department).



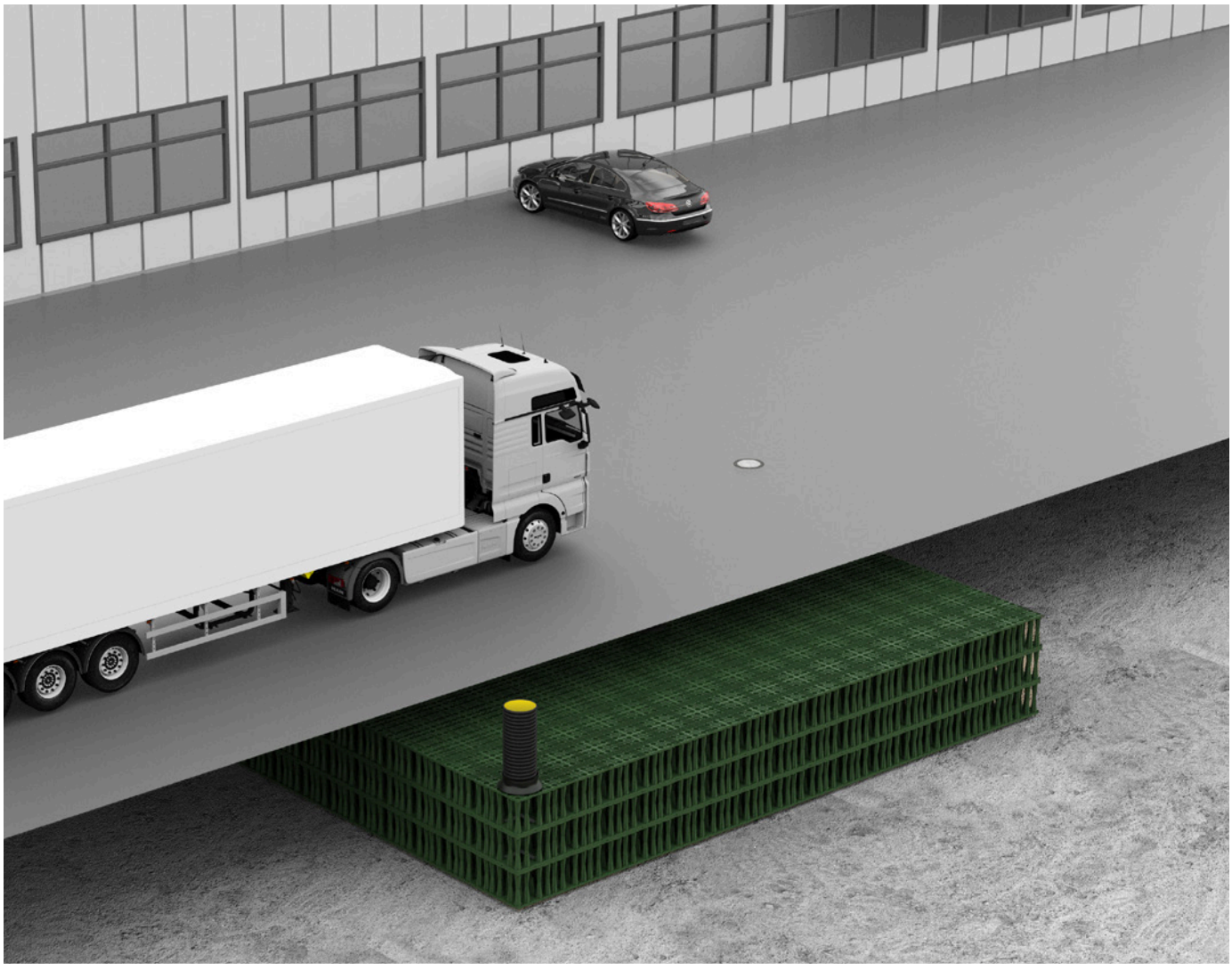
With conventional installation parameters*, depths of cover of DC 4 m and soil depths DSof 6 m are possible for infiltration systems. A project-specific stability analysis can be prepared by STORMCON.

*specific weight of soil 18 kN/m³
Mean soil temperature max. 23 °C,
6 m soil depth, = 0.3, 4-laye

*Rigofill ST product by FRÄNKISCHE

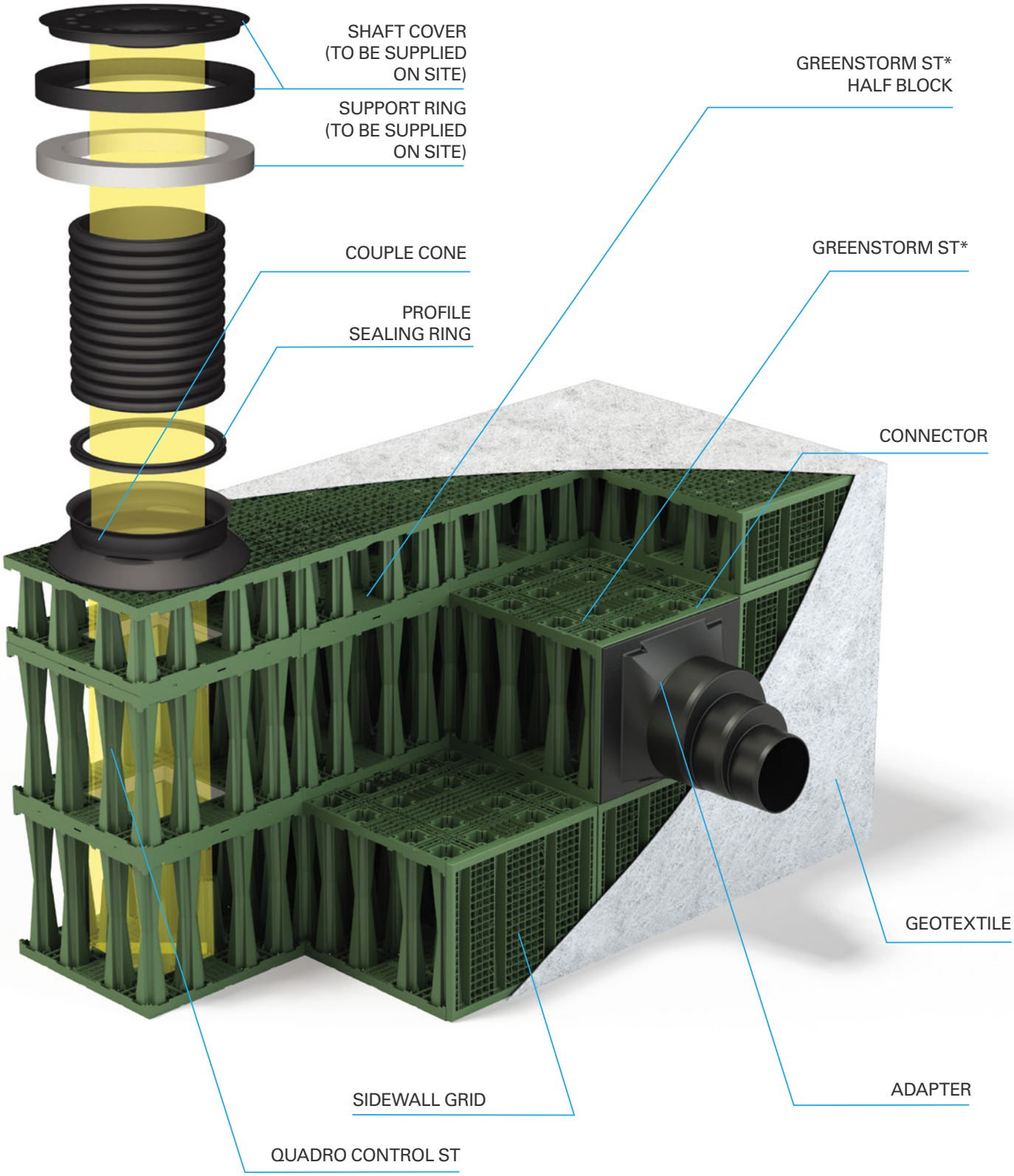
Example

GreenStorm ST* Heavy traffic



*Rigofill ST product by FRÄNKISCHE

Quadro® Control ST – system shaft



*Rigofill ST product by FRÄNKISCHE

Quadro® Control ST – system shaft

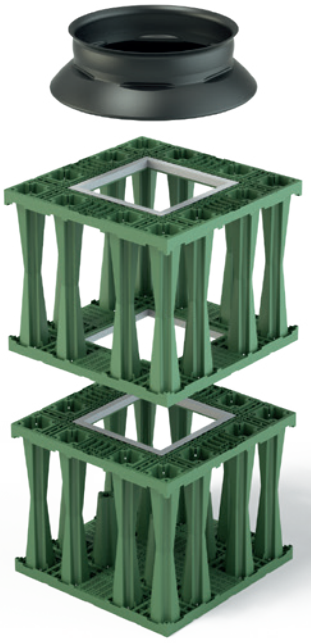
Integrated inspection shafts

Quadro® Control ST is a polypropylene inspection shaft which can be integrated in the storage/infiltration system.

It is square with a base of 800 x 800 mm and can be used in any position of the layout.

Its height results from the number of layers of the connected storage/infiltration system. The shaft allows for comfortable access to the inspection tunnel from aboveground. High-performance inspection and flushing equipment can easily be inserted into the inspection tunnel. The shaft is integrated in the storage/infiltration system and grows layer by layer as construction progresses. QuadroControl ST is delivered with all required components and will be assembled on site.

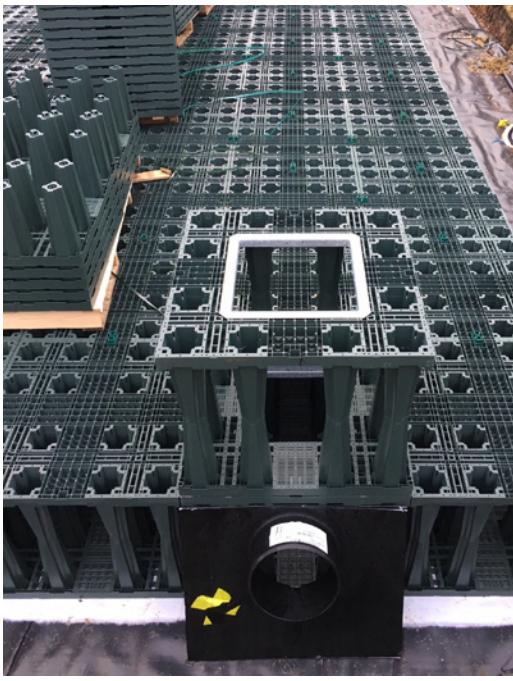
Structure



The shaft cone is the transition to the extension pipe. The length of the extension pipe is chosen depending on the installation depth.

The shaft is integrated in the storage/infiltration system and grows layer by layer as construction progresses.

The shaft components are stackable and delivery includes the cone with all required components as shaft package.

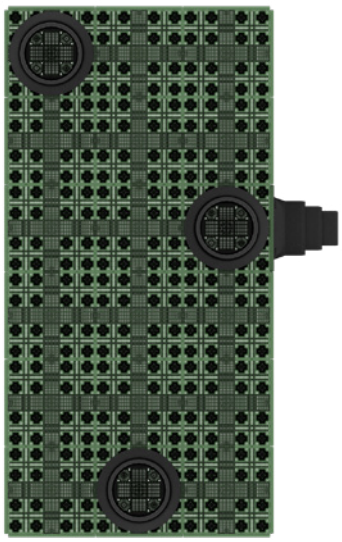


Arrangement of inspection shafts

Number of and position in the system are above all determined by the size of the system, access, pipe connections and design of the outdoor facilities.

In order to ensure that flushing of the complete system is possible, each module should comprise at least one inspection shaft. In addition, the shafts should be positioned such that the shaft covers do not interfere with the design of the outdoor facilities, but can easily be accessed by vehicles for maintenance purposes.

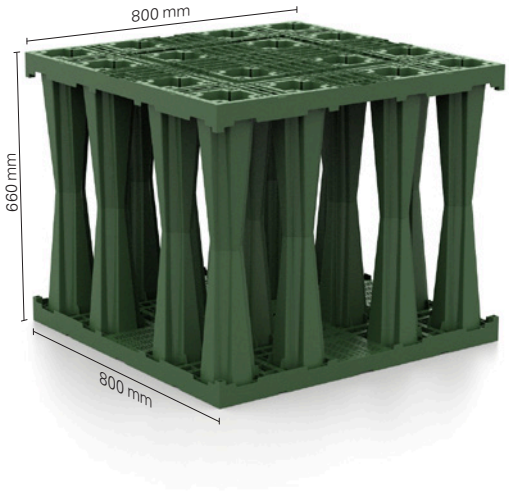
Adjacent shafts should be staggered in the layout.

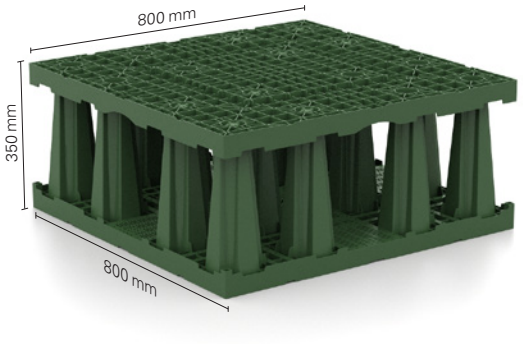


*Rigofill ST product by FRÄNKISCHE

GreenStorm ST* – Design-relevant dimensions

Dimensions





Sidewall grid connection options

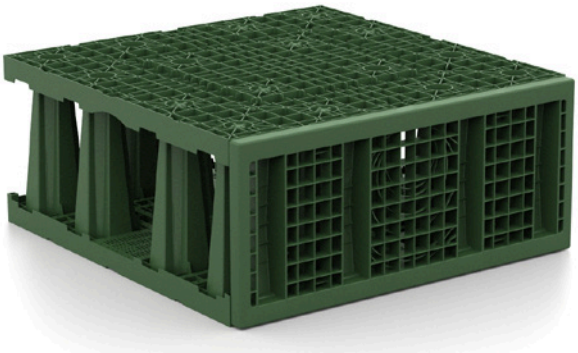
Full block connection options
Dia 100 mm, 135 mm, 150 mm, 200 mm,
250 mm, 300 mm, 375 mm et 450 mm

This allows all available nominal diameters to be realised both at the top and the bottom of the module.

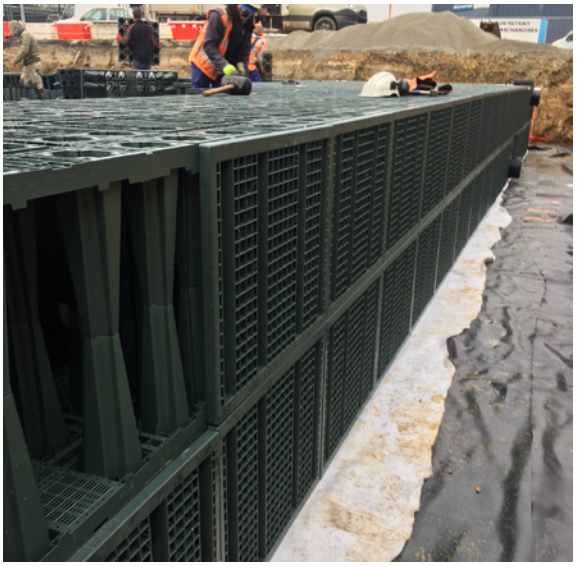
GreenStorm ST* – Design-relevant dimensions

Sidewall grid connection options

Half block connection options
Dia 100 mm, 135 mm, 150 mm, 200 mm
et 250 mm

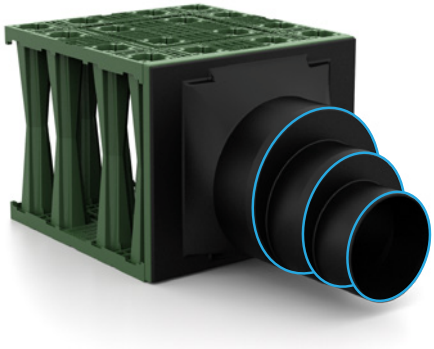


The side plates can be drilled to the height and desired position within the frame.

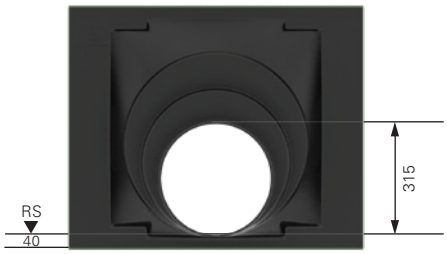


Adapter connection options

Connections:
Dia 300 mm, 450 mm
et 525 mm

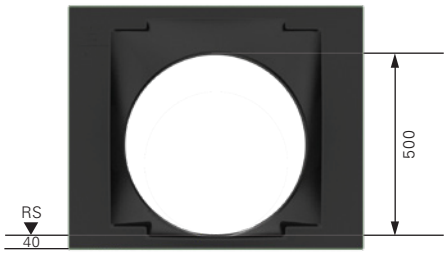


Outside diameter 315 mm for a pipe diameter 300 mm PVC



Outside diameter 400 mm for a pipe diameter 450 mm PVC. A flexible sleeve off center is required.

Outside diameter 500 mm for a pipe of diameter 525 mm. A flexible sleeve off center is required

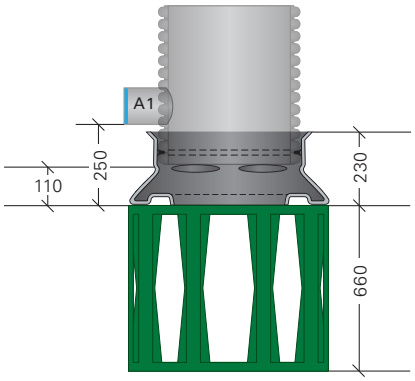


*Rigofill ST product by FRÄNKISCHE

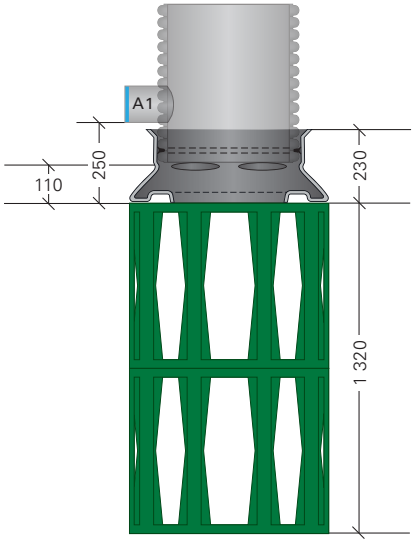
Quadro® Control ST – Design-relevant dimensions

Dimensions of Quadro® Control ST

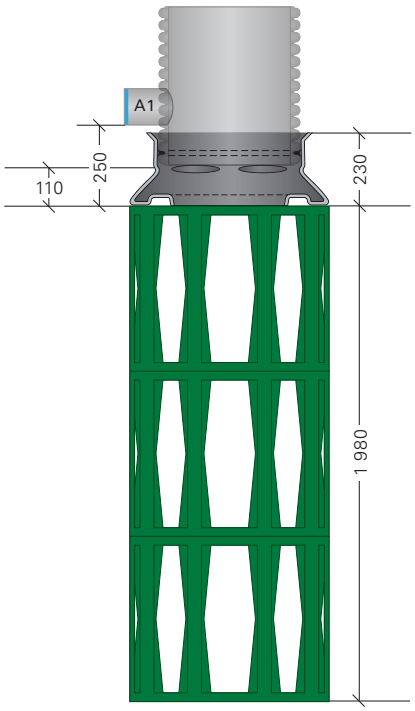
Connection options	
A1	DN/OD 200 or DN/OD 315 connection possible



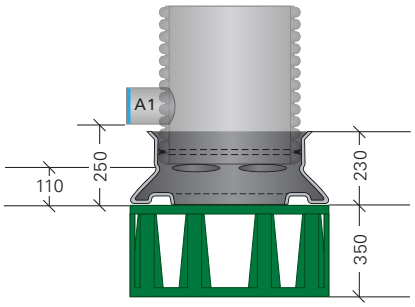
1-layer



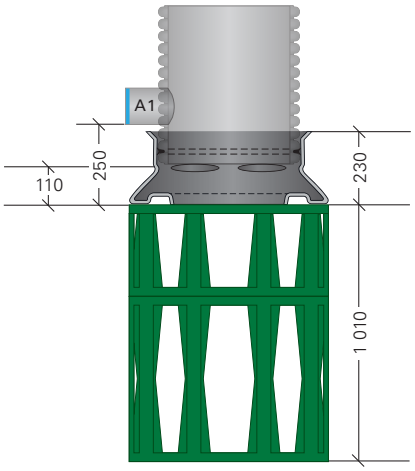
2-layer



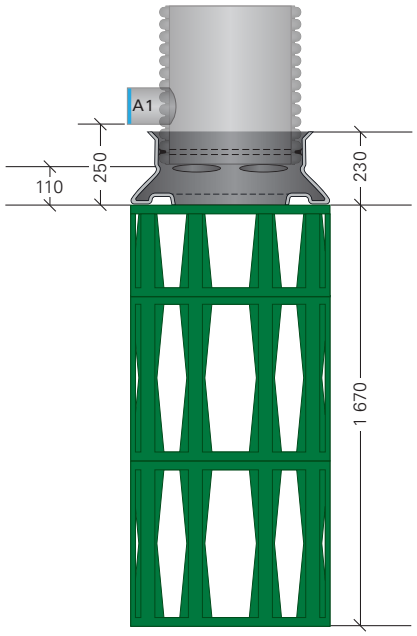
3-layer



1/2-layer



1 1/2-layer

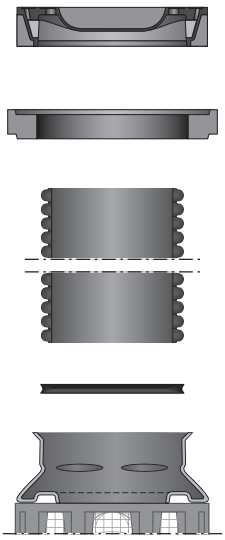


2 1/2-layer

Quadro® Control ST – Design-relevant dimensions

Shaft design of Quadro® Control ST

Structure of inspection shaft

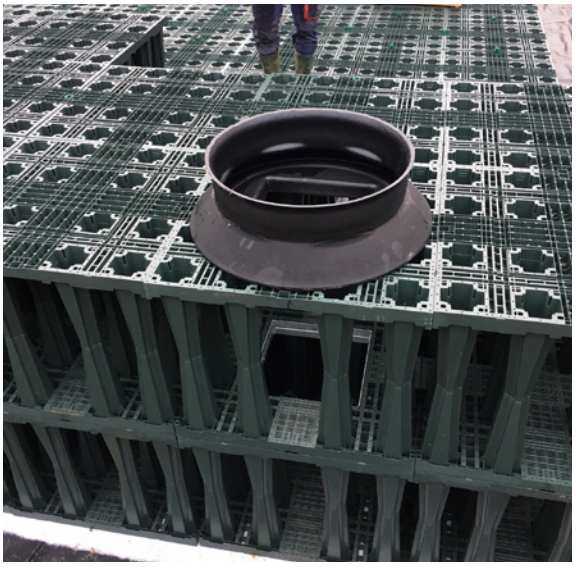


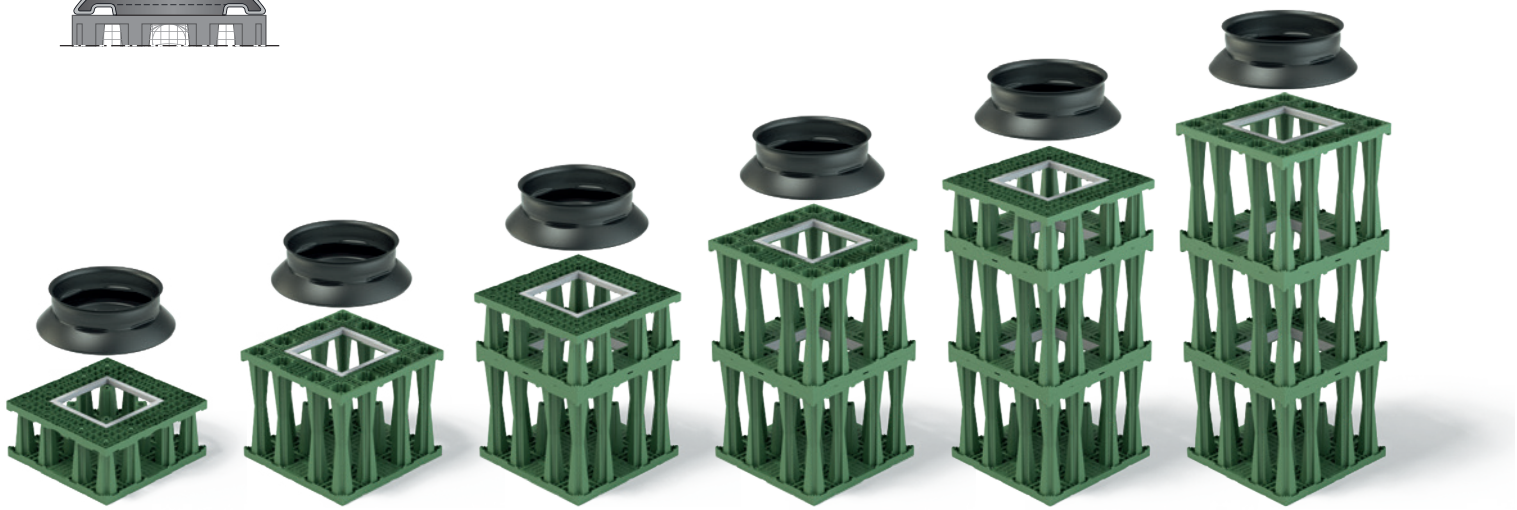
Class B or D
shaft cover acc. to DIN EN 124,
CW 610

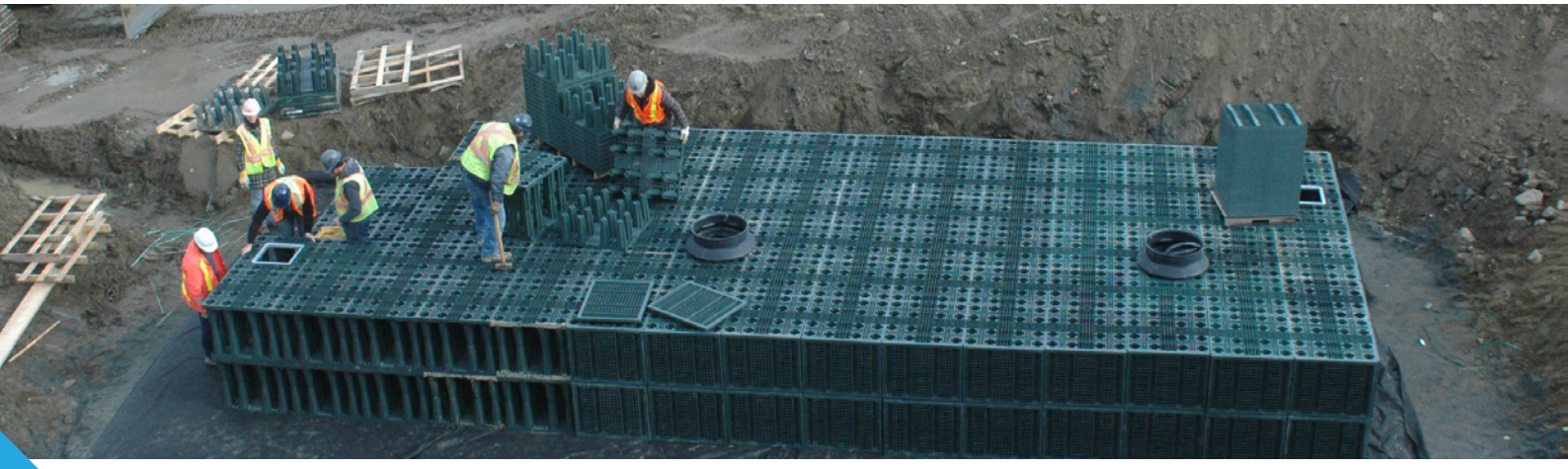
Support ring acc. to DIN 4034,
D_I = 625 mm

Extension pipe
D_O 600

Sealing ring







*Rigofill ST product by FRÄNKISCHE

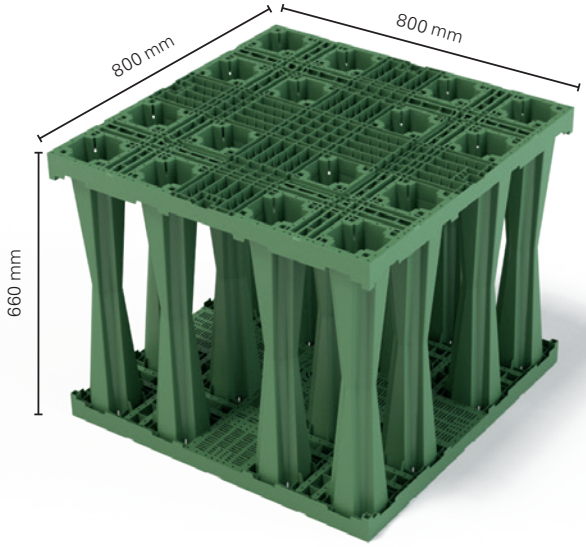
GreenStorm ST*

GreenStorm ST*

GreenStorm ST* IS highly durable and hard-wearing storage/infiltration module with a base of 800 x 800 mm and a height of 660 mm full blocks.

The polypropylene full block consists of two half elements to be installed on site and has a void ratio of more than 96 %. Water can flow through the module three-dimensionally almost without any obstacles. GreenStorm ST* allows for virtually any size and geometry of the systems.

The cross-shaped inspection tunnel in the storage/ infiltration modules has been designed for the use of automotive dollies. This allows the effective drainage surface and the entire system volume with all statically relevant bearing-type fixtures to be inspected.

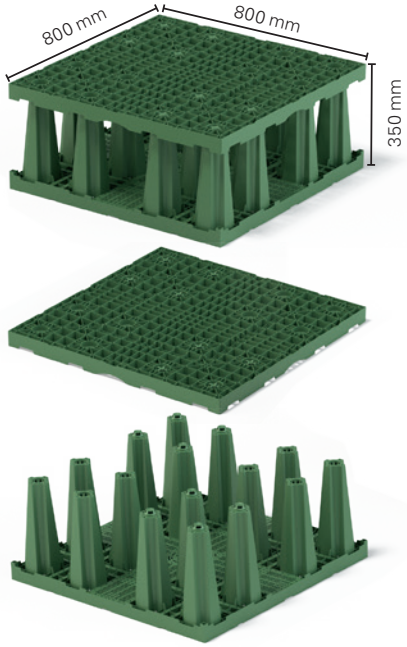


GreenStorm ST* – half block

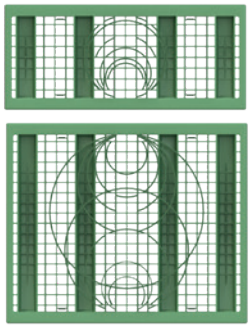
The GreenStorm ST* half block has a base of 800 x 800 mm and a height of 350 mm.

It consists of only one half element which must be assembled with a roof slab on site. This roof slab is only required for the half block. The GreenStorm ST* half block is used in particular for systems with shallow installation depths, e.g., in case of high groundwater levels.

Systems in various heights can be realised in 35 cm steps and adjusted to almost any layout in combination with the full block.



GreenStorm ST* – Accessories



Différentes hauteurs de connexion (indépendamment du diamètre nominal) sont requises au-dessus du fond selon le nombre d'étages :

Nombre d'étages	Hauteur de raccord
0.5-layer	40 mm
1-layer	40 mm
1.5-layer	700 mm
2-layer	700 mm
2.5-layer	1 360 mm
3-layer	1 360 mm

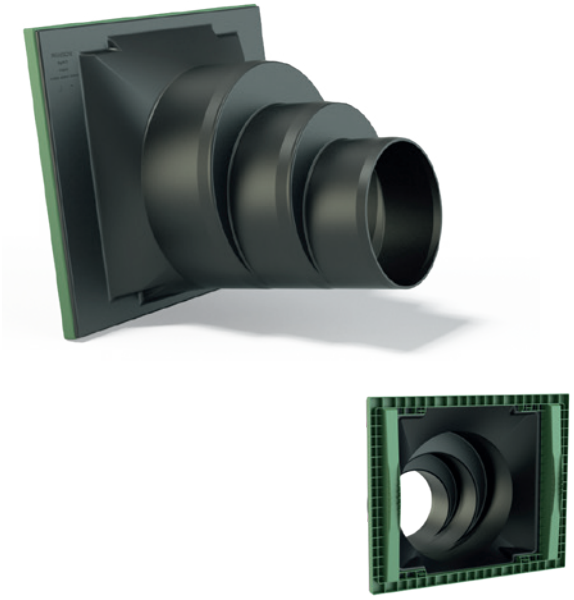
Sidewall grid

The sidewall grids serve as external boundary.

They can be assembled easily using snap connections. The predefined position of the connections at the sidewall grids guarantees that the connections of inlet pipe and outlet pipe and the tunnel are same level. The sidewall grids can be assembled easily also outside the excavation pit.

The sidewall grid for the full block and Quadro® Control ST has a size of W x D x H = 800 x 30 x 660 mm and is suited for connecting lateral solid wall pipes DN 110, 125, 160, 200, 225, 250, 315, 400 and 500.

The sidewall grid for the half block or the half-layer shaft has a size of W x D x H = 800 x 30 x 350 mm and is suited for connecting lateral solid wall pipes DN 110, 125, 160, 200, 225 and 250. In storage/infiltration designs with inside corners, shortened sidewall grids are used at one side.



Adapter

The adapter for GreenStorm ST* has a length of 800 mm and a height of 660 mm and serves as an inlet and outlet connection.

It provides an inlet connection with an optimised flow design with diffusor effect for solid wall pipes DN 315, 400 and 500. It can be connected to GreenStorm ST* easily and quickly thanks to the snap connection.

The predefined position of the snap connection at the module guarantees that inlet pipe and outlet pipe and tunnel connect same level.

The adapter ensures a connection with the same crown, as it is installed turned by 180°.

*Rigofill ST product by FRÄNKISCHE

STORMCON
STORMWATER MANAGEMENT SOLUTIONS.

407 Deerhurst Dr. | Brampton | Ontario L6T 5K3 | CANADA
Tel. +1 647 463 9803 | sales@stormcon.ca | www.stormcon.ca

Project Name	Agnes Subdivision - East of Block 16								
Location	Caledon, ON								
Date	September 27, 2022								
Chamber Model		**GreenStorm-ST**							
Number of Layers		4.0		Top Stone	0.00	m			
Height of Chambers		2.64	m	Bottom Stone	0.00	m			
Chamber Length		34.40		Perimeter Stone	0.00	m			
Chamber Width		12.00		Stone Qty	0.00	m^3			
Storage Void Ratio		0.96		Stone Void Ratio	40.00%				
System Perimeter		92.80							
System Area		412.80	m^2	Liner	Yes				
System Base Elevation		414.06	m						

Height of System		GreenStorm Volume		Stone Volume		Cumulative Storage Volume		Elevation		
mm	in	m^3	ft^3	m^3	ft^3	m^3	ft^3	m	ft	
2640	103.94	15.85	559.79	0.00	0.00	1,046.20	36,946.22	416.70	1367.13	Top of GreenStorm
2600	102.36	9.91	349.87	0.00	0.00	1,030.35	36,386.42	416.66	1366.99	
2575	101.38	9.91	349.87	0.00	0.00	1,020.44	36,036.55	416.64	1366.91	
2550	100.39	9.91	349.87	0.00	0.00	1,010.53	35,686.69	416.61	1366.83	
2525	99.41	9.91	349.87	0.00	0.00	1,000.63	35,336.82	416.59	1366.75	
2500	98.43	9.91	349.87	0.00	0.00	990.72	34,986.95	416.56	1366.67	
2475	97.44	9.91	349.87	0.00	0.00	980.81	34,637.08	416.54	1366.58	
2450	96.46	9.91	349.87	0.00	0.00	970.91	34,287.21	416.51	1366.50	
2425	95.47	9.91	349.87	0.00	0.00	961.00	33,937.34	416.49	1366.42	
2400	94.49	9.91	349.87	0.00	0.00	951.09	33,587.47	416.46	1366.34	
2375	93.50	9.91	349.87	0.00	0.00	941.18	33,237.60	416.44	1366.26	
2350	92.52	9.91	349.87	0.00	0.00	931.28	32,887.73	416.41	1366.17	
2325	91.54	9.91	349.87	0.00	0.00	921.37	32,537.86	416.39	1366.09	
2300	90.55	9.91	349.87	0.00	0.00	911.46	32,187.99	416.36	1366.01	
2275	89.57	9.91	349.87	0.00	0.00	901.56	31,838.12	416.34	1365.93	
2250	88.58	9.91	349.87	0.00	0.00	891.65	31,488.25	416.31	1365.85	
2225	87.60	9.91	349.87	0.00	0.00	881.74	31,138.38	416.29	1365.76	
2200	86.61	9.91	349.87	0.00	0.00	871.83	30,788.51	416.26	1365.68	
2175	85.63	9.91	349.87	0.00	0.00	861.93	30,438.64	416.24	1365.60	
2150	84.65	9.91	349.87	0.00	0.00	852.02	30,088.77	416.21	1365.52	
2125	83.66	9.91	349.87	0.00	0.00	842.11	29,738.90	416.19	1365.44	
2100	82.68	9.91	349.87	0.00	0.00	832.20	29,389.04	416.16	1365.35	
2075	81.69	9.91	349.87	0.00	0.00	822.30	29,039.17	416.14	1365.27	
2050	80.71	9.91	349.87	0.00	0.00	812.39	28,689.30	416.11	1365.19	
2025	79.72	9.91	349.87	0.00	0.00	802.48	28,339.43	416.09	1365.11	
2000	78.74	9.91	349.87	0.00	0.00	792.58	27,989.56	416.06	1365.03	
1975	77.76	9.91	349.87	0.00	0.00	782.67	27,639.69	416.04	1364.94	
1950	76.77	9.91	349.87	0.00	0.00	772.76	27,289.82	416.01	1364.86	
1925	75.79	9.91	349.87	0.00	0.00	762.85	26,939.95	415.99	1364.78	
1900	74.80	9.91	349.87	0.00	0.00	752.95	26,590.08	415.96	1364.70	
1875	73.82	9.91	349.87	0.00	0.00	743.04	26,240.21	415.94	1364.62	
1850	72.83	9.91	349.87	0.00	0.00	733.13	25,890.34	415.91	1364.53	
1825	71.85	9.91	349.87	0.00	0.00	723.23	25,540.47	415.89	1364.45	
1800	70.87	9.91	349.87	0.00	0.00	713.32	25,190.60	415.86	1364.37	
1775	69.88	9.91	349.87	0.00	0.00	703.41	24,840.73	415.84	1364.29	
1750	68.90	9.91	349.87	0.00	0.00	693.50	24,490.86	415.81	1364.21	
1725	67.91	9.91	349.87	0.00	0.00	683.60	24,140.99	415.79	1364.12	
1700	66.93	9.91	349.87	0.00	0.00	673.69	23,791.12	415.76	1364.04	
1675	65.94	9.91	349.87	0.00	0.00	663.78	23,441.25	415.74	1363.96	
1650	64.96	9.91	349.87	0.00	0.00	653.88	23,091.38	415.71	1363.88	
1625	63.98	9.91	349.87	0.00	0.00	643.97	22,741.52	415.69	1363.80	
1600	62.99	9.91	349.87	0.00	0.00	634.06	22,391.65	415.66	1363.71	
1575	62.01	9.91	349.87	0.00	0.00	624.15	22,041.78	415.64	1363.63	
1550	61.02	9.91	349.87	0.00	0.00	614.25	21,691.91	415.61	1363.55	
1525	60.04	9.91	349.87	0.00	0.00	604.34	21,342.04	415.59	1363.47	
1500	59.06	9.91	349.87	0.00	0.00	594.43	20,992.17	415.56	1363.39	
1475	58.07	9.91	349.87	0.00	0.00	584.52	20,642.30	415.54	1363.30	
1450	57.09	9.91	349.87	0.00	0.00	574.62	20,292.43	415.51	1363.22	
1425	56.10	9.91	349.87	0.00	0.00	564.71	19,942.56	415.49	1363.14	

Height of System		GreenStorm Volume		Stone Volume		Cumulative Storage Volume		Elevation		
mm	in	m^3	ft^3	m^3	ft^3	m^3	ft^3	m	ft	
1400	55.12	9.91	349.87	0.00	0.00	554.80	19,592.69	415.46	1363.06	
1375	54.13	9.91	349.87	0.00	0.00	544.90	19,242.82	415.44	1362.98	
1350	53.15	9.91	349.87	0.00	0.00	534.99	18,892.95	415.41	1362.89	
1325	52.17	9.91	349.87	0.00	0.00	525.08	18,543.08	415.39	1362.81	
1300	51.18	9.91	349.87	0.00	0.00	515.17	18,193.21	415.36	1362.73	
1275	50.20	9.91	349.87	0.00	0.00	505.27	17,843.34	415.34	1362.65	
1250	49.21	9.91	349.87	0.00	0.00	495.36	17,493.47	415.31	1362.57	
1225	48.23	9.91	349.87	0.00	0.00	485.45	17,143.60	415.29	1362.48	
1200	47.24	9.91	349.87	0.00	0.00	475.55	16,793.73	415.26	1362.40	
1175	46.26	9.91	349.87	0.00	0.00	465.64	16,443.86	415.24	1362.32	
1150	45.28	9.91	349.87	0.00	0.00	455.73	16,094.00	415.21	1362.24	
1125	44.29	9.91	349.87	0.00	0.00	445.82	15,744.13	415.19	1362.16	
1100	43.31	9.91	349.87	0.00	0.00	435.92	15,394.26	415.16	1362.07	
1075	42.32	9.91	349.87	0.00	0.00	426.01	15,044.39	415.14	1361.99	
1050	41.34	9.91	349.87	0.00	0.00	416.10	14,694.52	415.11	1361.91	
1025	40.35	9.91	349.87	0.00	0.00	406.20	14,344.65	415.09	1361.83	
1000	39.37	9.91	349.87	0.00	0.00	396.29	13,994.78	415.06	1361.75	
975	38.39	9.91	349.87	0.00	0.00	386.38	13,644.91	415.04	1361.66	
950	37.40	9.91	349.87	0.00	0.00	376.47	13,295.04	415.01	1361.58	
925	36.42	9.91	349.87	0.00	0.00	366.57	12,945.17	414.99	1361.50	
900	35.43	9.91	349.87	0.00	0.00	356.66	12,595.30	414.96	1361.42	
875	34.45	9.91	349.87	0.00	0.00	346.75	12,245.43	414.94	1361.34	
850	33.46	9.91	349.87	0.00	0.00	336.84	11,895.56	414.91	1361.25	
825	32.48	9.91	349.87	0.00	0.00	326.94	11,545.69	414.89	1361.17	
800	31.50	9.91	349.87	0.00	0.00	317.03	11,195.82	414.86	1361.09	
775	30.51	9.91	349.87	0.00	0.00	307.12	10,845.95	414.84	1361.01	
750	29.53	9.91	349.87	0.00	0.00	297.22	10,496.08	414.81	1360.93	
725	28.54	9.91	349.87	0.00	0.00	287.31	10,146.21	414.79	1360.84	
700	27.56	9.91	349.87	0.00	0.00	277.40	9,796.35	414.76	1360.76	
675	26.57	9.91	349.87	0.00	0.00	267.49	9,446.48	414.74	1360.68	
650	25.59	9.91	349.87	0.00	0.00	257.59	9,096.61	414.71	1360.60	
625	24.61	9.91	349.87	0.00	0.00	247.68	8,746.74	414.69	1360.52	
600	23.62	9.91	349.87	0.00	0.00	237.77	8,396.87	414.66	1360.43	
575	22.64	9.91	349.87	0.00	0.00	227.87	8,047.00	414.64	1360.35	
550	21.65	9.91	349.87	0.00	0.00	217.96	7,697.13	414.61	1360.27	
525	20.67	9.91	349.87	0.00	0.00	208.05	7,347.26	414.59	1360.19	
500	19.69	9.91	349.87	0.00	0.00	198.14	6,997.39	414.56	1360.10	
475	18.70	9.91	349.87	0.00	0.00	188.24	6,647.52	414.54	1360.02	
450	17.72	9.91	349.87	0.00	0.00	178.33	6,297.65	414.51	1359.94	
425	16.73	9.91	349.87	0.00	0.00	168.42	5,947.78	414.49	1359.86	
400	15.75	9.91	349.87	0.00	0.00	158.52	5,597.91	414.46	1359.78	
375	14.76	9.91	349.87	0.00	0.00	148.61	5,248.04	414.44	1359.69	
350	13.78	9.91	349.87	0.00	0.00	138.70	4,898.17	414.41	1359.61	
325	12.80	9.91	349.87	0.00	0.00	128.79	4,548.30	414.39	1359.53	
300	11.81	9.91	349.87	0.00	0.00	118.89	4,198.43	414.36	1359.45	
275	10.83	9.91	349.87	0.00	0.00	108.98	3,848.56	414.34	1359.37	
250	9.84	9.91	349.87	0.00	0.00	99.07	3,498.69	414.31	1359.28	
225	8.86	9.91	349.87	0.00	0.00	89.16	3,148.83	414.29	1359.20	
200	7.87	9.91	349.87	0.00	0.00	79.26	2,798.96	414.26	1359.12	
175	6.89	9.91	349.87	0.00	0.00	69.35	2,449.09	414.24	1359.04	
150	5.91	9.91	349.87	0.00	0.00	59.44	2,099.22	414.21	1358.96	
125	4.92	9.91	349.87	0.00	0.00	49.54	1,749.35	414.19	1358.87	
100	3.94	9.91	349.87	0.00	0.00	39.63	1,399.48	414.16	1358.79	
75	2.95	9.91	349.87	0.00	0.00	29.72	1,049.61	414.14	1358.71	
50	1.97	9.91	349.87	0.00	0.00	19.81	699.74	414.11	1358.63	
25	0.98	9.91	349.87	0.00	0.00	9.91	349.87	414.09	1358.55	
0	0.00	0.00	0.00	4.13	145.78	0.00	0.00	414.06	1358.46	System Bottom

Stage Storage LW Infiltration

Project Name	Agnes Subdivions				
Location	Caledon, ON				
Date	March 9, 2023				
Chamber Model	**GreenStorm-ST**				
Number of Layers	0.5		Top Stone	0.00	m
Height of Chambers	0.35	m	Bottom Stone	0.00	m
Chamber Length	20.00		Perimeter Stone	0.00	m
Chamber Width	18.40		Stone Qty	0.00	m^3
Storage Void Ratio	0.96		Stone Void Ratio	40.00%	
System Perimeter	76.80				
System Area	368.00	m^2	Liner	No	
System Base Elevation	414.25	m			

Height of System	GreenStorm Volume	Stone Volume	Cumulative Storage Volume	Elevation	
mm	m^3	m^3	m^3	m	
350	8.83	0.00	123.65	414.60	Top of GreenStorm
325	8.83	0.00	114.82	414.58	
300	8.83	0.00	105.98	414.55	
275	8.83	0.00	97.15	414.53	
250	8.83	0.00	88.32	414.50	
225	8.83	0.00	79.49	414.48	
200	8.83	0.00	70.66	414.45	
175	8.83	0.00	61.82	414.43	
150	8.83	0.00	52.99	414.40	
125	8.83	0.00	44.16	414.38	
100	8.83	0.00	35.33	414.35	
75	8.83	0.00	26.50	414.33	
50	8.83	0.00	17.66	414.30	
25	8.83	0.00	8.83	414.28	
0	0.00	3.68	0.00	414.25	System Bottom

AGNES SUBDIVISION
AGNES ST., CALEDON, ON

DRAWING INDEX

	PROJECT INFORMATION		
SITE CONTACT	PHIL ALLEN	416-286-5990	PHILALLEN@STORMCON.CA
ENGINEER / TECHNICAL SPECIALIST	ERIC CUMISKEY	289-380-3742	ECUMISKEY@STORMCON.CA
SALES REP:	GREG DZIEWIECKI	437-231-6080	GREGD@STORMCON.CA
PROJECT NO:	2023-033		

COMMENTS:

REVISION	DATE	COMMENT	BY
01	03/09/2023	SYSTEM VOLUME INCREASED	JD
02	12/01/2023	REVISED PER UPDATED STORAGE VOLUME	JD

STORMCON
69 CONNIE CRESCENT
CONCORD, ON
L4K 3W1

SALES@STORMCON.CA
www.STORMCON.CA

NOTE: THESE SHOP DRAWINGS MAY CONTAIN COMPONENTS INCLUDING BUT NOT LIMITED TO MANHOLES, CATCH BASINS, STORM PIPES AND FITTINGS, MANIFOLDS, CASTINGS AND OTHER NECESSARY APPURTENANCES THAT MAY NOT BE SUPPLIED BY STORMCRETE. IT IS THE RESPONSIBILITY OF THE CONTRACTOR AND/OR SUPPLIER TO CONFIRM THE MATERIALS PROVIDED.

PROPOSED SYSTEM ELEVATIONS

(TO BE APPROVED BY ENGINEER)

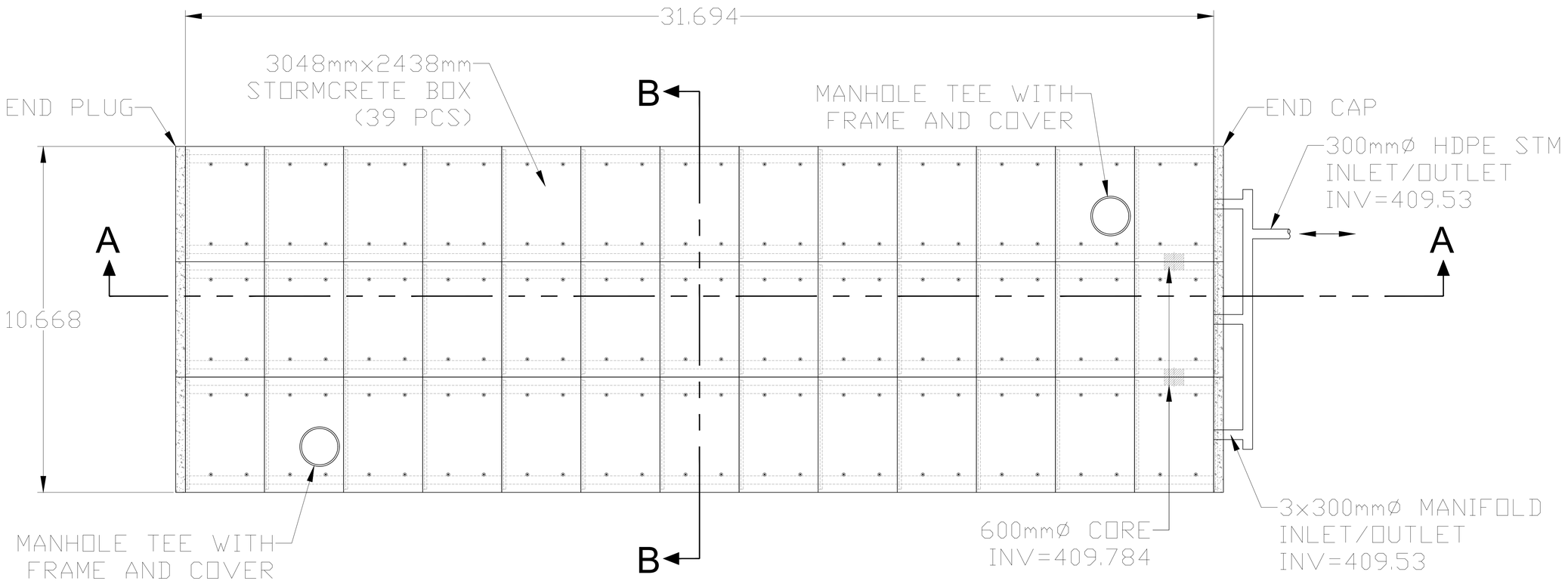
***ENGINEER TO CONFIRM MINIMUM AND MAXIMUM BURIAL REQUIREMENTS ARE MET**

415.82	MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED)
412.82	MINIMUM ALLOWABLE GRADE
<409.28	SEASONAL HIGH GROUNDWATER ELEVATION

STORMCRETE STORMWATER MANAGEMENT SYSTEM

TOTAL STORAGE PROVIDED: 694.29 m^3

SYSTEM AREA : 328.41 m^2



NOTE:*ALL EXTERNAL SYSTEM STRUCTURES, INLET/OUTLET PIPES, AND PROPOSED ELEVATIONS MUST BE DESIGNED AND APPROVED BY PROJECT ENGINEER OF RECORD. PROJECT ENGINEER OF RECORD MUST ENSURE CHAMBER BURIAL REQUIREMENTS ARE MET.

STORMCON

69 CONNIE CRESCENT
CONCORD, ON
L4K 1L3

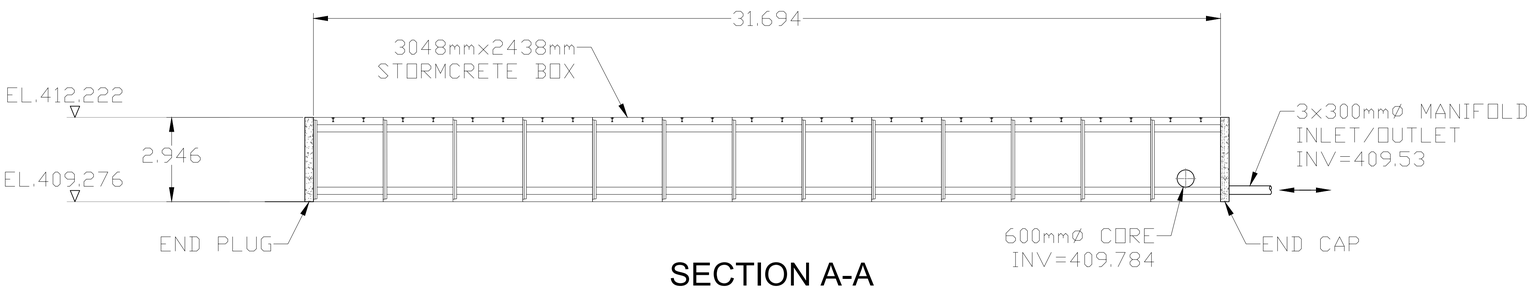
SALES@STORMCON.CA
www.STORMCON.CA

AGNES SUBDIVISION
AGNES ST., CALEDON, ON

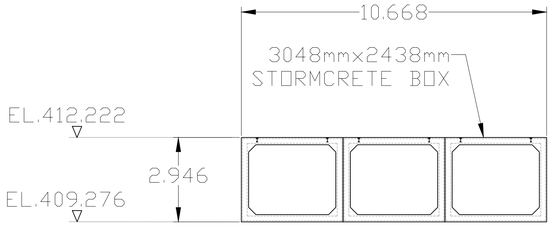
SYSTEM LAYOUT SHEET STORAGE TANK

STORMCRETE STORMWATER CHAMBER

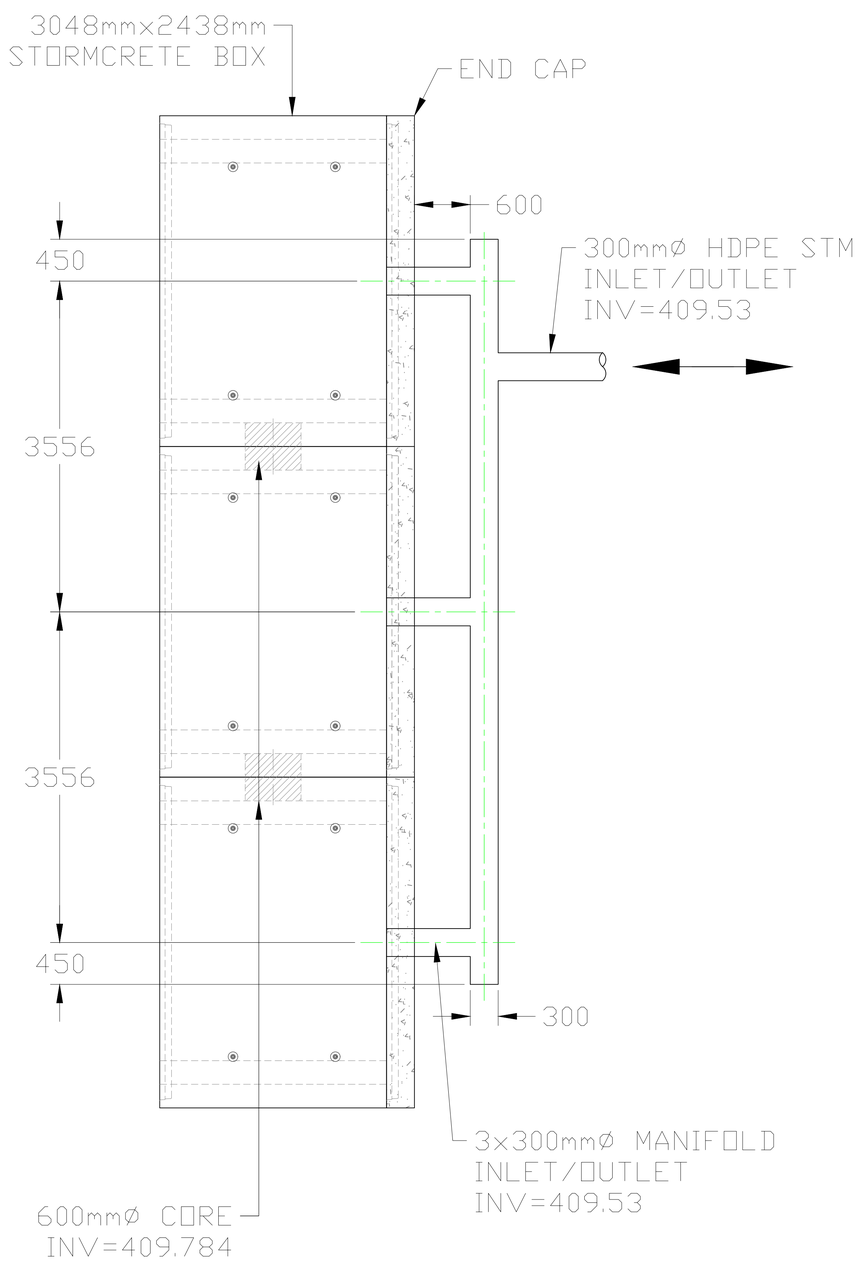
PROJECT NO:	2023-033	DATE:	03/07/2023
DESIGNED BY:	JD	CHECKED BY:	EC
SCALE:	N.T.S.	SHEET NO:	2 OF 6



SECTION A-A



SECTION B-B



MANIFOLD DETAILS

NOTE:*ALL EXTERNAL SYSTEM STRUCTURES, INLET/OUTLET PIPES, AND PROPOSED ELEVATIONS MUST BE DESIGNED AND APPROVED BY PROJECT ENGINEER OF RECORD. PROJECT ENGINEER OF RECORD MUST ENSURE CHAMBER BURIAL REQUIREMENTS ARE MET.

STORMCON
69 CONNIE CRESCENT
CONCORD, ON
L4K 1L3

SALES@STORMCON.CA
www.STORMCON.CA

AGNES SUBDIVISION
AGNES ST., CALEDON, ON

SYSTEM SECTIONS & MANIFOLD DETAILS

STORMCRETE STORMWATER CHAMBER

PROJECT NO:	2023-033	DATE:	03/07/2023
DESIGNED BY:	JD	CHECKED BY:	EC
SCALE:	N.T.S.	SHEET NO:	3 OF 6

Project Name	Agnes subdivision
Location	Agnes St., Caledon, ON
Date	November 30, 2023
Chamber Model	**StormCrete**
Height of System (m)	**2.438**
Area of System (m^2)	**328.41**
System Base Elevation (m)	**409.530**

Height of System	StormCrete Volume	Cumulative Storage Volume	Elevation				
mm	m^3	m^3	m				
2438	6.094756	694.29	411.968	1188	7.245248	338.18	410.718
2413	6.213609	688.19	411.943	1163	7.245248	330.94	410.693
2388	6.332461	681.98	411.918	1138	7.245248	323.69	410.668
2363	6.451314	675.65	411.893	1113	7.245248	316.45	410.643
2338	6.570166	669.20	411.868	1088	7.245248	309.20	410.618
2313	6.689019	662.63	411.843	1063	7.245248	301.96	410.593
2288	6.807871	655.94	411.818	1038	7.245248	294.71	410.568
2263	6.926724	649.13	411.793	1013	7.245248	287.47	410.543
2238	7.045576	642.20	411.768	988	7.245248	280.22	410.518
2213	7.164429	635.16	411.743	963	7.245248	272.98	410.493
2188	7.243347	627.99	411.718	938	7.245248	265.73	410.468
2163	7.245248	620.75	411.693	913	7.245248	258.49	410.443
2138	7.245248	613.50	411.668	888	7.245248	251.24	410.418
2113	7.245248	606.26	411.643	863	7.245248	244.00	410.393
2088	7.245248	599.01	411.618	838	7.245248	236.75	410.368
2063	7.245248	591.77	411.593	813	7.245248	229.51	410.343
2038	7.245248	584.52	411.568	788	7.245248	222.26	410.318
2013	7.245248	577.28	411.543	763	7.245248	215.01	410.293
1988	7.245248	570.03	411.518	738	7.245248	207.77	410.268
1963	7.245248	562.79	411.493	713	7.245248	200.52	410.243
1938	7.245248	555.54	411.468	688	7.245248	193.28	410.218
1913	7.245248	548.30	411.443	663	7.245248	186.03	410.193
1888	7.245248	541.05	411.418	638	7.245248	178.79	410.168
1863	7.245248	533.81	411.393	613	7.245248	171.54	410.143
1838	7.245248	526.56	411.368	588	7.245248	164.30	410.118
1813	7.245248	519.32	411.343	563	7.245248	157.05	410.093
1788	7.245248	512.07	411.318	538	7.245248	149.81	410.068
1763	7.245248	504.82	411.293	513	7.245248	142.56	410.043
1738	7.245248	497.58	411.268	488	7.245248	135.32	410.018
1713	7.245248	490.33	411.243	463	7.245248	128.07	409.993
1688	7.245248	483.09	411.218	438	7.245248	120.83	409.968
1663	7.245248	475.84	411.193	413	7.245248	113.58	409.943
1638	7.245248	468.60	411.168	388	7.245248	106.34	409.918
1613	7.245248	461.35	411.143	363	7.245248	99.09	409.893
1588	7.245248	454.11	411.118	338	7.245248	91.85	409.868
1563	7.245248	446.86	411.093	313	7.245248	84.60	409.843
1538	7.245248	439.62	411.068	288	7.245248	77.36	409.818
1513	7.245248	432.37	411.043	263	7.222429	70.11	409.793
1488	7.245248	425.13	411.018	238	7.112134	62.89	409.768
1463	7.245248	417.88	410.993	213	6.993281	55.78	409.743
1438	7.245248	410.64	410.968	188	6.874429	48.78	409.718
1413	7.245248	403.39	410.943	163	6.755576	41.91	409.693
1388	7.245248	396.15	410.918	138	6.636724	35.15	409.668
1363	7.245248	388.90	410.893	113	6.517871	28.52	409.643
1338	7.245248	381.66	410.868	88	6.399019	22.00	409.618
1313	7.245248	374.41	410.843	63	6.280166	15.60	409.593
1288	7.245248	367.17	410.818	38	6.161314	9.32	409.568
1263	7.245248	359.92	410.793	13	3.156913	3.16	409.543
1238	7.245248	352.67	410.768	0	0.000000	0.00	409.518
1213	7.245248	345.43	410.743				

SYSTEM STAGE-STORAGE TABLE

STORMCON
69 CONNIE CRESCENT
CONCORD, ON
L4K 1L3

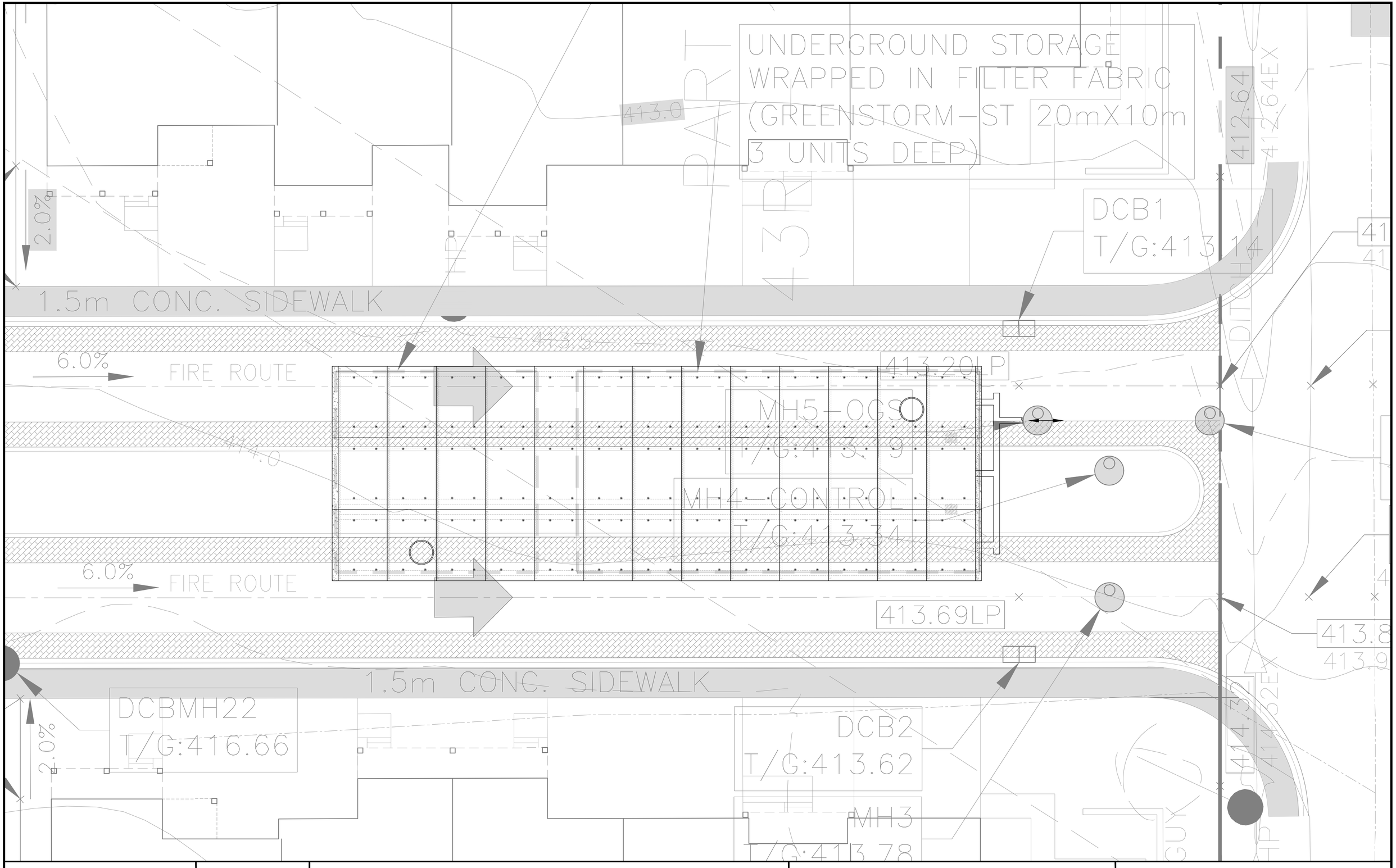
SALES@STORMCON.CA
www.STORMCON.CA

AGNES SUBDIVISION
AGNES ST., CALEDON, ON

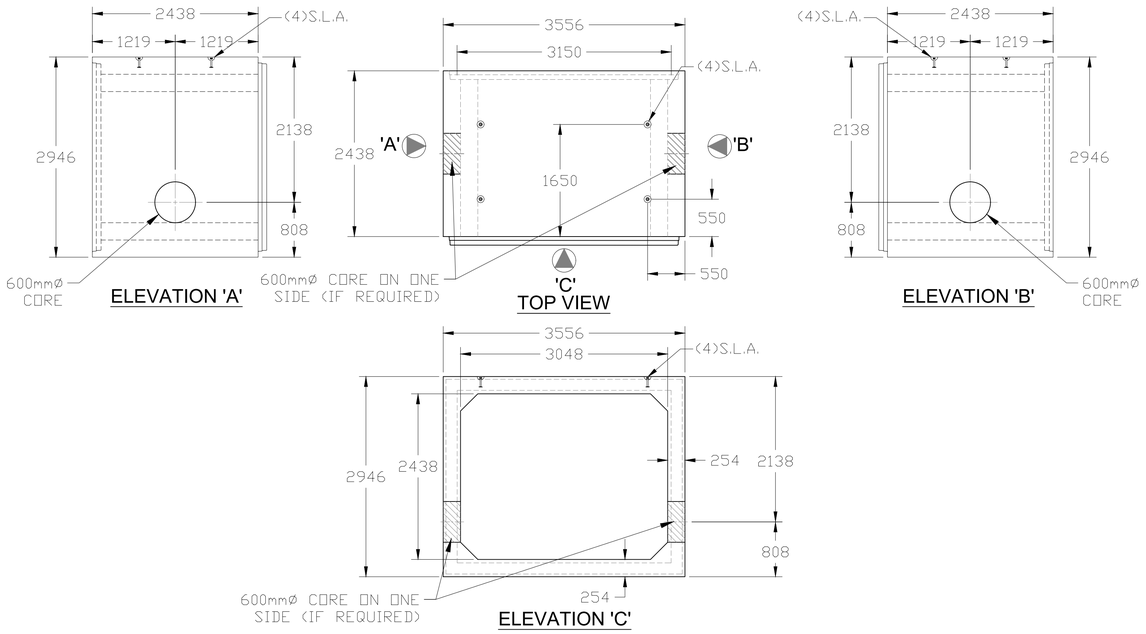
SYSTEM CALCULATION SHEET

STORMCRETE STORMWATER CHAMBER

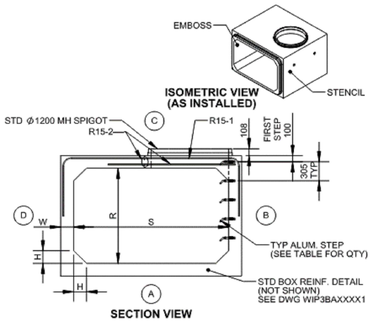
PROJECT NO:	2023-033	DATE:	03/07/2023
DESIGNED BY:	JD	CHECKED BY:	EC
SCALE:	N.T.S.	SHEET NO:	4 OF 6



STORMCON **69 CONNIE CRESCENT** **CONCORD, ON** **L4K 1L3**	**SALES@STORMCON.CA** **www.STORMCON.CA**	THIS DRAWING WAS PREPARED TO SUPPORT THE PROJECT ENGINEER OF RECORD FOR THE PROPOSED SYSTEM. IT IS THE ULTIMATE RESPONSIBILITY OF THE PROJECT ENGINEER OF RECORD TO ENSURE THAT THE SYSTEM'S DESIGN IS IN FULL COMPLIANCE WITH ALL APPLICABLE LAWS AND REGULATIONS. IT IS THE CONTRACTOR OF RECORD'S RESPONSIBILITY TO ENSURE THAT THE SYSTEM IS INSTALLED IN ACCORDANCE WITH STORMCON'S MINIMUM REQUIREMENTS. STORMCON DOES NOT APPROVE PLANS, SIZING, OR SYSTEM DESIGNS.	AGNES SUBDIVISION AGNES ST., CALEDON, ON SYSTEM OVERLAY SHEET	**STORMCRETE STORMWATER CHAMBER**	
			PROJECT NO: 2023-033	DATE: 03/07/2023
			DESIGNED BY: JD	CHECKED BY: EC
			SCALE: N.T.S.	SHEET NO: 5 OF 6

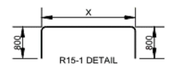


STORMCRETE BOX (3048mmx2438mm) DETAILS

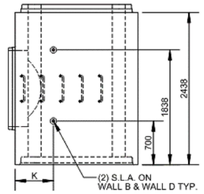


RIGHT

ADDITIONAL REINFORCING LIST				
MARK	QTY	SIZE	LENGTH	SPACING
R15-1	4	15M	L	50
R15-2	8	15M	2000	50



CAST IN MATERIAL LIST	
QTY	DESCRIPTION
4	SLA SEE PROD. VARIABLES TABLE FOR SIZE
SEE TABLE	16" HOLLOW ALUM. STEPS
1	STANDARD OPS BOX CULVERT CAGE (SEE WIP3BAXXXX1)



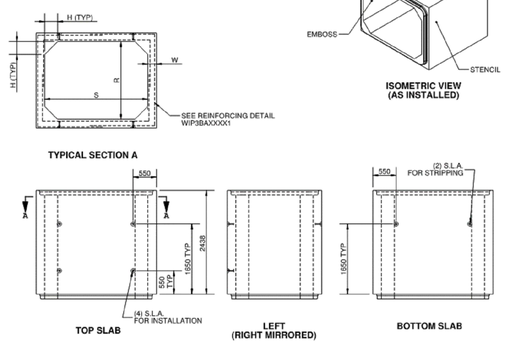
OPS STENCIL	OPS EMBOSS
CCP-GUELPH OPSS1821 (SIZE) MHT 4 (D.E.C) (DATE OF MFG) (MASS)KG	CC OPSS 1821 (D.E.C) (DATE OF MFG)

PRODUCT VARIABLES															
PART ID	VARIABLE DIMENSIONS										S.L.A.	STEPS	MASS (kg)	D.E.C
	S	R	W	H	J	K	M	X	L					
BOX1809MHT-001	1800	900	200	200	810	400	1470	2100	3700	4T x 5-1/2"	3	7358	0.6-5.5m
BOX1812MHT-001	1829	1219	203	203	813	400	1473	2135	3735	4T x 5-1/2"	4	8342	0.6-5.5m
BOX2412MHT-001	2438	1219	203	203	813	600	1473	2744	4344	4T x 5-1/2"	4	9830	0.6-3.6m
BOX2415MHT-001	2438	1524	203	203	813	600	1473	2744	4344	4T x 5-1/2"	5	10577	0.6-3.6m
BOX2418MHT-001	2438	1829	203	203	813	600	1473	2744	4344	4T x 5-1/2"	6	11323	0.6-3.6m
BOX3015MHT-001	3045	1524	254	254	864	900	1524	3456	5056	8T x 7-1/8"	5	15089	0.6-3.6m
BOX3018MHT-001	3045	1829	254	254	864	900	1524	3456	5056	8T x 7-1/8"	6	16506	0.6-3.6m
BOX3021MHT-001	3045	2134	254	254	864	900	1524	3456	5056	8T x 7-1/8"	7	17280	0.6-3.6m
BOX3024MHT-001	3045	2438	254	254	864	900	1524	3456	5056	8T x 7-1/8"	8	18372	0.6-3.6m

ALL DIMENSIONS ARE IN mm DRAWINGS ARE NOT TO SCALE WWF SHEETS TO CSA G.30.5 AND CSA G.30.15 WWF Fy = 500MPa REINFORCING TO CSA G.30.18 GRADE 400W WELD REINFORCING STEEL ACCORDING TO CWB APPROVED PROCEDURE CSA W186	MIN. CONC STRENGTH 35MPa CLEAR COVER = 40 mm ± 5 mm FOUNDATION TO OPSS 1821 FILL MINIMUM 300 TO OPSS SEE DWG BXXXXX1-JOINT FOR MH JOINT, SEE DWG MX-JOINT

STANDARD BOX 2438 LAY LENGTH (WET CAST GASKETED)

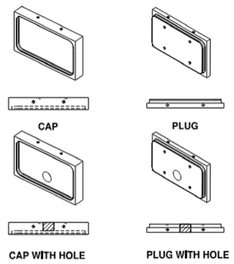
#1: OPS STENCIL	#1: OPS EMBOSS	#2: NON-OPS STENCIL	#2: NON-OPS EMBOSS
CCP-GUELPH OPSS1821 (SIZE) STD (D.E.C) TYPE HSb (DATE OF MFG) (MASS)KG	CC OPSS 1821 (D.E.C) (DATE OF MFG)	CCP-GUELPH CHBDC (SIZE) STD (D.E.C) TYPE HSb (DATE OF MFG) (MASS)KG	CC CHBDC (D.E.C) (DATE OF MFG)



PRODUCT VARIABLES							
PART ID	VARIABLE DIMENSIONS				S.L.A.	MASS (kg)	D.E.C	STENCIL/ EMBOSS
	S	R	W	H				
BA2418↑-1	2438	1829	203	305	4T x 5-1/2"	12566	0.6-3.6m	#1
BA3024↑-1	3048	2438	254	305	8T x 8-1/4"	19502	0.6-3.6m	#1
BA3030↑-1**	3048	3048	254	254	8T x 8-1/4"	21016	0.6-3.6m	#2

** STANDARD SIZE NOT LISTED IN OPSS 1821, DESIGNED TO CSA S6-06

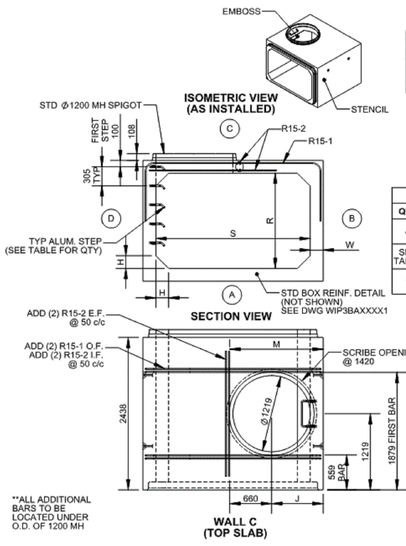
STANDARD END TREATMENTS AND FITTINGS



- CAP INSTALLED ON SPIGOT END OF BOX UNIT.
- PLUG INSTALLED ON BELL END OF BOX UNIT (INCL. GASKET).
- MIN. THICKNESS = 300 mm.
- CAP/PLUG STYLE TRANSITION TO SMALLER CIRCULAR, ELLIPTICAL, OR BOX UNIT AVAILABLE.
- CAP AND PLUG MADE OF WET CAST CONCRETE.

- CAP INSTALLED ON SPIGOT END OF BOX UNIT.
- PLUG INSTALLED ON BELL END OF BOX UNIT (INCL. GASKET).
- MIN. THICKNESS = 300 mm.
- CAP/PLUG STYLE TRANSITION TO SMALLER CIRCULAR, ELLIPTICAL, OR BOX UNIT AVAILABLE.

STANDARD BOX 2438 LAY LENGTH WITH MANHOLE TEE (DRY CAST)



ADDITIONAL REINFORCING LIST				
MARK	QTY	SIZE	LENGTH	SPACING
R15-1	4	15M	L	50
R15-2	8	15M	2000	50

CAST IN MATERIAL LIST	
QTY	DESCRIPTION
4	SLA SEE PROD. VARIABLES TABLE FOR SIZE
SEE TABLE	16" HOLLOW ALUM. STEPS
1	STANDARD OPS BOX CULVERT CAGE (WIP3BAXXXX1)

LEFT

STORMCON
69 CONNIE CRESCENT
CONCORD, ON
L4K 1L3

SALES@STORMCON.CA
www.STORMCON.CA

AGNES SUBDIVISION
AGNES ST., CALEDON, ON

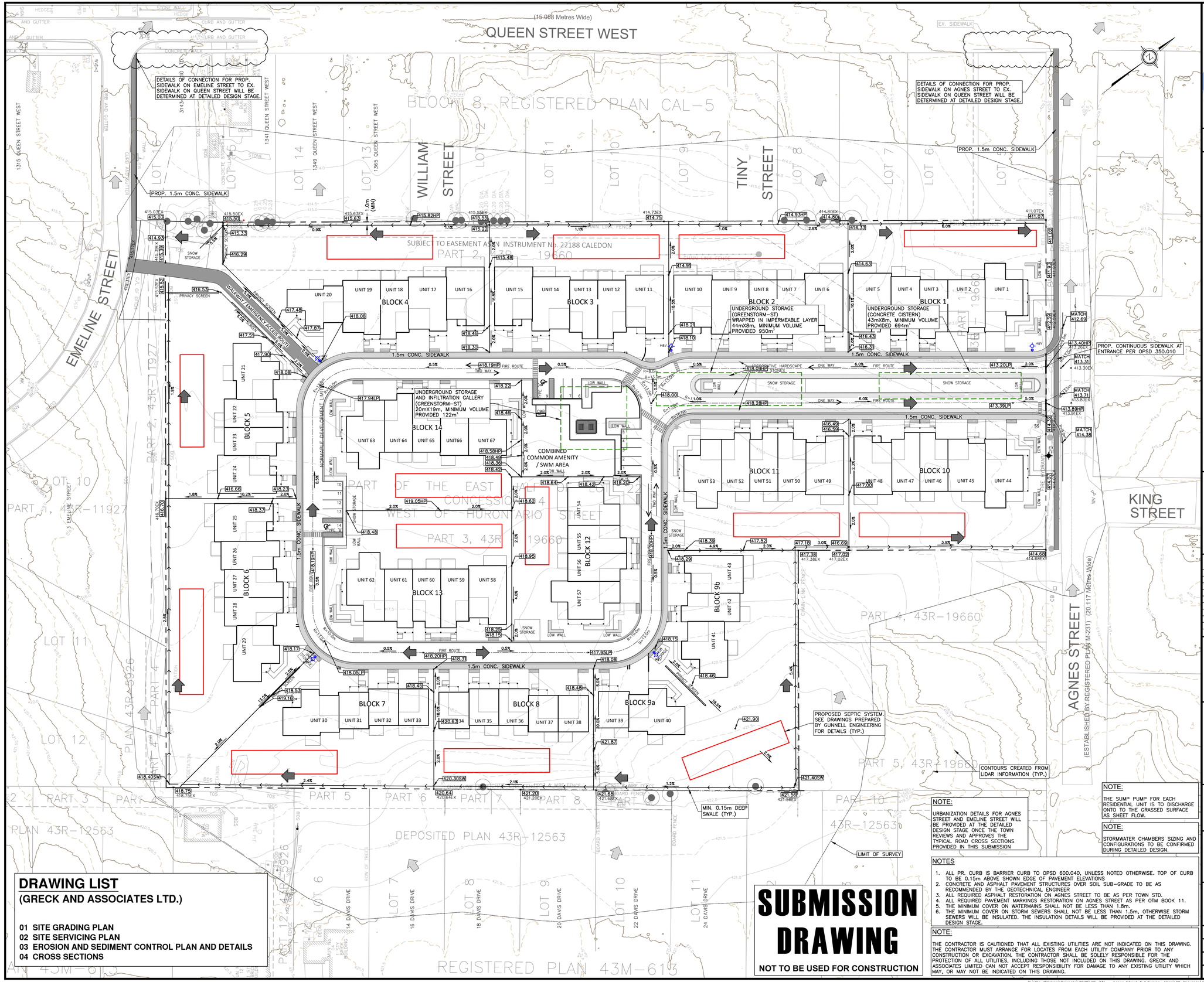
DETAILS

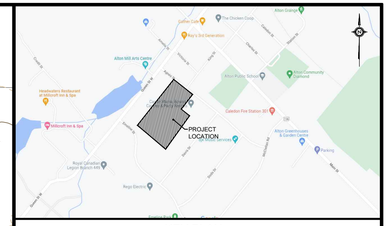
STORMCRETE STORMWATER CHAMBER

PROJECT NO:	2023-033	DATE:	03/07/2023
DESIGNED BY:	JD	CHECKED BY:	EC
SCALE:	N.T.S.	SHEET NO:	6 OF 6

APPENDIX F

Engineering Drawings





KEY PLAN
N.T.S.

LEGEND

EXISTING	PROPOSED	
MH1	MH1	STORM MANHOLE
CBMH1	CBMH1	STORM CATCHBASIN MANHOLE
CB	CB	SINGLE CATCHBASIN
DCB	DCB	DOUBLE CATCHBASIN
HYD&V	HYD&V	FIRE HYDRANT
VB	VB	VALVE & BOX
		LIMIT OF SUBJECT PROPERTY
		EASEMENT
		RIGHT OF WAY
		LOT LINE
x x	x—x—x	FENCE LINE
		CURB/SIDEWALK
		BUILDING
		MAJOR CONTOUR LABEL
		MINOR CONTOUR LABEL
		ASPHALT
		PAVING STONE
		1.5m WIDE CONCRETE SIDEWALK
x265.22EX	x265.22	ELEVATION
	x265.22SW	ELEVATION – SWALE
	x265.22LP	ELEVATION – LOW POINT
	x265.22HP	ELEVATION – HIGH POINT
		SWALE
		OVERLAND FLOW
		TREE
		TREE – TO REMAIN
		SEPTIC SYSTEM (BY OTHERS)

NOTES
1. ALL DIMENSIONS ARE IN METRES UNLESS OTHERWISE NOTED.
2. CONTOUR INTERVAL IS 0.50m.
3. ALL DIMENSIONS SHALL BE CHECKED AND VERIFIED IN THE FIELD BY THE CONTRACTOR PRIOR TO ANY CONSTRUCTION, AND ANY DISCREPANCIES SHALL BE REPORTED IMMEDIATELY TO THE ENGINEER.
4. ALL WORK SHALL BE IN ACCORDANCE WITH CURRENT TOWN OF CALEDON STANDARD SPECIFICATIONS AND DRAWINGS UNLESS OTHERWISE NOTED HEREIN.
5. ORDER OF PRECEDENCE OF STANDARDS DRAWINGS IS FIRSTLY TOWN OF CALEDON, AND SECONDLY ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD).

BENCHMARK

BENCHMARK No. N/A
ELEVATION = N/A
DESCRIPTION:
ELEVATIONS ARE BASED ON GPS OBSERVATIONS FROM PERMANENT REFERENCE STATIONS IN THE NAD83 (CSRS-2010) COORDINATE SYSTEM, WITH HEIGHTS CONVERTED TO ORTHOMETRIC ELEVATION ON THE CVD28 DATUM (1978 ADJUSTMENT) WITH GEOID MODEL HTV2.0, AS SUPPLIED BY NATURAL RESOURCES CANADA.
COMPLETED BY:
VAN HARTEN SURVEYING INC.
COMPLETED ON:
MAY 10, 2018
DEM SOURCE:
LIDAR DTM PEEL 2016 PACKAGE B AVAILABLE FROM LAND INFORMATION ONTARIO

NO.	REVISION	DATE	BY	APPROVED
01	ISSUED FOR 1ST SUBMISSION	2023/03/20	K.M.	
02	ISSUED FOR 2ND SUBMISSION	2023/12/20	K.M.	

Greck
5770 Highway 7, Woodbridge, Ontario, L4L 1T8 www.greck.ca

LICENSED PROFESSIONAL ENGINEER
K MAHMOOD
100160233
Dec. 20, 2023
PROVINCE OF ONTARIO

CLIENT NAME:
THE ALTON DEVELOPMENT INC.
1402 QUEEN STREET
ALTON, ON
L7K 0C3

PROJECT NAME:
AGNES STREET SUBDIVISION
AGNES STREET CALEDON, ON

PRELIMINARY SITE GRADING PLAN

NOTE:
THE SUMP PUMP FOR EACH RESIDENTIAL UNIT IS TO DISCHARGE ONTO TO THE GRASSED SURFACE AS SHEET FLOW.

NOTE:
STORMWATER CHAMBERS SIZING AND CONFIGURATIONS TO BE CONFIRMED DURING DETAILED DESIGN.

NOTE:
URBANIZATION DETAILS FOR AGNES STREET AND EMELINE STREET WILL BE PROVIDED AT THE DETAILED DESIGN STAGE ONCE THE TOWN REVIEWS AND APPROVES THE TYPICAL ROAD CROSS SECTIONS PROVIDED IN THIS SUBMISSION

NOTES
1. ALL PR. CURB IS BARRIER CURB TO OPSD 600.040, UNLESS NOTED OTHERWISE. TOP OF CURB TO BE 0.15m ABOVE SHOWN EDGE OF PAVEMENT ELEVATIONS
2. CONCRETE AND ASPHALT PAVEMENT STRUCTURES OVER SOIL SUB-GRADE TO BE AS RECOMMENDED BY THE GEOTECHNICAL ENGINEER
3. ALL REQUIRED ASPHALT RESTORATION ON AGNES STREET TO BE AS PER TOWN STD.
4. ALL REQUIRED PAVEMENT MARKINGS RESTORATION ON AGNES STREET AS PER OTM BOOK 11.
5. THE MINIMUM COVER ON WATERMAINS SHALL NOT BE LESS THAN 1.8m.
6. THE MINIMUM COVER ON STORM SEWERS SHALL NOT BE LESS THAN 1.5m, OTHERWISE STORM SEWERS WILL BE INSULATED. THE INSULATION DETAILS WILL BE PROVIDED AT THE DETAILED DESIGN STAGE.

NOTE:
THE CONTRACTOR IS CAUTIONED THAT ALL EXISTING UTILITIES ARE NOT INDICATED ON THIS DRAWING. THE CONTRACTOR MUST ARRANGE FOR LOCATES FROM EACH UTILITY COMPANY PRIOR TO ANY CONSTRUCTION OR EXCAVATION. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR THE PROTECTION OF ALL UTILITIES, INCLUDING THOSE NOT INCLUDED ON THIS DRAWING. GRECK AND ASSOCIATES LIMITED CAN NOT ACCEPT RESPONSIBILITY FOR DAMAGE TO ANY EXISTING UTILITY WHICH MAY, OR MAY NOT BE INDICATED ON THIS DRAWING.

DRAWING LIST
(GRECK AND ASSOCIATES LTD.)

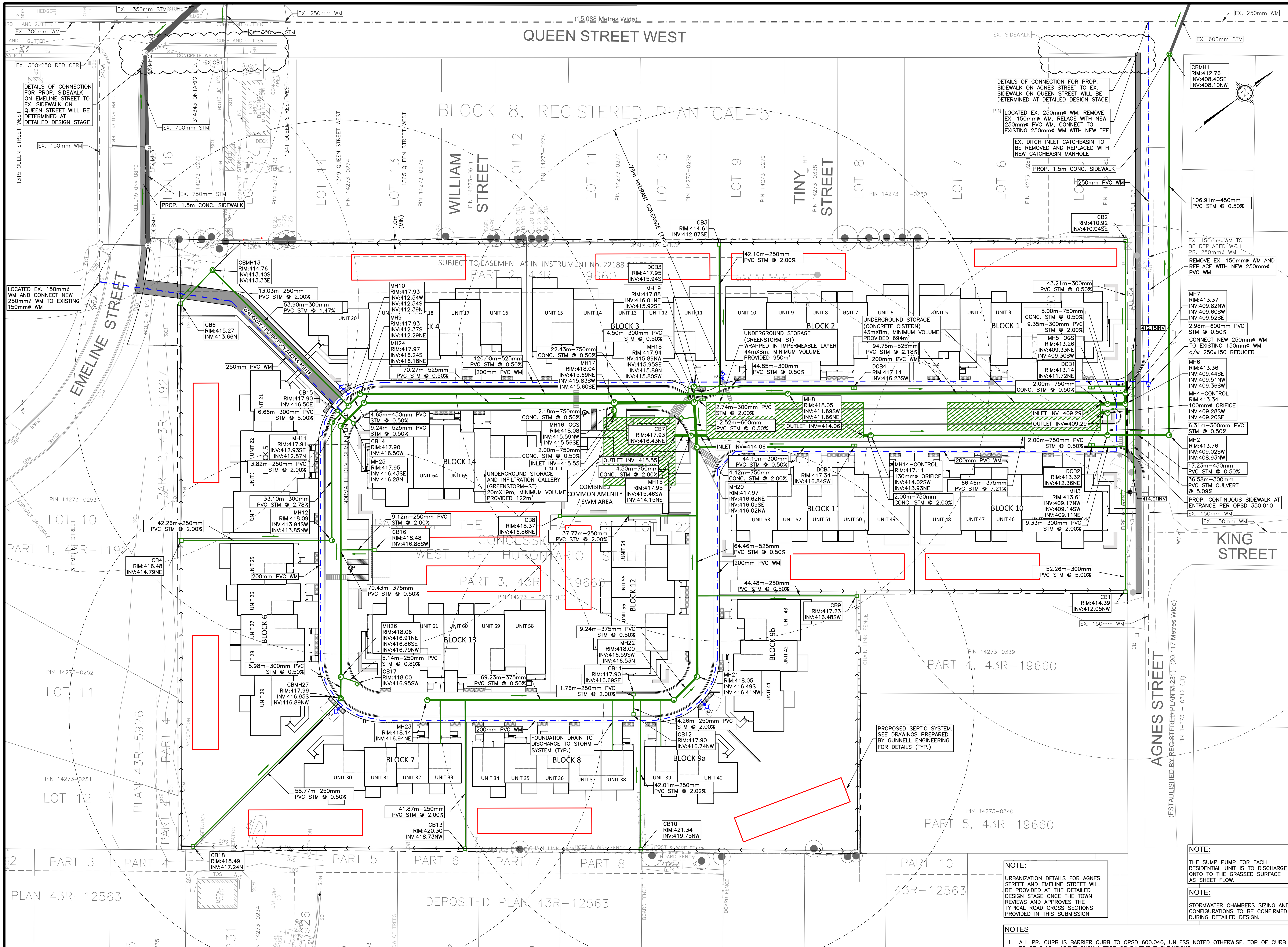
01 SITE GRADING PLAN
02 SITE SERVICING PLAN
03 EROSION AND SEDIMENT CONTROL PLAN AND DETAILS
04 CROSS SECTIONS

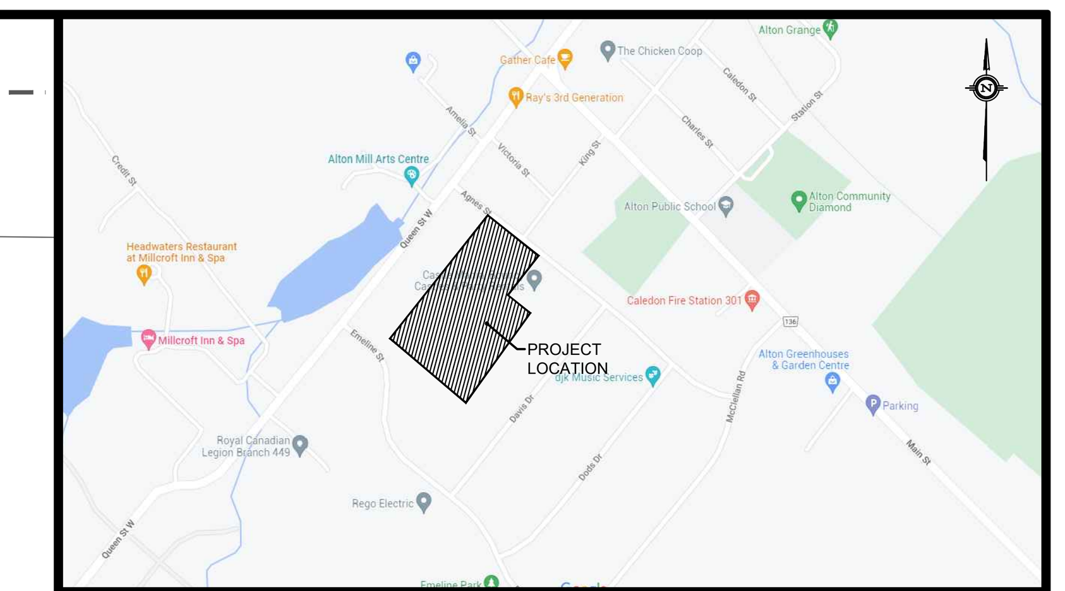
SUBMISSION DRAWING
NOT TO BE USED FOR CONSTRUCTION

DESIGNED BY:	J.N.	SCALES:	
CHECKED BY:	K.M.	HORIZONTAL:	1:500
DRAWN BY:	J.N.	VERTICAL:	N/A
DATE:	MAR. 08, 2023	SHEET SIZE:	24"x36"

PROJECT No. 20-731
DRAWING No.
SHEET No. 01

C:\CloudStation\Projects\2020\20-731 - Agnes Street Subdivision, Alton\05_Drawings\CAD\GRADING\20-731_SGP.dwg
Date Plotted: Dec 11, 2023 - 7:00 PM





KEY PLAN

N.T.S.

LEGEND

EXISTING	PROPOSED	
MH1	MH1	STORM MANHOLE
MH1	MH1	STORM CATCHBASIN MANHOLE
CB	CB	SINGLE CATCHBASIN
DCB	DCB	DOUBLE CATCHBASIN
HYD&V VB	HYD&V VB	FIRE HYDRANT
		VALVE & BOX
		STORM SEWER
		WATERMAIN
		LIMIT OF SUBJECT PROPERTY
		EASEMENT
		RIGHT OF WAY
		LOT LINE
		FENCE LINE
		CURB/SIDEWALK
		TREE
		TREE – TO REMAIN
		SEPTIC SYSTEM (BY OTHERS)
		SWALE

NOTES
1. ALL DIMENSIONS ARE IN METRES UNLESS OTHERWISE NOTED.
2. ALL DIMENSIONS SHALL BE CHECKED AND VERIFIED IN THE FIELD BY THE CONTRACTOR PRIOR TO ANY CONSTRUCTION, AND ANY DISCREPANCIES SHALL BE REPORTED IMMEDIATELY TO THE ENGINEER.
3. ALL WORK SHALL BE IN ACCORDANCE WITH CURRENT TOWN OF CALEDON STANDARD SPECIFICATIONS AND DRAWINGS UNLESS OTHERWISE NOTED HEREIN.
4. ORDER OF PRECEDENCE OF STANDARDS DRAWINGS IS FIRSTLY TOWN OF CALEDON, AND SECONDLY ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD).

BENCHMARK

BENCHMARK No. N/A
ELEVATION = N/A
DESCRIPTION:
ELEVATIONS ARE BASED ON GPS OBSERVATIONS FROM PERMANENT REFERENCE STATIONS IN THE NAD83 (CSRS–2010) COORDINATE SYSTEM, WITH HEIGHTS CONVERTED TO ORTHOMETRIC ELEVATION ON THE CVGD28 DATUM (1978 ADJUSTMENT) WITH GEOID MODEL HTV2.0, AS SUPPLIED BY NATURAL RESOURCES CANADA.

COMPLETED BY:
VAN HARTEN SURVEYING INC.
COMPLETED ON:
MAY 10, 2018

DEM SOURCE:
LIDAR DTM PEEL 2016 PACKAGE B AVAILABLE FROM LAND INFORMATION ONTARIO

NO.	REVISION	DATE	BY	APPROVED
01	ISSUED FOR 1ST SUBMISSION	2023/03/20	K.M.	
02	ISSUED FOR 2ND SUBMISSION	2023/12/20	K.M.	

Greck

5770 Highway 7, Woodbridge, Ontario, L4L 1T8 www.greck.ca

LICENSED PROFESSIONAL ENGINEER
K. MAHMOOD
100160233
Dec. 20, 2023
20-731
PROVINCE OF ONTARIO

CLIENT NAME:
THE ALTON DEVELOPMENT INC.
1402 QUEEN STREET
ALTON, ON
L7K 0C3

PROJECT NAME:

AGNES STREET SUBDIVISION

AGNES STREET CALEDON, ON

PRELIMINARY SITE SERVICING PLAN

DESIGNED BY:	J.N.	SCALES:		PROJECT No.	20-731
CHECKED BY:	K.M.	HORIZONTAL:	1:500	DRAWING No.	
DRAWN BY:	J.N.	VERTICAL:	N/A	SHEET No.	02
DATE: MAR. 08, 2023		SHEET SIZE:	24"x36"		

NOTE:
URBANIZATION DETAILS FOR AGNES STREET AND EMELINE STREET WILL BE PROVIDED AT THE DETAILED DESIGN STAGE ONCE THE TOWN REVIEWS AND APPROVES THE TYPICAL ROAD CROSS SECTIONS PROVIDED IN THIS SUBMISSION

NOTE:
THE SUMP PUMP FOR EACH RESIDENTIAL UNIT IS TO DISCHARGE ONTO TO THE GRASSED SURFACE AS SHEET FLOW.

NOTE:
STORMWATER CHAMBERS SIZING AND CONFIGURATIONS TO BE CONFIRMED DURING DETAILED DESIGN.

NOTES
1. ALL PR. CURB IS BARRIER CURB TO OPSD 600.040, UNLESS NOTED OTHERWISE. TOP OF CURB TO BE 0.15m ABOVE SHOWN EDGE OF PAVEMENT ELEVATIONS
2. CONCRETE AND ASPHALT PAVEMENT STRUCTURES OVER SOIL SUB–GRADE TO BE AS RECOMMENDED BY THE GEOTECHNICAL ENGINEER
3. ALL REQUIRED ASPHALT RESTORATION ON AGNES STREET TO BE AS PER TOWN STD.
4. ALL REQUIRED PAVEMENT MARKINGS RESTORATION ON AGNES STREET AS PER OTM BOOK 11.
5. THE MINIMUM COVER ON WATERMAINS SHALL NOT BE LESS THAN 1.8m.
6. THE MINIMUM COVER ON STORM SEWERS SHALL NOT BE LESS THAN 1.5m, OTHERWISE STORM SEWERS WILL BE INSULATED. THE INSULATION DETAILS WILL BE PROVIDED AT THE DETAILED DESIGN STAGE.

NOTE:
THE CONTRACTOR IS CAUTIONED THAT ALL EXISTING UTILITIES ARE NOT INDICATED ON THIS DRAWING. THE CONTRACTOR MUST ARRANGE FOR LOCATES FROM EACH UTILITY COMPANY PRIOR TO ANY CONSTRUCTION OR EXCAVATION. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR THE PROTECTION OF ALL UTILITIES, INCLUDING THOSE NOT INCLUDED ON THIS DRAWING. GRECK AND ASSOCIATES LIMITED CAN NOT ACCEPT RESPONSIBILITY FOR DAMAGE TO ANY EXISTING UTILITY WHICH MAY, OR MAY NOT BE INDICATED ON THIS DRAWING.

SUBMISSION DRAWING

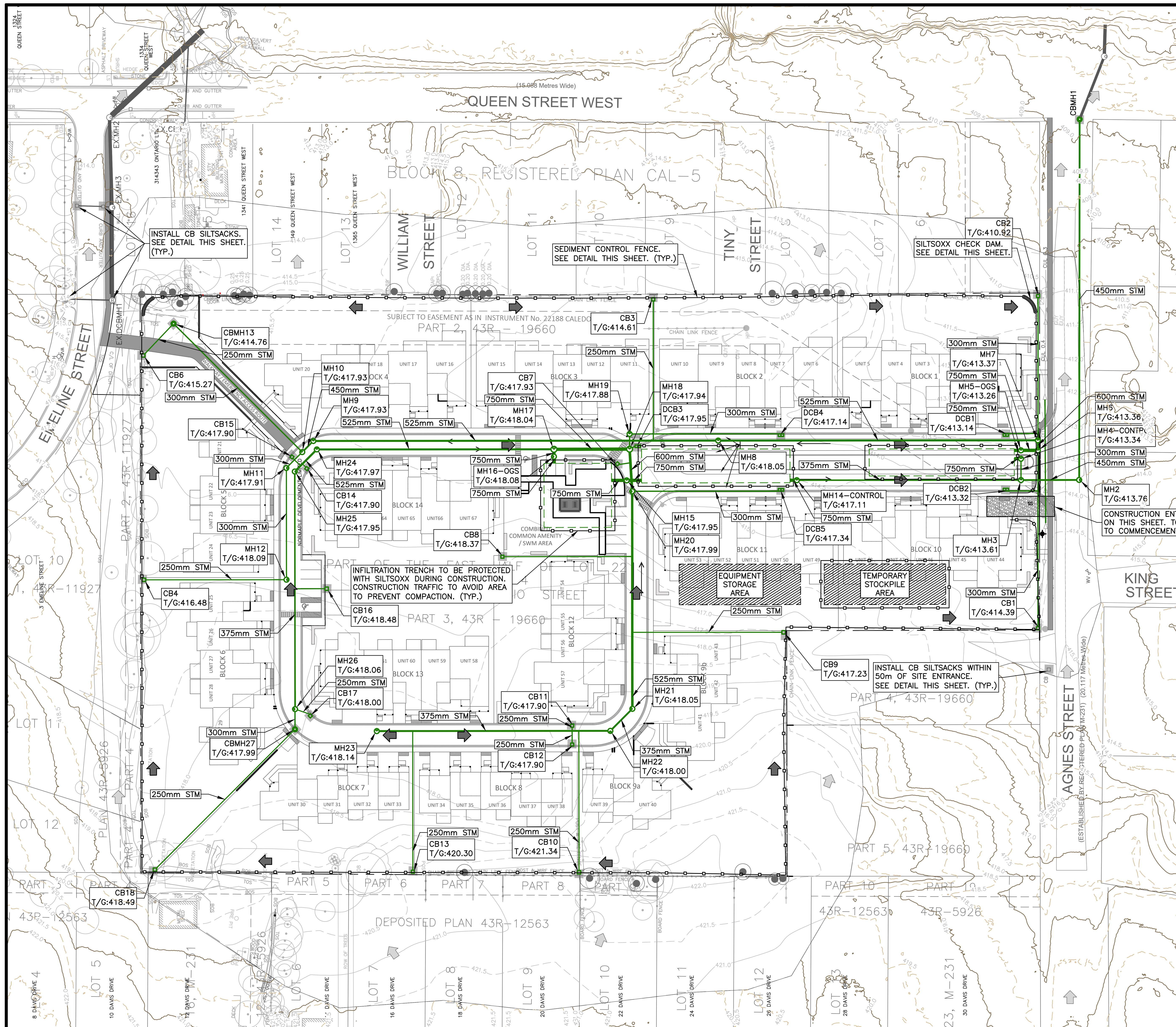
NOT TO BE USED FOR CONSTRUCTION

DRAWING LIST
(GRECK AND ASSOCIATES LTD.)

01 SITE GRADING PLAN
02 SITE SERVICING PLAN
03 EROSION AND SEDIMENT CONTROL PLAN AND DETAILS
04 CROSS SECTIONS

C:\CloudStation\Projects\2020\20-731 – Agnes Street Subdivision, Alton\05_Drawings\CAD\GENERAL PLAN\20-731_SSP.dwg

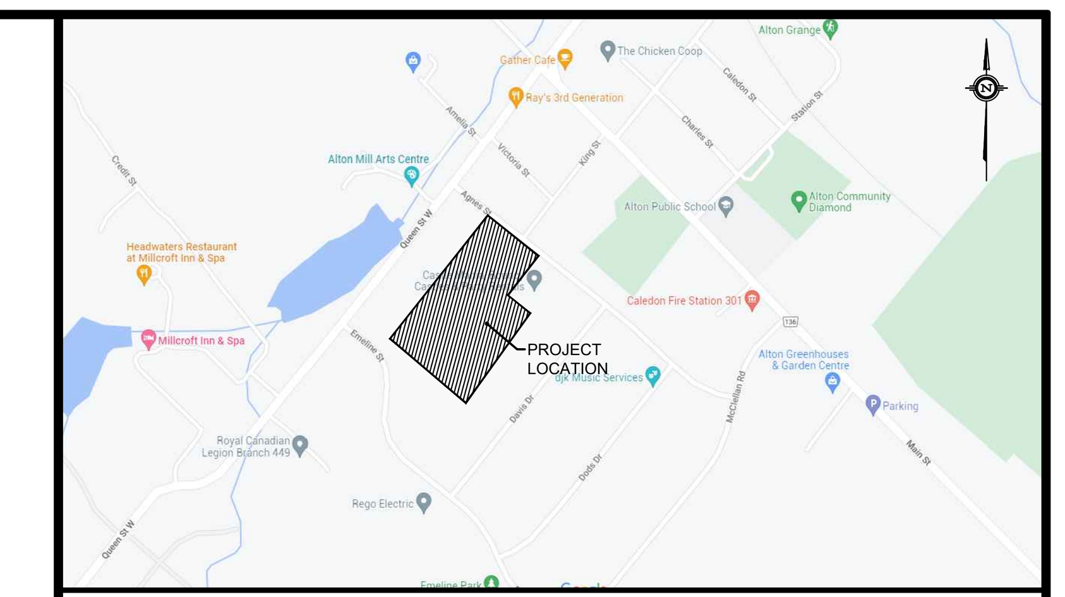
Date Plotted: Dec 11, 2023 – 7:02 PM



EROSION AND SEDIMENT CONTROL PLAN NOTES

THE FOLLOWING EROSION AND SEDIMENT CONTROL (ESC) MEASURES ARE IN ACCORDANCE WITH THE EROSION AND SEDIMENT CONTROL GUIDELINES FOR TOWN OF CALEDON AND CREDIT VALLEY CONSERVATION AUTHORITY (C.V.C.A.).

1. EROSION AND SEDIMENT CONTROL (ESC) MEASURES WILL BE IMPLEMENTED PRIOR TO, AND MAINTAINED DURING THE CONSTRUCTION PHASES, TO PREVENT SEDIMENT LADEN RUNOFF FROM LEAVING THE SITE. ALL DAMAGED EROSION AND SEDIMENT CONTROL MEASURES SHOULD BE REPAIRED AND/OR REPLACED WITHIN 48 HOURS OF THE INSPECTION.
2. ADDITIONAL MATERIALS SUCH AS CLEAR STONE, FILTER FABRIC, HOSES, SILTSOXX, AND STRAW BLANKET TO BE KEPT ONSITE OR ON HAND AT ALL TIMES FOR CONDUCTING IMMEDIATE REPAIRS TO SEDIMENT CONTROL MEASURES AS REQUIRED.
3. DISTURBED AREAS WILL BE MINIMIZED TO THE EXTENT POSSIBLE, AND TEMPORARILY OR PERMANENTLY STABILIZED OR RESTORED AS THE WORK PROGRESSES.
4. STOCKPILING ON SITE TO BE MINIMIZED. EXCESS FILL TO BE REMOVED IMMEDIATELY OFF SITE.
5. THE EROSION AND SEDIMENT CONTROL STRATEGIES OUTLINED ON THE PLANS ARE NOT STATIC AND MAY NEED TO BE UPGRADED/AMENDED AS SITE CONDITIONS CHANGE TO MINIMIZE SEDIMENT LADEN RUNOFF FROM LEAVING THE WORK AREAS. IF THE PRESCRIBED MEASURES ON THE PLANS ARE NOT EFFECTIVE IN PREVENTING THE RELEASE OF A DELETERIOUS SUBSTANCE, INCLUDING SEDIMENT, THEN ALTERNATIVE MEASURES MUST BE IMPLEMENTED IMMEDIATELY TO MINIMIZE POTENTIAL ECOLOGICAL IMPACTS. C.V.C.A. ENFORCEMENT OFFICER SHOULD BE IMMEDIATELY CONTACTED. ADDITIONAL ESC MEASURES TO BE KEPT ON SITE AND USED AS NECESSARY.
6. A SITE ENGINEER IS TO INSPECT ALL NEW CONTROLS, AS WELL AS ON A REGULAR BASIS, OR FOLLOWING RAIN/SNOWMELT EVENT, TO MONITOR ALL WORKS, AND IN PARTICULAR, WORKS RELATED TO EROSION AND SEDIMENT CONTROLS. SHOULD CONCERNS ARISE ON SITE, THE SITE ENGINEER WILL CONTACT THE C.V.C.A. ENFORCEMENT OFFICER AS WELL AS THE OWNER.
7. ALL ACTIVITIES, INCLUDING MAINTENANCE PROCEDURES, WILL BE CONTROLLED TO PREVENT ANY SPILLS OF PETROLEUM PRODUCTS, OR OTHER DELETERIOUS SUBSTANCES. VEHICULAR REFUELING AND MAINTENANCE WILL BE CONDUCTED A MINIMUM OF 30 METRES FROM THE WATER.
8. THE PROPONENT/CONTRACTOR SHALL MONITOR THE WEATHER SEVERAL DAYS IN ADVANCE OF GRADING WORKS TO ENSURE THAT THE WORKS WILL BE CONDUCTED DURING FAVOURABLE WEATHER CONDITIONS.
9. THE CONTRACTOR SHALL INSTALL SILTSOXX, AS REQUIRED TO CONTROL THE DISCHARGE OF EXPOSED SOIL OR TEMPORARY PILE(S) OF EXCAVATED SOILS OR, SOILS AND GRANULAR MATERIAL TO BE USED DURING CONSTRUCTION.
10. EROSION AND SEDIMENT CONTROL MEASURES ARE TO REMAIN IN PLACE AND IN WORKING ORDER UNTIL LANDSCAPING HAS STABILIZED.
11. EXCAVATION DEWATERING PROCEDURE TO BE COMPLETED USING A SUMP PUMP AND FILTER BAG SYSTEM. SUMP PUMPS TO BE PLACED WITHIN EXCAVATED TRENCH AND SHOVELED PUMP PITS, SEE DETAIL. PUMP TO BE PLACED ON AND SURROUNDED WITH 19mm CLEAR STONE. PUMP DISCHARGE HOSE TO OUTLET INTO FILTER BAG.
12. AREAS WHICH WILL REMAIN DISTURBED FOR MORE THAN 30 DAYS SHALL BE STABILIZED USING SEEDING OR SOD.
13. ALL SLOPES SHALL BE STABILIZED AFTER CONSTRUCTION USING SODDING OR SEEDING WITH TERRAFIX S100 BIODEGRADABLE STRAW BLANKETS OR APPROVED EQUIVALENT. NO EROSION CONTROL MEASURE SHALL HAVE ANY PLASTIC, EVEN IF IT IS BIODEGRADABLE.
14. PUBLIC WALKWAYS AND MUNICIPAL ROADS ARE TO BE KEPT CLEAR OF EXCESS SEDIMENT.
15. THE SITE ACCESS ROUTE AND CONSTRUCTION SITE ARE TO BE RESTORED TO ORIGINAL CONDITIONS OR BETTER. ALL EXPOSED SOIL AREAS ARE TO BE COVERED WITH NATIVE SEED MIX AND EROSION BLANKET, AS PER THE PLANTING PLAN AND EROSION AND SEDIMENT CONTROL PLAN RESPECTIVELY.
16. WHERE PRACTICAL, WORKS SHOULD BE COMPLETED IN STAGES TO REDUCE THE DURATION OF DISTURBED AREAS.
17. REFER TO EROSION AND SEDIMENT CONTROL GUIDELINE FOR URBAN CONSTRUCTION, DECEMBER 2006 FOR FURTHER EROSION AND SEDIMENT CONTROL MEASURES APPROVED BY THE C.V.C.A.
18. IN ORDER TO COMPLY WITH THE MIGRATORY BIRDS CONVECTION ACT, C.V.C.A. RECOMMENDS THAT TREE REMOVALS BE COMPLETED BETWEEN AUGUST 1 AND APRIL 1.
19. PLEASE NOTIFY C.V.C.A. ENFORCEMENT OFFICER AND C.V.C.A. PROJECT MANAGER 48 HOURS PRIOR TO COMMENCING CONSTRUCTION.
20. AN ENVIRONMENTAL MONITOR IS TO BE DESIGNATED ON SITE, AND PROVIDE ADVICE, TO ENSURE THAT ACTIVITIES THAT COULD HAVE A NEGATIVE IMPACT TO THE NATURAL ENVIRONMENT ARE EFFECTIVELY MITIGATED AS CONSTRUCTION PROCEEDS. THE ENVIRONMENTAL MONITOR SHALL NOTIFY THE C.V.C.A. ENFORCEMENT OFFICER AND PROJECT MANAGER IF AN ISSUE ARISES.



KEY PLAN

N.T.S.

LEGEND

EXISTING	PROPOSED	
MH1	MH1	STORM MANHOLE
MH1	MH1	STORM CATCHBASIN MANHOLE
CB	CB	SINGLE CATCHBASIN
DCB	DCB	DOUBLE CATCHBASIN
		LIMIT OF SUBJECT PROPERTY
		EASEMENT
		RIGHT OF WAY
		LOT LINE
		FENCE LINE
		CURB/SIDEWALK
		BUILDING
		RETAINING WALL
		MAJOR CONTOUR LABEL
		MINOR CONTOUR LABEL
		SILTSOXX CHECKDAM
		SILT FENCE/SILTSOXX
		SWALE
		OVERLAND FLOW
		CONSTRUCTION MUD-MAT
CB	CB	TEMP. CB SILTSACK PROTECTION
		TREE
		TREE – TO REMAIN

NOTES

1. ALL DIMENSIONS ARE IN METRES UNLESS OTHERWISE NOTED.
2. CONTOUR INTERVAL IS 0.50m.
3. ALL DIMENSIONS SHALL BE CHECKED AND VERIFIED IN THE FIELD BY THE CONTRACTOR PRIOR TO ANY CONSTRUCTION, AND ANY DISCREPANCIES SHALL BE REPORTED IMMEDIATELY TO THE ENGINEER.
4. ALL WORK SHALL BE IN ACCORDANCE WITH CURRENT TOWN OF CALEDON STANDARD SPECIFICATIONS AND DRAWINGS UNLESS OTHERWISE NOTED HEREIN.
5. ORDER OF PRECEDENCE OF STANDARDS DRAWINGS IS FIRSTLY TOWN OF CALEDON, AND SECONDLY ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD).

BENCHMARK

BENCHMARK No. N/A
ELEVATION = N/A
DESCRIPTION:
ELEVATIONS ARE BASED ON GPS OBSERVATIONS FROM PERMANENT REFERENCE STATIONS IN THE NAD83 (CSRS–2010) COORDINATE SYSTEM, WITH HEIGHTS CONVERTED TO ORTHOMETRIC ELEVATION ON THE CVGD28 DATUM (1978 ADJUSTMENT) WITH GEOID MODEL HTV2.0, AS SUPPLIED BY NATURAL RESOURCES CANADA.

COMPLETED BY:
VAN HARTEN SURVEYING INC.
COMPLETED ON:
MAY 10, 2018

DEM SOURCE:
LIDAR DTM PEEL 2016 PACKAGE B AVAILABLE FROM LAND INFORMATION ONTARIO

NO.	REVISION	DATE	BY	APPROVED
01	ISSUED FOR 1ST SUBMISSION	2023/03/20	K.M.	
02	ISSUED FOR 2ND SUBMISSION	2023/12/20	K.M.	

NOTE:

URBANIZATION DETAILS FOR AGNES STREET AND EMELINE STREET WILL BE PROVIDED AT THE DETAILED DESIGN STAGE ONCE THE TOWN REVIEWS AND APPROVES THE TYPICAL ROAD CROSS SECTIONS PROVIDED IN THIS SUBMISSION

DRAWING LIST
(GRECK AND ASSOCIATES LTD.)

01 SITE GRADING PLAN
02 SITE SERVICING PLAN
03 EROSION AND SEDIMENT CONTROL PLAN AND DETAILS
04 CROSS SECTIONS

NOTE:

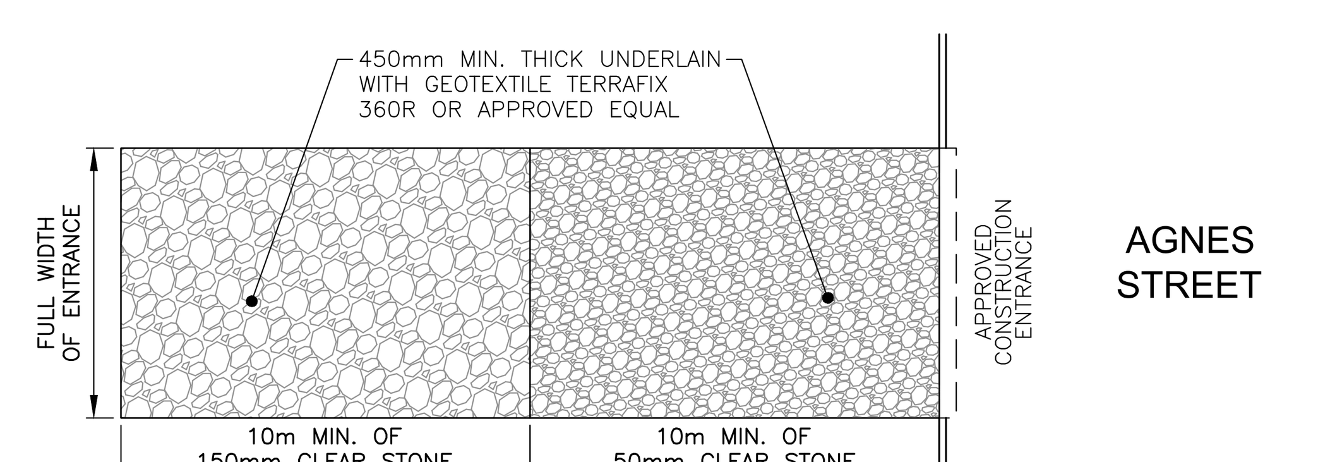
TOPSOIL STOCKPILES ARE NOT TO EXCEED 1.5m IN HEIGHT AND ARE TO BE LOCATED OUTSIDE OF TREE PROTECTION ZONE AND MINIMUM VEGETATION PROTECTION ZONES. ONLY THE AMOUNT OF SOIL TO REUSED ON SITE CAN BE STORED ON SITE.

NOTE:

THE CONTRACTOR IS CAUTIONED THAT ALL EXISTING UTILITIES ARE NOT INDICATED ON THIS DRAWING. THE CONTRACTOR MUST ARRANGE FOR LOCATES FROM EACH UTILITY COMPANY PRIOR TO ANY CONSTRUCTION OR EXCAVATION. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR THE PROTECTION OF ALL UTILITIES, INCLUDING THOSE NOT INCLUDED ON THIS DRAWING. GRECK AND ASSOCIATES LIMITED CAN NOT ACCEPT RESPONSIBILITY FOR DAMAGE TO ANY EXISTING UTILITY WHICH MAY, OR MAY NOT BE INDICATED ON THIS DRAWING.

SUBMISSION DRAWING

NOT TO BE USED FOR CONSTRUCTION

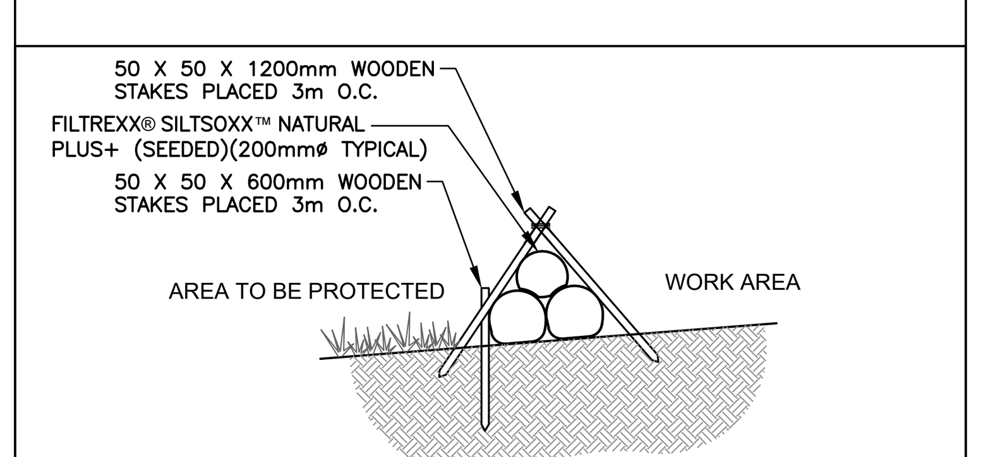


NOTES:

1. GRANULAR MATERIAL IS TO BE CLEAN APPROVED MATERIAL AND PLACED AT NOTED DIMENSIONS PRIOR TO LAND DISTURBANCE.
2. GEOTEXTILE IS TO BE UNDERLAIN OVER THE ENTIRE AREA PRIOR TO STONE PLACEMENT.
3. MAINTENANCE – THE ENTRANCE SHALL BE MAINTAINED IN A CONDITION WHICH WILL REDUCE TRACKING OR FLOWING OF SEDIMENT ONTO R.O.W. AND GRANULAR MATERIAL IS TO BE REPLACED AS WARRANTED OR DIRECTED BY THE SITE ENGINEER.

CONSTRUCTION MUDMAT DETAIL

N.T.S.

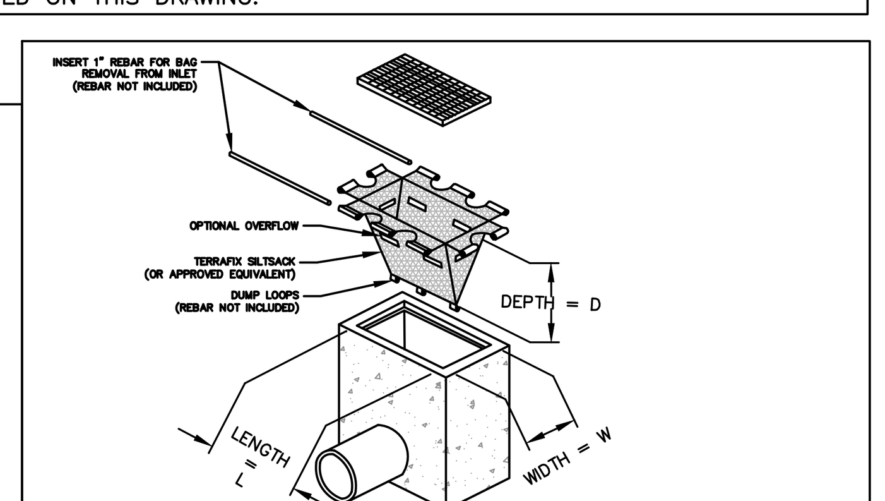


NOTES:

1. ALL MATERIAL TO MEET FILTREXX® (OR APPROVED EQUIVALENT) SPECIFICATIONS.
2. CHECK DAMS SHOULD BE USED IN AREAS THAT DRAIN 10 ACRES OR LESS.
3. SEDIMENT SHOULD BE REMOVED FROM BEHIND CHECK DAM ONCE THE ACCUMULATED HEIGHT HAS REACHED 1/2 THE HEIGHT OF THE CHECK DAM.
4. CHECK DAM TO BE DIRECT SEEDED WITH SEED MIX SPECIFIED BY FILTREXX CERTIFIED INSTALLER
5. CONTRACTOR IS REQUIRED TO BE A FILTREXX CERTIFIED INSTALLER

SILTSOXX CHECK DAM DETAIL

N.T.S.

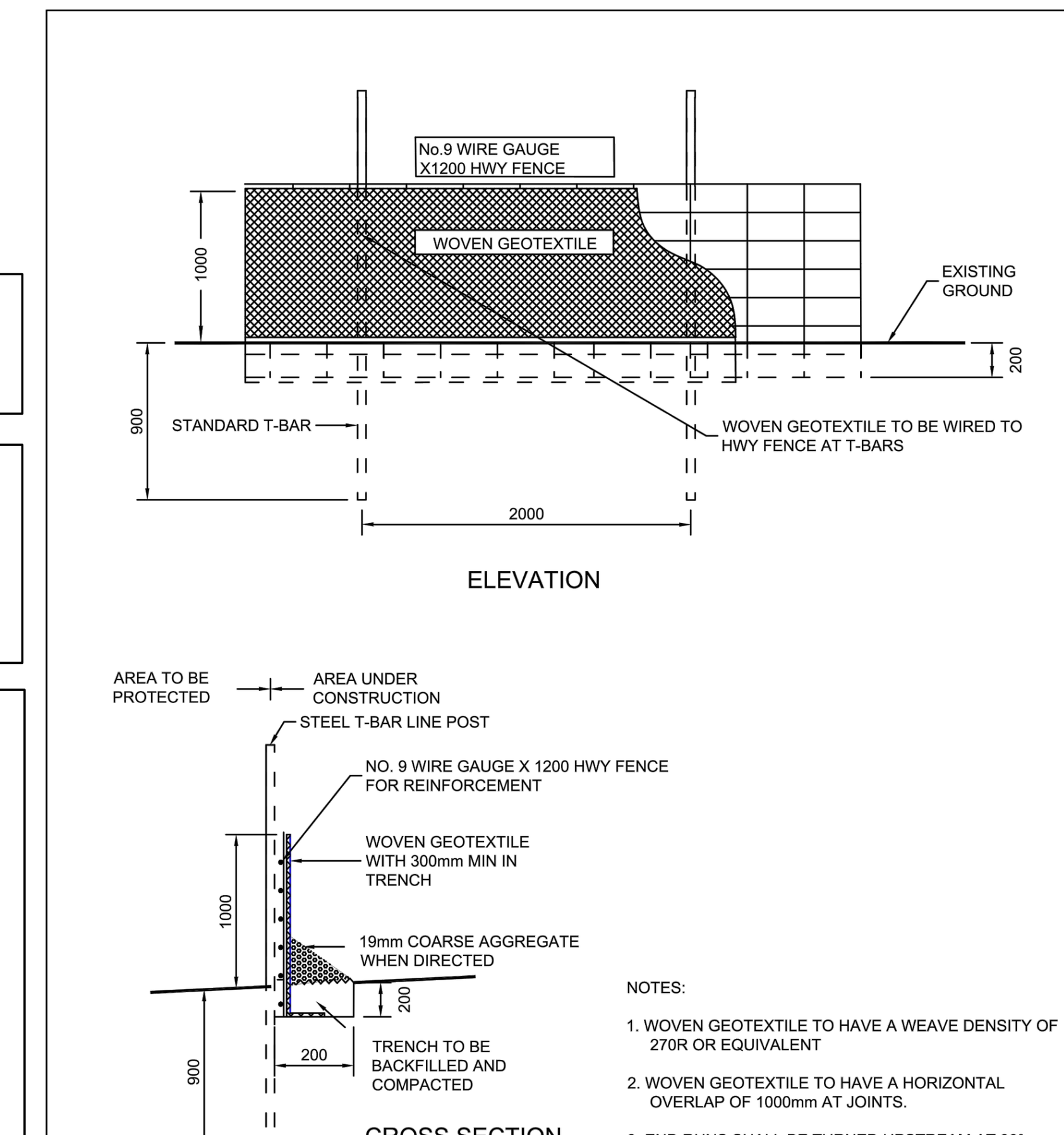


NOTES:

– BASIC INSTALLATION INSTRUCTION:
  * REMOVE DRAIN GRATE
  * INSERT SILTSACK
  * REPLACE GRATE TO HOLD SILTSACK IN POSITION
– CLEANING INSTRUCTION
  * WHEN THE YELLOW RESTRAINT CORD AT THE BOTTOM OF THE SILTSACK IS NOT VISIBLE IT IS TIME TO EMPTY THE SACK
  * USE REBAR/T–BAR TO INSERT INTO THE SLEVED OF THE SILTSACK AND LIFT THE SACK OUT OF THE CATCH BASIN (2 PEOPLE)
  * EMPTY CONTENTS OF THE SILTSACK IN DESIGNATED ESC AREA

TYPICAL SILTSACK CONSTRUCTION DETAIL

N.T.S.



NOTES:

1. WOVEN GEOTEXTILE TO HAVE A WEAVE DENSITY OF 270R OR EQUIVALENT
2. WOVEN GEOTEXTILE TO HAVE A HORIZONTAL OVERLAP OF 1000mm AT JOINTS.
3. END RUNS SHALL BE TURNED UPSTREAM AT 30°

NO.	REVISION	APP'D	DATE
2	NAME CHANGED, STANDARD No. 325 01 NOW 304		JUNE 08
1	SUPPORT FENCING CHANGED TO HWY FENCE		Oct 02

TOWN OF CALEDON

SEDIMENT CONTROL FENCE

APP'D: C.C. DATE: APRIL 2000

DRAWN: BJM SCALE: N.T.S.

STANDARD No. 304

Greck

5770 Highway 7, Woodbridge, Ontario, L4L 1T8 www.greck.ca

LICENSED PROFESSIONAL ENGINEER
K. MAHMOOD
100160233
Dec. 20, 2023
20-731
PROVINCE OF ONTARIO

CLIENT NAME:
THE ALTON DEVELOPMENT INC.
1402 QUEEN STREET
ALTON, ON
L7K 0C3

PROJECT NAME:

AGNES STREET SUBDIVISION

AGNES STREET CALEDON, ON

EROSION AND SEDIMENT CONTROL PLAN AND DETAILS

DESIGNED BY:	J.N.	SCALES:		PROJECT No.	20-731
CHECKED BY:	K.M.	HORIZONTAL:	1:750	DRAWING No.	
DRAWN BY:	J.N.	VERTICAL:	N/A	SHEET No.	03
DATE:	MAR. 08, 2023	SHEET SIZE:	24"x36"		

C:\CloudStation\Projects\2020\20-731 – Agnes Street Subdivision, Alton\05_Drawings\CAD\ESC\20-731_ESC.dwg

Date Plotted: Mar 20, 2023 – 6:01 PM

SUBMISSION DRAWING

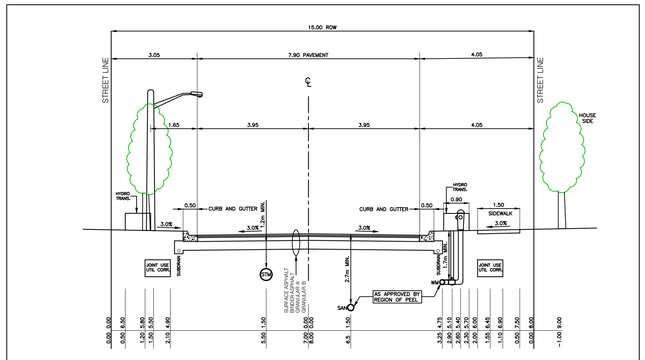
NOT TO BE USED FOR CONSTRUCTION

DRAWING LIST

(GRECK AND ASSOCIATES LTD.)

NOTE:

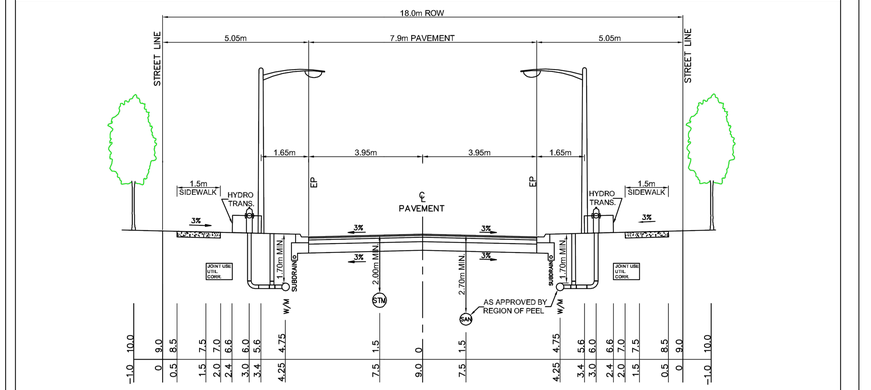
THE CONTRACTOR IS CAUTIONED THAT ALL EXISTING UTILITIES ARE NOT INDICATED ON THIS DRAWING. THE CONTRACTOR MUST ARRANGE FOR LOCATES FROM EACH UTILITY COMPANY PRIOR TO ANY CONSTRUCTION OR EXCAVATION. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR THE PROTECTION OF ALL UTILITIES, INCLUDING THOSE NOT INCLUDED ON THIS DRAWING. GRECK AND ASSOCIATES LIMITED CAN NOT ACCEPT RESPONSIBILITY FOR DAMAGE TO ANY EXISTING UTILITY WHICH MAY, OR MAY NOT BE INDICATED ON THIS DRAWING.



TYPICAL ROAD CROSS SECTION
15m LOCAL WINDOW STREET
7.90m PAVEMENT
SCALE 1:75

AGNES STREET CROSS SECTION

(QUEEN STREET WEST TO KING STREET)



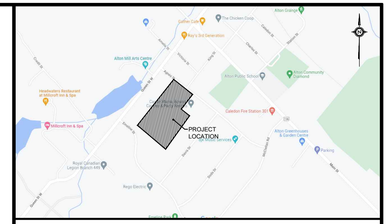
NOTES
1. WATERMAIN TO HAVE MINIMUM COVER OF 1.7m.
2. UTILITY CORRIDOR TO HAVE A MINIMUM COVER OF 0.9m.
3. TREES TO BE PLACED IN LOCATIONS PER APPROVED LANDSCAPE PLAN.
4. STREETLIGHT FIXTURE PER APPROVED TOWN STANDARD.
5. THE FOLLOWING IS A MINIMUM ROAD BASE AND WILL REQUIRE A SOILS REPORT VERIFICATION
   40 mm HL3
   65 mm HL8
   150 mm GRANULAR "A"
   300 mm GRANULAR "B"
6. THE BOULEVARDS REQUIRE A MINIMUM OF 300mm OF TOPSOIL AND NURSERY SOD.
7. ON A CRESCENT THE WATERMAIN SHALL BE PLACED ON THE OUTSIDE.
8. FULL LENGTH MINIMUM 100 MM DIA.SUB-DRAINS C/W FILTERCLOTH SHALL BE INSTALLED, AS PER APPROVED TOWN OF CALEDON STANDARD NO. 219.
9. SUB-GRADE SHALL BE COMPACTED TO A MINIMUM 95% OF S.P.D. AT OPTIMUM MOISTURE CONTENT.
10. WHERE POSSIBLE MANHOLE LIDS TO BE LOCATED OUT OF TIRE LANE OF TRAFFIC.
11. LONG DIMENSION OF TRANSFORMER TO BE PARALLEL TO STREETLINE.

TOWN OF CALEDON	NO.	REVISION	APR'D	DATE
18.0m LOCAL ROAD 8.5m ROADWAY (7.9m PAVEMENT)	3	DIMENSION AND TEXT REVISION		JAN. 09
	2	DIMENSION AND LAYOUT REVISION		JULY 08
	1	DIMENSION EDIT		JUNE 08

APR'D: C.C. DATE: JUNE 08
DRAWN: SCALE: N.T.S.
STANDARD No. 202

AGNES STREET CROSS SECTION

(KING STREET TO DAVIS DRIVE)



KEY PLAN
N.T.S.

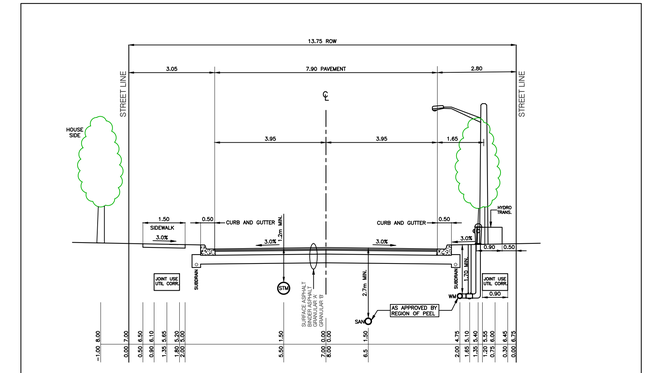
BENCHMARK

BENCHMARK No. N/A
ELEVATION = N/A
DESCRIPTION:
ELEVATIONS ARE BASED ON GPS OBSERVATIONS FROM PERMANENT REFERENCE STATIONS IN THE NAD83 (CSRS-2010) COORDINATE SYSTEM, WITH HEIGHTS CONVERTED TO ORTHOMETRIC ELEVATION ON THE CVGD28 DATUM (1978 ADJUSTMENT) WITH GEOID MODEL HTV2.0, AS SUPPLIED BY NATURAL RESOURCES CANADA.

COMPLETED BY:
VAN HARTEN SURVEYING INC.
COMPLETED ON:
MAY 10, 2018

DEM SOURCE:
LIDAR DTM PEEL 2016 PACKAGE B AVAILABLE FROM LAND INFORMATION ONTARIO

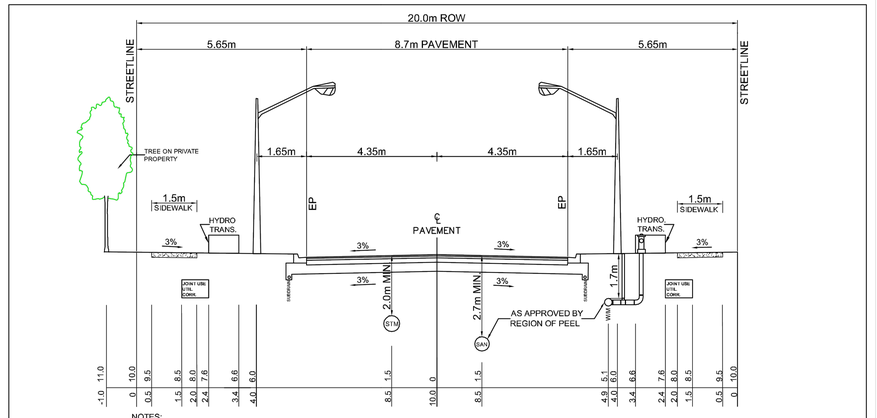
NO.	REVISION	DATE	BY	APPROVED
01	ISSUED FOR 2ND SUBMISSION	2023/12/20	K.M.	



TYPICAL ROAD CROSS SECTION
13.75m LOCAL WINDOW STREET
7.90m PAVEMENT
SCALE 1:75

EMELINE STREET CROSS SECTION

(QUEEN STREET TO DEVELOPMENT NORTH LIMIT)



NOTES:
1. UTILITY CORRIDOR TO HAVE A MINIMUM COVER OF 0.9m.
2. WATERMAIN TO HAVE MINIMUM COVER OF 1.7m.
3. THE FOLLOWING IS A MINIMUM ROAD BASE AND WILL REQUIRE A SOILS REPORT VERIFICATION
   40mm HL3
   65mm HL8
   150mm GRANULAR "A"
   300mm GRANULAR 'B'
4. THE BOULEVARDS REQUIRE A MINIMUM OF 300mm OF TOPSOIL AND NURSERY SOD
5. TREES TO BE PLACED IN LOCATIONS PER APPROVED LANDSCAPE PLAN
6. STREETLIGHT FIXTURE PER APPROVED TOWN STANDARD.
7. ON A CRESCENT THE WATERMAIN SHALL BE PLACED ON THE OUTSIDE.
8. FULL LENGTH MINIMUM 100MM DIA.SUB-DRAINS C/W FILTERCLOTH SHALL BE INSTALLED TO TOWN OF CALEDON STANDARD NO. 219.
9. SUB-GRADE SHALL BE COMPACTED TO A MINIMUM 95% OF S.P.D. AT OPTIMUM MOISTURE CONTENT.
10. WHERE POSSIBLE MANHOLE LIDS TO BE LOCATED OUT OF TIRE LANE OF TRAFFIC.
11. ESTATE RESIDENTIAL 4.0 METERS LANE WIDTH.

TOWN OF CALEDON	NO.	REVISION	APR'D	DATE
20.0m LOCAL URBAN/RURAL 9.3m ROADWAY (8.7m PAVEMENT)	4	DIMENSION AND TEXT REVISION		JAN. 09
	3	DIMENSION, LAYOUT REVISION		JULY 08
	2	DIMENSION EDIT, STD No. 201 NOW 203		JUNE 08
	1	OFFSETS		APRIL 08

APR'D: C.C. DATE: 19/01/00
DRAWN: BJM SCALE: N.T.S.
STANDARD No. 203

EMELINE STREET CROSS SECTION

(DEVELOPMENT NORTH LIMIT TO DAVIS DRIVE)

Greck
5770 Highway 7, Woodbridge, Ontario, L4L 1T8 www.greck.ca

LICENSED PROFESSIONAL ENGINEER
K. MAHMOOD
100160233
Dec. 20, 2023
20-731
PROVINCE OF ONTARIO

CLIENT NAME:
THE ALTON DEVELOPMENT INC.
1402 QUEEN STREET
ALTON, ON
L7K 0C3

PROJECT NAME:
AGNES STREET SUBDIVISION
AGNES STREET CALEDON, ON

CROSS SECTIONS

DESIGNED BY: J.N.	SCALES:	PROJECT No.	20-731
CHECKED BY: K.M.	HORIZONTAL: AS NOTED	DRAWING No.	CS
DRAWN BY: J.N.	VERTICAL: N/A	SHEET No.	04
DATE: MAR. 08, 2023	SHEET SIZE: 24"x36"		